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# **OPEN** ITO film stack engineering for low-loss silicon optical modulators

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The Indium Tin Oxide (ITO) platform is one of the promising solutions for state-of-the-art integrated optical modulators towards low-loss silicon photonics applications. One of the key challenges on this way is to optimize ITO-based thin films stacks for electro-optic modulators with both high extinction ratio and low insertion loss. In this paper we demonstrate the e-beam evaporation technology of 20 nm-thick ITO films with low extinction coefficient of 0.14 (N<sub>c</sub> = 3.7·10<sup>20</sup> cm<sup>-3</sup>) at 1550 nm wavelength and wide range of carrier concentrations (from 1 to 10×10<sup>20</sup> cm<sup>-3</sup>). We investigate ITO films with amorphous, heterogeneously crystalline, homogeneously crystalline with hidden coarse grains and pronounced coarsely crystalline structure to achieve the desired optical and electrical parameters. Here we report the mechanism of oxygen migration in ITO film crystallization based on observed morphological features under low-energy growth conditions. Finally, we experimentally compare the current-voltage and optical characteristics of three electro-optic active elements based on ITO film stacks and reach strong ITO dielectric permittivity variation induced by charge accumulation/depletion ( $\Delta n = 0.199$ ,  $\Delta k = 0.240$  at  $\lambda = 1550$  nm under  $\pm 16$  V). Our simulations and experimental results demonstrate the unique potential to create integrated GHz-range electro-optical modulators with sub-dB losses.

There are several promising fields of silicon photonics like quantum computing, LIDARs, high-performance datacenters, neuromorphic computing and precision optical spectroscopy<sup>1-5</sup>, which can extremely benefit from low loss integrated optical modulators. A number of optical modulator implementations based on various physical effects have been already demonstrated (Table 1). The devices performance is typically defined by high speed, low loss, small footprint, fabrication flexibility and integration capabilities. One of the most commonly used modulator types is a lithium niobate modulator (Table 1A) based on the Pockels effect<sup>6,7</sup>. It exhibits low propagation loss (less than 0.1 dB) and a high modulation rate (over 40 GHz). The key remaining issue of lithium niobate modulators is the excessive active element length, which can exceed 2 mm. The next optical modulators type (Table 1B) is based on the free-carrier plasma dispersion effect (FCPD), where the active element is a p-n or p-i-n junction. Such modulators are based on charge carrier concentrations change<sup>8,9</sup>, they demonstrate high speed (over 30 GHz) and medium footprint area (active element length is 100–2000 μm). However, their insertion loss is significantly higher than that of lithium niobate modulators. Organic electro-optical materials (Table 1C) are also used to create high-performance devices based on the Pockels effect<sup>10,11</sup>. They provide both high speed (over 40 GHz) and small footprint (active element length down to 5 µm), but suffer from high propagation loss (about 2.5 dB in the active part). Another type of optical modulators, based on the Franz-Keldysh effect and the quantum-confined Stark effect (Table 1D), is implemented mainly in InGaAsP/InP or GeSi structures<sup>12</sup>. These modulators exhibit high speed (over 40 GHz), low loss (about 1 dB in the active part) and medium footprint. However, they require high fabrication and integration complexity. In the last 10 years, optical modulators based on a change in the dielectric constant of transparent conducting oxides (TCO), such as indium tin oxide (ITO)<sup>13-16</sup>, have attracted great interest (Table 1E). The accumulation (depletion) of free carriers in ITO provides a small footprint (active element length of about 5  $\mu$ m) and low propagation loss (up to 0.5 dB). Their modulation frequency has been experimentally confirmed up to 1 GHz<sup>16</sup>, but higher rates can be achieved<sup>17</sup>. TCO-based devices demonstrate the trade-off between low propagation loss, small footprint and high modulation frequency,

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| Modulator type |  | Device active area length, um | Switch voltage, V | Extinction ratio, dB | 3 dB bandwidth, GHz | Insertion loss (in the active area of a modulation), dB | References |
|----------------|--|-------------------------------|-------------------|----------------------|---------------------|---|------------|
| A              | Lithium niobate based (MZM or MRR)           | 150-5000                      | 2.3-9             | < 20                 | >40                 | 0.1-4   | 6,7        |
| В              | p-i-n and p-n junction<br>based (MZM or MRR) | 100-2000                      | 1.8-6.5           | 3.1-7.5              | >30                 | 1.5-6   | 8,9        |
| С              | NLM based (MZM or MRR)                       | 4-1500                        | 3.3-4             | 4-5                  | >40                 | 2.5-8   | 10,11      |
| D              | InGaAsP/InP based (MZM,<br>EAM)              | 300-500                       | 1.5-3             | < 25                 | >40                 | <1  | 12         |
| Е              | TCO based (MZM or MRR, EAM)                  | 1.4-32                        | 4–16              | 2.1-5                | >1                  | 1–6   | 13,15–17   |

**Table 1.** Comparison of electro-optical modulators implementations.

making them one of the most promising solutions. Moreover, all materials used in these devices are well compatible with planar silicon technology, making the full power of mature CMOS technology applicable to large-scale production of TCO optical modulators.

