

# Correlation of Secondary Particle Number with the Debye–Hückel Parameter for Thickening Mesoporous Silica Shells Formed on Spherical Cores

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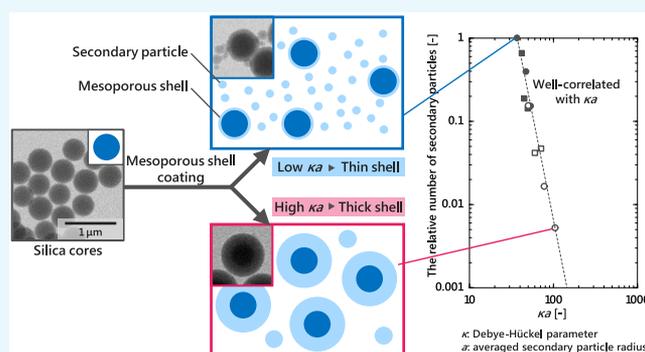


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**ABSTRACT:** Mesoporous silica shells were formed on nonporous spherical silica cores during the sol–gel reaction to elucidate the mechanism for the generation of secondary particles that disturb the efficient growth of mesoporous shells on the cores. Sodium bromide (NaBr) was used as a typical electrolyte for the sol–gel reaction to increase the ionic strength of the reactant solution, which effectively suppressed the generation of secondary particles during the reaction wherein a uniform mesoporous shell was formed on the spherical core. The number of secondary particles ( $N_{2nd}$ ) generated at an ethanol/water weight ratio of 0.53 was plotted against the Debye–Hückel parameter  $\kappa$  to quantitatively understand the Debye screening effect on secondary particle generation. Parameter  $\kappa a$ , where  $a$  is the average radius of the secondary particles finally obtained in the silica coating, expresses the trend in  $N_{2nd}$  at different concentrations of ammonia and NaBr.  $N_{2nd}$  was much lower than that expected theoretically from the variation of secondary particle sizes at a constant Debye–Hückel parameter. A similar correlation with  $\kappa a$  was observed at the high and low ethanol/water weight ratios of 0.63 and 0.53, respectively, with different hydrolysis rate constants. The good correlation between  $N_{2nd}$  and  $\kappa a$  revealed that controlling the ionic strength of the silica coating is an effective approach to suppress the generation of secondary particles for designing mesoporous shells with thicknesses appropriate for their application as high-performance liquid chromatography column packing materials.



## INTRODUCTION

Monodispersity in particle size distribution is important for extending the practical application scope of particulate functional materials.<sup>1–4</sup> The core–shell structure is a type of particle structure in which both monodispersity and functionality of particles are achieved.<sup>5–9</sup> In the field of column packing materials for high-performance liquid chromatography (HPLC),<sup>5,6</sup> monodisperse core particles coated with a mesoporous shell have been extensively used to enhance the separation performance in HPLC.

Five-micron-sized core–shell particles with porous shells were reported in the 1960s by Horvath<sup>5</sup> and Kirkland.<sup>6</sup> In their subsequent research,<sup>10</sup> relatively small-sized core–shell particles (average diameter: 2.7  $\mu\text{m}$ ) called halo particles were developed. Various core–shell particles in the size range of 2.7–5.0  $\mu\text{m}$ , including halo particles, were fabricated for use as commercial packing materials.<sup>10–12</sup> Decreasing the size of particles used for packing materials is an effective approach for improving the contact efficiency of the analyte solution with the packing material.<sup>13,14</sup> Core–shell particles smaller than 2  $\mu\text{m}$  were rarely studied until the early 2000s because the usage of downsized core–shell particles required high column pressure for the flow of the analyte solution. Further reduction

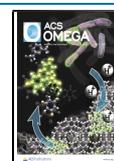
of the size of core–shell particles to sub-2  $\mu\text{m}$  was also achieved<sup>11–13,15–18</sup> because of the recent mechanical progress in the HPLC apparatus.<sup>19</sup>

