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Robustness of Voltage-induced Magnetocapacitance

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One of the most important achievements in the field of spintronics is the development of magnetic tunnel junctions (MTJs). MTJs exhibit a large tunneling magnetoresistance (TMR). However, TMR is strongly dependent on biasing voltage, generally, decreasing with applying bias. The rapid decay of TMR was a major deficiency of MTJs. Here we report a new phenomenon at room temperature, in which the tunneling magnetocapacitance (TMC) *increases* with biasing voltage in an MTJ system based on $\text{Co}_{40}\text{Fe}_{40}\text{B}_{20}/\text{MgO}/\text{Co}_{40}\text{Fe}_{40}\text{B}_{20}$. We have observed a maximum TMC value of 102% under appropriate biasing, which is the largest voltage-induced TMC effect ever reported for MTJs. We have found excellent agreement between theory and experiment for the bipolar biasing regions using Debye-Fröhlich model combined with quartic barrier approximation and spin-dependent drift-diffusion model. Based on our calculation, we predict that the voltage-induced TMC ratio could reach 1100% in MTJs with a corresponding TMR value of 604%. Our work has provided a new understanding on the voltage-induced AC spin-dependent transport in MTJs. The results reported here may open a novel pathway for spintronics applications, e.g., non-volatile memories and spin logic circuits.

A new class of electronic devices based on the spin degrees of freedom has been extensively studied and it has given rise to the field of spintronics^{1–7}. One of the most important achievements in this field is the development of magnetic tunnel junctions (MTJs), which has enabled the observation of a large tunneling magnetoresistance (TMR)^{3,4,8–12}. Practical applications relying on this TMR effect range from data read heads in hard disk drives to highly sensitive magnetic sensors. The magnetic states of MTJs can also be manipulated by the current induced spin-transfer torque (STT) effect^{13–17}. More applications have become possible, e.g., magnetic random access memories (MRAMs)^{18–21}, logic-in-memory circuits^{22,23} and random number (RN) generators^{24,25}. More recently, neuromorphic computing using spin-torque MTJ oscillators has been developed²⁶. Thus, MTJs can serve as one of the most crucial building blocks of spintronics-based computing.

It is well known that TMR is strongly dependent on biasing voltage, generally, decreasing with applying bias^{27–30}. One major challenge in MTJ research is to find ways to increase the half biasing voltage, $V_{1/2}$, at which the total TMR ratio near zero biasing is halved. For MgO-based MTJs³, $V_{1/2}$ is approximately 1 V. Normal electrical operations will always require certain applying biasing voltage, which renders TMR less optimal. Extensive efforts have been made to enhance $V_{1/2}$, but progress has come very slowly. Recently, it has been demonstrated that $V_{1/2}$ depends strongly on the interfacial structures between the ferromagnetic (FM) and the insulator layer. A high $V_{1/2}$ can be obtained in MTJs with i) few misfit dislocations near the interfaces, ii) a small lattice strain inside the insulator or iii) well-defined sharp interfaces^{31–35}. The value of $V_{1/2}$ in lattice-matched Fe/spinel $\text{MgAl}_2\text{O}_4/\text{Fe}(001)$ MTJs reaches +1.0 V (–1.3 V) for the positive (negative) bias³¹. In other studies, relatively high $V_{1/2}$ values, ranging from 0.5 to 1.0 V, have also been reported in fully epitaxial Fe/MgO/GaO_x/Fe³², NiFe(111)/AlO_x/CoFe³³, Fe(211)/AlO_x/CoFe³⁴ and epitaxial-Fe₄N/MgO/CoFeB MTJs³⁵.

Another approach to obtain a high $V_{1/2}$ is to explore organic spin valves (OSVs), where carbon-based molecules are used between FM electrodes. The value of $V_{1/2}$ for C₆₀- and carbon nanotubes-based OSVs is approximately 0.2 V at 5 K³⁶. In OSVs using tris(8-hydroxyquinolate) aluminum (Alq₃) or rubrene, the $V_{1/2}$ has been reported to be 0.1–0.2 V at room temperature^{37–39}. Interestingly, graphene-based OSVs show the robustness of spin polarization in a non-local scheme⁴⁰. The normalized spin polarization reaches up to 0.8 at 1.2 V, which is

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inferior to MgO-based MTJs. Overall, efforts in increasing $V_{1/2}$ have not been successful in MTJs or other spintronic devices.

Complementary to TMR effect, the tunneling magnetocapacitance (TMC) is also inherent to the capacitive MTJ structure^{41–44}. Recently TMC has been increasingly studied due to their fascinating spin phenomena, such as spin capacitance^{45–48}, frequency-dependent spin transport^{42,43,49} and potential applications^{41,50}. Though TMC and TMR share some similar origins and are correlated, TMC is unique in many aspects. For example, TMC is peaked at a specific frequency⁴³, but is weakly dependent on the temperature⁴⁴. Furthermore, $V_{1/2}$ of TMC is higher than that of TMR^{44,47}. The highest $V_{1/2}$ of TMC in MgO-based MTJs is 0.7 V, which is almost twice as high as that of TMR in the same device⁴⁷. Therefore, TMC is more robust against biasing than TMR, and the mechanism of this robustness remains unclear. It is beneficial to understand this mechanism as the TMC effect may lead to more spintronic applications as well as insight into fundamental spintronic behavior.

In this work we report a new phenomenon at room temperature in which the TMC *increases* with applying biasing voltage in an MTJ system based on $\text{Co}_{40}\text{Fe}_{40}\text{B}_{20}/\text{MgO}/\text{Co}_{40}\text{Fe}_{40}\text{B}_{20}$. This result means an unprecedented enhancement of $V_{1/2}$ with regard to TMC. We have observed a maximum TMC value of 102% under biasing, which is the largest voltage-induced TMC effect ever reported for MTJs. There is an excellent agreement between theory and experiment for the TMC in the bipolar bias regions using Debye-Fröhlich (DF) model combined with quartic barrier approximation (QBA) and spin-dependent drift-diffusion (SDD) model. Based on our calculations, we predict that the voltage-induced TMC ratio could reach 1100% in MTJs with a corresponding TMR ratio of 604%.