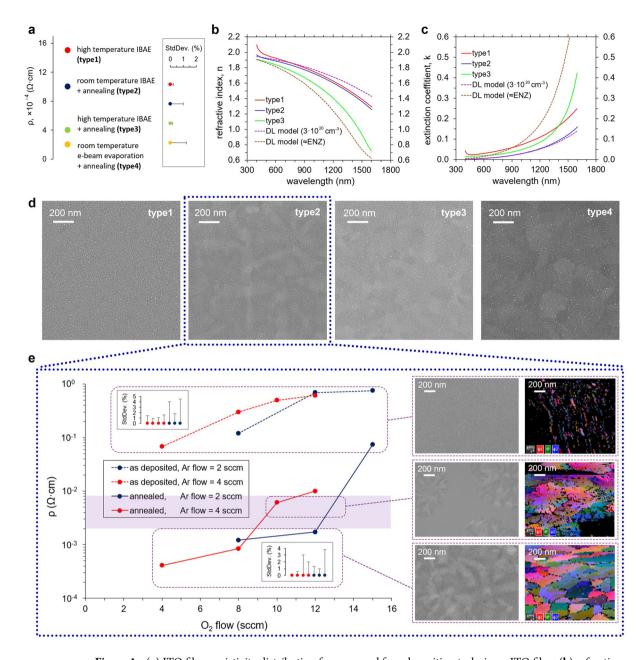
One of the most widely used TCO materials is indium tin oxide. Its dielectric constant depends on the carrier concentration and is described by the Drude-Lorentz model<sup>18</sup>, thus, it is possible to adjust both the real and the imaginary parts of the thin film refractive index<sup>19</sup>. This makes ITO a reasonable choice for the implementation of the modulator active element. Optical modulators based on thin film optical properties change effect could be realized as a hybrid waveguide, which represents a metal-oxide-semiconductor (MOS) capacitor with a built-in thin ITO layer. When an electrical potential is applied to active element, the charge accumulation layer is formed on the oxide/ITO interface where carrier concentration is significantly higher. The light mode localized in this sub-um volume is absorbed 13,14 or changes the phase <sup>15,16</sup>. One of the key challenges for high-performance optical modulators is to achieve the required ITO thin film carrier concentration, which strongly affects the propagation loss and modulation depth of the thin film. ITO thin films with controllable carrier concentration are usually deposited with high-energy PVD methods such as ion beam deposition 15,16, magnetron sputtering 20,21 and pulsed laser deposition 22 to avoid the following film annealing, which leads to strong carrier concentration increase. Ion-beam assisted deposition without subsequent annealing<sup>23,24</sup> can also be a good choice for this purpose as it provides very good process control, but morphology and extinction coefficient of such thin films have not been investigated for ultrathin layers.

In this paper, we propose ITO thin films ion-beam assisted e-beam evaporation (IBAE) technology with subsequent annealing which provides versatile and accurate control of carrier concentration. Opposed to sputtering and ion-beam deposition the proposed IBAE process is characterized by lower energies avoiding intensive crystallization and formation of transition layer<sup>25</sup>. Electron beam evaporation is a very flexible technique; it allows deposition in ultra-high vacuum conditions with quite a small amount of extremely pure materials allowing ion assistance during process. Subsequent annealing in an inert atmosphere<sup>26</sup> makes it possible to further improve the polycrystalline structure and properties of the film without a significant increase in the carrier concentration. In order to experimentally quantify the electro-optical effect, we fabricated and compared MOS capacitors based on the evaporated ITO films, which are similar to active elements of electro-optical modulators. The current-voltage characteristics of the capacitors and electro-optical effect in the accumulation/depletion layers were carefully measured and analyzed using spectroscopic ellipsometry<sup>22,27,28</sup> under electrical biasing. More than 80 samples were experimentally measured to determine the materials properties and films stack optimization.

#### Results and discussion

**ITO thin films investigation.** The key technology for modern ITO-based optical modulators is thin ITO films with a strong compromise between carrier concentration and optical properties. Using our optical modulator simulations (see Supplementary) we found that both minimal device length and propagation loss can be achieved with the ITO films carrier concentrations in the range of 0.5 to  $2\times10^{20}$  cm<sup>-3</sup>. With the typical value of the carrier mobility in ITO films equals to 15 cm<sup>2</sup>/(V s)<sup>18,29</sup> we calculated the resistivity ( $\rho = 1/\mu_c N_c e$ ), which should be in the range from 2 to  $8\times10^{-3}~\Omega$  cm. This range will be used to estimate resistivity values throughout the work.

