

Received 29 August 2015 Accepted 10 September 2015

Edited by M. Weil, Vienna University of Technology, Austria

Keywords: crystal structure; ruthenium complex; piano-stool coordination geometry; thiolate ligands

CCDC reference: 1423473 **Supporting information**: this article has supporting information at journals.iucr.org/e



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 $\kappa^2 S:S$)bis(μ -phenylmethanethiolato- $\kappa^2 S:S$)bis[(η^6 -1isopropyl-4-methylbenzene)ruthenium(II)] tetrafluoridoborate

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The crystal structure of the dinuclear arene ruthenium title complex, $[Ru_2(C_6H_5OS)(C_7H_7S)_2(C_{10}H_{14})_2]BF_4$, shows the two Ru^{II} atoms to be bridged by two benzylthiophenolate units and one 4-hydroxythiophenolate unit, with the remaining three coordination sites of each Ru^{II} atom being occupied by *p*-cymene ligands, completing the typical piano-stool coordination geometry. The BF₄⁻ counter-anion is surrounded by four cationic dinuclear complexes, showing an O-H···F hydrogen bond and several weak C-H···F interactions. This is the first example of an X-ray analysis of a mixed dinuclear trithiolate arene ruthenium(II) complex.

1. Chemical context

In the search for novel metal-based anticancer agents, several series of dinuclear trithiolate arene ruthenium complexes have been synthesized by our group (Gras et al., 2010; Giannini et al., 2012, 2013a). The biological studies in vitro showed the chloride salts of these complexes to have IC₅₀ values regularly in the nanomolar range, making them some of the most active ruthenium complexes found to date. The recent discovery of dithiolate complexes (Ibao et al., 2012) allowed us to synthesize the so-called mixed trithiolate complexes of the type $[(p-MeC_6H_4^{i}Pr)_2Ru_2(SCH_2R_1)_2(S-p-C_6H_4-R_2]^+ (R_1 = C_6H_5,$ $CH_2C_6H_5$, $p-C_6H_4'Bu$; $R_2 = H$, OH, F, Br, ^{*i*}Pr, ^{*i*}Bu). All of the complexes were found to be highly cytotoxic against ovarian cancer cell lines A2780 and A2780cisR as chloride salts, none of them could however be crystallized and analyzed by X-ray crystallography (Giannini et al., 2013b). Herein we report the isolation and the crystal structure of the title compound, $[(p-MeC_6H_4^{i}Pr)_2Ru_2(SCH_2C_6H_5)_2(S-p-C_6H_4OH)]BF_4, (I), the$ first reported structure of a mixed trithiolate complex.





Figure 1

The structure of the molecular components of (I). Displacement ellipsoids are drawn at the 50% probability level.

2. Structural commentary

The structures of the molecular components of compound (I) are presented in Fig. 1. Both Ru^{II} atoms adopt the typical piano-stool geometry with the *p*-cymene ligand being bound facially, formally occupying three coordination sites; the other three positions are occupied by two benzylthiophenolate units and one 4-hydroxythiophenolate unit. In agreement with the electron count, there is no metal-metal bond, the Ru...Ru distance being 3.3632 (4) Å. The interatomic distances between Ru1 and S1, S2 and S3 are 2.3878 (9), 2.4023 (9) and 2.3813 (8) Å, respectively, and between Ru2 and S1, S2 and S3 2.3992 (9), 2.3991 (8) and 2.3882 (8) Å, respectively, showing that the central diruthenium trithiolate unit is not symmetric. The presence of the two bent benzylthiolate ligands forces the dinuclear arene ruthenium unit to adopt a distorted geometry - the angle between the two p-cymene planes (C1-C6 and C11–C16) is 6.2 (2) $^{\circ}$. The distances between the Ru^{II} atoms and the centroids of the associated rings are 1.708 and 1.709 Å.



Figure 2 Surroundings of the BF_4^- anion in the crystal packing of (I).

Table 1	
Hydrogen-bond geometry (Å, $^{\circ}$).	

$D - H \cdots A$	$D-\mathrm{H}$	$H \cdots A$	$D \cdots A$	$D - H \cdot \cdot \cdot A$
O1−H1···F1	0.82	1.99	2.773 (9)	161
$C3-H3 \cdot \cdot \cdot F3^{i}$	0.93	2.52	3.340 (11)	148
$C30-H30\cdots F2^{i}$	0.93	2.60	3.472 (9)	156
C6−H6···F4 ⁱⁱ	0.93	2.34	3.249 (10)	166

Symmetry codes: (i) $x + \frac{1}{2}, y - \frac{1}{2}, z$; (ii) $x, -y + 1, z - \frac{1}{2}$.

3. Supramolecular features

In the crystal packing of (I), the BF_4^- anion interacts with the -OH group of the 4-hydroxythiophenolate unit. In addition, weak $C-H\cdots F$ interactions are observed (Table 1), thus creating around the BF_4 anion a densely packed arrangement (Fig. 2). No significant $C-H\cdots \pi$ or $\pi-\pi$ stacking interactions are observed in the crystal structure.

4. Synthesis and crystallization

Complex (I) was obtained from the reaction of 0.127 mmol (100 mg) of the neutral dithiolate precursor $[(p-MeC_6H_4^{i}Pr)_2-Ru_2(SCH_2C_6H_5)_2Cl_2]$ (Ibao *et al.*, 2012) with three equivalents of 4-hydroxythiophenol in refluxing ethanol. The product was isolated by column chromatography on silica gel, using the

Table 2	
Experimental details.	
Crystal data	
Chemical formula	$[Ru_2(C_6H_5OS)(C_7H_7S)_2(C_{10}H_{14})_2]-BF_4$
Mr	928.91
Crystal system, space group	Monoclinic, Cc
Temperature (K)	173
<i>a</i> , <i>b</i> , <i>c</i> (Å)	15.4807 (10), 14.3435 (11), 17.7605 (10)
β (°)	99.435 (5)
$V(Å^3)$	3890.3 (4)
Ζ	4
Radiation type	Μο Κα
$\mu \text{ (mm}^{-1})$	0.99
Crystal size (mm)	$0.22 \times 0.20 \times 0.18$
Data collection	
Diffractometer	Stoe IPDS
No. of measured, independent and observed $[I > 2\sigma(I)]$ reflections	34511, 10178, 8902
R _{int}	0.060
$(\sin \theta / \lambda)_{\max} (\text{\AA}^{-1})$	0.690
Refinement	
$R[F^2 > 2\sigma(F^2)], wR(F^2), S$	0.032, 0.074, 0.95
No. of reflections	10178
No. of parameters	466
No. of restraints	2
H-atom treatment	H-atom parameters constrained
$\Delta \rho_{\rm max}, \Delta \rho_{\rm min} ({\rm e} {\rm \AA}^{-3})$	0.52, -0.69
Absolute structure	Flack x determined using 3741 quotients $[(I^+)-(I^-)]/[(I^+)+(I^-)]$ (Parsons <i>et al.</i> , 2013).
Absolute structure parameter	-0.01(2)

Computer programs: *EXPOSE*, *CELL* and *INTEGRATE* in *IPDS Software* (Stoe & Cie, 2000), *SHELXS97* and *SHELXL97* (Sheldrick, 2008), *SHELXL2014* (Sheldrick, 2015) and *ORTEP-32* (Farrugia, 2012).

solvent mixture $CH_2Cl_2/EtOH$ 7:1 (ν/ν) as eluent. The orange band was collected; the product was stirred overnight with ten equivalents of NaBF₄ and isolated by filtration and evaporation of the solvent. X-ray quality crystals were obtained by slow diffusion of diethyl ether vapors into the solution of (I) in dichloromethane.

Yield: 111 mg (94%). ESI–MS (MeOH/CH₂Cl₂): $m/z = 842.3 \ [M]^+$. ¹H NMR (400 MHz, CDCl₃): $\delta = 7.41 \ (m, 10H, SCH₂C₆H₅; 2H, S-$ *p*-C₆H₄OH), 7.00 (*d*, ³*J*= 8 Hz, 2H, S-*p*-C₆H₄OH) 5.06 [*d*, ³*J*= 6.0 Hz, 2H,*p*-CH₃C₆H₄CH(CH₃)₂], 4.94 [*d*, ³*J*= 6.0 Hz, 2H,*p*-CH₃C₆H₄CH(CH₃)₂], 4.71 [*m*, 4H,*p*-CH₃C₆H₄CH(CH₃)₂], 3.62 (*s*, 2H, SCH₂C₆H₅), 3.45 (*s*, 2H, SCH₂C₆H₅), 2.04 [sept, ³*J*= 6.8 Hz, 2H,*p*-CH₃C₆H₄CH(CH₃)₂], 1.73 (*s*, 6H,*p*-CH₃C₆H₄CH(CH₃)₂), 1.05 [*d*, ³*J*= 6.8 Hz, 6H,*p*-CH₃C₆H₄CH(CH₃)₂], 0.99 [*d*, ³*J*= 6.8 Hz, 6H,*p* $-CH₃C₆H₄CH(CH₃)₂] p.p.m. ¹³C{¹H} NMR (100 MHz,CDCl₃): <math>\delta = 159.9, 139.9, 139.7, 133.3, 129.5, 129.2, 128.8, 128.7, 128.2, 128.1, 124.0, 117.1, 107.5, 99.7, 84.1, 83.7, 83.2, 82.0, 39.9, 39.5, 31.0, 23.1, 22.7, 18.0 p.p.m.$

5. Refinement

Crystal data, data collection and structure refinement details are summarized in Table 2. All H atoms were included in calculated positions and treated as riding atoms, with C-H =

0.93 Å for C_{arom} and 0.96 Å for CH_3 , and with $U_{iso}(H) = 1.2U_{eq}(C)$ or $1.5U_{eq}(C)$ for methyl H atoms.

