## Article

# Self-Avoiding Random Walks as a Model to Study Athermal Linear Polymers under Extreme Plate Confinement 

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#### Abstract

Monte Carlo (MC) simulations, built around chain-connectivity-altering moves and a wall-displacement algorithm, allow us to simulate freely-jointed chains of tangent hard spheres of uniform size under extreme confinement. The latter is realized through the presence of two impenetrable, flat, and parallel plates. Extreme conditions correspond to the case where the distance between the plates approaches the monomer size. An analysis of the local structure, based on the characteristic crystallographic element (CCE) norm, detects crystal nucleation and growth at packing densities well below the ones observed in bulk analogs. In a second step, we map the confined polymer chains into self-avoiding random walks (SAWs) on restricted lattices. We study all realizations of the cubic crystal system: simple, body centered, and face centered cubic crystals. For a given chain size (SAW length), lattice type, origin of SAW, and level of confinement, we enumerate all possible SAWs (equivalently all chain conformations) and calculate the size distribution. Results for intermediate SAW lengths are used to predict the behavior of long, fully entangled chains through growth formulas. The SAW analysis will allow us to determine the corresponding configurational entropy, as it is the driving force for the observed phase transition and the determining factor for the thermodynamic stability of the corresponding crystal morphologies.


Keywords: confinement; crystallization; entropy; hard sphere; polymer; random walk; Monte Carlo; phase transition; lattice model; cubic crystal system; direct enumeration

## 1. Introduction

Polymer based thin films have been used extensively for several decades in a varied range of applications from optical coatings and energy storage to smart appliances, semiconductors and pharmaceutics [1-19]. Further inclusion of nanoparticles or adhesion to complex interfaces allows efficient control, tuning, and magnification of the already exceptional base macromolecular properties. To achieve superior characteristics, it is paramount to understand the complex structural and dynamic behavior of macromolecules, ideally at the level of atoms and molecules, under confinement and to relate them with macroscopic properties of the end material.

Especially relevant for numerous applications is the phase behavior, as macromolecular crystals exhibit distinctly different characteristics compared to polymer glasses. While phase transition, as observed in complex atomic systems, is extensively studied it is still far from being fully understood. The early work of Alder and Wainwright, based on collision-driven molecular dynamics (MD), demonstrated that monomeric hard spheres crystallize at high concentrations [20]. It is now established that given enough observation time, hard spheres or corresponding colloidal entities show spontaneous crystallization under a variety of conditions (microgravity, impurities, size polydispersity etc) once a critical range of packing densities is reached [21-42]. Given the athermal nature of such systems, entropy is the driving force of crystal nucleation and growth and dictates the resulting, thermodynamically stable, ordered morphologies. Recently, it has been demonstrated that dense packing of chains of hard spheres also crystallize [43-46]. It is possible to effectively control the phase behavior and/or the state of jamming [47-50] for polymers by properly tuning the bond gaps (or bond tangency) between successive monomers along the chain [51,52] or the bending angles that dictate chain flexibility [53,54]. Similar control can be achieved by applying spatial confinement; in the most trivial case this can be realized through the presence of flat, impenetrable, and parallel walls in at least one dimension.

In the past, we used a Monte Carlo (MC) scheme [55], built around chain-connectivity-altering MC moves [56-59], to generate and equilibrate freely-jointed chains of hard spheres of uniform size in the bulk. This allowed us to systematically study the effect of packing density, chain length and bond tangency/gaps on the local and global structure of athermal macromolecules [48,60,61], on the primitive path network of entanglements [49,62] and on the ability of chains to crystallize [43-46,52]. Recently, based on the original scheme of Ref. [55], we introduced a more general method including a wall-displacing algorithm which allows the simulation of athermal polymer packings under confinement [63]. This more general method has allowed us to simulate systems of very long chains under extreme confinement and at very high packing density and at high cell shape anisotropy. For the linear chains considered here the number of monomers is, $N_{\text {mon }}=N+1$, where $N$ is the number of bonds. Confining agents are flat, parallel and impenetrable surfaces (walls). Packing density, $\phi$, is defined as the volume occupied by all chain monomers divided by the volume of the simulation cell. The number of confined dimensions, $d_{\text {conf }}$, ranges from zero (unconstraint, bulk case) to three (fully confined). Extreme confinement is reached when the distance between the walls, $d_{\text {wall }}$, in at least one dimension approaches the size of sphere monomers, $\sigma$. Cell shape anisotropy is quantified through the cell aspect ratio, $\zeta$, which is the ratio of longest length(s) divided by the shortest one(s). In all cases cell shape corresponds to an orthogonal parallelepiped.

Through the proposed MC scheme we equilibrate dense athermal chain packings under extreme confinement that correspond to quasi-1D (tube-like) and quasi-2D (plate-like) polymer thin films [63]. In both cases as a critical combination of concentration and confinement is reached polymers transit to ordered morphologies characterized by structural defects. For plate-like packings this ordered state is a blend of hexagonal close packed (HCP) and face centered cubic (FCC) domains. Given that the system is athermal, any phase transition is driven by a change (increase) in the total entropy. Accordingly, to predict the phase transitions and to identify the thermodynamically stable phase, a first step is to calculate the configurational entropy of chains. Towards this, we map the corresponding atomistic chains onto self-avoiding random walks (SAWs) grown step-by-step on regular lattices subject to specific spatial restrictions. During the growth, the next position to lattice has to be adjacent to the current one. Self-avoidance condition dictates that no lattice point can be visited twice. In addition, the imposed spatial restrictions on SAW lattices mimic the ones encountered at the atomistic level. In a previous paper we enumerated the total number of SAWs for two different lattices SC (simple cubic) and FCC as a function of the system geometry and the number of chain bonds (or equivalently SAW steps) for quasi-1D, tube-like morphologies [64]. Here, we employ the same methodology to identify the SAW number and size distribution in quasi-2D, plate-like polymer films. Apart from the direct enumeration for moderately long chains our goal is to provide the scaling exponents in the growth
formulas that can be used to predict the SAW behavior as a function of chain size, crystal structure, and level of confinement for significantly longer chains.

The concept of random walk is central to stochastic processes and is applicable to a very wide range of scientific fields and research topics from mathematics, economics, image processing, and social networks to computer science, biology, genetics, and materials [65-91]. Self-avoiding random walks have been used extensively to study randomness as observed in kinetics, dynamics, propagation, growth, percolation phenomena and molecular conformations in soft matter [92-98]. Of particular importance is the SAW model in polymer science as it is directly related to the free-flight models describing chain conformations under various conditions (bulk, confinement, surface adsorption, non-linear chain architecture, chain flexibility, nanofillers etc.) [99-121]. From the technical perspective, since the early work of Orr [112], significant progress has been made towards the development of algorithms that allow efficient SAW enumeration and calculation of the critical exponents in scaling expressions [87,122-133]. These are important algorithmic milestones in the SAW enumeration problem that becomes more than exponentially difficult as the number of steps increases.

## 2. Materials and Methods

In a first step, Monte Carlo simulations have been conducted using the algorithm described in Ref. [63] to generate and successively equilibrate freely-jointed chains of tangent hard spheres of uniform size under plate-like confinement $\left(d_{\text {conf }}=1\right)$. Average chain lengths range from $N_{\text {mon }}=8$ to 1000 and packing densities from $\phi=0.20$ to 0.55 . We recall here that the freezing and melting points for monomeric hard spheres in the bulk correspond to 0.494 and 0.545 , respectively. For chains of tangent hard spheres in the bulk, given the crucial effect of bond tangency/gaps [51,52], the melting point is delayed until a concentration range of $\phi \approx 0.58$ is reached [43-46].

Initial system configurations correspond to cubic cells $(\zeta=1)$ under full confinement $\left(d_{\text {conf }}=3\right)$ which have been generated at dilute conditions and compressed through the wall-displacement (MRoB) algorithm [63] until the desired volume fraction is reached. Then, MRoB is further employed to progressively increase the cell aspect ratio. This process results in the inter-wall distance, $D_{\text {wall }}$, being reduced until the limit of extreme confinement $D_{\text {wall }} \rightarrow \sigma$. System configurations are generated at regular intervals during the box transformation phase. Subsequent long MC simulations undertake the task of equilibration with a duration that exceeds hundreds of billions of steps.