The micelle templating method has been widely employed for preparing porous materials since its discovery by Beck et al.<sup>20</sup> in 1992. The micelle templating method is also applicable for coating spherical silica particles with mesoporous shells ( $\text{SiO}_2@m\text{SiO}_2$ ).<sup>21,22</sup> Our research group<sup>23–26</sup> succeeded in synthesizing spherical mesoporous silica particles with and without nonporous cores using the micelle templating method in which a cationic surfactant, cetyltrimethylammonium bromide (CTAB), was used.<sup>20,21,27,28</sup> Some other researchers reported an approach to effectively form mesoporous shells on the core particles. The conditions for the synthesis of  $\text{SiO}_2@m\text{SiO}_2$ , including the concentrations of the silica source<sup>24,25,29</sup> and core particles,<sup>21,25</sup> were varied to control the thickness of

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the mesoporous shells. A multistep coating process was also employed to further thicken the mesoporous shell.<sup>10,15,21</sup> The oil–water biphasic stratification reaction,<sup>30–33</sup> layer-by-layer method,<sup>11,34,35</sup> partial etching method,<sup>36,37</sup> and sonication-assisted synthesis method<sup>38</sup> are alternative approaches to control the shell thickness. In the previous reports based on the abovementioned methods, the monodispersity of the core–shell particles was sufficient for their application as column packing materials. However, the thickness of the mesoporous shells formed in the presence of micron-sized nonporous cores was insufficient to meet the dimension requirement for their commercial application as column packing materials because the generation of a large number of secondary particles suppressed efficient shell growth during the formation of mesoporous silica shells.

During the formation of silica-based materials wherein alkoxysilanes were used as silica sources, i.e., through the sol–gel method, the hydrolysis rate in the solution has been regarded as an important factor for tuning the growth rate of the mesoporous silica shell.<sup>39–41</sup> The rate of the sol–gel reaction depended on the concentration of  $[\text{OH}^-]$ .<sup>1,42</sup> Because of the high correlation between the hydrolysis rate and pH of the solution, ammonia ( $\text{NH}_3$ ) is commonly employed as a basic catalyst to promote the hydrolysis of alkoxysilanes, including tetraethyl orthosilicate (TEOS).<sup>42</sup>

During the initial or middle stage of the formation of porous shells on nonporous silica cores, the surface reaction rate between the cores and the silica moieties in the reactant solution should also be considered to suppress the generation of secondary particles.<sup>43,44</sup> This is because secondary particles are generated when the formation rate of silica moieties exceeds the rate at which the silica moieties are consumed during the surface reaction on the cores.<sup>28</sup> Moreover, the use of a reactant solution with high ionic strength weakens the electrostatic interaction between the ionized silica moieties and the charged cores, which also promotes the diffusivity of the charged silica moieties to the core surface with the same polarity as the silica moiety to suppress the generation of secondary particles.<sup>45,46</sup>

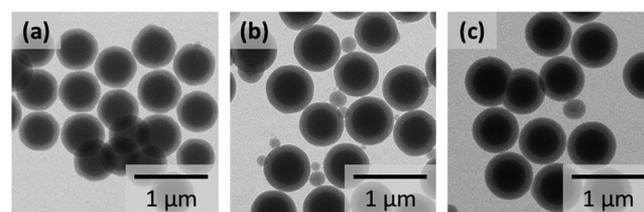
Many research groups<sup>15,31,38,47</sup> have attempted to thicken mesoporous shells formed on cores through the suppression of secondary particle generation. The addition of an electrolyte is a promising way to thicken the shell; however, the addition of an excessive amount of electrolyte reportedly leads to the inter-core aggregation due to the Debye screening effect.<sup>48</sup> Nevertheless, approaches for suppressing secondary particle generation during the sol–gel reaction need further investigation. To this end, in this study, the quantitative relationship between the mesoporous shell thickness and the silica moieties formed by the hydrolysis of TEOS was examined, considering the number of secondary particles generated in the sol–gel reaction to explore the efficient growth of mesoporous silica shells on the cores. We believe that this quantitative analysis of secondary particle generation deepens the understanding of the reaction system for further functionalization of particulate materials. The Debye–Hückel parameter  $\kappa$  of the solution was also calculated to clarify the relationship between the number of secondary particles and diffusivity of the ionized silica moiety toward the cores during the coating process.