Acknowledgements

We would like to acknowledge the financial support of the Swiss National Science Foundation (grant No. 200020-143254).

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supporting information

Acta Cryst. (2015). E71, 1174-1176 [doi:10.1107/S2056989015016953]

Crystal structure of (μ -4-hydroxybenzenethiolato- $\kappa^2 S$:S)bis(μ -phenylmethane-thiolato- $\kappa^2 S$:S)bis[(η^6 -1-isopropyl-4-methylbenzene)ruthenium(II)] tetrafluoridoborate

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Computing details

Data collection: *EXPOSE* in *IPDS Software* (Stoe & Cie, 2000); cell refinement: *CELL* in *IPDS Software* (Stoe & Cie, 2000); data reduction: *INTEGRATE* in *IPDS Software* (Stoe & Cie, 2000); program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL2014* (Sheldrick, 2015); molecular graphics: *ORTEP-32* (Farrugia, 2012); software used to prepare material for publication: *SHELXL97* (Sheldrick, 2008).

$(\mu$ -4-Hydroxybenzenethiolato- $\kappa^2 S$:S)bis $(\mu$ -phenylmethanethiolato- $\kappa^2 S$:S)bis $[(\eta^6-1-isopropy)]$ -4-methylbenzene)ruthenium(II)] tetrafluoridoborate

Crystal	data
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[Ru ₂ (C ₆ H ₅ OS)(C ₇ H ₇ S) ₂ (C ₁₀ H ₁₄) ₂]BF ₄
$M_r = 928.91$
Monoclinic, Cc
Hall symbol: C -2yc
a = 15.4807 (10) Å
b = 14.3435 (11) Å
c = 17.7605 (10) Å
$\beta = 99.435 \ (5)^{\circ}$
$V = 3890.3 (4) Å^3$
Z=4

Data collection

Stoe IPDS diffractometer Radiation source: fine-focus sealed tube Graphite monochromator Detector resolution: 0.81 pixels mm⁻¹ phi oscillation scans 34511 measured reflections

Refinement

Refinement on F^2 Least-squares matrix: full $R[F^2 > 2\sigma(F^2)] = 0.032$ $wR(F^2) = 0.074$ S = 0.9510178 reflections 466 parameters F(000) = 1888 $D_x = 1.586 \text{ Mg m}^{-3}$ Mo K α radiation, $\lambda = 0.71073 \text{ Å}$ Cell parameters from 8000 reflections $\theta = 2.1-28.7^{\circ}$ $\mu = 0.99 \text{ mm}^{-1}$ T = 173 KBlock, red $0.22 \times 0.20 \times 0.18 \text{ mm}$

10178 independent reflections 8902 reflections with $I > 2\sigma(I)$ $R_{int} = 0.060$ $\theta_{max} = 29.4^\circ, \ \theta_{min} = 2.0^\circ$ $h = -21 \rightarrow 21$ $k = -19 \rightarrow 19$ $l = -24 \rightarrow 24$

2 restraints
Primary atom site location: structure-invariant direct methods
Secondary atom site location: difference Fourier map
Hydrogen site location: inferred from neighbouring sites

H-atom parameters constrained $w = 1/[\sigma^2(F_o^2) + (0.0431P)^2]$ where $P = (F_o^2 + 2F_c^2)/3$ $(\Delta/\sigma)_{max} = 0.001$ $\Delta\rho_{max} = 0.52 \text{ e} \text{ Å}^{-3}$ $\Delta \rho_{\min} = -0.69 \text{ e} \text{ Å}^{-3}$ Absolute structure: Flack *x* determined using 3741 quotients [(*I*⁺)-(*I*)]/[(*I*⁺)+(*I*)] (Parsons *et al.*, 2013).
Absolute structure parameter: -0.01 (2)

Special details

Experimental. A crystal was mounted at 173 K on a Stoe Image Plate Diffraction System (Stoe & Cie, 2000) using Mo $K\alpha$ graphite monochromated radiation. Image plate distance 100 mm, φ oscillation scans 0 - 180°, step $\Delta \varphi = 1.2^{\circ}$, 5 minutes per frame.

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

Fractional atomic coordinates a	nd isotropic or	equivalent isotrop	oic displacement	parameters	$(Å^2)$
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	x	у	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	
C1	0.3292 (2)	0.1913 (3)	-0.0509 (2)	0.0418 (9)	
C2	0.3924 (2)	0.1437 (2)	0.0030(2)	0.0331 (8)	
H2	0.4249	0.0957	-0.0136	0.040*	
C3	0.4066 (2)	0.1680 (3)	0.0807 (3)	0.0374 (8)	
Н3	0.4490	0.1366	0.1146	0.045*	
C4	0.3569 (3)	0.2402 (3)	0.1080 (3)	0.0465 (10)	
C5	0.2935 (3)	0.2860 (3)	0.0556 (3)	0.0528 (13)	
Н5	0.2601	0.3330	0.0725	0.063*	
C6	0.2797 (3)	0.2620 (3)	-0.0221 (3)	0.0539 (13)	
H6	0.2369	0.2934	-0.0555	0.065*	
C7	0.3156 (3)	0.1726 (5)	-0.1358 (3)	0.0646 (15)	
H7	0.2531	0.1806	-0.1556	0.077*	
C8	0.3413 (5)	0.0761 (5)	-0.1566 (3)	0.085 (2)	
H8A	0.4037	0.0691	-0.1436	0.128*	
H8B	0.3238	0.0665	-0.2104	0.128*	
H8C	0.3130	0.0310	-0.1290	0.128*	
C9	0.3654 (6)	0.2436 (6)	-0.1742 (5)	0.110 (3)	
H9A	0.4271	0.2323	-0.1605	0.165*	
H9B	0.3520	0.3050	-0.1581	0.165*	
H9C	0.3489	0.2386	-0.2286	0.165*	
C10	0.3719 (3)	0.2648 (4)	0.1917 (3)	0.0667 (16)	
H10A	0.4222	0.3047	0.2030	0.100*	
H10B	0.3817	0.2088	0.2215	0.100*	
H10C	0.3213	0.2965	0.2038	0.100*	
C11	-0.0326 (3)	-0.0067 (3)	0.0892 (3)	0.0397 (10)	
C12	0.0199 (3)	-0.0321 (3)	0.1574 (3)	0.0441 (10)	
H12	0.0179	0.0032	0.2010	0.053*	
C13	0.0767 (3)	-0.1107 (3)	0.1620 (3)	0.0466 (10)	