As will be demonstrated in the continuation flexible chains, under extreme plate-like confinement, crystallize into well-defined patterns at concentrations significantly lower than the ones in the bulk. Based on this, in the second phase we map the flexible polymer chain onto a SAW on restricted lattice. Here, we follow the original concept presented by Benito et al. [64] according to which in such spatially restricted polymer crystals monomers adopt positions which closely approach the sites of regular lattices. Accordingly, information on the configurational entropy of the freely-jointed chains in plate-like templates can be extracted by analyzing the corresponding SAWs on restricted crystal lattices under the same geometry and conditions (SAW length, lattice type).

We enumerate all possible distinct SAWs on regular lattices corresponding to cubic crystals (SC, BCC and FCC with coordination numbers 6,8 , and 12 , respectively). The reference case is the unrestricted one: SAWs on bulk systems under periodic boundary conditions applied in all dimensions. For the bulk lattices and given a specific chain model (i.e., fully flexible one) the number of distinct SAW configurations, $c_{N}$, and the average SAW size, as quantified through the mean square end-to-end distance $\left.\left.\langle | \omega^{N}\right|^{2}\right\rangle$, depend solely on the number of SAW steps, $N$. However, by introducing plate-like confinement, the spatial group symmetry of the original unrestricted system is reduced from the original Ia $\overline{3} \mathrm{~d}$. As a result of this, and of the heterogeneity of the confined system, three additional parameters must be considered: level (or intensity) of confinement, the relative orientation of the regular lattice with respect to the axis of confinement, and the initial position (origin) of the SAW, which will be referenced to as "Type" throughout the manuscript. The confinement level can be
expressed in terms of the number of crystal layers, $n$, between the parallel plates or as the corresponding inter-plate distance, $D_{\text {wall }}$, measured in units of the SAW step length.

The inclusion of the SAW origin (or Type) parameter is a result of the spatial restrictions and the break of symmetry imposed by the plate confinement: the symmetry of Ia $\overline{3} \mathrm{~d}$ of the bulk case is reduced to $\mathrm{I}_{1} /$ acd due to the presence of the flat, impenetrable walls along the confined dimension. As in Ref. [64] the orientation of the plate axis is defined by direction indices according to the crystallographic practice: [ijk]. Given that the crystalline domains are formed with their orientation aligned along the plate section the confining plates are contained in the planes of the crystallographic form [100]. Effectively, a SAW grows on a restricted lattice, $\operatorname{RL}\left(D_{\text {wall }}\right)$ defined as:

$$
\mathbf{R L}(D)=\left\{\underline{x}\left|x_{1}, x_{2} \in \mathbf{Z},\left|x_{3}\right|<D_{\text {wall }}\right\}\right.
$$

where $\underline{x}$ defines the coordinates of every lattice node and $Z$ is the unit hypercube of dimension one. Due to the symmetry of the cubic system any axis can be designated as the confined one, denoted in the equation above as $x_{3}$. The enumeration process and successive analysis take into account the SAW Type as an additional system parameter: For a given number of steps SAWs starting from origins close to the plate boundaries are expected to show smaller $c_{N}$ number than the ones growing far from them. Figure 1 shows various cases of plate confinement and the corresponding distinction of lattice sites belonging to different types. For simplicity, a 2-D square lattice is displayed with a varied number of layers, $n$. For the cubic (or square) lattice the number of layers coincides with the inter-plate distance (measured in units of SAW step length). However, this is not the case for the BCC and FCC lattices. Due to symmetry, all nodes that belong to the same layer are characterized by the same Type. Layers are colored according to their Type (SAW origin), which in turn depends on the distance from the closest confining boundary. For example, for $n=2$, two layers of lattice points exist but both correspond to the same SAW Type as they are similarly adjacent to a different plate wall. The value $n=3$ leads to two different SAW origins, one in the center and one touching the wall. In general, for the cubic crystal system (SC, BCC and FCC) under plate confinement for even values of the number of layers, $n$, there exist in total $n / 2$ distinct SAW Types, while for odd ones the corresponding number changes to $(n-1) / 2+1$. In the present work, the assignment of Type starts from the layers adjacent to the walls (Type 1) and ends at the ones in the middle. In Figure 1 for $n=6$, red (closest to the confining plates), green and yellow (furthest from the confining planes) layers have been assigned Types of 1, 2, and 3, respectively. Multiplicity corresponds to the number of crystallographically equivalent restricted lattices points. For even numbers of $n$ all Types have a multiplicity equal to 2 , and the same is true for odd numbers with the only exception being the points of the central layer which show cardinality of unity. Multiplicity of SAW Type is important to determine symmetry as it effectively reduces the number of studied systems and the corresponding computational time in SAW enumeration.


$$
n=4, \text { Types: } 1,2
$$


$n=6$, Types: 1,2 ,


Figure 1. Schematic representation (side view) of distinct origins to be considered for the enumeration of self-avoiding random walks (SAWs) for systems under plate-like confinement. Black lines at the top and bottom parts mark the confining boundaries (plates). Level of confinement is quantified through the number of crystal layers between the plates, $n$, along the axis of confinement. Labeling according to SAW origin depends on the distance from the closest plate. Different color corresponds to different SAW origin (Type). Red, green and yellow colors correspond to Type 1 (closest to the plates), 2 and 3 (furthest from the plates).

A distinction between the different lattices of the cubic system can be established once the number of layers between plates becomes equal or exceeds 2 . Obviously, the most extreme case corresponds to a single layer under confinement, i.e., $n=1$. In such 2-D templates the corresponding lattices, studied in the present work, are honeycomb (coordination number of 3), square (coordination number of 4 ) and triangular (coordination number of 6) as seen in Figure 2.


Figure 2. Schematic representation (top view) of the 2-D lattice templates studied here corresponding to extreme thin-film confinement (one layer between confining plates, $n=1$ ). From left to right: honeycomb (coordination number of 3 ), square lattice (coordination number of 4 ) and triangular (coordination number of 6) lattices.

To summarize, for the given chain architecture (fully flexible linear chains) the number and size of SAWs depend on (i) number of steps, $N$, (ii) lattice type, (iii) level of plate confinement, quantified primarily here through the number of crystal layers between the parallel plates, $n$ and (iv) Type (point of SAW origin). The parametric analysis per regular lattice is as follows: $\mathrm{SC}: N \in[1,18], n \in[1,5]$; BCC: $N \in[1,15], n \in[1,5] ;$ FCC: $N \in[1,13], n \in[1,5]$. Obviously, in direct enumeration for a fixed number of SAW steps computational time increases as the coordination number of the lattice increases. Accordingly, the longest chains were accessed for the SC lattice and the shortest SAWs were modeled for the FCC crystal.

In total 376 different 3-D systems were studied: 150 for SC, 117 for BCC and 109 for FCC restricted lattices. In the most extreme case, corresponding to 2 -D polymer films, 58 systems were studied: 25 for the honeycomb, 18 for the square, and 15 for the triangular lattices. The main parameters of the modeled systems are reported in Table 1. A home-made SAW code for direct enumeration was developed and all simulations were conducted on Linux-based Intel i7-8700K CPU architectures with 32 Gb of memory.

Table 1. Regular lattices studied in three dimensions (simple cubic (SC), body centered cubic (BCC) and face centered cubic, (FCC)), and in two dimensions (honeycomb (HON), square (SQU) and triangular (TRI)). Also shown are the number of layers, $n$, and the distance, $D_{\text {wall }}$, between the confining plates and the different SAW Types (points of origin). Inter-plate distance is measured in units of the SAW step length.

| Lattice Type | Number of Layers <br> between Plates, $\boldsymbol{n}$ | Distance between <br> Plates, $\boldsymbol{D}_{\text {wall }}$ | Type (SAW Origin) |
| :---: | :---: | :---: | :---: |
| SC | 2 | 1 | 1 |
|  | 3 | 2 | 1,2 |
|  | 4 | 3 | 1,2 |
| BCC | 5 | 4 | $1,2,3$ |
|  | 2 | $1 / \sqrt{3}$ | 1 |
|  | 3 | $2 / \sqrt{3}$ | 1,2 |
|  | 4 | $3 / \sqrt{3}$ | 1,2 |
| FCC | 5 | $4 / \sqrt{3}$ | $1,2,3$ |
|  | 2 | $1 / \sqrt{2}$ | 1 |
|  | 3 | $\sqrt{2}$ | 1,2 |
|  | 4 | $3 / \sqrt{2}$ | 1,2 |
| HON | 5 | $2 \sqrt{2}$ | $1,2,3$ |
| SQU | 1 | 0 | 1 |
| TRI | 1 | 0 | 1 |

## 3. Results

### 3.1. Monte Carlo Simulations

Snapshots at the end of the MC equilibration for the $N_{\text {mon }}=12$ system can be seen in Figure 3. The system contains 100 chains with a minimum and maximum chain length of 8 and 16 , respectively, at $\phi=0.50$ under unidimensional, plate confinement $\left(d_{\text {conf }}=1\right)$ and for various cell aspect ratios. The packing density $\phi=0.50$ of all structures in Figure 3 is well below the transition point for athermal chains in the bulk ( $\phi \approx 0.58$ ). Still, as can be seen from a visual inspection of the bottom-right panel of Figure 3, which corresponds to extreme confinement ( $\zeta=12$ and $D_{\text {wall }}=2$ ), monomers on both surfaces show very clear signs of ordering.