We first compared the resistivity, optical properties, and surface morphology (Fig. 1) of the 20 nm-thick ITO films evaporated with four different techniques: (1) high temperature IBAE (type1); (2) room temperature IBAE with the subsequent 300 °C annealing (type2); (3) high temperature IBAE with the subsequent 300 °C annealing (type3); (4) room temperature e-beam evaporation with the subsequent 300 °C annealing (type4). We observe strong variation in films resistivity measured by the four-probe method with respect to evaporation technology and annealing parameters (Fig. 1a, for a detailed description see the Supplementary). The resistivity of the ITO film deposited at room temperature without annealing (not shown) is more than  $10^{-1} \Omega$  cm, which indicates insufficient crystallization of the film and a large amount of nonactivated interstitial oxygen<sup>30-32</sup>. All the evaporated ITO films are ultra-flat with the film surface RMS roughness of  $0.7 \pm 0.2$  nm. By analyzing high quality SEM images of films one can observe a strong



**Figure 1.** (a) ITO films resistivity distribution for proposed four deposition technique; ITO films (b) refractive index and (c) extinction coefficient dependences on wavelength; (d) High-resolution SEM images of the ITO films surface; (e) Room temperature IBAE + annealing ITO films resistivity dependence on  $Ar/O_2$  mixture composition during evaporation. Resistivity standard deviation error bars are shown for each point of the graphs from left to right correspondingly. Selected areas show the surface (SEM images) and crystallography (SEM EBSD maps) of films with different resistivity values.

texture growth for the annealed films (Fig. 1d, type 2-4) and homogeneous microstructure for the film evaporated under elevated temperature without subsequent annealing.

The optical constants of films (type 1–3) were measured in the wavelength range from 400 to 1600 nm (Fig. 1b,c). Film type4 was not investigated, because its carrier concentration was too high (estimated carrier concentration from the resistivity measurement was about  $8.3 \times 10^{20}$  cm<sup>-3</sup>, which is above the epsilon-near-zero point (ENZ)—about  $6.5 \times 10^{20}$  cm<sup>-3</sup> for  $\lambda = 1550$  nm, this value will lead to extremely high losses in device). Obviously, film type1 has a much higher extinction coefficient in the entire visible range (Fig. 1c), which can be explained by low crystallization of the film during evaporation. The strong texture of the film type2 indicates an intense crystallization process that results in the lowest absorption over the entire wavelength range. ITO film type3 also has a strong crystalline structure (Fig. 1d) and a relatively low extinction coefficient in the visible region. Carrier concentrations for ITO films (type 1–3) are calculated based on the measured plasma frequency  $\omega_p$  from ellipsometry data (see Supplementary) to

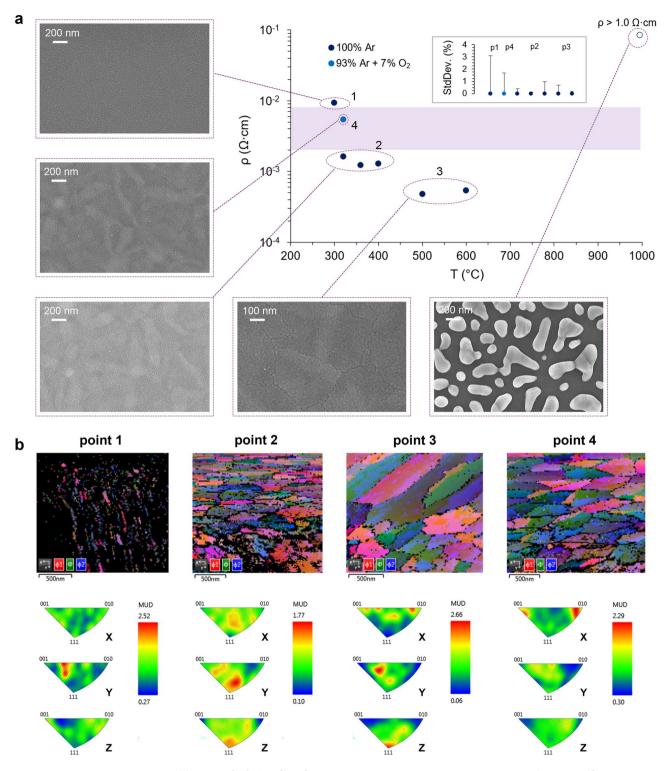
be  $4.2 \times 10^{20}$  cm<sup>-3</sup> (type1),  $3.7 \times 10^{20}$  cm<sup>-3</sup> (type2),  $5.7 \times 10^{20}$  cm<sup>-3</sup> (type3). The carrier mobilities for films (type 1–3) are calculated as  $\mu = 1/\rho e N_c$  and equal 9.4 cm<sup>2</sup>/V s (type1), 15.5 cm<sup>2</sup>/V s (type2), 27.0 cm<sup>2</sup>/V s (type3). According to previously published data<sup>18</sup>, ITO films (type1 and 2) are promising candidates to be successfully used in electro-optical modulators in both n-dominant (Mach–Zehnder) and k-dominant (electro-absorption) regions. The value for film type3 is closest to the ENZ point at  $\lambda = 1550$  nm (Fig. 1b,c, Drude–Lorenz model for ENZ), therefore, it can be used for electro-optical elements that require switching the dielectric constant through the ENZ point<sup>33,34</sup>.