LI12	0 1105	-0.1269	0 2084	0.056*
П13 С14	0.1103	-0.1208 -0.1642(2)	0.2064	0.030°
C14	0.0818(3)	-0.1045(3)	0.0902(3)	0.0484(11)
	0.0298 (3)	-0.1365 (5)	0.0277 (3)	0.0472 (10)
HI5	0.0328	-0.1/01	-0.0166	0.05/*
C16	-0.0262 (2)	-0.0602 (3)	0.0242 (3)	0.0419 (9)
HI6	-0.0601	-0.0443	-0.0222	0.050*
C17	-0.0956 (3)	0.0766 (3)	0.0801 (3)	0.0545 (12)
H17	-0.0907	0.1071	0.0316	0.065*
C18	-0.0757 (4)	0.1487 (4)	0.1421 (5)	0.082 (2)
H18A	-0.0799	0.1208	0.1905	0.123*
H18B	-0.1170	0.1989	0.1324	0.123*
H18C	-0.0175	0.1724	0.1430	0.123*
C19	-0.1899 (3)	0.0414 (4)	0.0745 (6)	0.095 (3)
H19A	-0.2025	-0.0017	0.0328	0.143*
H19B	-0.2296	0.0932	0.0660	0.143*
H19C	-0.1967	0.0107	0.1212	0.143*
C20	0.1397 (3)	-0.2491 (3)	0.0989 (5)	0.091 (3)
H20A	0.1881	-0.2428	0.1399	0.137*
H20B	0.1613	-0.2550	0.0515	0.137*
H20C	0.1065	-0.3037	0.1071	0.137*
C21	0.1759 (2)	0.1523 (2)	0.2144 (2)	0.0318 (7)
C22	0.1763 (2)	0.1270 (3)	0.2903 (2)	0.0381 (8)
H22	0.1959	0.0680	0.3069	0.046*
C23	0.1479 (3)	0.1880 (3)	0.3412 (2)	0.0456 (9)
H23	0.1476	0.1698	0.3914	0.055*
C24	0.1202 (2)	0.2753(3)	0.3176 (2)	0.0431(9)
C25	0.1177(3)	0.3026 (3)	0.2427(2)	0.0407(8)
H25	0.0976	0.3617	0.2269	0.049*
C26	0.1457(2)	0.2409(3)	0.1908(2)	0.0365 (8)
H26	0.1440	0.2589	0.1403	0.0303 (0)
C27	0.1440 0.3138 (2)	-0.1002(3)	0.1405 0.0697 (3)	0.0413(9)
H27A	0.3150	-0.0850	0.0097(3)	0.0413 ())
1127A 1127B	0.3139	-0.1646	0.1234	0.050*
1127B	0.2933	-0.0887(2)	0.0017	0.030°
C20	0.4040(2) 0.4722(2)	-0.0887(3)	0.0494(3)	0.0382(9)
U29	0.4752 (5)	-0.0340(3)	0.1000 (5)	0.0403 (10)
П29	0.4000	-0.0401	0.1497	0.030°
C30	0.5545 (5)	-0.0392(3)	0.0774 (3)	0.0540 (12)
H30	0.6005	-0.0153	0.1121	0.065*
C31	0.5663 (3)	-0.0597 (3)	0.0048 (3)	0.0536 (11)
H31	0.6203	-0.0487	-0.0101	0.064*
C32	0.4971 (3)	-0.0975 (3)	-0.0476 (3)	0.0601 (13)
H32	0.5052	-0.1129	-0.0968	0.072*
C33	0.4171 (3)	-0.1112 (3)	-0.0250 (3)	0.0500 (11)
H33	0.3710	-0.1358	-0.0595	0.060*
C34	0.0879 (2)	0.1145 (3)	-0.0955 (2)	0.0406 (8)
H34A	0.1073	0.1690	-0.1205	0.049*
H34B	0.1209	0.0612	-0.1088	0.049*
C35	-0.0078 (2)	0.0988 (3)	-0.1235 (2)	0.0376 (8)

C36	-0.0411 (3)	0.0170 (3)	-0.1584 (3)	0.0511 (10)
H36	-0.0032	-0.0302	-0.1678	0.061*
C37	-0.1319 (4)	0.0053 (4)	-0.1796 (3)	0.0602 (13)
H37	-0.1538	-0.0494	-0.2036	0.072*
C38	-0.1877 (3)	0.0729 (4)	-0.1652 (3)	0.0652 (14)
H38	-0.2478	0.0638	-0.1782	0.078*
C39	-0.1565 (3)	0.1543 (5)	-0.1317 (3)	0.0691 (15)
H39	-0.1950	0.2013	-0.1229	0.083*
C40	-0.0678 (3)	0.1665 (3)	-0.1112 (3)	0.0494 (10)
H40	-0.0472	0.2222	-0.0882	0.059*
01	0.0975 (2)	0.3350 (3)	0.3719 (2)	0.0593 (8)
H1	0.0820	0.3852	0.3519	0.089*
S1	0.22003 (5)	0.07062 (6)	0.15529 (5)	0.02976 (16)
S2	0.23352 (5)	-0.02440 (6)	0.01262 (5)	0.02999 (17)
S3	0.11024 (5)	0.13178 (6)	0.00909 (5)	0.02880 (17)
Ru1	0.265363 (15)	0.136095 (17)	0.044464 (15)	0.02751 (6)
Ru2	0.107114 (15)	-0.013494 (17)	0.074285 (15)	0.02631 (6)
B1	0.1140 (3)	0.5937 (4)	0.2810 (3)	0.0508 (12)
F1	0.0880 (5)	0.5128 (3)	0.3096 (4)	0.161 (3)
F2	0.1726 (2)	0.5769 (3)	0.23242 (19)	0.0842 (11)
F3	0.0429 (4)	0.6320 (7)	0.2444 (4)	0.196 (4)
F4	0.1457 (4)	0.6454 (6)	0.3380 (4)	0.212 (5)

Atomic displacement parameters $(Å^2)$

	U^{11}	U^{22}	U^{33}	U^{12}	U^{13}	U^{23}
C1	0.0331 (17)	0.046 (2)	0.049 (2)	-0.0089 (16)	0.0128 (17)	0.0188 (18)
C2	0.0272 (16)	0.0314 (17)	0.043 (2)	-0.0065 (13)	0.0120 (15)	0.0043 (15)
C3	0.0244 (15)	0.0380 (19)	0.050(2)	-0.0071 (14)	0.0069 (15)	0.0017 (18)
C4	0.0360 (18)	0.035 (2)	0.070 (3)	-0.0164 (16)	0.0148 (19)	-0.009(2)
C5	0.044 (2)	0.0277 (19)	0.093 (4)	-0.0083 (16)	0.030 (3)	0.002 (2)
C6	0.037 (2)	0.037 (2)	0.091 (4)	-0.0002 (16)	0.020 (2)	0.033 (2)
C7	0.044 (2)	0.104 (4)	0.048 (3)	-0.009 (3)	0.015 (2)	0.029 (3)
C8	0.111 (5)	0.102 (5)	0.041 (3)	-0.062(4)	0.011 (3)	-0.002 (3)
C9	0.147 (7)	0.088 (4)	0.119 (6)	0.024 (4)	0.089 (5)	0.058 (4)
C10	0.048 (2)	0.073 (3)	0.082 (4)	-0.022 (2)	0.021 (2)	-0.042 (3)
C11	0.0280 (17)	0.0348 (19)	0.060 (3)	-0.0046 (14)	0.0184 (18)	0.0097 (18)
C12	0.046 (2)	0.050(2)	0.044 (2)	-0.0096 (18)	0.0295 (19)	0.0008 (19)
C13	0.0347 (18)	0.058 (2)	0.049 (2)	-0.0050 (17)	0.0108 (17)	0.030 (2)
C14	0.0350 (19)	0.0304 (18)	0.086 (4)	-0.0031 (15)	0.029 (2)	0.017 (2)
C15	0.041 (2)	0.040 (2)	0.066 (3)	-0.0169 (17)	0.028 (2)	-0.014 (2)
C16	0.0275 (17)	0.054 (2)	0.045 (2)	-0.0154 (17)	0.0077 (16)	0.0044 (19)
C17	0.038 (2)	0.041 (2)	0.088 (4)	0.0049 (17)	0.020 (2)	0.014 (2)
C18	0.058 (3)	0.047 (3)	0.147 (6)	0.004 (2)	0.034 (4)	-0.018 (3)
C19	0.036 (2)	0.049 (3)	0.205 (8)	0.001 (2)	0.032 (4)	-0.002 (4)
C20	0.051 (3)	0.037 (2)	0.197 (8)	0.004 (2)	0.053 (4)	0.031 (4)
C21	0.0247 (14)	0.0372 (18)	0.0332 (18)	-0.0013 (13)	0.0034 (13)	0.0016 (14)
C22	0.0385 (18)	0.041 (2)	0.0360 (19)	0.0022 (15)	0.0097 (15)	0.0095 (15)