## RESULTS AND DISCUSSION

**Ammonia and Electrolyte Concentrations Appropriate for Uniform Silica Coating.** Ammonia is commonly

used as a basic catalyst in the sol–gel method. The effect of ammonia concentration on particle growth has been studied to primarily examine the kinetic balance between hydrolysis and condensation of TEOS.<sup>50</sup> Another advantage of using ammonia is the availability of cationic species ( $\text{NH}_4^+$ ), which increases the ionic strength of the reactant solution.<sup>42,46</sup> In this section, various concentrations of ammonia and electrolytes added to the solution of CTAB were investigated to determine the optimal experimental conditions for the uniform silica coating of the cores. Several concentrations of ammonia and electrolytes were tested to obtain mononuclear core–shell silica particles with an ethanol/water weight ratio of 0.53.

Figure 1 shows the transmission electron microscopy (TEM) images of  $\text{SiO}_2@m\text{SiO}_2$  obtained at different ammonia



**Figure 1.** TEM images of  $\text{SiO}_2@m\text{SiO}_2$  prepared at different  $\text{NH}_3$  concentrations: 10 mM (a), 50 mM (b), and 100 mM (c). An ethanol/water weight ratio of 0.53. The images were taken for the samples obtained after several centrifugations to clearly observe the silica shell formed on the cores.

concentrations and a fixed CTAB concentration of 20 mM. The images were taken for the samples obtained after centrifugation, to clearly observe the silica shell formed on the cores. In the ammonia concentration range of 10–100 mM, a uniform coating of the core with silica shells was observed along with the generation of secondary silica particles. The average diameter and shell thickness of each particle are summarized in Table 1, where the porosities of  $\text{SiO}_2@m\text{SiO}_2$  are also listed. The estimation of the secondary particle number from the mass balance of the silicon atoms during shell formation is discussed in the following section.

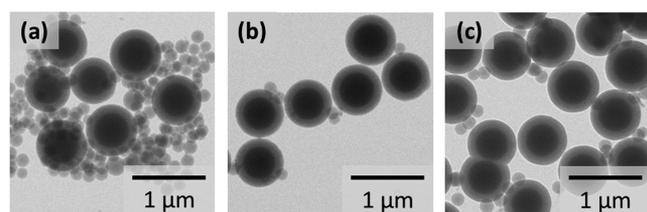
Furthermore, the effect of ionic strength on shell formation was investigated by an electrolyte addition experiment, in which sodium bromide (NaBr) was chosen because it offers a typical alkaline metal cation and the anion same as CTAB. Figure 2 shows the TEM images of  $\text{SiO}_2@m\text{SiO}_2$  obtained at different concentrations of NaBr in the CTAB solution. The TEM images illustrate that the silica cores were uniformly coated with a silica shell when the NaBr concentration was 0–4 mM at  $[\text{NH}_3] = 10$  mM. The number of secondary particles formed when the NaBr concentration was  $\leq 4$  mM can also be estimated from the Si balance in the sol–gel reaction to correlate the shell thickness with the number of secondary particles in the following section.