However, low-loss n-dominant electro-optic modulator requires ITO films with higher resistance values (from  $2 \times 10^{-3}$  to  $8 \times 10^{-3}$   $\Omega$  cm). One can clearly see that the resistance of ITO films is directly related to their crystalline structure and morphology. Two methods of controlling the resistance of ITO films have been studied: (1) annealing at different temperatures; (2) Ar/O<sub>2</sub> gas mixture variation during IBAE with subsequent annealing. Due to the minimal extinction coefficient and close to the desired resistivity, we chose the film type2 deposition recipe for further investigation. We studied ion-beam assisted e-beam evaporation of 20 nm-thick ITO films at room temperature with the various Ar/O<sub>2</sub> mixture ratio (Ar flow of 2 and 4 sccm, O<sub>2</sub> flow of 4, 8, 10, 12, 15 sccm) without and with subsequent 20-min annealing in argon atmosphere at 300 °C (Fig. 1e). One can see that annealing of the films makes it possible to reduce their resistance close to the desired region in a controlled manner. ITO films with a relatively high resistance (more than  $10^{-2} \Omega$  cm) have amorphous or nanocrystalline structure (Fig. 1e, no crystalline phases were found in the SEM EBSD analysis). Films with relatively low resistivity (less than  $10^{-3} \Omega$  cm) have direct evidence of forming crystalline structure (grains with hidden boundaries were detected by SEM EBSD analysis). Unfortunately, the film (Fig. 1e, Ar flow of 4 sccm, O<sub>2</sub> flow of 10 sccm) with the resistance from the desired region from 2 to  $8 \times 10^{-3} \,\Omega$  cm (corresponds to the required range of charge carrier concentrations) have a crystalline structure with inclusions amorphous phase. This is a stoichiometrically heterogeneous structure that can lead to an uneven carrier distribution in optical modulator devices.

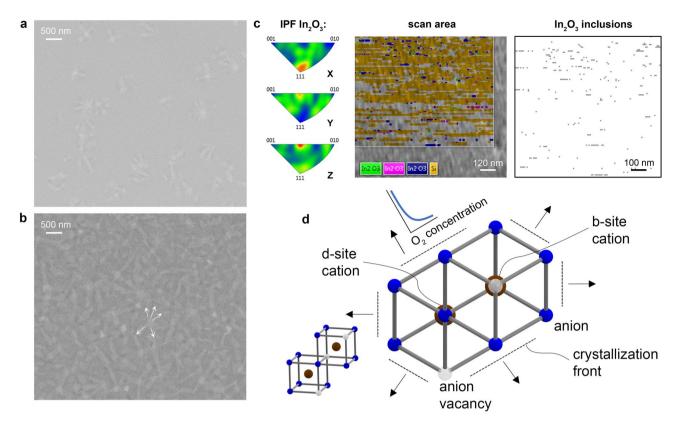
In order to achieve much wider process window and get electrical, optical, and morphological properties of ITO films simultaneously, we investigated the dependence of the resistance and the crystalline structure on annealing parameters (Fig. 2a). We chose the closest resistivity value to the desired range which corresponds to IBAE at room temperature in an Ar/O<sub>2</sub> mixture (Ar flow = 4 sccm and O<sub>2</sub> flow = 12 sccm) and varied annealing temperature and atmosphere. One can notice that the ITO film annealed at 300 °C remains amorphous (Fig. 2a, point 1), while increasing the temperature by only 20 °C immediately initiates crystallization (Fig. 2a, point 2). We marked stepwise crystallization behavior, which results in a well-defined ITO crystalline structure when the annealing temperature rises above 500 °C (Fig. 2a, point 3). Under higher temperatures (in the range from 600 to 1000 °C) films damage, melt and break into islands by surface tension forces. It should be noted that annealing in the atmosphere with a small fraction of oxygen increases resistance significantly (Fig. 2a, point 4). In this case, films have a crystalline structure, in contrast to partial crystallization (Fig. 1e), which is observed for the films with a resistivity in the range from 2 to  $8 \times 10^{-3} \Omega$  cm, which were annealed in an atmosphere of pure argon. All resistivity values correlate with carrier concentration values obtained from the ellipsometry data with Tauc-Lorenz model for each ITO film in the UV range (see Supplementary). SEM EBSD analysis (Fig. 2b) demonstrates that raising the annealing temperature in an argon atmosphere (Fig. 2b, points 1-3) leads to increasing the pole density of reflecting planes orientations of ITO films (see inverse pole figures—IPF). This indicates the appearance of preferred grains orientations in ITO films. It should be noticed, that the film annealed in the oxygen-diluted atmosphere (point 4) had another grains orientation.

One can notice that IBAE films have structural crystalline features and represent chemically heterogeneous systems prior to annealing. Since the energy in the IBAE processes is higher, the formation of crystal nuclei occurs during the evaporation process (which is confirmed by the EBSD analysis for the non-annealed thin film—Fig. 3c). Based on the SEM image analysis (Fig. 3a,b), we assume that during annealing the propagation of the crystallization front from the nucleus along the growth channels occurs in preferred orientations similar to processes in liquid-phase epitaxy<sup>35</sup>. In this case, the movement of the crystallization front can form the opposite diffusion flow which is perpendicular to the growing surface (Fig. 3d). We suggest that during ITO crystallization a depletion zone appears where oxygen diffuses to form a crystal lattice. SEM images (Fig. 3a,b) demonstrate from 2 to 6 channels extending radially from each central point, which may be oxygen diffusion channels.