Figure 3. Snapshots of the 100-chain $N_{\text {mon }}=12$ hard sphere system at $\phi=0.50$ and under unidimensional confinement $\left(d_{\text {conf }}=1\right)$ for various cell aspect ratios, $\zeta$, corresponding to plate-like geometries. From left to right and from top to bottom: $\zeta=1(10.8), 3(5.2), 7(3.0)$ and $12(2.0)$. Number in parenthesis indicates the inter-wall distance in the direction of confinement (in units of sphere diameter). Sphere monomers are color-coded according to the parent chain. Image panels created with the VMD software [134]. (please see supplementary materials for 3D version).

Crystal nucleation and growth can be accurately identified and then quantified by applying the characteristic crystallographic element (CCE) norm, which is able to distinguish between different competing crystal structures $[44,135,136]$. As the athermal chain packings correspond to high concentration, we employ the CCE norm with respect to the FCC and HCP crystals as well as the fivefold local symmetry. The CCE norm is applied on all sites/monomers present in the system. Once the value of the CCE norm with respect to a specific crystal $X, \varepsilon^{X}$, is lower than a critical threshold $\left(\varepsilon^{X}<0.245\right)$, the site is identified as of $X$ similarity. Due to the distinguishing nature of the crystallographic elements, no site can possess dual crystal similarity. Figure 4 hosts configurations, as the MC simulation evolves, for the 10 -chains $N_{\text {mon }}=1000$ system at $\phi=0.55$ (still quite below the bulk melting point of athermal polymers), showing only monomers with HCP (blue), FCC (red) and fivefold (green) local environment. All other sites, labeled as "amorphous", are not shown for clarity purposes. Starting from the initially amorphous state (upper panel), the system shows a clear disorder-order transition with the stable crystal increasing in size as the observation time increases. The final stable configuration is highly close packed with predominant HCP character.


Figure 4. Snapshots of the 10-chain $N_{\text {mon }}=1000$ system at $\phi=0.55$ under plate-like confinement with cell anisotropy index, $\zeta=5$ and interwall distance, $D_{\text {wall }} \approx 7$. Top: very early in the simulation ( $10^{9} \mathrm{MC}$ steps); middle: (left) $2 \times 10^{10}$ and $5 \times 10^{10}$ (right) MC steps; bottom: $12 \times 10^{10}$ (left) and at the end of simulation, $14 \times 10^{11}$ (right) MC steps. Monomers with HCP, FCC and fivefold similarity as identified by the CCE norm, are shown in blue, red and green, respectively. All other, "amorphous" sites do not appear for clarity. Image created with the VMD software [134]. (please see supplementary materials for 3D version).

### 3.2. Verification with Available Literature Data

As mentioned in Section 2, centers of the spherical monomers adopt positions that resemble closely nodes of a perfect crystal. For example, this tendency is particularly evident for the case shown in the bottom-right panel of Figure 3. Thus, we model linear flexible polymers in confined space as self-avoiding random walks on restricted lattices.

First, results are compared against literature data on the well-studied SAWs on bulk 3-D SC, BCC and FCC lattices and on most extremely confined ones that correspond to 2-D lattices (HON, SQU and TRI). The unrestricted (bulk) case can be modeled either by removing any spatial conditions related to confinement or by having the number of lattice layers, $n$, to be larger than the maximum possible chain extension, i.e. $n>N+1$. Data on the number of distinct SAWs, $c_{N}$, and on the mean square end-to-end distance, $\left.\left.\langle | \omega^{N}\right|^{2}\right\rangle$, as a function of SAW steps, $N$, can be found in Tables A1 and A2 of the Appendix A for the extremely confined 2-D and the unrestricted 3-D lattices, respectively. For all regular lattices studied here extreme confinement $(n=1)$ involves a single SAW origin (Type 1 ); the same is true for the 3-D bulk cases due to symmetry considerations. Results for the bulk SC and FCC lattices are in perfect quantitative agreement with our past work conducted through a different numerical algorithm [64]. Furthermore, for both SAW populations and average sizes our enumeration data coincide with the ones in Refs. [131] and [132] for SC; in Ref. [133] for bulk BCC and FCC; in Ref. [137] for the 2-D triangular and in Ref. [128] for square, honeycomb, and SC lattices. We should note here that, given the large number of systems to be studied (three different lattice types, different Types and levels of confinement), our goal is not to exceed or even reach the current state-of-the-art in modeled SAW lengths but rather to establish asymptotic scaling formulas for the confined cases. These will allow us to predict the behavior of long SAWs (and equivalently of long chains) from results on short or intermediate ones and establish a systematic connection between plate-like confinement and properties of the corresponding SAWs. Tables A3-A12 host the properties of SAWs ( $c_{N}$ and $\left.\left.\langle | \omega^{N}\right|^{2}\right\rangle$ ) for all confined lattices with the number of layers between plates lying in the interval $n \in[2,5]$. An interesting trend can be observed for the BCC lattice with $n=2$ (Table A3): the number of distinct SAWs coincides with the one extracted for the SQU lattice (Table A1). This is because with respect to connectivity there is no distinction between the square and the 2-layer BCC lattices.

### 3.3. Direct SAW Enumeration

Data ( $c_{N}$ vs. $N$ and $\left.\left.\langle | \omega^{N}\right|^{2}\right\rangle$ vs. $N$ ) as presented in Tables A1-A12, obtained from SAWs of short to intermediate length, can be used in the asymptotic formulas [131,133,137] for the scaling of the number of distinct SAWs in the limit of $N \rightarrow \infty$ :

$$
\begin{equation*}
c_{N} \sim A \mu^{N} N^{\gamma-1} \tag{1}
\end{equation*}
$$

and of the mean-square, end-to-end distance:

$$
\begin{equation*}
\left.\left.\langle | \omega^{N}\right|^{2}\right\rangle \sim D N^{2 v} \tag{2}
\end{equation*}
$$

where $\gamma$ and $v$ are the critical exponents, $A$ and $D$ are the critical amplitudes, and $\mu$ is the connective constant. While $A, D$, and $\mu$ depend on lattice type the critical exponents $\gamma$ and $v$ are considered universal [133,137-139]. As proven by Duminil-Copin and Smirnov [140] the connective constant for the honeycomb lattice is equal to $\mu=\sqrt{2+\sqrt{2}}$, as originally conjectured by Nienhuis [141,142].

Figures 5-7 present the logarithm of the number of distinct SAWs versus the logarithm of the number of SAW steps for the restricted SC, BCC, and FCC lattices, respectively. For all systems studied here, the combination of SAW size (chain length) and applied confinement force the self-avoiding random walks to "feel" the imposed spatial constraints. In all cases the obvious trend is fully established: the stronger the restrictions imposed by the film-like confinement the smaller the number of available

SAWs, or equivalently, the fewer the number of distinct chain configurations and accordingly reduced configurational entropy. The most extremely confined system ( $n=1$ for SC (SQU) or $n=2$ for BCC and FCC) is the one that deviates markedly from the unrestricted bulk case. As film thickness (inter-plate distance) increases SAW properties converge to the ones in the bulk. Between different Types, the lattice nodes and layers lying closer to the confining surfaces are characterized systematically by smaller $c_{N}$ than the ones near the center. This is manifestly valid for the SC and FCC lattices, but not always true for the BCC, as can be readily observed by comparing the different Type columns in the Appendix A Tables. This difference in trends can be explained by the coordination number which remains the same for SC but depends on the layer index for BCC. In general, the effect of SAW origin (Type) on SAW properties is smaller in plate-like (quasi 2-D) confinement, as established here, than in tube-like (quasi 1-D) restricted lattices, as reported in Ref. [64].