**Effect of the Debye Screening Effect on the Suppression of Secondary Particle Generation.** The discussion about the number of secondary particles generated was preceded by confirming the conversion of TEOS during the sol–gel reaction at  $[\text{NH}_3] = 10$ –100 mM. According to hydrolysis rate constants ( $k_h$ ) listed in Table 1, >99% of TEOS in the concentration range of ammonia was expected to be hydrolyzed within 8 h. The hydrolysis rates in Table 1 suggest that almost all TEOS molecules hydrolyzed in the reaction system were dissolved in the solution and condensed into silica

**Table 1. Characteristics of SiO<sub>2</sub>@mSiO<sub>2</sub> Particles Synthesized at Different NH<sub>3</sub> Concentrations Ranging from 10 to 100 mM**

NH <sub>3</sub> conc. [mM]	D <sub>V</sub> [nm]	T <sub>S</sub> [nm]	C <sub>V</sub> [%]	S <sub>BET</sub> [m <sup>2</sup> /g] <sup>a</sup>	V <sub>P</sub> [cm <sup>3</sup> /g] <sup>b</sup>	d <sub>p, BJH</sub> [nm] <sup>c</sup>	k <sub>h</sub> [min <sup>-1</sup> ] <sup>d</sup>	[Si] <sub>soln</sub> [mmol/L] <sup>e</sup>
10	596	73	3.7	265	0.22	2.7	0.0178	0.21
50	658	103	3.8	416	0.37	2.7	0.0764	0.16
100	663	106	3.5	426	0.35	2.7	0.147	0.086

<sup>a</sup>Calculated by the Brunauer–Emmett–Teller (BET) method. <sup>b</sup>At  $p/p_0 = 0.990$ . <sup>c</sup>Calculated by the Barrett–Joyner–Halenda (BJH) method. <sup>d</sup>Calculated from the TEOS concentration measured by GC. <sup>e</sup>Measured by an inductively coupled plasma mass spectrometer (ICP-MS).



**Figure 2.** TEM images of SiO<sub>2</sub>@mSiO<sub>2</sub> prepared at different NaBr concentrations: 1 mM (a), 2 mM (b), and 4 mM (c). NH<sub>3</sub> concentration was 10 mM and the ethanol/water weight ratio was 0.53. The images were taken for the samples obtained after several centrifugations to clearly observe the silica shell formed on the cores.

to be precipitated as a shell on the core or generated as secondary particles. Because the amount of silica dissolved in a mixed solvent of alcohol and water is much lower than the number of TEOS molecules present in the reaction system,<sup>51,52</sup> we calculated the number of secondary particles from a combination of the average size of secondary particles finally obtained ( $D_{V,2nd}$ ) and Si concentration in the solution ( $[Si]_{soln}$ ). Here, the secondary particles were collected from the supernatant of the reaction mixture after one-time centrifugation (see the Supporting Information for details).

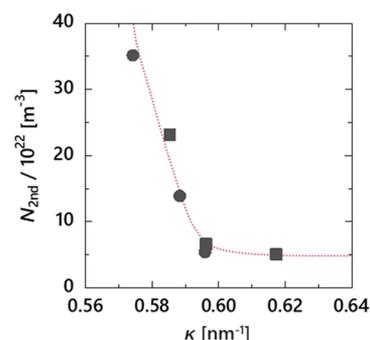
The upper part of Table 2 summarizes the values of shell thickness ( $T_S$ ), secondary particle size ( $D_{V,2nd}$ ), and number of

**Table 2. Mesoporous Shell Thickness of SiO<sub>2</sub>@mSiO<sub>2</sub> ( $T_S$ ) and the Secondary Particle Size ( $D_{V,2nd}$ ) and the Number of Secondary Particles ( $N_{2nd}$ ) Generated**

NH <sub>3</sub> [mM]	NaBr [mM]	ethanol/water weight ratio	T <sub>S</sub> [nm]	D <sub>V,2nd</sub> [nm]	N <sub>2nd</sub> /10 <sup>19</sup> [L <sup>-1</sup> ] <sup>a</sup>	N <sub>2nd</sub> /N <sub>max</sub>
10	0	0.53	73	129	35.1	1
50	0	0.53	103	161	13.9	0.39
100	0	0.53	106	180	5.34	0.15
10	1	0.53	110	144	23.1	0.66
10	2	0.53	111	152	6.54	0.19
10	4	0.53	117	161	4.97	0.14
10	0	0.63	130	178	5.40	0.15
50	0	0.63	142	265	0.578	0.016
100	0	0.63	194	354	0.183	0.0052
10	2	0.63	135	205	1.46	0.042
10	4	0.63	129	234	1.64	0.047