We observed that annealing of ITO films deposited without ion assistance causes a greater drop in resistance (Fig. 1a). Upon an e-beam evaporation process some part of ITO thin film can crystallize (Fig. 3c). For ion-assisted processes, oxygen atoms and ions outside the crystal lattice are embedded into the volume of the film<sup>30–32</sup>. This affects further crystallization during annealing when oxygen is annihilated with vacancies<sup>36</sup>. Wherein the crystalline phase is more localized in films e-beam evaporated with ion assistance. Thus, the proposed deposition technique utilizes lower energies and higher oxygen concentrations, which distinguishes it from methods described in recent papers<sup>23,24</sup>. These deposition conditions favor the formation of noncrystalline films, as evidenced by their low carrier concentration (all non-annealed ITO films in this work have  $N_c < 4 \times 10^{18}$  cm<sup>-3</sup> when deposited at a room temperature). The films deposited at a higher energy and lower oxygen concentration without further annealing show higher carrier concentrations ( $N_c > 1 \times 10^{19}$  cm<sup>-3</sup>) and higher degree of crystallization. In this case oxygen has enough time and energy to integrate into the crystal lattice vacancies and initiate crystal lattice. The annealing process under controlled temperature and ambient provides the certain amount of energy to activate oxygen, which guarantee precise regulation of the carrier concentration:  $N_c$  in the range from 1 to  $10 \times 10^{20}$  cm<sup>-3</sup>.



**Figure 2.** (a) 20 nm-thick ITO films [IBAE at room temperature in an  $Ar/O_2$  mixture (4/12 sccm)] resistivity dependency on annealing temperature and atmosphere; high-resolution SEM images of the ITO films surface for each annealing parameters region; resistivity standard deviation error bars are shown for each point of the graphs from left to right correspondingly. (b) SEM EBSD analysis for the typical ITO films corresponding to each annealing parameters region.



**Figure 3.** 20 nm-thick ITO films (room temperature IBAE in an  $Ar/O_2$  mixture 2/10 sccm) with different annealing temperatures: (a) 300 °C—crystalline structure with inclusions of amorphous phases; (b) 320 °C—crystalline structure; (c) SEM EBSD analysis of an non-annealed ITO film (room temperature IBAE in an  $Ar/O_2$  mixture 2/10 sccm), one can see nucleus of crystalline  $In_2O_3$  phase; (d) Projection of the ITO lattice on < 222 > plane and the crystallization process (oxygen diffusion along the direction of the crystallization front).

**Electro-optical modulation.** We fabricated MOS capacitors (Si/SiO<sub>2</sub>/ITO/Me, Fig. 4a) based on ITO films (type 1–3) using aluminum (Al, work function 4.2 eV) and silver (Ag, 4.8 eV) electrodes (see "Methods"). MOS capacitors with the aluminum electrodes exhibit breakdown voltages of less than 20 mV (Fig. 4b, red vertical curve). When replacing aluminum electrode with the silver one, a significantly higher breakdown voltage of 17 V was observed at the leakage current of less than 4 nA (Fig. 4b, blue curve). Additionally, we tested the structure (Si/SiO<sub>2</sub>/ITO) without metal electrode (the probes were placed in direct contact with ITO film) that showed biggest breakdown voltage of 29 V (Fig. 4b, yellow curve). High noise level in this case can be explained by poor contact between the probe and ITO film surface. Based on these measurements we assumed that Al/ITO pair forms an energy barrier at their interface. When an electric potential is applied, electrons are emitted due to the lower Al work function compared to ITO (4.2 eV versus 4.7 eV, respectively, Fig. 4a—dotted area). This means that an energy barrier of 0.5 eV appears at the Al/ITO interface ( $\Delta \varphi_{ms} = \Phi_{ITO} - \Phi_{Al}$ ). The emission current density in this case is defined as:

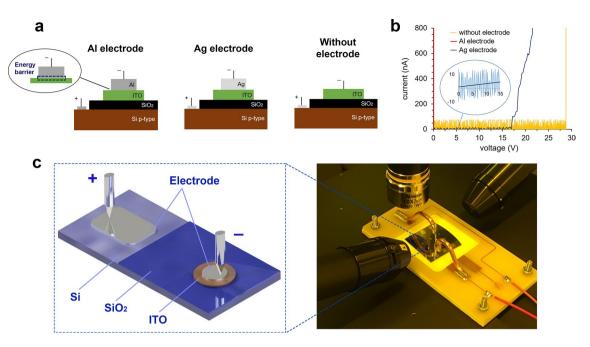
$$j = j_{ITO \to Al} - j_{Al \to ITO} = \frac{1}{4} q n_S v_0 \left( e^{\beta Vg} - 1 \right), \tag{1}$$

where q is an electron charge,  $n_s = n_0 e^{-\beta \Delta \phi}$ —surface concentration in a semiconductor/metal interface,  $\beta = q/kT$ ,  $\upsilon_0$ —thermal velocity of electrons. In this case the free path of electrons in ITO equals to 17.8 nm:

$$l_e = \frac{h}{\rho q^2 N \lambda_e},\tag{2}$$

where h is the Plank's constant,  $1/\lambda_e = (3\pi^2 N)^{1/3}$ .