Figure 5. Logarithm of the number of distinct $\mathrm{SAWs}, c_{N}$, versus the logarithm of the number of SAW steps, $N$, as obtained from direct enumeration on the SC lattice under plate-like confinement. n corresponds to the number of layers between the confining plates. Label "Type" corresponds to different SAW origin as explained in Figure 1 and related text. The most extremely confined case of $n=1$ corresponds to the 2-D square lattice (SQU).


Figure 6. Logarithm of the number of distinct $\mathrm{SAWs}, c_{N}$, versus the logarithm of the number of SAW steps, $N$, as obtained from direct enumeration on the BCC lattice under plate-like confinement.


Figure 7. Logarithm of the number of distinct $\mathrm{SAWs}, c_{N}$, versus the logarithm of the number of SAW steps, $N$, as obtained from direct enumeration on the FCC lattice under plate-like confinement.

Comparing the different restricted lattices of the cubic system trends analogous to the bulk case are established as the number of distinct SAWs increases significantly with the coordination number. For example, for a fixed number of SAW steps $(N=12)$, film thickness $(n=3)$, and SAW origin (Type 1), SAW population starts from $c_{N}=33,574,732$ (SC), increases to $47,788,288$ (BCC), and end ups at $56,963,463,220$ (FCC); an increment that spans three orders of magnitude for identical conditions of spatial restriction and which can be purely attributed to the increase in coordination number.

The dependence of SAW size, as quantified by the mean square end-to-end distance, on the number of SAW steps is presented in Figures $8-10$ for the SC, BCC, and FCC restricted lattices, respectively.


Figure 8. Logarithm of the mean square end-to-end SAW distance, $\left.\left.\langle | \omega^{N}\right|^{2}\right\rangle$, as a function of the logarithm of SAW steps, $N$, as obtained for the SC lattice under plate-like confinement. $n$ corresponds to the number of layers between the confining plates. Label "Type" corresponds to different SAW origin as explained in Figure 1 and related text. The limiting case of $n=1$ corresponds to the 2-D square lattice (SQU). Dashed black line corresponds to best linear fit on bulk SAW data.


Figure 9. Logarithm of the mean square end-to-end SAW distance, $\left.\left.\langle | \omega^{N}\right|^{2}\right\rangle$, as a function of the logarithm of SAW steps, $N$, as obtained for the BCC lattice under plate-like confinement. Dashed black line corresponds to best linear fit on the bulk case over the whole range of available data.


Figure 10. Logarithm of the mean square end-to-end SAW distance, $\left.\left.\langle | \omega^{N}\right|^{2}\right\rangle$, as a function of the logarithm of SAW steps, $N$, as obtained for the FCC lattice under plate-like confinement. Dashed black line corresponds to best linear fit on the bulk case over the whole range of available data.

Based on the $\log \left(c_{N}\right)-v s .-\log (N)$ (Figures 5-7) and the $\left.\log \left(\left.\langle | \omega^{N}\right|^{2}\right\rangle\right)-v s .-\log (N)$ (Figures 8-10), non-linear fits on the growth formulas in Equations (1) and (2) yield all critical parameters $(A, D$, $\mu, \gamma$ and $v$ ). Results from such statistical analysis can be found in Tables $2-4$ for the restricted SC,

BCC, and FCC lattices, respectively. In all cases data are compared with the reference bulk crystal. The connectivity constant, $\mu$, decreases as the spatial restriction becomes stronger. It adopts the lowest value for the most extremely confined system and as the number of layers increases it progressively converges to the limiting value of the bulk counterpart. Compared to the connectivity constant the critical amplitude, $A$ and the exponent $\gamma$ depend rather weakly on level of confinement and SAW origin. Under the same conditions of confinement, connectivity constant increases as the lattice coordination number increases ( $\mu_{\mathrm{SC}}<\mu_{\mathrm{BCC}}<\mu_{\mathrm{FCC}}$ ). In general, for SC and FCC restricted lattices, for layers closer to the confining agents, $\mu$ is higher than for layers near the center, i.e., the connectivity constant decreases with increasing Type index for SC and FCC while the opposite trend is observed for the BCC lattice.

Table 2. Critical parameters of the asymptotic formulas (Equations (1) and (2)) as obtained from non-linear fits on the SAW data presented in Figures 5 and 8 for the confined SC lattice. Also shown for comparison are the results for the bulk (unrestricted) SC.

| $\boldsymbol{N}$ | Type | $\boldsymbol{A}$ | $\boldsymbol{\mu}$ | $\boldsymbol{\gamma}$ | $\boldsymbol{D}$ | $\boldsymbol{v}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 1 | 1.375 | 3.622 | 1.181 | 0.958 | 0.631 |
| 3 | 1 | 1.214 | 4.090 | 1.097 | 0.903 | 0.619 |
|  | 2 | 1.515 | 3.963 | 1.236 | 0.761 | 0.650 |
| 4 | 1 | 1.137 | 4.373 | 0.988 | 1.267 | 0.552 |
|  | 2 | 1.430 | 4.188 | 1.226 | 0.942 | 0.598 |
| 5 | 1 | 1.102 | 4.523 | 0.919 | 1.445 | 0.535 |
|  | 2 | 1.377 | 4.353 | 1.165 | 1.103 | 0.569 |
|  | 3 | 1.387 | 4.308 | 1.258 | 0.983 | 0.585 |
| Bulk |  | 1.270 | 4.717 | 1.103 | 1.026 | 0.607 |

Table 3. Critical parameters of the asymptotic formulas (Equations (1) and (2)) as obtained from non-linear fits on the SAW data presented in Figures 6 and 9 for the confined BCC lattice. Also shown for comparison are the results for the bulk (unrestricted) case.

| $\boldsymbol{N}$ | Type | $\boldsymbol{A}$ | $\boldsymbol{\mu}$ | $\boldsymbol{\gamma}$ | $\boldsymbol{D}$ | $\boldsymbol{v}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 1 | 1.480 | 2.658 | 1.228 | 0.625 | 0.725 |
| 3 | 1 | 1.087 | 3.765 | 1.559 | 0.553 | 0.720 |
|  | 2 | 1.783 | 4.326 | 0.849 | 0.597 | 0.709 |
| 4 | 1 | 0.888 | 4.548 | 1.527 | 0.602 | 0.682 |
|  | 2 | 1.634 | 4.860 | 1.116 | 0.603 | 0.682 |
| 5 | 1 | 0.782 | 5.133 | 1.384 | 0.847 | 0.605 |
|  | 2 | 1.455 | 5.420 | 1.058 | 0.662 | 0.651 |
|  | 3 | 1.580 | 5.115 | 1.308 | 0.641 | 0.656 |
| Bulk |  | 1.214 | 6.580 | 1.108 | 1.101 | 0.600 |

Table 4. Critical parameters of the asymptotic formulas (Equations (1) and (2)) as obtained from non-linear fits on the SAW data presented in Figures 7 and 10 for the confined FCC lattice. Also shown for comparison are the results for the bulk (unrestricted) case.

| $\boldsymbol{N}$ | Type | $\boldsymbol{A}$ | $\mu$ | $\boldsymbol{\gamma}$ | $\boldsymbol{D}$ | $\boldsymbol{v}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 1 | 1.358 | 5.888 | 1.257 | 0.606 | 0.707 |
| 3 | 1 | 1.088 | 7.346 | 1.307 | 0.653 | 0.659 |
|  | 2 | 1.605 | 7.473 | 1.163 | 0.604 | 0.676 |
| 4 | 1 | 0.941 | 8.462 | 1.145 | 0.889 | 0.586 |
|  | 2 | 1.468 | 8.178 | 1.233 | 0.687 | 0.634 |
| 5 | 1 | 0.869 | 9.171 | 1.010 | 1.217 | 0.525 |
|  | 2 | 1.356 | 8.836 | 1.148 | 0.860 | 0.584 |
|  | 3 | 1.425 | 8.439 | 1.359 | 0.625 | 0.649 |
| Bulk |  | 1.191 | 10.08 | 1.129 | 0.975 | 0.587 |

The SAW generating function (Equation (1)) is valid for the whole range of available data, independently of dimensionality, lattice type, level of confinement, and point of origin (Type). However, the same is not true for the dependence of SAW size on number of SAW steps (Equation (2)). While the unrestricted lattices show linear scaling all confined ones at short- $N$ deviate significantly from linearity. Such trends have also been observed in the SAW analysis of restricted lattices under tube-like confinement [64]. The larger the lattice coordination number and the closer to the confining plates (low Type index), the most prolonged the duration of the anomalous regime, as can be seen in Figure 11 where the SAW size evolution is presented for the SC, BCC, and FCC lattices with $n=3$ and Type 1.