<sup>a</sup>Measured by ICP-MS.

secondary particles ( $N_{2nd}$ ) generated from the data shown in Figures 1 and 2. Because the highest  $[Si]_{soln}$  was measured for the thinnest silica shell of 73 nm,  $N_{2nd}$  values at  $[NH_3] = 10$  mM and  $[NaBr] = 0$  mM were used for normalizing other  $N_{2nd}$  values such as  $N_{max}$ . As shown in Table 2, the shell formed on the core was thickened upon a decrease in the number of secondary particles generated in the sol–gel reaction. The decrease in  $N_{2nd}$  is presented in Figure 3, wherein the Debye–Hückel parameter ( $\kappa$ ) is used to evaluate the Debye screening

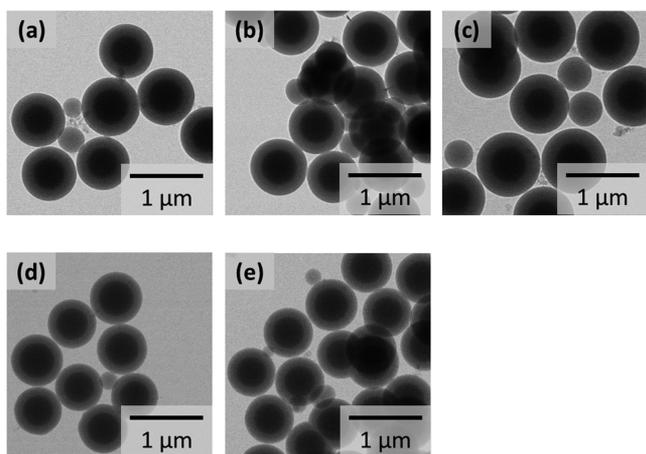


**Figure 3.** Relationship between the number of secondary particles ( $N_{2nd}$ ) and the Debye–Hückel parameter ( $\kappa$ ) at an ethanol/water weight ratio of 0.53. Filled circles (●) show  $N_{2nd}$  at different NH<sub>3</sub> concentrations without any electrolyte addition. Filled squares (■) show  $N_{2nd}$  at  $[NH_3] = 10$  mM and different NaBr concentrations.

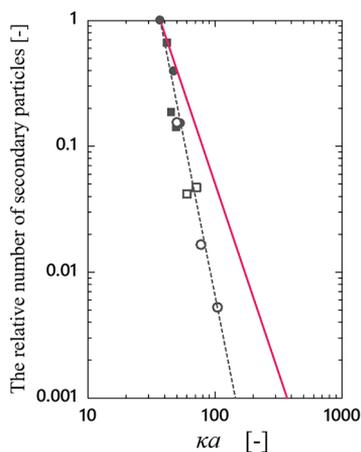
effect on the suppression of secondary particle generation. The decrease in  $N_{2nd}$  with increasing  $\kappa$  in Figure 3 suggests that the destabilization caused by the Debye screening effect for ionized silica moieties in the reactant solution could suppress the generation of secondary particles. Interestingly, as shown in Table 2, the size of the secondary particles generated during the formation of a thick silica shell exceeded that during the formation of a thin shell, implying that the presence of ionized silica with high ionic strength facilitates its diffusivity to form large secondary particles. Another interesting point is that the secondary particles were not twice as large as  $T_S$ , which can be supported by the surface-reaction-limited growth mechanism proposed for the formation of silica particles in the absence of CTAB.<sup>43,53</sup>

Similar experiments on shell formation were conducted at a higher ethanol/water weight ratio of 0.63 to clarify the relationship between the Debye screening effect and  $N_{2nd}$  in the solution, which is presented in the TEM images of Figure 4. The results for  $T_S$ ,  $D_{V,2nd}$ , and  $N_{2nd}$  at high ethanol/water weight ratios are summarized in the lower part of Table 2. Figure 4c shows the image of the thickest shell of the core–shell particles with the lowest number of secondary particles in this study, whereas Figure 4a depicts the smallest size of the secondary particles generated when the ethanol/water weight ratio is high. The TEM images illustrate that the formation of the thickest silica shell was accompanied by the generation of the largest secondary particles in the silica-coating experiments.