Results and Discussion

Device structure and TMR and TMC under no bias voltage. Figure 1a shows the device structure prepared by a magnetron sputtering system with a base pressure of 2×10^{-8} Torr, with the following layer sequence: $\text{SiO}_2/\text{Ta}(5)/\text{Co}_{50}\text{Fe}_{50}(2)/\text{IrMn}(15)/\text{Co}_{50}\text{Fe}_{50}(2)/\text{Ru}(0.8)/\text{Co}_{40}\text{Fe}_{40}\text{B}_{20}(3)/\text{MgO}(2)/\text{Co}_{40}\text{Fe}_{40}\text{B}_{20}(3)/\text{contact layer}$ (thickness in nm). Details of the device fabrication procedure are described in the Experimental Section. Using standard photolithography, we have patterned the multilayer MTJ stacks into a junction area of $1800 \mu\text{m}^2$ with an elliptical shape with Ar ion-milling and SiO_2 insulation overlayer. The frequency characteristics and the bias voltage dependence of the TMR and TMC for MTJs were measured by an AC four-probe method at room temperature. The AC voltage was set to 2.6 mV_{rms}. The magnetic field was applied along the magnetic easy-axis direction to 1.4 kOe.

Figure 1b,c show the TMR and TMC curves at 60 Hz. The DC applied voltage is 0 V. Clear TMR and TMC effects are observed, i.e., $R_p < R_{AP}$ and $C_p > C_{AP}$. Large TMR and TMC ratios of approximately 100% are obtained at room temperature. Figure 1d,e shows the frequency characteristics of TMC, TMR and $C_{P(AP)}$. We calculated the frequency characteristics of the TMC and $C_{P(AP)}$ using the DF model^{43,51}. Based on the model, the capacitance $C_{P(AP)}^{\text{DF}}(f)$ as a function of frequency f for the P(AP) configuration in MTJs can be expressed by

$$C_{P(AP)}^{\text{DF}}(f) = \text{Re} \left[C_{\infty, P(AP)} + \frac{C_{0, P(AP)} - C_{\infty, P(AP)}}{1 + (i2\pi f\tau_{P(AP)})^{\beta_{P(AP)}}} \right], \quad (1)$$

where $C_{\infty, P(AP)}$ and $C_{0, P(AP)}$ are the high-frequency and static capacitances, $\tau_{P(AP)}$ is the relaxation time of electric dipoles, consisting of electrons and holes, formed near the interface between the FM layer and insulator, and $\beta_{P(AP)}$ is the exponent showing the distribution of the relaxation time, respectively, for the P(AP) configuration. After a straightforward calculation of Eq. (1), we can obtain

$$C_{P(AP)}^{\text{DF}}(f) = C_{\infty, P(AP)} + \frac{C_{0, P(AP)} - C_{\infty, P(AP)}}{2} \left[1 - \frac{\sinh[\beta_{P(AP)} \ln(2\pi f\tau_{P(AP)})]}{\cosh[\beta_{P(AP)} \ln(2\pi f\tau_{P(AP)})] + \cos(\beta_{P(AP)}\pi/2)} \right]. \quad (2)$$

The relation between τ_P and τ_{AP} in FM/insulator/FM is given by $\tau_{AP} = \tau_P(1 + P_{\text{TMC}}^2)/(1 - P_{\text{TMC}}^2)$, where P_{TMC} is the spin polarization inside the FM layer^{43,51}. Using these formula, we can calculate the frequency characteristics of the TMC ratio, defined by $\text{TMC}(f) = (C_p^{\text{DF}}(f) - C_{AP}^{\text{DF}}(f))/C_{AP}^{\text{DF}}(f)$. From Fig. 1d,e, it is evident that the theoretical results of the TMC and $C_{P(AP)}$ fit the experimental data very well. The calculation was based on the following parameters: $C_{\infty, P(AP)} = 1.45$ (1.5) nF, $C_{0, P(AP)} = 630$ (590) nF, $\beta_{P(AP)} = 0.998$ (0.977), $\tau_P = 0.0071$ s and $P_{\text{TMC}} = 0.46$. As for the magnetoresistance, we calculated the TMR ratio using the Julliere formula⁵², assuming a spin polarization P_{TMR} of 0.59. The difference between P_{TMC} and P_{TMR} is attributed to the different penetration lengths of spin-dependent carriers (inside $\text{Co}_{40}\text{Fe}_{40}\text{B}_{20}$) contributing to TMC and TMR. Our previous paper reveals that the penetration length (λ_{TMC}) of TMC is longer than that (λ_{TMR}) of TMR⁴³. Here, as is well known, the spin polarization of surface atoms in the FM layer or the interfacial FM atoms between FM/insulator is higher than that of inner atoms from the surface/interface due to the two-dimensional surface/interface effect^{53–55}. This picture can be applied to our MTJ system. Namely, the spin polarization (P_{inter}) of the first interfacial atoms in $\text{Co}_{40}\text{Fe}_{40}\text{B}_{20}$ layers is considered to be higher than that (P_{inner}) of inner atoms from the $\text{Co}_{40}\text{Fe}_{40}\text{B}_{20}/\text{MgO}$ interface (See Fig. S1). In fact, according to the first-principles calculation using the Vienna *Ab Initio* Simulation Package (VASP), the spin polarization at the Co terminated interface is higher than that of the inner Co and Fe atoms in CoFeB/MgO system⁵⁶. From these spin-polarization behavior, it is found that P_{TMC} is low for a long λ_{TMC} , and P_{TMR} is high for a short λ_{TMR} . According to the above fitting results, P_{TMC} is 0.46, and P_{TMR} is 0.59. The spin polarization P_{TMR} of 0.59 is in good agreement with the experimental value (0.57–0.65) of CoFeB alloy obtained by point-contact Andreev reflection⁵⁷. Also, we herein note that a negative TMC, i.e., $C_p < C_{AP}$, is observed in the high-frequency region. This can be understood from the fitting results, i.e., $C_{\infty, P(AP)} = 1.45$ (1.5) nF, as well as the