Figure 11. Logarithm of the mean square end-to-end SAW distance, $\left.\left.\langle | \omega^{N}\right|^{2}\right\rangle$, as a function of logarithm of number of SAW steps for the SC, BCC and FCC lattices under plate confinement ( $n=3$, Type 1 ). Also shown are the lines that correspond to best linear fits in the large-N data range once normal scaling has been established.

Based on the parameters extracted from the linear fitting in the range of large- $N$ data the following conclusions can be established: in general, the critical exponent, $v$, adopts its maximum value under the most confined case while its minimum corresponds to the unrestricted (bulk) case. All confined systems are characterized by amplitude values $D$ which are significantly different than the ones of the bulk lattice. For restricted SC and FCC lattices, SAW origin (practically the distance of the layer from the confining agents) has an appreciable effect on $D$ and $v$ values. As Type index increases $D$ decreases appreciably and the opposite trend is observed for $v$. The behavior of the BCC restricted lattice does not follow the trends of the other two crystals. Accordingly, no systematic behavior can be identified for BCC crystal.

### 3.4. SAW Size Distribution

Information is also available not only on the average SAW size but also on the probability distribution function (PDF) and cumulative distribution function (CDF) as a function of lattice type, level of confinement and SAW origin (Type). Additional information can be extracted from the analysis of the folded CDF variant focusing on the median and the corresponding deviation. Given the plethora of systems studied and due to space limitations, in the following only selected systems are presented
for the size distribution. Figure 12 shows the PDF of size as a function of the number of layers between confinement, $n$, for the restricted SC having fixed $N=16$ and Type 1 . As stated before, the case of $n=1$ corresponds to the 2-D square lattice. The number of confined layers has a significant effect on the size distribution: the most extreme confinement $(n=1)$ and the least confined $(n=5)$ cases correspond to the broadest and narrowest distributions, respectively. In general, as confinement increases, the size distribution becomes broader and shifts to higher values.


Figure 12. Probability distribution function (PDF) of the square end-to-end distance for the SC restricted lattice for SAWs of fixed length $(N=16)$ and point of origin (Type 1). Different curves correspond to differ number of layers between the confining plates, $n$. The case of $n=1$ corresponds to the 2-D square lattice (SQU).

Not surprisingly, the number of SAW steps has a stronger effect on the SAW size distribution as seen in Figure 13 for the BCC restricted lattice ( $n=5$, Type 3). As chain length increases the distribution becomes broader, it shifts to higher values and the corresponding maxima get significantly reduced. The effect of point of SAW origin (Type) on the SAW distribution is presented in Figure 14 for the FCC lattice $(N=11, n=5)$. For up to two layers in plate-like confinement there is no distinction in SAW Type. Based on the results in Figure 14 it can be concluded that Type (in other words the starting layer) has a minor effect on SAW size, which is further diminishing as the number of SAW steps increases.


Figure 13. Probability distribution function (PDF) of the square end-to-end distance for the BCC restricted lattice for SAWs of fixed number of layers between confining plates $(n=5)$ and point of origin (Type 3). Different curves correspond to different number of SAW steps, $N$.


Figure 14. Probability distribution function (PDF) of the square end-to-end distance for the FCC restricted lattice for SAWs of fixed length $(N=11)$ and number of layers between confining plates ( $n=$ 5). Different curves correspond to different point of origin (Type).

Cumulative distribution functions and the folded variants for SAW size, as quantified by the square end-to-end distance, are presented in Figure 15 (SC lattice with fixed $n=5$, Type 3 and varied $N$ ), Figure 16 (BCC lattice with fixed $N=14, n=5$ and varied Type), and Figure 17 (FCC lattice with fixed $N=11$, Type 1 and varied $n$ ).


Figure 15. (Left Panel) Cumulative distribution function (CDF) and (Right Panel) the folded variant of the square end-to-end distance for the SC restricted lattice for SAWs of fixed number of confined layers $(n=5)$ and point of origin (Type 3). Different curves correspond to different number of SAW steps, $N$.


Figure 16. (Left Panel) Cumulative distribution function (CDF) and (Right Panel) the folded variant of the square end-to-end distance for the BCC restricted lattice for SAWs of fixed length $(N=14)$ and number of layers between confining planes $(n=5)$. Different curves correspond to different SAW origins (Types).


Figure 17. (Left Panel) Cumulative distribution function (CDF) and (Right Panel) the folded variant for the square end-to-end distance for the FCC restricted lattice for SAWs of fixed length $(N=11)$ and point of origin (Type 1). Different curves correspond to different number of layers between the confining plates, $n$.

The same conclusions can be drawn from the data of the cumulative and folded distributions. As the number of SAW steps increases, the distribution of size becomes broader, shifts to higher values, and the intensity of the observed maxima drops. SAW origin has a minor effect on size statistics. The inter-plate thickness has the strongest effect as the more confined the polymer chain, the more extended it becomes. The statistics of the selected folded distributions (most probable, median, and deviation values) can be found in Tables A13-A18 of the Appendix A. All lattice types show identical trends, especially the strong dependence on film thickness and the very weak one on SAW origin, as validated by the comparison of the mean value and the corresponding deviation.

## 4. Conclusions and Future Plans

In the present contribution, we have studied the behavior of athermal polymer chains under extreme confinement realized through the presence of parallel, flat, and impenetrable walls in one dimension. The inter-plate distance is so small that it practically adopts values similar to the size of the spherical monomers. Presently, Monte Carlo simulations show that dense packings of highly confined chains tend to crystallize at volume fractions which are significantly lower than the corresponding threshold of the bulk case. In an effort to identify the thermodynamic stability of the corresponding structures and the entropic origins of the phase transitions, we have mapped the athermal chains onto self-avoiding random walks (SAWs) on lattices which are further spatially confined as the atomistic analogs. Given that the applied confinement breaks the original maximal symmetry of the original crystal, we have analyzed the effect of number of SAW steps (chain length), the level of confinement (film thickness quantified by the number of lattice layers between the plates), and point of origin on the size of chains and on their number of distinct conformations. The latter is important as it is directly related to the configurational entropy of the chains.

The present work on plate-like (quasi 2-D) confinement, as well as the past on tube-like (quasi 1-D) restrictions [64], constitute the first step of an ongoing research effort. The final goal is to investigate and predict phase (disorder-order) transitions in confined athermal polymeric systems, for which entropy is the sole driving force. The entropy of the freely-jointed chains in plate-like templates can be obtained by direct enumeration of SAWs on restricted crystal lattices under the same geometry and conditions (SAW length, lattice type).

Supplementary Materials: The following are available online at http://www.mdpi.com/2073-4360/12/4/799/s1: An interactive, 3-D version of the manuscript; 3-D versions of Figures 3 and 4; 3-D video showing animated the panels of Figure 4.
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## Abbreviations

The following abbreviations have been used in this manuscript:
MC Monte Carlo
MD Molecular Dynamics
SAW Self-Avoiding Random Walk
CCE Characteristic Crystallographic Element (norm)
SC Simple Cubic
BCC Body Center Cubic
FCC Face Center Cubic
PDF Probability Distribution Function
CDF Cumulative Distribution Function
HON Honeycomb
SQU Square
TRI Triangular

## Appendix A

In the following Tables, we present the number of distinct configurations, $c_{N}$, and the mean square end-to-end distance, $\left.\left.\langle | \omega^{N}\right|^{2}\right\rangle$, for the self-avoiding random walks (SAWs) as a function of the number of SAW steps, $N$, under plate-like confinement. System parameters include lattice type, number of layers between confining plates, $n$, and Type (SAW origin). Also shown for comparison are the results obtained from simulations on corresponding 2-D lattices (honeycomb (HON), square (SQU) and triangular (TRI)) corresponding to extreme (single-layer) confinement.