To comprehend the effect of the diffusivity of ionized silica on secondary particle generation in all silica-coating experiments, the normalized  $N_{2nd}$  values are plotted against  $\kappa a$ , which is the Debye–Hückel parameter multiplied by the average secondary particle radius ( $a (= D_{V,2nd}/2)$ ) in Figure 5. Because it has been reported that the electrical double layer at  $\kappa a > 10$  can be regarded as a layer that is sufficiently thinner than the secondary particle size,<sup>54</sup> the overlapping of the electrical double layers of adjacent secondary particles can be neglected



**Figure 4.** TEM images of  $\text{SiO}_2@m\text{SiO}_2$  prepared at an ethanol/water weight ratio of 0.63. The sol–gel reactions without any electrolyte addition were conducted at different  $\text{NH}_3$  concentrations: 10 mM (a), 50 mM (b), 100 mM (c). For the addition of electrolyte at the fixed  $\text{NH}_3$  concentration of 10 mM, the NaBr concentration was set to 2 mM (d) and 4 mM (e). The images were taken for the samples obtained after several centrifugations to clearly observe the silica shell formed on the cores.



**Figure 5.** Relationship between  $\kappa a$  and the relative number of secondary particles. The red solid line shows the theoretical  $N_{2\text{nd}}$  expected from variation in the secondary particle size ( $a$ ) at the same  $\kappa$  and  $[\text{Si}]_{\text{soln}}$ . The squares (■, □) show the relative  $N_{2\text{nd}}$  generated at different concentrations of NaBr. The circles (●, ○) indicate those generated at different concentrations of  $\text{NH}_3$  without any addition of NaBr. Filled and open symbols represent the relative  $N_{2\text{nd}}$  formed at the ethanol/water weight ratios of 0.53 and 0.63, respectively.

in the present silica coatings. Figure 5 clearly shows that the normalized  $\kappa a$  can effectively express the generation trend of secondary particles and predict the number of secondary particles generated at different agent concentrations. The red line in Figure 5 shows  $N_{2\text{nd}}$  expected at a fixed concentration of  $[\text{Si}]_{\text{soln}}$ , which was measured at  $[\text{NH}_3] = 10$  mM and the low ethanol/water weight ratio without the addition of any electrolyte. It indicates the maximum number of secondary particles completely collected by centrifugation when secondary particles of different sizes were finally obtained. For the experimental  $N_{2\text{nd}}$  at the different concentrations of ammonia and NaBr, it is noteworthy that the  $N_{2\text{nd}}$  values almost lie on a single line steeper than the red line.

Because it was reported that the rate of hydrolysis of TEOS is barely changed upon the addition of an electrolyte with several millimolar (mM) concentration,<sup>55</sup> the significant decrease in  $N_{2\text{nd}}$  with the addition of NaBr (Figure 5) must originate predominantly from the Debye screening effect on ionized silica moieties in the coating experiments.

An increase in ammonia concentration without the addition of any electrolyte, which is depicted by circles in Figure 5, not only promotes both hydrolysis and condensation reactions but also weakens the electrostatic interaction in the reactant solution.<sup>56</sup> Although the former effect facilitates the generation of secondary particles during the early stage of silica coating, the latter is attributable to the Debye screening effect, which can impact the secondary particle generation promoted by the hydrolysis and condensation reactions, thereby thickening the silica shell formed on the cores. Good correlations of  $N_{2\text{nd}}$  with  $\kappa a$  were observed at the low and high ethanol/water weight ratios, which are indicated by the filled and open symbols in Figure 5, respectively, indicating that the variation of reaction rates by changing the solvent composition is less significant for determining  $N_{2\text{nd}}$  in the studied silica coating.