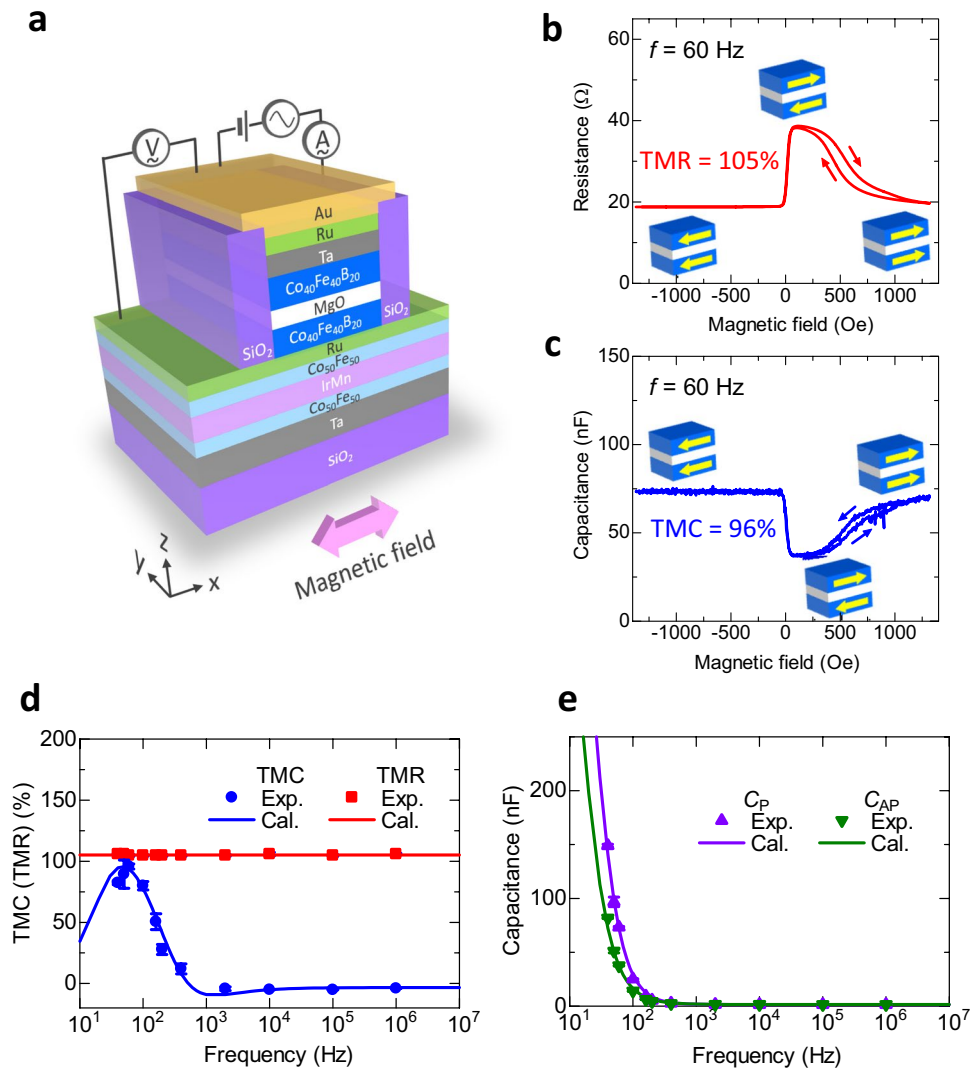


Figure 1. Device structure and TMR and TMC under no bias voltage. **(a)** Schematic of an MgO-based MTJ, with the structure: SiO₂/Ta(5 nm)/Co₅₀Fe₅₀(2 nm)/IrMn(15 nm)/Co₅₀Fe₅₀(2 nm)/Ru(0.8 nm)/Co₄₀Fe₄₀B₂₀(3 nm)/MgO(2 nm)/Co₄₀Fe₄₀B₂₀(3 nm)/contact layer. The measurement set-up for TMC and TMR is also shown. The magnetic field is applied along the magnetic easy-axis direction of Co₄₀Fe₄₀B₂₀ layers. **(b)** TMR and **(c)** TMC curves of an MgO-based MTJ. The frequency is 60 Hz and the DC voltage is 0 V. Frequency dependence of **(d)** TMC and TMR and **(e)** the capacitance $C_{P(AP)}$ in the P(AP) configuration. The solid plots represent the experimental data and the solid lines represent the calculation results obtained by Debye-Fröhlich model, described by Eq. (2).

experimental results shown in Fig. 1d. This is due to the appearance of the spin capacitance originated from the accumulation of spin-polarized carriers at the two FM/insulator interfaces. The detailed results and discussion are described in the Supplementary Information section. The excellent agreement between theory and experiment reveals that the TMC shows a maximum value of 96% at 60 Hz. Hence, we will use operation frequency of 60 Hz to study the bias dependence of TMC effect. Here, it is noted that we reported a high TMC of 155% in our previous paper⁴³. This result was obtained near zero bias voltage. In contrast, it is found that MTJs showing such high TMC tend to bring about the breakdown under the bias voltage. MTJs showing about 100% do not break down under the bias voltage, and the reproducibility is also good. From this reason, we have studied the bias dependence of TMC using MTJs with a TMC of about 100%.

Voltage-induced TMC and TMR. Figure 2 shows the bias dependence of TMC and TMR curves at 60 Hz. The TMC ratio under the applied bias voltage V_{DC} at the frequency f is defined by $TMC(f, V_{DC}) = (C_P(f, V_{DC}) - C_{AP}(f, V_{DC})) / C_{AP}(f, V_{DC})$. Interestingly, the TMC increases from 96% to 102% as the magnitude of bias voltage increases from 0 to 184 mV, whereas TMR rapidly decreases from 105% to 53%. As described earlier, the enhancement of $V_{1/2}^{TMR}$ is an important issue in the development of high-performance TMR devices. The typical value of $V_{1/2}^{TMR}$ is 0.1–1 V in MgO-based MTJs^{3,30,58,59}. In our devices, $V_{1/2}^{TMR}$ is 184 mV. In contrast, since the TMC does not decrease with the increasing bias voltage, the value of $V_{1/2}^{TMC}$ cannot be defined. In fact, TMC