Table A1. Properties of SAWs on 2-D regular lattices corresponding to extreme, plate-like confinement: honeycomb (HON), square (SQU) and triangular (TRI). In all cases $n=1$ and Type 1 .

|  | HON ( $n=1$, Type 1) |  | SQU ( $n=1$, Type 1 ) |  | TRI ( $n=1$, Type 1) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $N$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ |
| 1 | 3 | 1.000 | 4 | 1.000 | 6 | 1.000 |
| 2 | 6 | 3.000 | 12 | 2.667 | 30 | 2.400 |
| 3 | 12 | 5.500 | 36 | 4.556 | 138 | 4.217 |
| 4 | 24 | 8.250 | 100 | 7.040 | 618 | 6.350 |
| 5 | 48 | 11.13 | 284 | 9.563 | 2730 | 8.741 |
| 6 | 90 | 15.00 | 780 | 12.57 | 11,946 | 11.36 |
| 7 | 174 | 18.69 | 2172 | 15.56 | 51,882 | 14.20 |
| 8 | 336 | 22.50 | 5916 | 19.01 | 224,130 | 17.24 |
| 9 | 648 | 26.42 | 16,268 | 22.41 | 964,134 | 20.47 |
| 10 | 1218 | 31.18 | 44,100 | 26.24 | 4,133,166 | 23.87 |
| 11 | 2328 | 35.59 | 120,292 | 30.02 | 17,668,938 | 27.43 |
| 12 | 4416 | 40.34 | 324,932 | 34.19 | 75,355,206 | 31.16 |
| 13 | 8388 | 45.14 | 881,500 | 38.30 | 320,734,686 | 35.03 |
| 14 | 15,780 | 50.49 | 2,374,444 | 42.79 | 1,362,791,250 | 39.06 |
| 15 | 29,892 | 55.59 | 6,416,596 | 47.22 | 5,781,765,582 | 43.22 |
| 16 | 56,628 | 61.13 | 17,245,332 | 51.99 |  |  |
| 17 | 106,200 | 66.60 | 46,466,676 | 56.72 |  |  |
| 18 | 199,350 | 72.53 | 124,658,732 | 61.77 |  |  |
| 19 | 375,504 | 78.29 |  |  |  |  |
| 20 | 704,304 | 84.46 |  |  |  |  |
| 21 | 1,323,996 | 90.53 |  |  |  |  |
| 22 | 2,479,692 | 97.01 |  |  |  |  |
| 23 | 4,654,464 | 103.4 |  |  |  |  |
| 24 | 8,710,212 | 110.1 |  |  |  |  |
| 25 | 16,328,220 | 116.7 |  |  |  |  |

Table A2. Number of distinct configurations of SAWs on 3-D regular lattices without spatial restrictions (bulk case): simple cubic (SC), body center cubic (BCC) and face center cubic (FCC). Due to symmetry all nodes correspond to a single SAW origin (Type 1).

|  | SC (bulk, Type 1) | BCC (bulk, Type 1) | FCC (bulk, Type 1) |
| :---: | ---: | ---: | ---: | ---: |
| $\boldsymbol{N}$ | $\boldsymbol{c}_{\boldsymbol{N}}$ | $\boldsymbol{c}_{\boldsymbol{N}}$ | $\boldsymbol{c}_{\boldsymbol{N}}$ |
| 1 | 6 | 8 | 12 |
| 2 | 30 | 56 | 132 |
| 3 | 150 | 392 | 1404 |
| 4 | 726 | 2648 | 14,700 |
| 5 | 3534 | 17,960 | 152,532 |
| 6 | 16,926 | 120,056 | $1,573,716$ |
| 7 | 81,390 | 804,824 | $16,172,148$ |
| 8 | 387,966 | $5,351,720$ | $165,697,044$ |
| 9 | $1,853,886$ | $35,652,680$ | $1,693,773,924$ |
| 10 | $8,809,878$ | $236,291,096$ | $17,281,929,564$ |
| 11 | $41,934,150$ | $1,568,049,560$ | $176,064,704,412$ |
| 12 | $198,842,742$ | $10,368,669,992$ | $1,791,455,071,068$ |
| 13 | $943,974,510$ | $68,626,647,608$ | $18,208,650,297,396$ |
| 14 | $4,468,911,678$ | $453,032,542,040$ |  |
| 15 | $21,175,146,054$ | $2,992,783,648,424$ |  |
| 16 | $100,121,875,974$ |  |  |
| 17 | $473,730,252,102$ |  |  |
| 18 | $2,237,723,684,094$ |  |  |

Table A3. Properties of SAWs on the SC, BCC and FCC lattices with two layers between the confining plates ( $n=2$, Type 1 ).

|  | SC $(n=2$, Type 1) |  | BCC $(n=2$, Type 1) |  | FCC $(n=2$, Type 1) |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $\boldsymbol{N}$ | $\boldsymbol{c}_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{\mathbf{2}}\right\rangle$ | $\boldsymbol{c}_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{\mathbf{2}}\right\rangle$ | $\boldsymbol{c}_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ |
| 1 | 5 | 1.000 | 4 | 1.000 | 8 | 1.000 |
| 2 | 20 | 2.400 | 12 | 1.778 | 56 | 2.000 |
| 3 | 80 | 3.800 | 36 | 3.370 | 368 | 3.152 |
| 4 | 304 | 5.421 | 100 | 4.693 | 2336 | 4.510 |
| 5 | 1168 | 7.000 | 284 | 6.709 | 14,576 | 6.037 |
| 6 | 4348 | 8.854 | 780 | 8.383 | 89,928 | 7.713 |
| 7 | 16,336 | 10.68 | 2172 | 10.70 | 550,504 | 9.523 |
| 8 | 60,208 | 12.77 | 5916 | 12.68 | $3,349,864$ | 11.46 |
| 9 | 223,352 | 14.83 | 16,268 | 15.27 | $20,290,360$ | 13.51 |
| 10 | 817,852 | 17.14 | 44,100 | 17.50 | $122,445,504$ | 15.68 |
| 11 | $3,008,872$ | 19.43 | 120,292 | 20.35 | $736,685,008$ | 17.95 |
| 12 | $10,968,400$ | 21.94 | 324,932 | 22.79 | $4,421,048,016$ | 20.32 |
| 13 | $40,123,760$ | 24.42 | 881,500 | 25.87 |  |  |
| 14 | $145,783,980$ | 27.12 | $2,374,444$ | 28.52 |  |  |
| 15 | $531,100,496$ | 29.78 | $6,416,596$ | 31.81 |  |  |
| 16 | $1,924,770,512$ | 32.65 |  |  |  |  |
| 17 | $6,990,248,624$ | 35.49 |  |  |  |  |
| 18 | $25,282,157,540$ | 38.52 |  |  |  |  |

Table A4. Properties of SAWS on SC lattice with 3 layers between the confining plates ( $n=3$, Type 1,2 ).

| SC ( $n=3$, Type 1) |  |  | SC ( $n=3$, Type 2) |  |
| :---: | :---: | :---: | :---: | :---: |
| $N$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ |
| 1 | 5 | 1.000 | 6 | 1.000 |
| 2 | 21 | 2.476 | 28 | 2.286 |
| 3 | 92 | 3.957 | 124 | 3.581 |
| 4 | 392 | 5.571 | 516 | 5.054 |
| 5 | 1684 | 7.090 | 2156 | 6.492 |

Table A4. Cont.

| SC $(n=3$, Type 1) |  | SC $(n=3$, Type 2) |  |  |
| :---: | ---: | ---: | ---: | ---: |
| $\boldsymbol{N}$ | $\boldsymbol{c}_{\boldsymbol{N}}$ | $\left.\left.\langle \| \omega^{N}\right\|^{\mathbf{2}}\right\rangle$ | $\boldsymbol{c}_{\boldsymbol{N}}$ | $\left.\left.\langle \| \omega^{N}\right\|^{\mathbf{2}}\right\rangle$ |
| 6 | 7036 | 8.748 | 8804 | 8.125 |
| 7 | 29,396 | 10.35 | 36,388 | 9.717 |
| 8 | 120,776 | 12.10 | 148,452 | 11.50 |
| 9 | 497,196 | 13.81 | 609,812 | 13.25 |
| 10 | $2,026,220$ | 15.68 | $2,478,484$ | 15.19 |
| 11 | $8,278,076$ | 17.53 | $10,113,692$ | 17.10 |
| 12 | $33,574,732$ | 19.53 | $40,934,604$ | 19.18 |
| 13 | $136,456,380$ | 21.52 | $166,170,388$ | 21.23 |
| 14 | $551,445,764$ | 23.67 | $670,410,548$ | 23.44 |
| 15 | $2,232,227,600$ | 25.81 | $2,711,129,404$ | 25.63 |
| 16 | $8,995,089,168$ | 28.09 | $10,911,074,820$ | 27.97 |
| 17 | $36,297,709,788$ | 30.36 | $43,995,500,972$ | 30.28 |