supporting information

C23	0.047 (2)	0.060 (3)	0.033 (2)	0.0005 (19)	0.0154 (17)	0.0044 (18)
C24	0.0354 (19)	0.056 (2)	0.041 (2)	0.0008 (17)	0.0153 (16)	-0.0088 (18)
C25	0.0425 (19)	0.0381 (19)	0.042 (2)	0.0079 (16)	0.0078 (17)	-0.0012 (16)
C26	0.0432 (19)	0.0360 (18)	0.0303 (18)	0.0049 (15)	0.0062 (15)	0.0029 (14)
C27	0.0338 (18)	0.0351 (19)	0.058 (3)	0.0087 (15)	0.0176 (18)	0.0067 (18)
C28	0.0307 (17)	0.0327 (19)	0.054 (2)	0.0045 (14)	0.0142 (17)	0.0050 (17)
C29	0.041 (2)	0.045 (2)	0.054 (3)	0.0077 (17)	0.0079 (18)	0.0115 (19)
C30	0.0323 (19)	0.056 (3)	0.070 (3)	-0.0020 (18)	-0.002 (2)	0.014 (2)
C31	0.034 (2)	0.051 (3)	0.080 (3)	0.0052 (18)	0.022 (2)	0.006 (2)
C32	0.054 (3)	0.053 (3)	0.082 (4)	-0.005 (2)	0.038 (3)	-0.015 (3)
C33	0.040 (2)	0.047 (2)	0.067 (3)	-0.0054 (17)	0.020 (2)	-0.014 (2)
C34	0.0354 (18)	0.058 (2)	0.0292 (19)	0.0035 (16)	0.0076 (15)	0.0106 (17)
C35	0.0370 (18)	0.043 (2)	0.033 (2)	-0.0005 (15)	0.0069 (15)	0.0046 (16)
C36	0.064 (3)	0.050 (2)	0.040 (2)	0.003 (2)	0.008 (2)	-0.0050 (19)
C37	0.067 (3)	0.054 (3)	0.055 (3)	-0.022 (2)	-0.004 (2)	-0.005 (2)
C38	0.047 (2)	0.079 (4)	0.064 (3)	-0.006 (3)	-0.008 (2)	0.008 (3)
C39	0.039 (2)	0.092 (4)	0.071 (4)	0.010 (2)	-0.006 (2)	-0.015 (3)
C40	0.039 (2)	0.048 (2)	0.057 (3)	0.0047 (17)	-0.0073 (19)	-0.005 (2)
01	0.071 (2)	0.064 (2)	0.0481 (18)	0.0128 (17)	0.0241 (16)	-0.0114 (16)
S 1	0.0282 (4)	0.0300 (4)	0.0310 (4)	0.0016 (3)	0.0046 (3)	0.0047 (3)
S2	0.0257 (4)	0.0291 (4)	0.0370 (5)	-0.0027 (3)	0.0104 (3)	0.0007 (3)
S3	0.0242 (4)	0.0319 (4)	0.0307 (4)	-0.0001 (3)	0.0057 (3)	0.0069 (3)
Ru1	0.02280 (11)	0.02572 (12)	0.03464 (14)	-0.00190 (10)	0.00659 (10)	0.00523 (11)
Ru2	0.02355 (11)	0.02625 (12)	0.03065 (13)	-0.00107 (11)	0.00895 (9)	0.00414 (12)
B1	0.045 (2)	0.054 (3)	0.053 (3)	0.005 (2)	0.008 (2)	-0.008 (2)
F1	0.235 (7)	0.072 (3)	0.220 (7)	0.026 (3)	0.171 (6)	0.007 (3)
F2	0.080 (2)	0.118 (3)	0.060 (2)	0.033 (2)	0.0282 (17)	0.0103 (19)
F3	0.111 (4)	0.341 (11)	0.141 (5)	0.118 (5)	0.035 (4)	0.067 (6)
F4	0.189 (6)	0.306 (9)	0.170 (6)	-0.184 (7)	0.113 (5)	-0.171 (6)

Geometric parameters (Å, °)

C1—C6	1.416 (7)	C20—H20A	0.9600
C1—C2	1.425 (6)	C20—H20B	0.9600
C1—C7	1.513 (7)	C20—H20C	0.9600
C1—Ru1	2.240 (4)	C21—C26	1.395 (5)
C2—C3	1.406 (6)	C21—C22	1.396 (5)
C2—Ru1	2.213 (3)	C21—S1	1.782 (4)
С2—Н2	0.9300	C22—C23	1.382 (6)
C3—C4	1.421 (6)	C22—H22	0.9300
C3—Ru1	2.224 (4)	C23—C24	1.367 (6)
С3—Н3	0.9300	С23—Н23	0.9300
C4—C5	1.400 (7)	C24—O1	1.376 (5)
C4—C10	1.508 (7)	C24—C25	1.382 (6)
C4—Ru1	2.233 (4)	C25—C26	1.396 (5)
C5—C6	1.404 (8)	C25—H25	0.9300
C5—Ru1	2.196 (4)	C26—H26	0.9300
С5—Н5	0.9300	C27—C28	1.508 (5)

C6—Ru1	2.189 (4)	C27—S2	1.828 (4)
С6—Н6	0.9300	С27—Н27А	0.9700
C7—C8	1.504 (9)	С27—Н27В	0.9700
С7—С9	1.507 (8)	C28—C29	1.375 (6)
С7—Н7	0.9800	C28—C33	1.406 (6)
C8—H8A	0 9600	C_{29} C 30	1 395 (6)
C8—H8B	0.9600	C29—H29	0.9300
C8—H8C	0.9600	C_{30} C_{31}	1 364 (8)
	0.9600	C_{30} H30	0.9300
	0.9600	C_{31} C_{32}	1 408 (8)
C9—119B	0.9000	$C_{21} = U_{21}$	1.408 (8)
	0.9000	C31—H31	0.9300
	0.9600	C32—C33	1.377 (0)
CIO—HIOB	0.9600	С32—Н32	0.9300
CI0—HIOC	0.9600	С33—Н33	0.9300
C11—C12	1.392 (7)	C34—C35	1.501 (5)
C11—C16	1.403 (6)	C34—S3	1.849 (4)
C11—C17	1.534 (6)	C34—H34A	0.9700
C11—Ru2	2.223 (4)	C34—H34B	0.9700
C12—C13	1.424 (6)	C35—C40	1.385 (6)
C12—Ru2	2.174 (4)	C35—C36	1.386 (6)
C12—H12	0.9300	C36—C37	1.405 (7)
C13—C14	1.411 (7)	С36—Н36	0.9300
C13—Ru2	2.199 (4)	C37—C38	1.350 (8)
С13—Н13	0.9300	С37—Н37	0.9300
C14—C15	1.402 (7)	C38—C39	1.363 (8)
C14—C20	1.507 (6)	С38—Н38	0.9300
C14—Ru2	2.244 (4)	C39—C40	1.372 (6)
C15—C16	1.391 (6)	С39—Н39	0.9300
C15—Ru2	2.215 (4)	C40—H40	0.9300
C15—H15	0.9300	01—H1	0.8200
$C16$ — Ru^2	2 213 (4)	S1—Rul	23878(9)
C16_H16	0.9300	S1Ru2	2.3070(9)
C17 - C18	1 505 (8)	S_{2}	2.3992(9)
C17 = C10	1.505 (6)	$S_2 = Ru_2$	2.3771(0)
C17 - C19	0.0800	$S_2 = R_{11}$	2.4023(9)
$C_1/-H_1/$	0.9800	55—KUI 52 Du2	2.3013(0)
	0.9000	55—KU2	2.3002(0)
	0.9600	B1—F4	1.286 (7)
CI8—HI8C	0.9600	BI—F3	1.304 (7)
CI9—HI9A	0.9600		1.355 (7)
С19—Н19В	0.9600	B1—F2	1.372 (6)
С19—Н19С	0.9600		
C6—C1—C2	117.0 (4)	C25—C26—H26	119.8
C6—C1—C7	119.4 (4)	C28—C27—S2	112.0 (3)
C2—C1—C7	123.6 (4)	С28—С27—Н27А	109.2
C6—C1—Ru1	69.4 (2)	S2—C27—H27A	109.2
C2—C1—Ru1	70.3 (2)	С28—С27—Н27В	109.2
C7—C1—Ru1	133.2 (3)	S2—C27—H27B	109.2