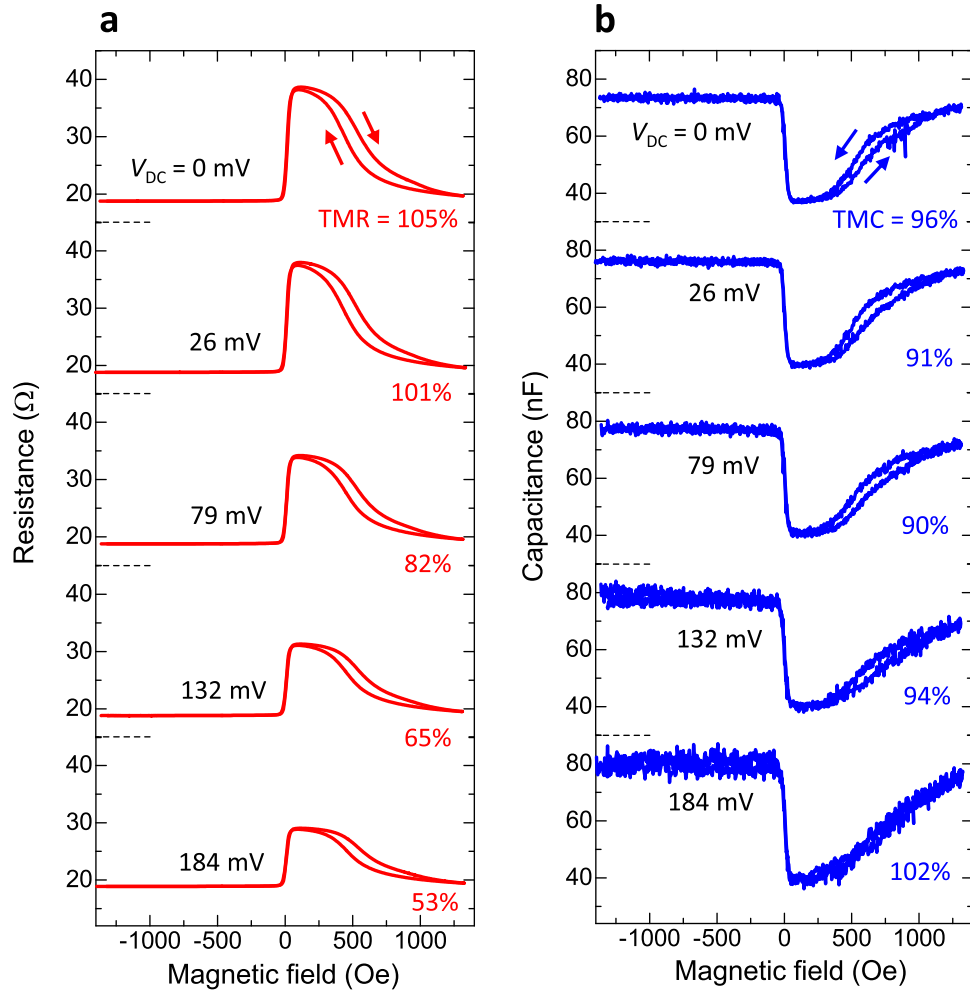


Figure 2. Bias dependence of TMR and TMC. **(a)** TMR and **(b)** TMC curves at 60 Hz in an MgO-based MTJ for positive DC voltages of 0, 26, 79, 132 and 184 mV. The AC voltage is $2.6 \text{ mV}_{\text{rms}}$.

remain robust against bias voltage which weakens the corresponding TMR quickly. Both the large TMC and its robustness are highly beneficial to spintronics applications associated with the TMC effect.

Modeling of voltage-induced TMC. Figure 3 shows the bias voltage dependence of $R_{P(\text{AP})}$, $C_{P(\text{AP})}$ and the modeling of the voltage-induced TMC. According to Zhang's theory²⁷, the tunnel conductance in FM/insulator/FM strongly depends on the bias voltage, especially within the order of a few hundred millivolts, due to hot electrons producing spin excitations. The conductance $G_{P(\text{AP})}(V_{\text{DC}})$ at the bias voltage V_{DC} in the P(AP) configuration can be expressed by $G_{P(\text{AP})}(V_{\text{DC}}) = G_{P(\text{AP})}^0(1 + \gamma_{P(\text{AP})}V_{\text{DC}})$, where $G_{P(\text{AP})}^0$ is the conductance at zero bias in the P(AP) configuration and $\gamma_{P(\text{AP})}$ is a parameter determined by the Curie temperatures of FM, the density of states (DOS) of itinerant electrons in FM, direct and spin-dependent transfers and spin quantum number within the framework of the transfer Hamiltonian. The resistance $R_{P(\text{AP})}(V_{\text{DC}})$ can be calculated from $R_{P(\text{AP})}(V_{\text{DC}}) = 1/G_{P(\text{AP})}(V_{\text{DC}})$. As shown in Fig. 3a, the experimental data of $R_{P(\text{AP})}(V_{\text{DC}})$ are in good agreement with the calculation using Zhang's model, where $\gamma_{P(\text{AP})}$ is set to 0.0188 (1.87). This means that Zhang's model is effective for explaining the bias dependence of TMR under both AC and DC mode.

The calculation of $C_p(f, V_{\text{DC}})$ is performed using the DF model combined with QBA. In the QBA, the potential profile of the barrier is assumed to be a quartic function, which is considered to be a good approximation to describe an AC tunneling transport⁵¹. The potential function $\phi_p(\eta)$ under the bias voltage V_{DC} in the P configuration can be expressed by $\phi_p(\eta) = 16\phi_{0,P}\eta^4 - 8\phi_{0,P}\eta^2 + \phi_{0,P} + eV_{\text{DC}}(1 - 2\eta)/2$, where $\eta = x/d$ is the reduced spatial variable, x is the distance from the center of the barrier, d and $\phi_{0,P}$ are the barrier thickness and height in the absence of the bias voltage, respectively, and e is the electron charge. The potential profile is depicted in Fig. 3b. The solution of $\phi_p(\eta) = eV_{\text{DC}}$ is $\eta_1 = -1/2$, η_2 , η_3 and η_4 (for $\eta_2 < 0$, η_3 and $\eta_4 > 0$, $\eta_3 < \eta_4$). Since the values of η_2 , η_3 and η_4 can be calculated by the Cardano's method, the effective barrier thickness d_{eff} can be represented by $d_{\text{eff}} = (1/2 + \eta_3)d$, where η_3 depends on V_{DC} and $\phi_{0,P}$. Therefore, $C_p(f, V_{\text{DC}})$ at the applied DC voltage in the P configuration can be written by

