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Data Article

Conversion of flaxseed oil into biodiesel using KOH catalyst: Optimization and characterization dataset



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ABSTRACT

The dataset presented here are part of the data planned to produce biodiesel from flaxseed. Biodiesel production from flaxseed oil through transesterification process using KOH as catalyst, and the operating parameters were optimized with the help of face-centered central composite design (FCCD) of response surface methodology (RSM). The operating independent variables selected such as, methanol oil ratio (4:1 to 6:1), catalyst (KOH) weight (0.40–1.0%), temperature (35 °C–65 °C), and reaction time (30 min–60 min) were optimized against biodiesel yield as response. The maximum yield (98.6%) of biodiesel from flaxseed can achieved at optimum methanol oil ratio (5.9:1), catalyst (KOH) weight (0.51%), reaction temperature (59.2 °C), and reaction time (33 min). The statistical significance

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of the data set was tested through the analysis of variance (ANOVA). These data were the part of the results reported in "Optimization of process variables for biodiesel production by transesterification of flaxseed oil and produced biodiesel characterizations" Renewable Energy [1].

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Abbreviations

FCCD	Face-centered central composite design
RSM	Response surface methodology
ANOVA	Analysis of variance
Std. Dev.	Standard deviation
Std Err	Standard error
DF	Degree of freedom
Obs	Observed
VIF	Variance inflation factor
POE	Propagation of error
FI	Interactive factor
C.V	Coefficient of variance

Specifications Table

Subject	Energy
Specific subject area	Renewable energy, sustainability and the Environment
Type of data	Table
•••	Graph
	Figure
How data were acquired	Titration method was used for biodiesel yield estimation and the yield
•	data were set in face centered cubic design of response surface
	methodology approach using Design-Expert 6.0.6 (Stat-Ease, Inc.
	Minneapolis, USA)
Data format	Raw (.dx6 file)
	Analyzed data
Parameters for data collection	Volume ratio of methanol/oil, catalyst (KOH) weight percent, reaction
	temperature, and reaction time.
Description of data collection	The biodiesel was prepared under different operating conditions, and
	the data were collected through titration methods for estimating the
	biodiesel vield.
Data source location	Biodiesel synthesized in chemistry laboratory, college of Natural and
	Computational science, Madda Walabu University, Bale-Robe, Ethiopia
	City/Town/Region: Bale-Robe
	Country: Ethiopia
Data accessibility	All data is along with this article.
Related research article	T. Ahmad, M. Danish, P. Kale, B. Geremew, S.B. Adeloju, M. Nizami, M.
	Ayoub, Optimization of process variables for biodiesel production by
	transesterification of flaxseed oil and produced biodiesel
	characterizations. Renewable Energy, 139 (2019) 1272–1280. DOI.org/
	10.1016/j.renene.2019.03.036

Value of the Data

- The data set reported in this article will provide researchers with better understanding of the effects of operating parameters on the yield of biodiesel production.
- The four operating parameters such as, volume ratio of methanol/oil, KOH weight percent to oil, reaction temperature, and reaction time, were selected to optimize for maximum production of biodiesel.
- The face-centered central composite design (FCCD) of RSM was used to obtain the optimum value of each parameters for maximum biodiesel yield.
- The data describes the optimum conditions under which flaxseed oils can be converted into biodiesel with cost effective and energy saving approach.

1. Data

Table 1

The exponential growth of world population and its consequence on energy demand consumes the limited source of conventional non-renewable fossil fuel at much faster rate than expected. The rise of energy demand and fast depletion in fossil fuel triggered the research for finding the alternate source of energy. Biodiesel is one of the solutions to fulfil the energy demand as well as safety of the environment, because it is free from Sulphur, biodegradable, non-toxic, and renewable [2–4]. The fatty acid content of the flaxseed oil is reported elsewhere [5]. The data reported here is for the optimum production of the biodiesel from flaxseed oil. Table 1 shows the data obtained from the face-centered composite design (FCCD) approach of response surface methodology for the independent factors (methanol to oil ratio, catalyst (KOH) weight, temperature, and reaction time) and dependent factor (actual percentage yield of biodiesel) based on design of experiments. The levels