C3—C2—C1	121.4 (4)	H27A—C27—H27B	107.9
C3—C2—Ru1	71.9 (2)	C29—C28—C33	118.7 (4)
C1—C2—Ru1	72.4 (2)	C29—C28—C27	122.4 (4)
С3—С2—Н2	119.3	C33—C28—C27	118.8 (4)
C1—C2—H2	119.3	C28—C29—C30	120.6 (4)
Ru1—C2—H2	128.7	С28—С29—Н29	119.7
C2—C3—C4	120.6 (4)	С30—С29—Н29	119.7
C2—C3—Ru1	71.1 (2)	$C_{31} - C_{30} - C_{29}$	120.5 (4)
C4-C3-Ru1	71.7 (2)	$C_{31} - C_{30} - H_{30}$	119.7
$C_2 = C_3 = H_3$	1197	C_{29} C_{30} H_{30}	119.7
C4-C3-H3	119.7	C_{30} C_{31} C_{32}	120.0(4)
Ru1 C3 H3	130.0	$C_{30} = C_{31} = C_{32}$	120.0 (4)
$C_5 C_4 C_3$	118 A (A)	$C_{30} = C_{31} = H_{31}$	120.0
$C_{5} = C_{4} = C_{10}$	110.4(4) 121.5(4)	$C_{22} = C_{21} = C_{21}$	120.0
C_{3} C_{4} C_{10}	121.3(4)	$C_{22} = C_{22} = C_{21}$	119.1 (5)
C_{3} C_{4} C_{10}	120.1(4)	C33—C32—H32	120.5
C_{3} C_{4} R_{1}	70.2 (2)	C31—C32—H32	120.5
C3—C4—Rul	/1.1 (2)	C32—C33—C28	121.0 (4)
C10—C4—Ru1	129.5 (3)	С32—С33—Н33	119.5
C4—C5—C6	121.0 (4)	С28—С33—Н33	119.5
C4—C5—Ru1	73.0 (2)	C35—C34—S3	111.4 (3)
C6—C5—Ru1	71.1 (2)	С35—С34—Н34А	109.3
C4—C5—H5	119.5	S3—C34—H34A	109.3
С6—С5—Н5	119.5	C35—C34—H34B	109.3
Ru1—C5—H5	128.8	S3—C34—H34B	109.3
C5—C6—C1	121.7 (4)	H34A—C34—H34B	108.0
C5—C6—Ru1	71.6 (2)	C40—C35—C36	117.0 (4)
C1C6Ru1	73.3 (2)	C40—C35—C34	119.6 (4)
С5—С6—Н6	119.1	C36—C35—C34	123.4 (4)
С1—С6—Н6	119.1	C35—C36—C37	120.3 (4)
Ru1—C6—H6	128.2	С35—С36—Н36	119.9
C8—C7—C9	109.5 (5)	С37—С36—Н36	119.9
C8—C7—C1	114.1 (4)	C38—C37—C36	120.4 (4)
C9—C7—C1	109.5 (6)	C38—C37—H37	119.8
C8—C7—H7	107.8	C36—C37—H37	119.8
C9-C7-H7	107.8	$C_{37} - C_{38} - C_{39}$	120.4(5)
C1H7	107.8	C_{37} C_{38} H_{38}	110.8
C7 C8 H8A	107.8	C_{30} C_{38} H_{38}	110.8
$C_7 = C_8 = H_8 R$	109.5	$C_{39} = C_{30} = C_{40}$	119.8
	109.5	$C_{38} = C_{39} = C_{40}$	119.3 (3)
HoA - Co - HoB	109.5	C40 C20 H20	120.3
$C = C = H \delta C$	109.5	C40—C39—H39	120.3
H8A—C8—H8C	109.5	$C_{39} - C_{40} - C_{35}$	122.5 (5)
H8B—C8—H8C	109.5	C39—C40—H40	118.8
С/—С9—Н9А	109.5	C35—C40—H40	118.8
С'/—С9—Н9В	109.5	C24—O1—H1	109.5
Н9А—С9—Н9В	109.5	C21—S1—Ru1	114.81 (12)
С7—С9—Н9С	109.5	C21—S1—Ru2	111.85 (11)
Н9А—С9—Н9С	109.5	Ru1—S1—Ru2	89.27 (3)
Н9В—С9—Н9С	109.5	C27—S2—Ru2	108.48 (13)

C4—C10—H10A	109.5	C27—S2—Ru1	110.18 (15)
C4—C10—H10B	109.5	Ru2—S2—Ru1	88.93 (3)
H10A—C10—H10B	109.5	C34—S3—Ru1	106.43 (12)
C4—C10—H10C	109.5	C34—S3—Ru2	110.79 (14)
H10A—C10—H10C	109.5	Ru1—S3—Ru2	89.68 (3)
H10B-C10-H10C	109.5	C6—Ru1—C5	37.3 (2)
C12—C11—C16	117.6 (4)	C6—Ru1—C2	66.74 (14)
C12—C11—C17	124.4 (4)	C5—Ru1—C2	78.89 (15)
C16-C11-C17	1180(4)	C6-Ru1-C3	78 73 (16)
C_{12} C_{11} R_{11}	69.6 (2)	C5— $Ru1$ — $C3$	66 47 (16)
C_{16} C_{11} R_{12}	71.2(2)	$C_2 = R_{\rm H} 1 = C_3$	36.95 (15)
$C_{10} = C_{11} = R_{12}$	1205(3)	C_{2} Rul C_{3}	66 98 (19)
$C_{11} = C_{12} = C_{13}$	129.5(3) 121.6(4)	C_{0} Ru1 C_{4}	26.93(19)
$C_{11} = C_{12} = C_{13}$	121.0(4)	$C_3 = Ru_1 = C_4$	50.05(10)
C12 - C12 - Ruz	75.5 (2)	C_2 —Ru1—C4	07.04(13)
C13 - C12 - Ru2	/1.9(2)	C_3 —Ru1—C4	37.19(15)
C11—C12—H12	119.2	C6—Ru1—C1	37.27 (17)
C13—C12—H12	119.2	C5— $Ru1$ — $C1$	67.45 (18)
Ru2—C12—H12	127.5	C2—Ru1—C1	37.31 (14)
C14—C13—C12	120.1 (4)	C3—Ru1—C1	67.13 (15)
C14—C13—Ru2	73.2 (2)	C4—Ru1—C1	79.82 (16)
C12—C13—Ru2	70.0 (2)	C6—Ru1—S3	93.80 (11)
C14—C13—H13	119.9	C5—Ru1—S3	103.06 (12)
С12—С13—Н13	119.9	C2—Ru1—S3	145.72 (11)
Ru2—C13—H13	129.1	C3—Ru1—S3	169.43 (11)
C15—C14—C13	117.4 (4)	C4—Ru1—S3	132.82 (11)
C15—C14—C20	120.7 (5)	C1—Ru1—S3	111.14 (11)
C13—C14—C20	121.8 (5)	C6—Ru1—S1	147.03 (15)
C15—C14—Ru2	70.5 (2)	C5—Ru1—S1	113.05 (15)
C13—C14—Ru2	69.7 (2)	C2—Ru1—S1	133.72 (11)
C20—C14—Ru2	131.6 (3)	C3— $Ru1$ — $S1$	104.49 (11)
C16-C15-C14	121.9 (4)	C4— $Ru1$ — $S1$	95 42 (12)
C_{16} C_{15} R_{12}	71.6(2)	$C1_Ru1_S1$	170.98(11)
C_{14} C_{15} R_{u2}	71.0(2) 72.8(2)	$S_3 = R_{11} = S_1$	77 72 (3)
$C_{14} = C_{15} = K_{02}$	110.1	C6 Pu1 S2	13430(16)
$C_{10} = C_{15} = H_{15}$	119.1	C_{0} Ru1 S2	134.30(10) 171.64(15)
$C_{14} - C_{15} - II_{15}$	119.1	$C_3 = Ru_1 = S_2$	171.04(13)
Ru2—C15—H15	129.0	C_2 —Ru1—S2	97.38 (10)
	121.4 (4)	C3—Ru1—S2	114.82 (11)
C15-C16-Ru2	/1.8 (2)	C4—Ru1—S2	148.05 (12)
C11—C16—Ru2	72.0 (2)	C1—Ru1—S2	105.05 (12)
C15—C16—H16	119.3	S3—Ru1—S2	75.75 (3)
C11—C16—H16	119.3	S1—Ru1—S2	74.95 (3)
Ru2—C16—H16	129.5	C12—Ru2—C13	38.01 (17)
C18—C17—C19	110.6 (5)	C12—Ru2—C16	66.05 (17)
C18—C17—C11	114.1 (5)	C13—Ru2—C16	78.40 (16)
C19—C17—C11	109.4 (4)	C12—Ru2—C15	78.34 (16)
С18—С17—Н17	107.5	C13—Ru2—C15	66.03 (18)
С19—С17—Н17	107.5	C16—Ru2—C15	36.62 (17)
C11—C17—H17	107.5	C12—Ru2—C11	36.90 (18)