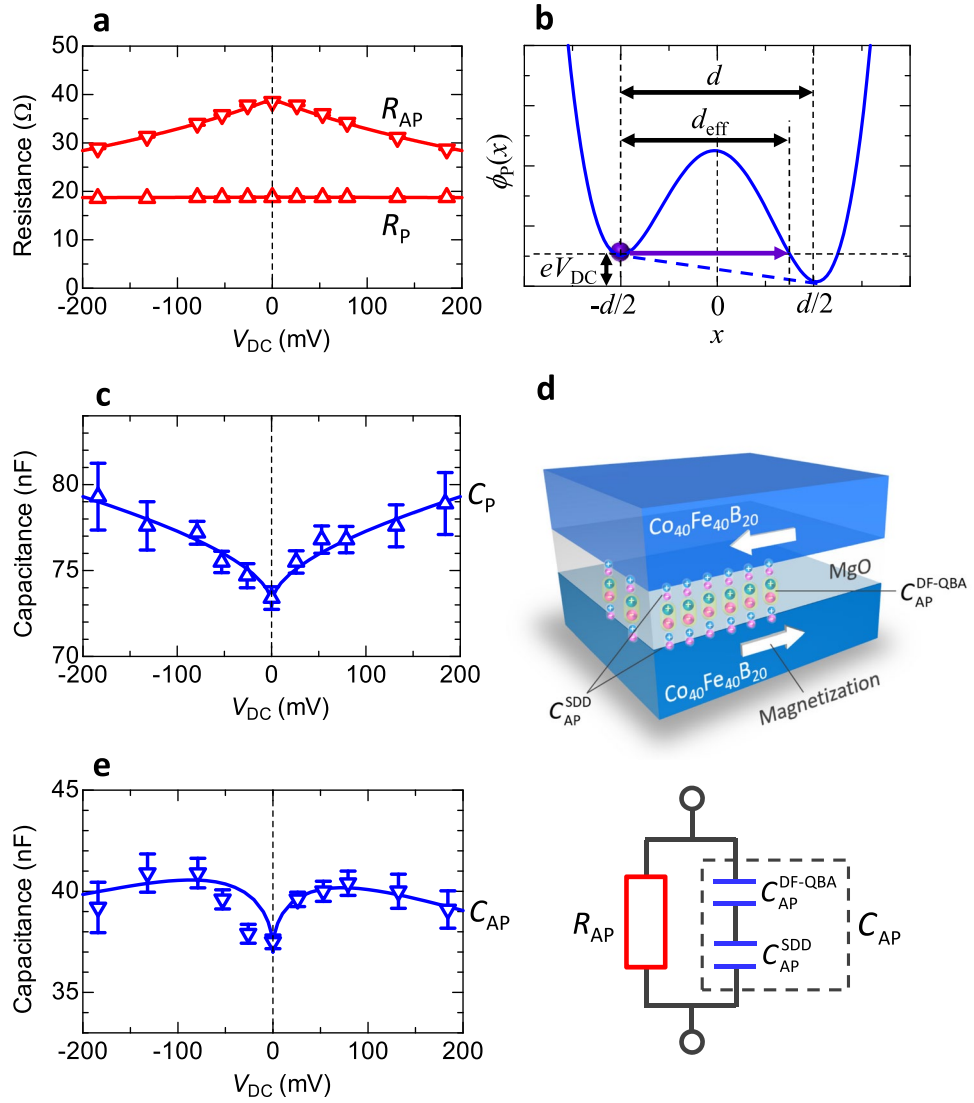


Figure 3. Modeling of the voltage-induced TMC. DC voltage dependence of (a) the resistance $R_{P(AP)}$ in the P(AP) configuration. The calculation of $R_{P(AP)}$ is performed using Zhang’s theory. (b) Schematic of the electric potential profile of MTJs under DC voltage. The QBA is used to calculate the effective barrier thickness, which contributes to the measured capacitance. DC voltage dependence of (c) the capacitance C_P in the P configuration. The C_P is calculated using DF model under the QBA, described by Eq. (3). (d) Schematic of charge accumulation, contributing to $C_{AP}^{DF-QBA}(f, V_{DC})$ and $C_{AP}^{SDD}(f, V_{DC})$, and the equivalent circuit in the AP configuration. $C_{AP}^{DF-QBA}(f, V_{DC})$ is described by the DF model combined with QBA under the DC voltage V_{DC} at the frequency f [Eq. (6)]. $C_{AP}^{SDD}(f, V_{DC})$ is obtained from the SDD model [Eq. (4)]. The equivalent circuit of the MTJ is modeled by the RC parallel network, consisting of the resistance $R_{AP}(V_{DC})$ and capacitance $C_{AP}(f, V_{DC})$. DC voltage dependence of (e) the capacitance C_{AP} in the AP configuration.

$$C_P(f, V_{DC}) = \frac{1}{1/2 + \eta_3(V_{DC}, \phi_{0,P})} \left[C_{\infty,P} + \frac{C_{0,P} - C_{\infty,P}}{2} \left(1 - \frac{\sinh[\beta_P \ln(2\pi f \tau_P)]}{\cosh[\beta_P \ln(2\pi f \tau_P)] + \cos(\beta_P \pi/2)} \right) \right]. \quad (3)$$

As shown in Fig. 3c, the measured capacitance $C_P(f, V_{DC})$ exhibiting a cusp-like behavior, is very well described by Eq. (3), using parameters of $C_{\infty,P} = 1.45$ nF, $C_{0,P} = 630$ nF, $\beta_P = 0.998$, $\tau_P = 0.0075$ s, $f = 60$ Hz and $\phi_{0,P} = 2.15$ eV. Hence, the QBA is a good approximation for the expression of the potential-barrier profile in MTJs based on $Co_{40}Fe_{40}B_{20}/MgO/Co_{40}Fe_{40}B_{20}$ in calculating the bias dependence of C_P under AC field.