Table A5. Properties of SAWs on SC lattice with four layers between the confining plates ( $n=4$, Type 1, 2).

| SC ( $n=4$, Type 1) |  |  | SC ( $n=4$, Type 2) |  |
| :---: | :---: | :---: | :---: | :---: |
| $N$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ |
| 1 | 5 | 1.000 | 6 | 1.000 |
| 2 | 21 | 2.476 | 29 | 2.345 |
| 3 | 93 | 4.011 | 136 | 3.706 |
| 4 | 408 | 5.745 | 604 | 5.205 |
| 5 | 1832 | 7.410 | 2676 | 6.644 |
| 6 | 8084 | 9.192 | 11,564 | 8.218 |
| 7 | 35,752 | 10.88 | 50,228 | 9.737 |
| 8 | 155,756 | 12.65 | 215,492 | 11.39 |
| 9 | 677,856 | 14.34 | 929,136 | 13.01 |
| 10 | 2,920,764 | 16.11 | 3,972,948 | 14.76 |
| 11 | 12,582,860 | 17.84 | 17,048,772 | 16.48 |
| 12 | 53,858,044 | 19.65 | 72,685,616 | 18.33 |
| 13 | 230,643,688 | 21.45 | 310,668,724 | 20.16 |
| 14 | 983,162,808 | 23.34 | 1,320,897,848 | 22.12 |
| 15 | 4,193,819,200 | 25.22 | 5,626,979,444 | 24.06 |
| 16 | 17,824,575,272 | 27.20 | 23,868,686,764 | 26.12 |
| 17 | 75,809,092,412 | 29.17 | 101,405,080,196 | 28.15 |

Table A6. Properties of SAWs on SC lattice with 5 layers between the confining planes ( $n=5$, Type 1, 2, 3).

| SC ( $n=5$, Type 1) |  |  | SC ( $n=5$, Type 2) |  | SC ( $n=5$, Type 3) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $N$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ |
| 1 | 5 | 1.000 | 6 | 1.000 | 6 | 1.000 |
| 2 | 21 | 2.476 | 29 | 2.345 | 30 | 2.400 |
| 3 | 93 | 4.011 | 137 | 3.745 | 148 | 3.811 |
| 4 | 409 | 5.770 | 620 | 5.329 | 692 | 5.318 |
| 5 | 1852 | 7.514 | 2824 | 6.875 | 3196 | 6.747 |
| 6 | 8308 | 9.431 | 12,616 | 8.547 | 14,324 | 8.275 |
| 7 | 37,620 | 11.29 | 56,668 | 10.14 | 64,076 | 9.748 |
| 8 | 168,768 | 13.23 | 251,500 | 11.83 | 282,716 | 11.33 |
| 9 | 758,340 | 15.09 | 1,119,212 | 13.46 | 1,251,044 | 12.88 |
| 10 | 3,379,476 | 16.98 | 4,939,768 | 15.19 | 5,493,804 | 14.54 |

Table A6. Cont.

| SC $(n=5$, Type 1) |  |  | SC ( $n=5$, Type 2) |  | SC ( $n=5$ 5, Type 3) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\boldsymbol{N}$ | $\boldsymbol{c}_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | $\boldsymbol{c}_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | $\boldsymbol{c}_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ |
| 11 | $15,051,324$ | 18.80 | $21,845,116$ | 16.86 | $24,207,436$ | 16.17 |
| 12 | $66,608,060$ | 20.66 | $96,043,836$ | 18.63 | $106,083,764$ | 17.92 |
| 13 | $294,573,648$ | 22.46 | $422,938,080$ | 20.37 | $466,189,268$ | 19.64 |
| 14 | $1,296,739,560$ | 24.31 | $1,854,194,080$ | 22.21 | $2,039,686,412$ | 21.47 |
| 15 | $5,706,787,808$ | 26.13 | $8,139,479,608$ | 24.01 | $8,943,399,564$ | 23.28 |
| 16 | $25,029,783,540$ | 28.01 | $35,603,096,872$ | 25.91 | $39,068,913,604$ | 25.20 |
| 17 | $109,780,078,372$ | 29.87 | $155,900,872,104$ | 27.79 | $170,957,960,396$ | 27.09 |

Table A7. Properties of SAWs on BCC lattice with 3 layers between the confining planes ( $n=3$, Type 1,2 ).

| BCC ( $n=3$, Type 1) |  |  | BCC ( $n=3$, Type 2) |  |
| :---: | :---: | :---: | :---: | :---: |
| $N$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ |
| 1 | 4 | 1.000 | 8 | 1.000 |
| 2 | 28 | 2.286 | 24 | 1.778 |
| 3 | 84 | 3.032 | 168 | 3.032 |
| 4 | 560 | 4.495 | 448 | 4.381 |
| 5 | 1512 | 5.854 | 3024 | 5.854 |
| 6 | 10,024 | 7.471 | 7776 | 7.671 |
| 7 | 26,016 | 9.276 | 52,032 | 9.276 |
| 8 | 172,144 | 11.01 | 131,392 | 11.49 |
| 9 | 437,216 | 13.21 | 874,432 | 13.21 |
| 10 | 2,888,704 | 15.04 | 2,184,192 | 15.76 |
| 11 | 7,242,304 | 17.59 | 14,484,608 | 17.59 |
| 12 | 47,788,288 | 19.52 | 35,913,728 | 20.46 |
| 13 | 118,793,664 | 22.37 | 237,587,328 | 22.37 |
| 14 | 783,007,232 | 24.39 | 585,931,008 | 25.53 |
| 15 | 1,934,717,312 | 27.53 | 3,869,434,624 | 27.53 |

Table A8. Properties of SAWs on the BCC lattice with 4 layers between the confining planes $(n=4$, Type 1, 2).

| BCC ( $n=4$, Type 1 ) |  |  | BCC ( $n=4$, Type 2 ) |  |
| :---: | :---: | :---: | :---: | :---: |
| $N$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ |
| 1 | 4 | 1.000 | 8 | 1.000 |
| 2 | 28 | 2.286 | 40 | 2.133 |
| 3 | 148 | 3.883 | 216 | 2.975 |
| 4 | 752 | 4.482 | 1100 | 4.422 |
| 5 | 3928 | 6.279 | 5516 | 5.502 |
| 6 | 19,240 | 7.061 | 27,436 | 7.195 |
| 7 | 96,800 | 9.129 | 135,308 | 8.501 |
| 8 | 471,652 | 10.12 | 662,208 | 10.41 |
| 9 | 2,324,620 | 12.42 | 3,234,984 | 11.92 |
| 10 | 11,266,332 | 13.59 | 15,695,400 | 14.02 |
| 11 | 54,928,996 | 16.10 | 76,139,448 | 15.71 |
| 12 | 264,967,864 | 17.44 | 367,445,292 | 17.98 |
| 13 | 1,283,256,176 | 20.12 | 1,773,482,796 | 19.83 |
| 14 | 6,167,881,032 | 21.62 | 8,526,698,460 | 22.26 |
| 15 | 29,733,461,768 | 24.46 | 41,001,069,836 | 24.27 |

Table A9. Properties of SAWs on the BCC lattice with five layers between the confining plates $(n=5$, Type 1, 2, 3).

| BCC $(n=5$, Type 1) |  | BCC $(n=5$, Type 2) |  | BCC ( $n=5$ 5, Type 3) |  |  |
| :---: | :---: | :---: | ---: | :---: | ---: | :---: |
| $\boldsymbol{N}$ | $\boldsymbol{c}_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | $\boldsymbol{c}_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ |
| 1 | 4 | 1.000 | 8 | 1.000 | 8 | 1.000 |
| 2 | 28 | 2.286 | 40 | 2.133 | 56 | 2.286 |
| 3 | 148 | 3.883 | 280 | 3.438 | 264 | 2.939 |
| 4 | 1008 | 5.376 | 1292 | 4.425 | 1752 | 4.432 |
| 5 | 4696 | 6.361 | 8700 | 5.904 | 8008 | 5.369 |
| 6 | 31,208 | 7.957 | 38,956 | 7.001 | 52,600 | 7.015 |
| 7 | 140,576 | 8.985 | 258,124 | 8.614 | 235,096 | 8.172 |
| 8 | 923,408 | 10.70 | $1,137,676$ | 9.908 | $1,534,264$ | 9.947 |
| 9 | $4,088,104$ | 11.93 | $7,467,996$ | 11.65 | $6,759,784$ | 11.31 |
| 10 | $26,673,936$ | 13.75 | $32,589,060$ | 13.14 | $43,920,344$ | 13.20 |
| 11 | $116,790,808$ | 15.20 | $212,627,204$ | 15.000 | $191,672,792$ | 14.76 |
| 12 | $758,669,728$ | 17.14 | $921,579,828$ | 16.68 | $1,241,447,848$ | 16.75 |
| 13 | $3,296,625,336$ | 18.78 | $5,987,539,924$ | 18.65 | $5,381,829,176$ | 18.49 |
| 14 | $21,347,913,984$ | 20.82 | $25,824,254,724$ | 20.50 | $34,775,532,088$ | 20.58 |
| 15 | $92,254,133,376$ | 22.64 | $167,265,106,124$ | 22.57 | $150,021,945,496$ | 22.48 |