C17—C18—H18A	109.5	C13—Ru2—C11	67.55 (15)
C17—C18—H18B	109.5	C16—Ru2—C11	36.87 (16)
H18A—C18—H18B	109.5	C15—Ru2—C11	66.59 (15)
C17—C18—H18C	109.5	C12—Ru2—C14	67.56 (16)
H18A—C18—H18C	109.5	C13—Ru2—C14	37.03 (19)
H18B—C18—H18C	109.5	C16—Ru2—C14	66.43 (17)
С17—С19—Н19А	109.5	C15—Ru2—C14	36.65 (19)
C17—C19—H19B	109.5	C_{11} Ru2 $-C_{14}$	79.68 (14)
H19A—C19—H19B	109.5	C12—Ru2—S3	120.02 (12)
C17—C19—H19C	109.5	C13— $Ru2$ — $S3$	157.02 (13)
H19A—C19—H19C	109.5	C16—Ru2—S3	99.26 (12)
H19B—C19—H19C	109.5	C15 - Ru2 - S3	124.53 (14)
C14-C20-H20A	109.5	$C_{11} = R_{11} = S_{12}$	96 70 (10)
C14-C20-H20B	109.5	C14—Ru2—S3	160 63 (15)
$H_{20}A = C_{20} = H_{20}B$	109.5	C12 = Ru2 = S2	161.04(13)
C14 - C20 - H20C	109.5	C13 = Ru2 = S2	124 58 (12)
H_{20}^{-} $H_{$	109.5	C_{16} Ru2 S2	124.98(12)
$H_{20B} = C_{20} = H_{20C}$	109.5	$C_{15} = R_{12} = S_{2}^{2}$	121.90(12) 102.07(11)
$C_{26} = C_{21} = C_{22}$	118 4 (3)	$C_{11} = R_{11} = S_2$	159.91 (13)
$C_{26} = C_{21} = C_{22}$	1244(3)	C14—Ru2—S2	101 26 (10)
$C_{22} = C_{21} = S_{1}$	1172(3)	S_{3} Ru ² S ²	75 68 (3)
C_{23} C_{22} C_{21} C_{21}	121 1 (4)	$C_{12}^{$	97 29 (12)
$C_{23} = C_{22} = H_{22}$	119 5	C13 = Ru2 = S1	96 53 (12)
C_{21} C_{22} H_{22}	119.5	C_{16} Ru2 S1	158 92 (12)
C_{24} C_{23} C_{22}	119.9 (4)	C_{15} Ru2 S1	150.92(12) 157.00(14)
$C_{24} = C_{23} = H_{23}$	120.1	C_{11} Ru2 SI	122 26 (13)
$C_{22} = C_{23} = H_{23}$	120.1	C14— $Ru2$ — $S1$	120.75 (14)
C_{23} C_{24} C	117 3 (4)	$S_3 = R_{12} = S_1$	77 37 (3)
C_{23} C_{24} C_{25}	120 8 (4)	S_{2}^{2} Ru2 S_{1}^{2}	74.81 (3)
$01 - C^{24} - C^{25}$	121.9 (4)	F4 - B1 - F3	109 4 (7)
C_{24} C_{25} C_{26}	1196(4)	F4—B1—F1	107 3 (6)
C_{24} C_{25} H_{25}	120.2	F3—B1—F1	105 7 (6)
$C_{26} = C_{25} = H_{25}$	120.2	F4—B1—F2	113.0 (5)
$C_{21} - C_{26} - C_{25}$	120.3 (4)	F3 - B1 - F2	110.6 (5)
C21—C26—H26	119.8	F1 - B1 - F2	110.6 (5)
C6—C1—C2—C3	-1.9(5)	C2—C1—Ru1—S2	-82.3(2)
C7—C1—C2—C3	175.7 (4)	C7—C1—Ru1—S2	35.7 (5)
Ru1—C1—C2—C3	-54.9 (3)	C34—S3—Ru1—C6	63.2 (2)
C6—C1—C2—Ru1	53.1 (3)	Ru2—S3—Ru1—C6	174.80 (16)
C7—C1—C2—Ru1	-129.4 (4)	C34—S3—Ru1—C5	99.8 (2)
C1—C2—C3—C4	1.1 (5)	Ru2—S3—Ru1—C5	-148.57 (15)
Ru1—C2—C3—C4	-54.1 (3)	C34—S3—Ru1—C2	10.4 (2)
C1—C2—C3—Ru1	55.1 (3)	Ru2—S3—Ru1—C2	122.06 (17)
C2—C3—C4—C5	0.2 (5)	C34—S3—Ru1—C3	107.7 (6)
Ru1—C3—C4—C5	-53.6(3)	Ru2—S3—Ru1—C3	-140.7 (6)
C2—C3—C4—C10	179.2 (4)	C34—S3—Ru1—C4	125.0 (2)
Ru1—C3—C4—C10	125.4 (4)	Ru2—S3—Ru1—C4	-123.41 (17)
			(1/)

C2—C3—C4—Ru1	53.8 (3)	C34—S3—Ru1—C1	29.23 (19)
C3—C4—C5—C6	-0.5 (6)	Ru2—S3—Ru1—C1	140.85 (12)
C10—C4—C5—C6	-179.5 (4)	C34—S3—Ru1—S1	-149.03 (15)
Ru1—C4—C5—C6	-54.6 (3)	Ru2—S3—Ru1—S1	-37.41 (3)
C3—C4—C5—Ru1	54.1 (3)	C34—S3—Ru1—S2	-71.67 (15)
C10—C4—C5—Ru1	-124.9 (4)	Ru2—S3—Ru1—S2	39.95 (3)
C4—C5—C6—C1	-0.4 (6)	C21—S1—Ru1—C6	1.2 (3)
Ru1—C5—C6—C1	-55.9 (3)	Ru2—S1—Ru1—C6	115.0 (2)
C4—C5—C6—Ru1	55.5 (3)	C21—S1—Ru1—C5	22.52 (19)
C2-C1-C6-C5	1.6 (5)	Ru2—S1—Ru1—C5	136.35 (13)
C7—C1—C6—C5	-176.1 (4)	C21—S1—Ru1—C2	119.24 (18)
Ru1—C1—C6—C5	55.1 (3)	Ru2—S1—Ru1—C2	-126.92 (14)
C2-C1-C6-Ru1	-53.5 (3)	C21—S1—Ru1—C3	92.76 (17)
C7—C1—C6—Ru1	128.8 (4)	Ru2—S1—Ru1—C3	-153.41 (11)
C6—C1—C7—C8	-156.4 (4)	C21—S1—Ru1—C4	56.07 (17)
C2—C1—C7—C8	26.1 (6)	Ru2—S1—Ru1—C4	169.91 (11)
Ru1—C1—C7—C8	-67.8 (6)	C21—S1—Ru1—S3	-76.62 (13)
C6-C1-C7-C9	80.4 (6)	Ru2—S1—Ru1—S3	37.22 (3)
C2—C1—C7—C9	-97.1 (6)	C21—S1—Ru1—S2	-154.94 (13)
Ru1—C1—C7—C9	169.0 (4)	Ru2—S1—Ru1—S2	-41.11 (3)
C16—C11—C12—C13	-1.5 (5)	C27—S2—Ru1—C6	129.7 (2)
C17—C11—C12—C13	179.6 (3)	Ru2—S2—Ru1—C6	-120.97 (15)
Ru2—C11—C12—C13	-55.8 (3)	C27—S2—Ru1—C2	65.17 (18)
C16—C11—C12—Ru2	54.4 (3)	Ru2—S2—Ru1—C2	174.49 (11)
C17—C11—C12—Ru2	-124.6 (4)	C27—S2—Ru1—C3	31.07 (18)
C11—C12—C13—C14	1.0 (6)	Ru2—S2—Ru1—C3	140.39 (12)
Ru2—C12—C13—C14	-55.6 (3)	C27—S2—Ru1—C4	7.6 (3)
C11—C12—C13—Ru2	56.5 (3)	Ru2—S2—Ru1—C4	116.9 (2)
C12—C13—C14—C15	0.4 (5)	C27—S2—Ru1—C1	102.46 (17)
Ru2—C13—C14—C15	-53.7 (3)	Ru2—S2—Ru1—C1	-148.22 (11)
C12—C13—C14—C20	-178.8(4)	C27—S2—Ru1—S3	-149.06 (14)
Ru2—C13—C14—C20	127.1 (3)	Ru2—S2—Ru1—S3	-39.74(3)
C12—C13—C14—Ru2	54.1 (3)	C27—S2—Ru1—S1	-68.20 (14)
C13—C14—C15—C16	-1.1 (5)	Ru2—S2—Ru1—S1	41.11 (3)
C20-C14-C15-C16	178.0 (3)	C11—C12—Ru2—C13	-132.2 (4)
Ru2—C14—C15—C16	-54.5 (3)	C11—C12—Ru2—C16	-30.0(2)
C13—C14—C15—Ru2	53.3 (3)	C13—C12—Ru2—C16	102.2 (3)
C20—C14—C15—Ru2	-127.5(3)	C11—C12—Ru2—C15	-66.4(3)
C14—C15—C16—C11	0.6 (6)	C13—C12—Ru2—C15	65.8 (3)
Ru2—C15—C16—C11	-54.4 (3)	C13—C12—Ru2—C11	132.2 (4)
C14—C15—C16—Ru2	55.0 (3)	C11—C12—Ru2—C14	-103.1(3)
C12—C11—C16—C15	0.7 (5)	C13—C12—Ru2—C14	29.0 (3)
C17—C11—C16—C15	179.7 (3)	$C_{11} - C_{12} - R_{12} - S_{3}$	57.0 (3)
Ru2-C11-C16-C15	54.3 (3)	C13 - C12 - Ru2 - S3	-170.9(2)
C12—C11—C16—Ru2	-53.6 (3)	C11—C12—Ru2—S2	-159.6(3)
C17—C11—C16—Ru2	125.4 (3)	C13-C12-Ru2-S2	-27.4(5)
C12—C11—C17—C18	20.0 (6)	$C_{11} - C_{12} - R_{u2} - S_{1}$	136.5 (2)
C16-C11-C17-C18	-1590(4)	C13 - C12 - Ru2 - S1	-913(3)
			1.5 (5)