The calculation of $C_{AP}(f, V_{DC})$ is performed using the DF model combined with QBA and SDD model. Based on the SDD model⁶⁰, the accumulation of minority spins and the depletion of majority spins take place at the interface between the $Co_{40}Fe_{40}B_{20}$ and MgO layers in the AP configuration. The spin accumulation causes a difference in the chemical potential between majority and minority spins, resulting in a different diffusion length in each spin. The difference in the diffusion length gives rise to the creation of tiny screening charge dipoles, which

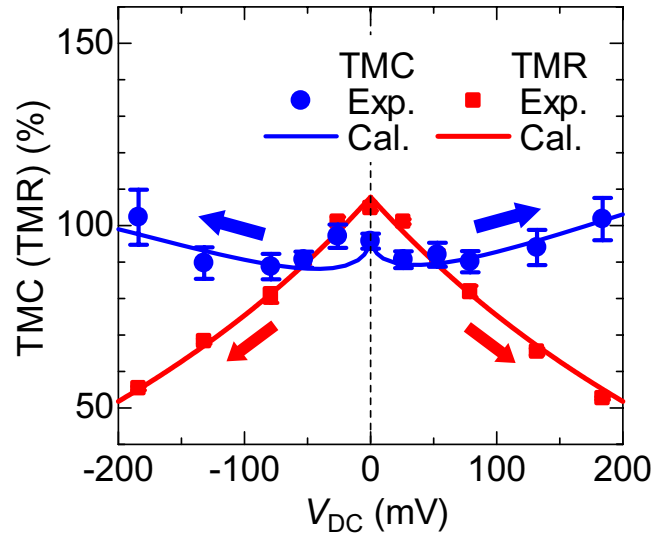


Figure 4. Bias dependence of TMC and TMR ratio. The solid lines represent the calculation results performed using Eqs (3)–(6) for TMC and Zhang formula for TMR. The parameters used in this calculation are described in the main text. The TMC and TMR provide excellent fits to experimental data in bipolar bias regions.

act as an additional serial capacitance, i.e., spin capacitance. The screening charge density is given by $en_{\text{AP}}(x_i) = en_{0,\text{AP}} \exp(-x_i/\lambda)$, where x_i is the distance from the interface between the $\text{Co}_{40}\text{Fe}_{40}\text{B}_{20}$ and MgO , λ is a characteristic screening length and $en_{0,\text{AP}}$ is a screening charge density at the interface in the AP configuration. The spin capacitance can be expressed by $C_{\text{AP}}^{\text{SDD}}(V_{\text{DC}}) = \Delta Q_{\text{AP}}/\Delta V_{\text{DC}}$, where ΔQ_{AP} is the screening charge for the AP configuration and ΔV_{DC} is the electrical potential difference applied in the charging space. Therefore, the spin capacitance can be obtained as $C_{\text{AP}}^{\text{SDD}}(V_{\text{DC}}) = eSn_{\text{AP}}(x_i)dx_i/dV_{\text{DC}}(x_i)$, where S is a junction area and $V_{\text{DC}}(x_i)$ is an electrical potential as a function of x_i in the charging space, i.e., $V_{\text{DC}}(x_i) = V_{\text{eff}} \exp(-x_i/\lambda)$. V_{eff} is an effective applied voltage, which is expressed by κV , where κ is an adjustable positive parameter of much smaller than 1.0. Consequently, the spin capacitance can be represented by

$$C_{\text{AP}}^{\text{SDD}}(V_{\text{DC}}) = eS \frac{n_{0,\text{AP}} \lambda}{\kappa V_{\text{DC}}}. \quad (4)$$

Since this screening charge acts as a serial capacitance, the capacitance $C_{\text{AP}}(f, V_{\text{DC}})$ under the applied DC voltage V_{DC} in the AP configuration,

$$C_{\text{AP}}(f, V_{\text{DC}}) = \left(\frac{1}{C_{\text{AP}}^{\text{DF-QBA}}(f, V_{\text{DC}})} + \frac{1}{C_{\text{AP}}^{\text{SDD}}(V_{\text{DC}})} \right)^{-1}, \quad (5)$$

where the capacitance $C_{\text{AP}}^{\text{DF-QBA}}(f, V_{\text{DC}})$ based on the DF model combined with QBA in the AP configuration is represented by

$$C_{\text{AP}}^{\text{DF-QBA}}(f, V_{\text{DC}}) = \frac{1}{1/2 + \eta_3(1 - \kappa)V_{\text{DC}}\phi_{0,\text{AP}}} \times \left[C_{\infty,\text{AP}} + \frac{C_{0,\text{AP}} - C_{\infty,\text{AP}}}{2} \left(1 - \frac{\sinh[\beta_{\text{AP}} \ln(2\pi f \tau_{\text{AP}})]}{\cosh[\beta_{\text{AP}} \ln(2\pi f \tau_{\text{AP}})] + \cos(\beta_{\text{AP}} \pi / 2)} \right) \right]. \quad (6)$$

The behavior of charge accumulation, contributing to $C_{\text{AP}}^{\text{DF-QBA}}$ and $C_{\text{AP}}^{\text{SDD}}$, is illustrated in Fig. 3d. The bias voltage dependence of the capacitance C_{AP} in the AP configuration is shown in Fig. 3e. The capacitance C_{AP} increases at around zero bias and then it decreases at higher voltages. This behavior is in good agreement with the results calculated by Eqs (4)–(6) with parameters of $C_{\infty,\text{AP}} = 1.5$ nF, $C_{0,\text{AP}} = 590$ nF, $\beta_{\text{AP}} = 0.977$, $\tau_{\text{P}} = 0.0075$ s, $P_{\text{TMC}} = 0.46$, $f = 60$ Hz, $\kappa = 0.1$, $S = 1800 \mu\text{m}^2$ and $\lambda = 0.1$ nm. $\phi_{0,\text{AP}}$ is 0.144 (0.153) eV and $n_{0,\text{AP}}$ is 0.94 (0.92) $\times 10^{23} \text{ cm}^{-3}$ for the positive (negative) bias region. The increase of C_{AP} near zero bias is attributed to the decrease of the effective barrier thickness d_{eff} . As seen from the potential profile $\phi_{\text{P}}(x)$ of MTJs shown in Fig. 3b, d_{eff} decreases with increasing bias voltage V_{DC} . This corresponds to the decrease of η_3 . According to our calculation, η_3 is 0.5, 0.35 and 0.28 for V_{DC} of 0, 50 and 100 mV, respectively. From Eq. (6), it is found that $C_{\text{AP}}^{\text{DF-QBA}}(f, V_{\text{DC}})$ increases with decreasing η_3 . Therefore, $C_{\text{AP}}(f, V_{\text{DC}})$ increases with increasing V_{DC} . The reduction of C_{AP} at higher voltages is attributed to the spin capacitance, described in Eq. (4), i.e., the spin capacitance decreases with increasing V_{DC} .