The calculated electric current in this barrier for the chosen electrode area (about 2 mm²) is about 0.19 A (at applied voltage of 20 mV—Eq. 1). Additionally, free electrons can be accelerated by external electric field and pass through ITO layer (electron mean free path is comparable to the film thickness), which can lead to oxide destruction and breakdown. Next, we investigated ITO films optical characteristics switching under applied voltage (for detailed information see Supplementary). First, the structure (Si/SiO<sub>2</sub>/ITO) without electrode was used in order to achieve better ellipsometry sensitivity (due to the lack of a semitransparent layer) and a higher breakdown voltage (Fig. 5a). Then, ellipsometry parameters psi and delta ( $\psi$ ,  $\Delta$ ) were carefully measured in the wavelength range from 400 to 1600 nm for multilayer stacks with ITO films (type 1–3). We observed stronger effect of the applied voltage on Psi and delta at longer wavelengths in the range from 1400 to 1600 nm (Fig. 5c,d).



**Figure 4.** (a) Three ITO-based films stacks (MOS capacitors) for electrical characterization (the breakdown zone is shown with dotted area); (b) current–voltage characteristics of the fabricated MOS capacitors; (c) 3D-model and photograph of the experimental setup.

The dependences of the applied voltage (the data was validated only from 0 to +3 V for the ITO film type3) on the ellipsometry parameters  $\psi$  and  $\Delta$  were measured at a standard telecommunication wavelength of 1550 nm (Fig. 5b).

The optical parameters of the ITO thin films were carefully investigated based on ellipsometry measurements (see Supplementary). The complex refractive index of the accumulation layer was calculated using the Drude–Lorentz model in the wavelength range from 550 to 1600 nm (Fig. 5e). Note, that we adopted a homogeneous uniform accumulation layer approximation in the ellipsometry model (Fig. 5a) that satisfied the required level of detail. One can see, that the effect on the ellipsometry parameters of the film type1 turns out to be lower than that of the film type2, despite higher carrier concentration. Presumably, this can be explained by the presence of electron traps arises from the less crystallized structure of the film type1, which prevents the accumulation of charge. The film type3 has the strongest electro-optical effect due to the highest carrier concentration. We compared  $\Delta n$  and  $\Delta k$  for the ITO films (type 1–3) at 1550 nm (Table 2), the refractive index change under applied voltage for them is lower than indicated in recent works (Table 3). We assume that this associated with the large area of the millimeter-size electrode we used, which results in weaker accumulation (depletion) in the ellipsometer spot region due to unevenly distributed probe charge.

Finally, we calculated (see Supplementary), that such device implementation can potentially provide an electro-optical modulation frequency of approximately 3.4 GHz (with silver electrodes placed on top of the ITO layer). In further work, we suppose device implementation with single-crystalline Ag electrode  $^{38,39}$ , which could abate losses induced by SPP propagation at electrode interfaces. Moreover, there are ITO MOS capacitor designs based on the tunable guided-mode resonance effect, which can greatly increase the  $\Delta n$  value $^{40}$ .

#### Summary and conclusions

In conclusion, we developed ITO thin films and MOS capacitors deposition technique using ion-beam assisted e-beam evaporation with subsequent annealing for low-loss electro-optical modulation devices. With the proposed technique we deposited ultra-flat (RMS surface roughness from 0.6 to 0.8 nm) 20 nm-thick ITO films with the low carrier concentration up to  $1\times10^{20}$  cm $^{-3}$ . A direct dependence of ITO thin films resistivity on their crystal structure has been demonstrated. SEM film surface and SEM EBSD analysis allowed us to propose a mechanism of putative oxygen diffusion channels arising during films crystallization deposited using ion-beam assisted e-beam evaporation, which is the result of growing  $\rm In_2O_3$  nucleus crystalline phase during deposition. To experimentally quantify an electro-optical modulation effect we designed, fabricated and tested MOS structures based on ITO thin films stacks (with Al, Ag and without electrode) with high breakdown voltages of 17 to 29 V. A model that explains the experimental breakdown voltages for the different types of electrodes of the MOS capacitors is proposed and experimentally evaluated. The MOS structure with the silver electrode demonstrated significantly higher breakdown voltage compared to the aluminum one. Finally, we observed a strong electro-optical modulation of the complex refractive index  $(\Delta n = 0.199, \, \Delta k = 0.240)$  at a wavelength of 1550 nm in a voltage range from + 16 to - 16 V. It is worth noticing, that ITO films deposited at a higher temperature without subsequent annealing had the worst electro-optical the effect. These results demonstrate the possibility to create