The comparison of  $N_{2\text{nd}}$  generated at different agent concentrations revealed that the control of ionic strength in the silica coating based on the Debye screening effect is an effective approach to suppress the generation of secondary particles for thickening the mesoporous shell, which can facilitate its application as an HPLC column packing material.

## CONCLUSIONS

The number of secondary particles generated in the sol–gel reaction in the presence of nonporous spherical cores and a cationic surfactant, CTAB, was examined to determine the thickening of the mesoporous shell formed on the cores. At ammonia concentrations of  $\geq 150$  mM, uniform mesoporous shells were not formed on the cores because of core aggregation during the reaction. The addition of NaBr of several millimolar concentrations to the reaction system could suppress the generation of secondary particles and cause minimal aggregation of cores, thereby thickening the mesoporous shell formed on the cores. The drastic decrease in  $N_{2\text{nd}}$  observed at different concentrations of ammonia and NaBr correlated well with  $\kappa a$ , which was the Debye–Hückel parameter normalized with the secondary particle radius. The good correlation of  $N_{2\text{nd}}$  observed at different ethanol/water weight ratios indicated that the generation of secondary particles was predominantly suppressed by the Debye screening effect. These results revealed that the control of the Debye–Hückel parameter can be an effective approach for tuning the thickness of functional shells formed on cores during the sol–gel reaction.

## MATERIALS AND METHODS

**Materials.** Submicron-sized silica particles (Sciqaq series, Sakai Chemical Industry Co., Ltd. (Sakai, Japan)) were used as received as core particles. The average diameter of the silica core particles ( $D_{\text{core}}$ ) was 451 nm. The coefficient of variation of diameters ( $C_V$ ), which is commonly used to evaluate the monodispersity of particles, was 4.9%. Sodium bromide (NaBr, 99.9%), tetraethyl orthosilicate (TEOS, 95%), cetyltrimethylammonium bromide (CTAB, 98%), ammonia aqueous solution ( $\text{NH}_3$ , 25%), and ethanol (99.5%) were purchased from FUJIFILM Wako Pure Chemical Corporation (Osaka,

Japan). Deionized water (>18.2 MΩ-cm) was prepared by Direct-Q3 UV (Merck KGaA; Darmstadt, Germany).

**Mesoporous Shell Coating of Silica Cores.** The formation of mesoporous silica shells on core particles was conducted by the micelle templating method using CTAB as a cationic surfactant. A suspension of the core particles in the presence of CTAB was sonicated for 1 h. In the case of electrolyte addition, the electrolyte was added after the sonication. An aqueous solution of NH<sub>3</sub> and ethanol was added to the suspension and this mixture was stirred by a magnetic stirrer bar at 35 °C for 30 min. The reaction for shell formation was initiated by TEOS injection, and the mixed suspension was reacted at 35 °C for 18 h. The reaction was carried out in a sealed glass reactor with a total reaction volume of 50 mL. The volume fraction of core particles was 0.40 vol % (the number of core particles:  $8.39 \times 10^{16} \text{ m}^{-3}$ ). The concentrations of CTAB and TEOS were 20 and 60 mM, respectively. After the reaction, silica particles coated with mesoporous shell (SiO<sub>2</sub>@mSiO<sub>2</sub>) were separated by centrifugation and were washed twice with water to collect secondary particles. The SiO<sub>2</sub>@mSiO<sub>2</sub> particles separated were dried under reduced pressure at 60 °C overnight. The dried particles were calcined at 550 °C for 4 h to remove the CTAB templates in the particles.

**Hydrolysis Rates of TEOS.** An aliquot of the reactant suspension was sampled during the reaction to measure the concentration of unreacted TEOS with a gas chromatograph (GC: GC-4000 Plus, GL Science (Tokyo, Japan)). The hydrolysis rate constant of TEOS,  $k_b$ , was estimated assuming a first-order reaction of the TEOS concentration.