Ru2—C11—C17—C18	-71.1 (6)	C14—C13—Ru2—C12	131.8 (4)
C12—C11—C17—C19	-104.6(6)	C14—C13—Ru2—C16	66.1 (3)
C16—C11—C17—C19	76.4 (6)	C12—C13—Ru2—C16	-65.8(3)
Ru2-C11-C17-C19	1644(5)	C14-C13-Ru2-C15	29.7 (2)
C_{26} C_{21} C_{22} C_{23}	-0.4(6)	C_{12} C_{13} R_{12} C_{15}	-1021(3)
S1 C21 C22 C23	176 A (3)	$C_{12} = C_{13} = R_{12} = C_{13}$	102.1(3)
$C_{21} C_{22} C_{23} C_{24}$	-1.0(6)	$C_{14} = C_{13} = R_{u2} = C_{11}$	-28.8(3)
$C_{21} = C_{22} = C_{23} = C_{24} = C_{24}$	-176.2(4)	$C_{12} = C_{13} = R_{u2} = C_{14}$	-131.8(4)
$C_{22} = C_{23} = C_{24} = C_{25}$	-1/0.3(4)	C12 - C13 - Ru2 - C14	-131.0(4)
$C_{22} = C_{23} = C_{24} = C_{23}$	1.9(6)	C14 - C13 - Ru2 - S3	132.4(3)
$C_{23} - C_{24} - C_{25} - C_{26}$	-1.4(6)	C12—C13—Ru2—S3	20.6 (5)
01	176.8 (4)	C14—C13—Ru2—S2	-58.6 (3)
C22—C21—C26—C25	1.0 (5)	C12—C13—Ru2—S2	169.5 (2)
S1—C21—C26—C25	-175.6 (3)	C14—C13—Ru2—S1	-134.7 (2)
C24—C25—C26—C21	-0.1 (6)	C12—C13—Ru2—S1	93.5 (3)
S2—C27—C28—C29	115.2 (4)	C15—C16—Ru2—C12	-103.1 (3)
S2—C27—C28—C33	-62.6 (4)	C11—C16—Ru2—C12	30.0 (2)
C33—C28—C29—C30	1.6 (6)	C15—C16—Ru2—C13	-65.2 (3)
C27—C28—C29—C30	-176.2 (4)	C11—C16—Ru2—C13	67.9 (3)
C28—C29—C30—C31	-0.5 (7)	C11—C16—Ru2—C15	133.1 (4)
C29—C30—C31—C32	-1.1 (7)	C15—C16—Ru2—C11	-133.1 (4)
C30—C31—C32—C33	1.5 (7)	C15—C16—Ru2—C14	-28.3(3)
C31—C32—C33—C28	-0.3(7)	C11—C16—Ru2—C14	104.8 (3)
C_{29} C_{28} C_{33} C_{32}	-1.1(7)	C15-C16-Ru2-S3	138.0 (3)
C_{27} C_{28} C_{33} C_{32}	1767(4)	C11-C16-Ru2-S3	-88.8(2)
S_{3} C_{34} C_{35} C_{40}	59 4 (5)	C15-C16-Ru2-S2	591(3)
$S_{3} = C_{34} = C_{35} = C_{40}$	-1173(4)	C13 - C10 - Ru2 - S2	-167.78(19)
C_{40} C_{35} C_{36} C_{37}	-0.1(7)	$C_{11} = C_{10} = Ru_2 = S_2$	-143 1 (3)
$C_{40} = C_{35} = C_{30} = C_{37}$	0.1(7)	C_{13} $-C_{10}$ $-K_{02}$ $-S_{1}$	-10.0(5)
$C_{34} = C_{35} = C_{30} = C_{37}$	170.0(4)	C11 - C10 - Ru2 - S1	-10.0(3)
$C_{33} = C_{30} = C_{37} = C_{38}$	-0.9(8)	C16 - C15 - Ru2 - C12	(7.0(2))
$C_{36} - C_{37} - C_{38} - C_{39}$	1.7 (9)	C14— $C15$ — $Ru2$ — $C12$	-67.9(3)
C37—C38—C39—C40	-1.3 (9)	C16—C15—Ru2—C13	103.3 (3)
C38—C39—C40—C35	0.3 (9)	C14—C15—Ru2—C13	-30.0 (2)
C36—C35—C40—C39	0.4 (7)	C14—C15—Ru2—C16	-133.3 (4)
C34—C35—C40—C39	-176.4 (5)	C16—C15—Ru2—C11	28.5 (3)
C26—C21—S1—Ru1	17.9 (3)	C14—C15—Ru2—C11	-104.8 (3)
C22—C21—S1—Ru1	-158.7 (2)	C16—C15—Ru2—C14	133.3 (4)
C26—C21—S1—Ru2	-81.9 (3)	C16—C15—Ru2—S3	-53.2 (3)
C22—C21—S1—Ru2	101.5 (3)	C14—C15—Ru2—S3	173.49 (19)
C28—C27—S2—Ru2	-162.8 (3)	C16—C15—Ru2—S2	-134.0 (2)
C28—C27—S2—Ru1	-67.0 (3)	C14—C15—Ru2—S2	92.7 (2)
C35—C34—S3—Ru1	173.0 (3)	C16—C15—Ru2—S1	146.4 (2)
C35—C34—S3—Ru2	76.9 (3)	C14—C15—Ru2—S1	13.2 (4)
C1—C6—Ru1—C5	132.7 (4)	C16—C11—Ru2—C12	-130.4(4)
C5—C6—Ru1—C2	-102.6 (3)	C17—C11—Ru2—C12	118.4 (6)
C1—C6—Ru1—C2	30.1 (2)	C12—C11—Ru2—C13	29.6 (3)
C5-C6-Ru1-C3	-65.8(3)	C16-C11-Ru2-C13	-100.9(3)
C1 - C6 - Ru1 - C3	66 9 (3)	C17-C11-Ru2-C13	1480(5)
C_{5} C_{6} R_{u1} C_{4}	-287(2)	C_{12} C_{11} R_{12} C_{15}	1304(4)
00 IUI UT	20.1 (2)	-12 -11 -10	1,20,7 (7)