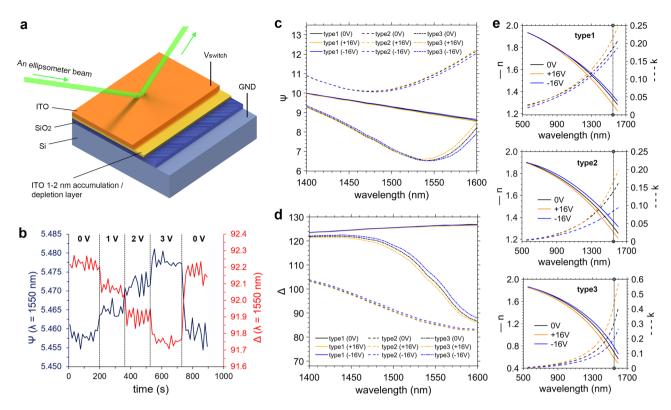


Figure 5. (a) Ellipsometry model measurement scheme; (b) ITO (type3)  $\psi$  and  $\Delta$  at wavelength of 1550 nm; (c)  $\psi$ ; (d)  $\Delta$  of the multilayer stack in the wavelength range from 1400 to 1600 nm at voltages of – 16 V and + 16 V; (e) film types 1–3 accumulation layer n and k in the wavelength range from 550 to 1600 nm at voltages of 0, + 16 and – 16 V.

integrated electro-optical modulators in the GHz range with low propagation losses (theoretically estimated losses are less than 4 dB without device design optimization).

### Methods

**ITO deposition.** ITO thin films were deposited on prime-grade doped Si < 100 > substrates (10–20  $\Omega$  cm) using a 10 kW electron beam evaporator (Angstrom Engineering) at a base pressure below  $3\times10^{-8}$  Torr. We first cleaned the substrates in a 2:1 solution of sulfuric acid and hydrogen peroxide (80 °C) and then rinsed with isopropanol to remove organic matter. We then immersed the plates in 49% hydrofluoric acid for about 20 s to remove the natural oxide layer. All films were grown using pieces of ITO with a 99.999% purity (In<sub>2</sub>O<sub>3</sub>—90%, SnO<sub>2</sub>—10%). The films were deposited at a rate of 2 Å/s, measured with a quartz monitor at an approximate distance from the source to the substrate of 30 cm. The thickness of all ITO thin films was  $20\pm2$  nm. Ion assistance (accelerating voltage 70 V) and deposition on a substrate with an elevated temperature (150 °C) were performed to study their effect on the structure of the thin film, resistivity, and carrier concentration. Subsequent annealing was carried out in an argon atmosphere for 20 min.

**Resistivity measurement.** The resistivity was measured using a four-point probe method using a ResMap 178 (CDE) four-probe surface resistance measurement system. We used a soft probe with a large footprint (500-µm tip radius semispherical probe) and a low clamping force (70 g) to ensure defect-free contact for the deposited films. A series of at least 5 measurements for more than 80 samples showed the same stable linear current-voltage characteristics. SEM analysis shows no damaged ITO films after measurements with a four-point probe.

**Scanning electron microscopy.** To check the quality and uniformity of the deposited layers, the surfaces of the ITO films were examined using a Zeiss Merlin scanning electron microscope with a Gemini II column immediately after deposition. All SEM images were obtained using an in-lens detector and an accelerating voltage of 5 kV at a working distance from the sample to the detector of 1 to 4 mm. Magnifications of 3 k, 7 k, 15 k and 50 k were used for complete analysis of the samples.

**Electron backscatter diffraction.** The crystallinity of the obtained ITO thin films was investigated by electron backscattering diffraction (EBSD) using a Nordlys-II S electron backscattering detector (Oxford Instruments) at an accelerating voltage of 10 keV at a working distance of 12.5 mm and a tilt angle of the sample into the microscope chamber of 70°. The AZtec 3.3 software was used to analyze the area. In paper Quaas et al. Al XRD analysis of ITO films showed In and  $In_2O_3$  phases, while Sn and  $SnO_x$  phases were not detected (it is assumed that the phases are embedded in the  $In/In_2O_3$  lattice). Here, the analysis similarly used the  $In_2O_3$  phases (lattice—

| Parameter                | type1                | type2                | type3                |  |
|--------------------------|----------------------|----------------------|----------------------|--|
| $N_c$ , cm <sup>-3</sup> | $4.2 \times 10^{20}$ | $3.7 \times 10^{20}$ | $5.7 \times 10^{20}$ |  |
| $\Delta n (0 + 16 V)$    | 0.053                | 0.048                | 0.101                |  |
| Δn (0-16 V)              | 0.030                | 0.053                | 0.098                |  |
| Δk (0+16 V)              | 0.030                | 0.028                | 0.119                |  |
| Δk (0-16 V)              | 0.016                | 0.056                | 0.121                |  |
| Δn                       | 0.083                | 0.101                | 0.199                |  |
| Δk                       | 0.046                | 0.084                | 0.240                |  |
| n (at 0 V)               | 1.342                | 1.308                | 0.675                |  |
| k (at 0 V)               | 0.226                | 0.141                | 0.329                |  |

**Table 2.** Comparison of refractive index and extinction coefficient change for the various ITO films at  $\lambda = 1550$  nm.