Figure 4 shows the bias-voltage dependence of the TMC and TMR ratios. The calculation of the TMC is performed using Eqs (3)–(6) for setting the same parameters used in the calculation of $C_{\text{P(AP)}}(f, V_{\text{DC}})$ in Fig. 3c,e. The TMR is obtained from the Zhang formula. The calculation results of the TMC and TMR provide excellent fits to experimental data in bipolar bias regions. The reduction of TMR can be easily understood from the experimental

results of both no significant change of $R_p(V_{DC})$ and the reduction of $R_{AP}(V_{DC})$ in higher voltages, as shown in Fig. 3a. In particular, the reduction of $R_{AP}(V_{DC})$ is due to the existence of hot electrons tunneling through the barrier, which brings about the decrease of TMR. The enhancement of TMC can also be clearly understood from the results of both the increase of $C_p(f, V_{DC})$ and the reduction of $C_{AP}(f, V_{DC})$ in higher voltages, as shown in Fig. 3c,e. The reduction of $C_{AP}(f, V_{DC})$ is attributed to the emergence of the spin capacitance, which promotes the increase of TMC. Thus, the spin capacitance gives a significant influence on TMC, and it will play an important role on future application.

Though the application of the interesting TMC effect is not well understood at this stage, we venture to discuss the application potential of TMC devices. As can be seen from Fig. 4, TMR is larger than TMC in the low bias region. In considering the application, the important factor in sensing is an electric sensitivity. The electric sensitivity is generally expressed by the signal-to-noise (S/N) ratio, which is defined as $20\log V_s/V_N$. Here V_s is a signal voltage and V_N is a noise voltage. In the case of TMR sensing under the applied voltage V_{DC} , since V_s is given by $TMR \cdot V_{DC}$ and V_N is proportional to $\sqrt{V_{DC}}$, V_s/V_N is proportional to $TMR \cdot \sqrt{V_{DC}}$. Therefore, the increase of V_{DC} is necessary for the improvement of the S/N ratio. In fact, magnetic read heads, sensors, or MRAMs are designed for operation under a bias of a few hundred mV⁶¹. Additionally, the enhancement of TMR at a higher voltage is of importance. As shown in Fig. 4, the TMR decreases with increasing V_{DC} , whereas TMC increases at higher voltages. Since V_s/V_N is proportional to $TMC \cdot \sqrt{V_{DC}}$ in TMC sensing, the TMC is superior to TMR from the viewpoint of the S/N ratio. Furthermore, the impedance Z of TMC devices can be reduced in the high frequency region since the impedance of the capacitor is expressed as $Z = 1/j\omega C$, where ω is the angular frequency. This means that the noise voltage V_N could be reduced. The high V_s and low V_N lead to the enhancement of the S/N ratio. Also, the AC technique allows for the performance of various functions such as modulation/demodulation, filtering, oscillation and resonance. In fact, magnetoimpedance devices using the AC technique have enabled the application to geomagnetic sensors or positioning sensors of GPS^{62–65}. Also, a capacitive magnetic sensing, in which an RC parallel circuit module consisting semiconductor magnetoresistance device and capacitor was used in the feedback loop of a Hartley or Colpitts oscillator, has been proposed and demonstrated by our group^{66–68}. In short, TMC devices may pave a new way for various applications to the next generation of magnetic read heads, MRAMs, logic circuits, and highly sensitive magnetic sensors (including geomagnetic sensors, positioning sensors, etc.).

Prediction of an extremely large voltage-induced TMC. Finally, the spin polarization dependence of the voltage-induced TMC is calculated for the prediction of an extremely large TMC. Figure 5a,b shows the calculated frequency dependence of the TMC under no bias voltage and the bias dependence of the TMC with varying P , respectively. Here, P_{TMC} is assumed to be equal to P_{TMR} , which is denoted by P . The assumed maximum value of P is 0.87, which is estimated experimentally for high-performance MgO-based MTJs at room temperature¹². The parameters used in the calculation of the TMC are $C_{\infty, P(AP)} = 1.45$ (1.5) nF, $C_{0, P(AP)} = 184$ (172) nF, $\beta_{P(AP)} = 0.998$ (0.932) and $\tau_p = 0.0033$ s. As can be seen from Fig. 5a, the TMC ratio at $V_{DC} = 0$ V shows the maximum value at $f = 60$ Hz for the P of 0.70, 0.79 and 0.87, respectively, and it increases from 273% to 995% with increasing P from 0.70 to 0.87. The maximum TMC of 273%, 505% and 995% are larger than TMR ratios of 192%, 325% and 604%, which are calculated from Julliere formula using $P = 0.70, 0.79$ and 0.87, respectively. The parameters used in the calculation of the bias dependence of TMC are $f = 60$ Hz, $\kappa = 0.1$, $S = 1800 \mu\text{m}^2$ and $\lambda = 0.1$ nm. The barrier height $\phi_{0,p}$ is 2.15 eV, and $\phi_{0,AP}$ is 0.144 (0.153) eV in the positive (negative) bias voltage. The screening charge densities $n_{0,AP}$ are 0.312 (0.306), 0.208 (0.204) and 0.125 (0.123) $\times 10^{23} \text{ cm}^{-3}$ in the positive (negative) bias voltage for the spin polarizations P of 0.70, 0.79 and 0.87, respectively. The TMC increases from 995% to 1119% with increasing V_{DC} from 0 to 200 mV. Figure 5c shows the calculated frequency dependence of the TMC at $V_{DC} = 200$ mV with varying τ_p . The maximum peak of the TMC is shifted to a high frequency region on the order of MHz for a short τ_p in the sub- μs scale. According to the DF model, τ_p can be tuned by changing the oscillation speed of electric dipoles formed near the FM/insulator interfaces; τ_p is short for a high oscillation speed. From the viewpoint of MTJ device structure, τ_p can be tuned by changing the thickness of the insulating barrier; τ_p could shorten in MTJs with a thinner barrier. Although this realization in MTJs is future work, the recent study using FeCo-MgF nanogranular films has demonstrated that the TMC peak is observed at a high frequency of 220 MHz, which corresponds to τ_p of 0.72 ns⁶⁹. Our calculations predict that a large TMC of over 1100% could be possibly observed using MTJs with a realistic P of 0.87. Furthermore, this large TMC can be tuned from low to high frequencies by shortening τ_p .