**Evaluation of Electrostatic Interparticle Interactions Based on the Debye–Hückel Parameter.** The Debye–Hückel parameter was calculated as eq 1, where  $\epsilon$  is the relative dielectric constant of the solvent,  $\epsilon_0$  is the dielectric constant of the vacuum, and  $k_b$ ,  $T$ , and  $e$  are Boltzmann's constant, reaction temperature, and elementary charge, respectively. The ionic strength ( $I$ ) in eq 1 was calculated based on the measured pH at the time of 50% TEOS conversion (see Figure S1). The other parameters used for the calculation of  $I$  are shown in Tables S1 and S2.

$$\kappa = \left( \frac{2e^2 I}{\epsilon \epsilon_0 k_b T} \right)^{1/2} \quad (1)$$

**Thickness of the Mesoporous Shell.** SiO<sub>2</sub>@mSiO<sub>2</sub> synthesized in the present work was observed with FE-STEM (Hitachi, HD-2700). The diameter ( $D_{\text{core-shell}}$ ) and monodispersity ( $C_V$ ) of SiO<sub>2</sub>@mSiO<sub>2</sub> were determined by directly measuring particles in the TEM images (200 particles or more). The shell thickness  $T_s$  was calculated by the following equation:

$$T_s = \frac{1}{2}(D_{\text{core-shell}} - D_{\text{core}}) \quad (2)$$

**Number of Secondary Particles.** The number of secondary particles ( $N_{2\text{nd}}$ ) was calculated in eq 3 with the average size of secondary particles ( $D_{V,2\text{nd}}$ ) and the Si atomic concentration ( $[\text{Si}]_{\text{soln}}$ ) measured by an inductively coupled plasma-mass spectrometer (ICP-MS, Agilent-8800 (Agilent Technologies, Santa Clara, CA)). The  $[\text{Si}]_{\text{soln}}$  in eq 3 is the total concentration of silicon, including secondary silica particles and other silica moieties in the supernatant, that was obtained by centrifuging the resultant suspension.

$$N_{2\text{nd}} = \left( \frac{[\text{Si}]_{\text{soln}} \times V}{M\rho} \right) / \left( \frac{\pi}{6} D_{V,2\text{nd}}^3 \right) \quad (3)$$

where  $M$  is the molecular weight of silica (= 60.08 g/mol),  $\rho$  is the density of silica, and  $V$  is the reaction volume (50 mL). A density of 1.9 g/cm<sup>3</sup> was used as a typical value for silica formed in sol–gel reactions<sup>43,49</sup> because the exact density of secondary particles is unknown in this study. The average diameter of secondary particles ( $D_{V,2\text{nd}}$ ) was obtained from TEM images.

To examine the porosity of SiO<sub>2</sub>@mSiO<sub>2</sub>, N<sub>2</sub> adsorption–desorption isotherms were measured with BELSORP-mini II (Bel Japan Inc.) at 77 K. Their pore size distributions were calculated by Barrett–Joyner–Halenda (BJH) method. The surface areas and the total pore volumes of SiO<sub>2</sub>@mSiO<sub>2</sub> were determined using the adsorption isotherms with Brunauer–Emmett–Teller (BET) analysis from the adsorbed amounts of nitrogen at a relative pressure ( $p/p_0$ ) of 0.99.

## ■ ASSOCIATED CONTENT

### Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/acsomega.1c02293>.

Variations of pH in the reaction mixtures of SiO<sub>2</sub>@mSiO<sub>2</sub> synthesis at different NH<sub>3</sub> concentrations (Figure S1); equations for calculation of ionic strength, parameters used for the calculation, and solvent properties at different ethanol/water weight ratios (Tables S1 and S2); and the detailed procedure of evaluation of secondary particles generated in the silica-coating process by ICP-MS (PDF)

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