| Device p | arameters                            |                         | ITO characteristics   |                                   |                            |                            |                             |                             |            |  |
|----------|--------------------------------------|-------------------------|-----------------------|-----------------------------------|----------------------------|----------------------------|-----------------------------|-----------------------------|------------|--|
| IL, dB   | L <sub>device</sub> , um             | V <sub>switch</sub> , V | t <sub>ITO</sub> , nm | N <sub>c</sub> , cm <sup>-3</sup> | n <sub>ITO</sub> (1550 nm) | k <sub>ITO</sub> (1550 nm) | Δn <sub>ITO</sub> (1550 nm) | Δk <sub>ITO</sub> (1550 nm) | References |  |
| Electroa | Electroabsorption design             |                         |                       |                                   |                            |                            |                             |                             |            |  |
| 1        | 5                                    | ±5                      | 10                    | $1.1 \times 10^{19}$              | 1.964<br>(1310 nm)         | 0.002<br>(1310 nm)         | 0.922<br>(1310 nm)          | 0.271<br>(1310 nm)          | 13         |  |
| -        | 1700                                 | - 5                     | 50                    | $1.87 \times 10^{20}$             | 1.75                       | 0.195                      | 0.08                        | 0.075                       | 23         |  |
| Mach-Z   | Mach-Zehnder design                  |                         |                       |                                   |                            |                            |                             |                             |            |  |
| 6        | 32                                   | ±6                      | 10                    | $2.29 \times 10^{20}$             | 1.45                       | 0.18                       | ~1                          | -                           | 15         |  |
| -        | 2                                    | ±16                     | 10                    | $2.3 \times 10^{20}$              | 1.62                       | 0.15                       | 0.15                        | 0.1                         | 37         |  |
| 6        | 1.5                                  | ±13                     | 10                    | $3.13 \times 10^{20}$             | 1.44                       | 0.12                       | 0.44                        | 0.11                        | 16         |  |
| MOS-sta  | MOS-stack ellipsometry investigation |                         |                       |                                   |                            |                            |                             |                             |            |  |
| -        | -                                    | + 5                     | 40                    | $6.62 \times 10^{20}$             | 0.63                       | 0.57                       | 0.061                       | 0.079                       | 22         |  |
| -        | -                                    | ±16                     | 20                    | $5.70 \times 10^{20}$             | 0.81                       | 0.33                       | 0.199                       | 0.240                       | Our work   |  |
| -        | -                                    | ±16                     | 20                    | $3.79 \times 10^{20}$             | 1.31                       | 0.14                       | 0.101                       | 0.084                       | Our work   |  |

**Table 3.** Comparison of ITO characteristics and electro-optical device parameters in recent works.

cubic minimum; space group—206; diffraction symmetry class: m-3, a, b, c=10.12 Å, Alpha—90°, Beta—90°, Gamma—90°). The search for the SnO<sub>x</sub> phases gave no results, as expected.

**Stylus profilometry.** The stylus profiler KLA Tencor P17 (with Durasharp 38-nm tip radius stylus) was used. All measurements were completed using 0.5 mg taping strength, scan rate 2  $\mu$ m/s and 20  $\mu$ m scanned line length.

Active element layer stack fabrication. To fabricate a multilayer stack, the p-type doped Si < 100 > substrates (0.001  $\Omega$  cm) were oxidized for 6 min at 1000 °C forming 20 nm-thick silicon oxide layer. 20 nm-thick ITO films with an area from 2 to 5 mm² were formed on oxidized silicon substrates by the deposition of shadow masks. Then, 100 nm-thick aluminum or silver electrodes were deposited at room temperature (deposition parameters can be found elsewhere<sup>42</sup>) on the ITO and Si surfaces (Fig. 4a) to ensure better contact during electrical tests. The sample was connected to the power supply unit using a homemade contact tool mounted on the table of the ellipsometer (Fig. 4c). For optical measurements, we used additional focusing on a microspot about 200  $\mu$ m in size. Experimental benches based on Sentech SE 800 PV and Woollam V-VASE ellipsometers have been developed. It allows to measure the change in ellipsometric parameters  $\psi$  and  $\Delta$  for MOS structures and the optical properties of thin films under the action of an applied voltage.

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### **Author contributions**

E.S.L., A.S.B., I.A.R. (Ilya A. Ryzhikov) and I.R. (Ilya A. Rodionov) conceptualized the ideas of the project. E.S.L. performed device simulation, optimization of the thin films stack and the device parameters. E.S.L. fabricated thin films and devices. O.S.S., E.S.L., I.A.R., A.S.B. and I.R. performed morphology characterization and discussed microscopy/diffraction results. E.S.L., A.V.Z., Y.V.P. and I.A.R. conducted the electrical characterization of the experimental stacks. E.S.L., I.V.B., A.I.I., A.V.B and V.V.R. conducted characterization of ITO films optical parameters and electro-optical modulation, performed ellipsometry measurements, contributed to ellipsometry model, validation, calculation and mapping the carrier concentration. E.S.L., I.A.R. and A.S.B. prepared writing-original draft. I.R. reviewed and edited the manuscript. I.R. supervised the project. All authors analyzed the data and contributed to writing the manuscript.

## Competing interests

The authors declare no competing interests.

# Additional information

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