Table A10. Properties of SAWS on FCC lattice with 3 layers between the confining planes $(n=3$, Type 1, 2).

|  | FCC $(n=3$, Type 1) |  | FCC $(n=3$, Type 2) |  |
| :---: | ---: | ---: | ---: | ---: |
| $\boldsymbol{N}$ | $\boldsymbol{c}_{\boldsymbol{N}}$ |  |  | $\left.\left.\langle \| \omega^{N}\right\|^{\mathbf{2}}\right\rangle$ |

Table A11. Properties of SAWS on FCC lattice with 4 layers between the confining plates $(n=4$, Type 1,2$)$.

|  | FCC $(n=4$, Type 1) |  | FCC $(n=4$, Type 2) |  |
| :---: | ---: | ---: | ---: | ---: |
| $N$ | $c_{N}$ |  | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | $c_{N}$ |

Table A12. Properties of SAWs on FCC lattice with 5 layers between the confining plates $(n=5$, Type 1, 2, 3).

| FCC ( $n=5$, Type 1$)$ |  |  | FCC ( $n=5$, Type 2 ) |  | FCC ( $n=5$, Type 3) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $N$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | $c_{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ |
| 1 | 8 | 1.000 | 12 | 1.000 | 12 | 1,000 |
| 2 | 72 | 2.222 | 116 | 2.069 | 132 | 2.182 |
| 3 | 672 | 3.607 | 1100 | 3.313 | 1276 | 3.245 |
| 4 | 6348 | 5.138 | 10,240 | 4.558 | 11,756 | 4.340 |
| 5 | 59,564 | 6.634 | 93,864 | 5.810 | 106,484 | 5.501 |
| 6 | 550,524 | 8.062 | 852,080 | 7.087 | 957,524 | 6.730 |
| 7 | 5,021,572 | 9.447 | 7,680,816 | 8.397 | 8,578,324 | 8.022 |
| 8 | 45,364,428 | 10.82 | 68,862,952 | 9.750 | 76,622,980 | 9.375 |
| 9 | 407,048,708 | 12.21 | 614,763,576 | 11.15 | 682,422,404 | 10.79 |
| 10 | 3,634,621,916 | 13.62 | 5,469,051,720 | 12.60 | 6,060,924,172 | 12.26 |
| 11 | 32,334,144,252 | 15.07 | 48,511,115,392 | 14.10 | 53,692,606,892 | 13.78 |
| 12 | 286,791,329,140 | 16.57 | 429,222,436,536 | 15.65 | 475,067,855,437 | 16.03 |

In the continuation, we present results from the statistical analysis based on the PDF and the folded variant for the SAW size as a function of lattice type, SAW length, point of origin (Type), and level of confinement for selected systems. Calculated statistical variables include the mean value, the most repeated one and for the folded variant the top point, $\mu_{\mathrm{H}}$, corresponding to the half of the distribution when the representation changes from upslope to downslope, and the mean absolute deviation, $\sigma$.

Table A13. Statistical parameters of SAW size for the SC restricted lattice as a function of system characteristics (fixed: $N=16$ ) for selected systems.

| System | $\left.\left.\langle \| \omega^{\mathbf{1 6}}\right\|^{\mathbf{2}}\right\rangle$ | $\begin{array}{c}\text { Most Repeated } \\ \text { Value (PDF) }\end{array}$ | $\mu_{\mathrm{H}}$ (Top Pointed Distribution |  |
| :---: | :---: | :---: | :---: | :---: |
| $\boldsymbol{\sigma}$ (68.3\%) |  |  |  |  |$]$| $n=1$, Type 1 | 51.99 | 50 | 50 | $\pm 22$ |
| :---: | :---: | :---: | :---: | :---: |
| $n=2$, Type 1 | 32.65 | 26 | 26 | $\pm 20$ |
| $n=3$, Type 2 | 27.97 | 26 | 26 | $\pm 18$ |
| $n=4$, Type 2 | 26.12 | 26 | 22 | $\pm 16$ |
| $n=$ 5, Type 1 | 28.01 | 14 | 24 | $\pm 16$ |
| $n=$ 5, Type 2 | 25.91 | 14 | 22 | $\pm 16$ |
| $n=$ 5, Type 3 | 25.20 | 14 | 20 |  |

Table A14. Statistical parameters of SAW size for the SC restricted lattice as a function of SAW steps (fixed: $n=5$, Type 3 ) for selected systems.

| $\boldsymbol{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | Most Repeated <br> Value (PDF) | $\mu_{\mathrm{H}}$ (Top Poided Distribution |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| 13 | 19.64 | 14 | 17 | $\pm 13$ |
| 14 | 21.47 | 14 | 18 | $\pm 14$ |
| 15 | 23.28 | 17 | 19 | $\pm 16$ |
| 16 | 25.20 | 14 | 20 | $\pm 16$ |

Table A15. Statistical parameters of SAW size for the BCC restricted lattice as a function of system characteristics (fixed: $N=14$ ) for selected systems.

| System | $\left.\left.\langle \| \omega^{14}\right\|^{2}\right\rangle$ | Most Repeated Value (PDF) | Folded Distribution |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\mu_{\mathrm{H}}$ (Top Point) | $\sigma$ (68.3\%) |
| $n=2$, Type 1 | 28.52 | 34 | 27 | $\pm 19$ |
| $n=3$, Type 2 | 25.53 | 34 | 23 | $\pm 17$ |
| $n=4$, Type 2 | 22.26 | 14 | 19 | $\pm 15$ |
| $n=5$, Type 1 | 20.82 | 22 | 19 | $\pm 14$ |
| $n=5$, Type 2 | 20.50 | 14 | 18 | $\pm 14$ |
| $n=5$, Type 3 | 20.58 | 7 | 18 | $\pm 14$ |

Table A16. Statistical parameters of SAW size for the BCC restricted lattice as a function of SAW steps (fixed: $n=5$, Type 3) for selected systems.

| $\boldsymbol{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | Most Repeated <br> Value (PDF) | $\mu_{\mathrm{H}}$ (Top Poided Distribution |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| 11 | 14.76 | 17 | 12 | $\pm 9$ |
| 12 | 16.75 | 7 | 14 | $\pm 11$ |
| 13 | 18.49 | 12 | 17 | $\pm 14$ |
| 14 | 20.58 | 7 | 18 | $\pm 14$ |

Table A17. Statistical parameters of SAW size for the FCC restricted lattice as a function of system characteristics (fixed: $N=11$ ) for selected systems.

| System | $\left.\left.\langle \| \omega^{11}\right\|^{2}\right\rangle$ | Most Repeated Value (PDF) | Folded Distribution |  |
| :---: | :---: | :---: | :---: | :---: |
| $n=2$, Type 1 | 17.95 | 13 | 16 | $\pm 12$ |
| $n=3$, Type 2 | 15.47 | 13 | 13 | $\pm 11$ |
| $n=4$, Type 2 | 14.32 | 13 | 13 | $\pm 10$ |
| $n=5$, Type 1 | 15.07 | 7 | 13 | $\pm 10$ |
| $n=5$, Type 2 | 14.10 | 7 | 12 | $\pm 10$ |
| $n=5$, Type 3 | 13.78 | 7 | 12 | $\pm 10$ |

Table A18. Statistical parameters of SAW size for the FCC restricted lattice as a function of SAW steps (fixed: $n=5$, Type 3) for selected systems.

| $\boldsymbol{N}$ | $\left.\left.\langle \| \omega^{N}\right\|^{2}\right\rangle$ | Most Repeated <br> Value (PDF) | $\boldsymbol{\mu}_{\mathrm{H}}$ (Top Poided Distribution |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |

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