In summary, we observed a new phenomenon in which the TMC *increases* with the bias voltage in MgO-based MTJs at room temperature. The enhancement of TMC is attributed to the emergence of the spin capacitance in the AP configuration of MTJs. The voltage-induced TMC increases to 102%, which is the largest value ever reported for MTJs. We also found the voltage-induced TMC can be well explained by a newly proposed theoretical calculation using DF model combined with QBA and SDD model. This calculation predicts that the voltage-induced TMC could potentially reach 1100% in MTJs with a corresponding TMR value of 604%. These theoretical and experimental findings provide a deep insight into the voltage-induced AC spin transport in MTJs. We demonstrated that the complementary TMR and TMC effects must be treated on equal footing. The large TMC effect and the associated robustness against biasing may open up new avenues for spintronics applications and electrical modeling.

Methods

Preparation of the samples. The MTJs were prepared by using a magnetron sputtering system with a base pressure of 2×10^{-8} Torr. The MTJs have the following layer sequence: SiO₂/Ta(5)/Co₅₀Fe₅₀(2)/IrMn(15)/Co₅₀Fe₅₀(2)/Ru(0.8)/Co₄₀Fe₄₀B₂₀(3)/MgO(2)/Co₄₀Fe₄₀B₂₀(3)/contact layer (thickness in nm). We deposited all the metallic layers in DC mode under a sputtering Ar gas pressure of 1.5 mTorr. The MgO layer was deposited with

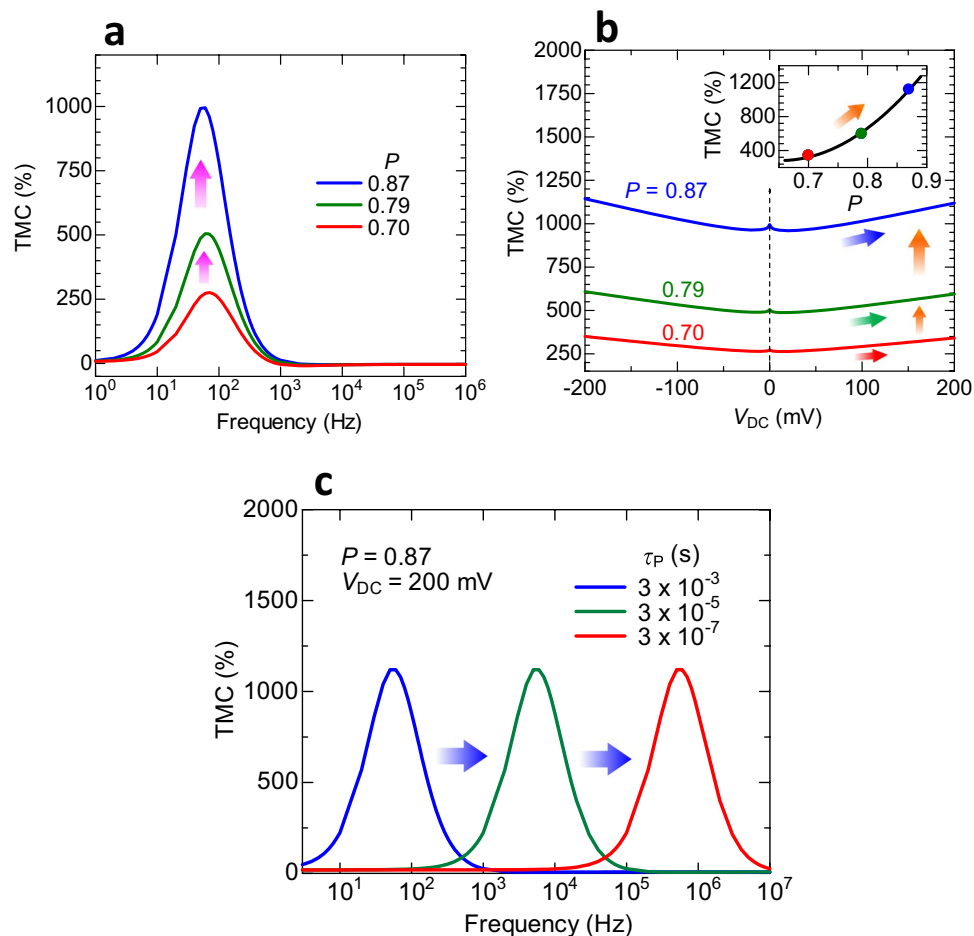


Figure 5. Calculated frequency dependence of extremely large voltage-induced TMC. (a) Calculated frequency dependence of the TMC at $V_{DC} = 0$ V in varying P . The TMC, showing the maximum value at $f = 60$ Hz, increases from 273% to 995% with increasing P from 0.70 to 0.87. (b) Calculated DC voltage dependence of the TMC. The calculation result predicts that the voltage-induced TMC could potentially reach 1100% in MTJs with a P of 0.87, which is within the realm of high-performance MTJs (See ref.¹²). (c) Calculated frequency dependence of the voltage-induced TMC with varying τ_P . The peak position of the TMC is shifted to a high frequency region for a short τ_P .

radio frequency (RF) magnetron sputtering at an Ar gas pressure of 1.1 mTorr. Using standard photolithography, we have patterned the multilayer MTJ stacks into a junction area of 1800 μm^2 with an elliptical shape with Ar ion-milling and SiO₂ insulation overlayer. Finally, we annealed the MTJs at 310 °C for 4 h in vacuum of 10⁻⁶ Torr under a uniform magnetic field of 4.5 kOe to define the pinning axis for the Co₄₀Fe₄₀B₂₀ bottom electrode.

Measurements of the voltage-induced TMC. The frequency characteristics and the bias voltage dependence of the TMR and TMC for MTJs were measured by an AC four-probe method using an Agilent Technologies 4284 A LCR meter at room temperature. The frequency ranged from 50 Hz to 1 MHz and the bipolar bias voltage was applied up to 200 mV. The AC voltage was set to 2.6 mV_{rms}. The magnetic field was applied along the magnetic easy-axis direction to 1.4 kOe.

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Author Contributions

H.K. and G.X. conceived and designed the experiments using the help of other authors. G.X. performed the sample preparation and structural analysis. H.K., T.M. and T.N. performed dc measurements. H.K., M.F. and J.N. performed ac impedance measurements. H.K., G.X., T.K. and O.K. performed the theoretical analysis and calculation. All the authors contributed to analyzing and interpreting the data, and to writing the manuscript.

Additional Information

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