C1—C6—Ru1—C4	104.0 (3)	C17—C11—Ru2—C16	-111.2 (6)
C5—C6—Ru1—C1	-132.7 (4)	C12—C11—Ru2—C15	102.1 (3)
C5—C6—Ru1—S3	106.6 (2)	C16—C11—Ru2—C15	-28.3(3)
C1—C6—Ru1—S3	-120.7(3)	C17—C11—Ru2—C15	-139.5(5)
C5—C6—Ru1—S1	33.5 (4)	C12—C11—Ru2—C14	66.2 (3)
C1—C6—Ru1—S1	166.17 (19)	C16—C11—Ru2—C14	-64.2(3)
C5-C6-Ru1-S2	-179.61(19)	C17—C11—Ru2—C14	-175.4(5)
C1 - C6 - Ru1 - S2	-46.9(3)	C12—C11—Ru2—S3	-133.0(2)
C4-C5-Ru1-C6	-132.4(4)	C16-C11-Ru2-S3	96.5 (2)
C4-C5-Ru1-C2	-664(3)	C17 - C11 - Ru2 - S3	-147(5)
$C_{6} = C_{5} = R_{1} = C_{2}^{2}$	66.0.(2)	C_{12} C_{11} R_{12} S_{2}	160.8(3)
C4-C5-Ru1-C3	-29.8(3)	C16 - C11 - Ru2 - S2	303(4)
$C_{1} = C_{2}$ Rul C_{3}	102.7(3)	C17 - C11 - Ru2 - S2	-80.9(6)
C6 C5 Ru1 C4	102.7(5) 132 4 (4)	$C_{17} = C_{11} = R_{12} = S_2$	-53.8(3)
$C_0 = C_0 = R_{u1} = C_1$	-103.6(3)	$C_{12} = C_{11} = R_{u2} = S_1$	175.8(3)
C_{4} C_{5} C_{1} C_{1}	103.0(3)	$C_{10} = C_{11} = R_{u2} = S_{1}$	175.8(2)
C_{0} C_{0} C_{0} C_{0} C_{0} C_{1} C_{1} C_{1} C_{2} C_{1} C_{2} C_{1} C_{2} C_{1} C_{2} C_{2} C_{1} C_{2} C_{2} C_{2} C_{2} C_{1} C_{2} C_{2	20.0(2)	C1/-C11-Ru2-S1	1000(3)
C4 - C5 - Ru1 - S3	148.7(2)	C13 - C14 - Ru2 - C12	100.9(3)
C_{0} C_{0	-78.9(2)	C13 - C14 - Ru2 - C12	-29.8(3)
C4 - C5 - Rul - Sl	66.6 (3)	C_{20} $-C_{14}$ $-R_{u2}$ $-C_{12}$	-144.9 (7)
C6—C5—Rul—SI	-161.0(2)	C15—C14—Ru2—C13	130.6 (3)
C3—C2—Ru1—C6	102.6 (3)	C20—C14—Ru2—C13	-115.1 (7)
C1—C2—Ru1—C6	-30.1 (3)	C15—C14—Ru2—C16	28.3 (2)
C3—C2—Ru1—C5	65.4 (3)	C13—C14—Ru2—C16	-102.4 (3)
C1—C2—Ru1—C5	-67.2 (3)	C20—C14—Ru2—C16	142.5 (7)
C1—C2—Ru1—C3	-132.7 (3)	C13—C14—Ru2—C15	-130.6 (3)
C3—C2—Ru1—C4	28.8 (2)	C20—C14—Ru2—C15	114.3 (7)
C1—C2—Ru1—C4	-103.8 (3)	C15—C14—Ru2—C11	64.4 (3)
C3—C2—Ru1—C1	132.7 (3)	C13—C14—Ru2—C11	-66.2 (3)
C3—C2—Ru1—S3	162.38 (19)	C20—C14—Ru2—C11	178.7 (7)
C1—C2—Ru1—S3	29.7 (3)	C15—C14—Ru2—S3	-16.3 (5)
C3—C2—Ru1—S1	-45.9 (3)	C13—C14—Ru2—S3	-147.0 (3)
C1—C2—Ru1—S1	-178.6(2)	C20—C14—Ru2—S3	97.9 (7)
C3—C2—Ru1—S2	-122.1 (2)	C15—C14—Ru2—S2	-95.1 (2)
C1—C2—Ru1—S2	105.2 (2)	C13—C14—Ru2—S2	134.2 (2)
C2—C3—Ru1—C6	-66.1 (3)	C20—C14—Ru2—S2	19.1 (6)
C4—C3—Ru1—C6	66.6 (3)	C15—C14—Ru2—S1	-174.05 (19)
C2—C3—Ru1—C5	-103.2(3)	C13—C14—Ru2—S1	55.3 (3)
C4-C3-Ru1-C5	29 5 (3)	C_{20} C_{14} R_{12} S_{1}	-59.8(7)
C4-C3-Ru1-C2	132.7(4)	C_{34} S3 Ru2 C12	-124.07(19)
$C^2 - C^3 - Ru1 - C^4$	-132.7(4)	Ru1 = S3 = Ru2 = C12	12845(14)
$C_2 = C_3 = Ru_1 = C_1$	-28.9(2)	C_{34} S_{3} $R_{11}2$ C_{12}	-1386(3)
C4-C3-Ru1-C1	$103 \ 8 \ (3)$	R_{11} = S_{12} = R_{12} = C_{13}	1140(3)
C^{2} C^{3} Ru^{1} S^{3}	-111 6 (6)	C_{34} S_{3} R_{11}^{2} C_{15}^{10}	-56.46(17)
$C_2 = C_3 = R_{11} = S_3$	21.1.(8)	R_{11} = S_{12} = R_{12} = C_{16}	-163.04(17)
$C_{1} = C_{2} = R_{11} = S_{2}$	$\frac{21.1}{1476(2)}$	C_{34} S_{3} R_{12} C_{15}	-27 50 (12)
$C_2 = C_3 = Ku_1 = S_1$	-707(2)	C_{3} $- C_{13}$ $-$	-134.09(10)
$C_{\tau} = C_{\sigma} = Ku_1 = \sigma_1$	(3)	$C_{24} = S_{2} = R_{12} = C_{13}$	-03 62 (10)
$C_2 = C_3 = Ku_1 = S_2$	0/.7(2)	C_{34} C_{33} Ku_{2} C_{11}	-93.02(18)
U 1 −U3−KU1−82	-139.0(2)	ли1—33—Ku2—U11	130.90(13)

	20.1(2)	G24 G2 D 2 G14	15.7(2)
C5—C4—Ru1—C6	29.1 (3)	C34—S3—Ru2—C14	-15.7 (3)
C3—C4—Ru1—C6	-102.0 (3)	Ru1—S3—Ru2—C14	-123.2 (3)
C10—C4—Ru1—C6	144.1 (5)	C34—S3—Ru2—S2	67.45 (13)
C3—C4—Ru1—C5	-131.1 (4)	Ru1—S3—Ru2—S2	-40.03 (3)
C10—C4—Ru1—C5	115.0 (5)	C34—S3—Ru2—S1	144.75 (13)
C5—C4—Ru1—C2	102.5 (3)	Ru1—S3—Ru2—S1	37.27 (3)
C3—C4—Ru1—C2	-28.6 (2)	C27—S2—Ru2—C12	2.7 (4)
C10—C4—Ru1—C2	-142.5 (5)	Ru1—S2—Ru2—C12	-108.2 (4)
C5—C4—Ru1—C3	131.1 (4)	C27—S2—Ru2—C13	-17.4 (2)
C10—C4—Ru1—C3	-113.8 (5)	Ru1—S2—Ru2—C13	-128.38 (16)
C5—C4—Ru1—C1	65.8 (3)	C27—S2—Ru2—C16	-118.1 (2)
C3—C4—Ru1—C1	-65.4 (3)	Ru1—S2—Ru2—C16	130.99 (14)
C10—C4—Ru1—C1	-179.2 (5)	C27—S2—Ru2—C15	-86.5 (2)
C5—C4—Ru1—S3	-43.7 (3)	Ru1—S2—Ru2—C15	162.55 (14)
C3—C4—Ru1—S3	-174.84 (19)	C27—S2—Ru2—C11	-139.8 (3)
C10—C4—Ru1—S3	71.3 (5)	Ru1—S2—Ru2—C11	109.3 (3)
C5—C4—Ru1—S1	-122.0 (3)	C27—S2—Ru2—C14	-49.1 (2)
C3—C4—Ru1—S1	106.9 (2)	Ru1—S2—Ru2—C14	-160.00 (15)
C10—C4—Ru1—S1	-6.9 (4)	C27—S2—Ru2—S3	150.56 (16)
C5—C4—Ru1—S2	167.9 (2)	Ru1—S2—Ru2—S3	39.61 (3)
C3—C4—Ru1—S2	36.8 (4)	C27—S2—Ru2—S1	70.03 (15)
C10—C4—Ru1—S2	-77.0 (5)	Ru1—S2—Ru2—S1	-40.91 (3)
C2—C1—Ru1—C6	130.4 (4)	C21—S1—Ru2—C12	-39.83 (18)
C7—C1—Ru1—C6	-111.6 (6)	Ru1—S1—Ru2—C12	-156.38 (13)
C6—C1—Ru1—C5	-28.9(3)	C21—S1—Ru2—C13	-78.12 (18)
C2—C1—Ru1—C5	101.6 (3)	Ru1—S1—Ru2—C13	165.33 (12)
C7—C1—Ru1—C5	-140.4 (5)	C21—S1—Ru2—C16	-3.5 (3)
C6—C1—Ru1—C2	-130.4 (4)	Ru1—S1—Ru2—C16	-120.1 (3)
C7—C1—Ru1—C2	118.0 (6)	C21—S1—Ru2—C15	-117.1 (3)
C6—C1—Ru1—C3	-101.8 (3)	Ru1—S1—Ru2—C15	126.3 (3)
C2—C1—Ru1—C3	28.7 (2)	C21—S1—Ru2—C11	-10.60 (19)
C7—C1—Ru1—C3	146.7 (5)	Ru1—S1—Ru2—C11	-127.14 (13)
C6—C1—Ru1—C4	-65.2 (3)	C21—S1—Ru2—C14	-108.01 (18)
C2—C1—Ru1—C4	65.3 (2)	Ru1—S1—Ru2—C14	135.44 (13)
C7—C1—Ru1—C4	-176.7 (5)	C21—S1—Ru2—S3	79.40 (13)
C6—C1—Ru1—S3	67.0 (3)	Ru1—S1—Ru2—S3	-37.15 (3)
C2—C1—Ru1—S3	-162.58 (19)	C21—S1—Ru2—S2	157.76 (13)
C7—C1—Ru1—S3	-44.6 (5)	Ru1—S1—Ru2—S2	41.21 (3)
C6—C1—Ru1—S2	147.2 (3)		X- /
	× /		

Hydrogen-bond geometry (Å, °)

D—H···A	D—H	H···A	D····A	<i>D</i> —H··· <i>A</i>
01—H1…F1	0.82	1.99	2.773 (9)	161
C3—H3···F3 ⁱ	0.93	2.52	3.340 (11)	148

supporting information		
156		

Symmetry codes: (i) *x*+1/2, *y*-1/2, *z*; (ii) *x*, -*y*+1, *z*-1/2.