Std	Run	Factor 1 A:(Methanol to oil)	Factor 2 B:(Catalyst wt.% to oil)	Factor 3 C:(Temperature) °C	Factor 4 D:(Reaction time) min	Response 1 Yield %
21	1	5 (0)	0.7 (0)	35 (-1)	45 (0)	93.30
8	2	6(1)	1.0 (1)	65 (1)	30 (-1)	95.88
23	3	5 (0)	0.7 (0)	50 (0)	30 (-1)	96.62
20	4	5 (0)	1.0 (1)	50 (0)	45 (0)	94.90
2	5	6(1)	0.4 (-1)	35 (-1)	30 (-1)	96.40
15	6	4 (-1)	1.0 (1)	65 (1)	60(1)	92.26
10	7	6(1)	0.4 (-1)	35 (-1)	60(1)	96.84
28	8	5 (0)	0.7 (0)	50 (0)	45 (0)	94.22
11	9	4 (-1)	1.0 (1)	35 (-1)	60(1)	91.04
9	10	4 (-1)	0.4 (-1)	35 (-1)	60(1)	84.14
17	11	4 (-1)	0.7 (0)	50 (0)	45 (0)	95.09
14	12	6(1)	0.4 (-1)	65 (1)	60(1)	98.10
4	13	6(1)	1.0 (1)	35 (-1)	30 (-1)	96.86
12	14	6(1)	1.0 (1)	35 (-1)	60(1)	98.72
29	15	5 (0)	0.7 (0)	50 (0)	45 (0)	96.66
16	16	6(1)	1.0 (1)	65 (1)	60(1)	95.50
19	17	5 (0)	0.4 (-1)	50 (0)	45 (0)	94.58
18	18	6(1)	0.7 (0)	50 (0)	45 (0)	99.54
24	19	5 (0)	0.7 (0)	50 (0)	60(1)	95.68
3	20	4 (-1)	1.0 (1)	35 (-1)	30 (-1)	94.86
6	21	6(1)	0.4 (-1)	65 (1)	30 (-1)	98.41
1	22	4 (-1)	0.4 (-1)	35 (-1)	30 (-1)	85.88
27	23	5 (0)	0.7 (0)	50 (0)	45 (0)	96.86
5	24	4 (-1)	0.4 (-1)	65 (1)	30 (-1)	96.48
22	25	5 (0)	0.7 (0)	65 (1)	45 (0)	94.52
13	26	4 (-1)	0.4 (-1)	65 (1)	60 (1)	92.26
25	27	5 (0)	0.7 (0)	50 (0)	45 (0)	96.14
7	28	4 (-1)	1.0(1)	65 (1)	30 (-1)	89.32
26	29	5 (0)	0.7 (0)	50 (0)	45 (0)	96.18

The parameter factors and actual percentage yield based on FCCD design of experiments.

Table 2
Levels and ranges of independent factors used during biodiesel production from flaxseed oil.

Response	Name	Units	Obs	Minimum	Maximum	Trans	Model
Y1	Yield (%)	%	29	84.14	99.14	None	R Quadratic
Factor	Name	Units	Туре	Low Actual	High Actual	Low Coded	High Coded
Α	Methanol/oil ratio		Numeric	4	6	-1	1
В	Catalyst Weight %	%	Numeric	0.4	1	-1	1
С	Temperature C	0	Numeric	35	65	-1	1
D	Reaction Time min.	Min	Numeric	30	60	-1	1

Table 3Power at 5% alpha level for effect of following Standard Deviation.

Term	Std Err	VIF	Ri-Squared	1/2 Std. Dev.	1 Std. Dev.	2 Std. Dev.
Α	0.24	1	0.0	16.7%	50.6%	97.6%
В	0.24	1	0.0	16.7%	50.6%	97.6%
С	0.24	1	0.0	16.7%	50.6%	97.6%
D	0.24	1	0.0	16.7%	50.6%	97.6%
A ²	0.62	2.64	0.6213	11.7%	32.2%	84.8%
B^2	0.62	2.64	0.6213	11.7%	32.2%	84.8%
C^2	0.62	2.64	0.6213	11.7%	32.2%	84.8%
D^2	0.62	2.64	0.6213	11.7%	32.2%	84.8%
AB	0.25	1	0	15.4%	46.1%	96.0%
AC	0.25	1	0	15.4%	46.1%	96.0%
AD	0.25	1	0	15.4%	46.1%	96.0%
BC	0.25	1	0	15.4%	46.1%	96.0%
BD	0.25	1	0	15.4%	46.1%	96.0%
CD	0.25	1	0	15.4%	46.1%	96.0%

Basis std dev.=1.

Table 4

Parameters	for	pred	liction	design
1 arameters	101	picu	neuon	ucsign.

Parameters	Value
Maximum Prediction Variance (at a design)	0.659
Average Prediction Variance	0.517
Condition Number of Coefficient Matrix	10.655
G Efficiency (calculated from the design points) (%)	78.500
Scaled D-optimality Criterion	2.510
Determinant (X'X)-1	1.148×10^{-16}
Trace of (X'X)-1	2.251

and ranges of independent factors and their effect on standard deviation with measures derived from the (X'X)⁻¹ matrix are elaborated in Tables 2 and 3. The parameters for prediction design and the correlation matrix of regression coefficients with correlation matrix of factors are described in Table 4. The 3D interactive effects of the process variables for the percent yield of the flaxseed biodiesel is shown in Fig. 1 while deviation of input values of different parameter from reference point depicted in Fig. 2. The sequential model sum of squares and lack of fit test and model summary statistics are discussed in Tables 5 and 6. Analysis of variance (ANOVA) table for response surface reduced quadratic model was reported elsewhere [1]. The adjustment of R-squared value parameters and coefficient estimation for final model equation along with diagnostics case statistics are illustrated in Tables 7–9. Fig. 3 shows contour plot for maximum biodiesel yield within the selected independent variables (methanol to oil ratio, catalyst (KOH) weight, temperature, and reaction time) ranges. In addition, cubic graph for the maximum percent yield of the flaxseed biodiesel against independent

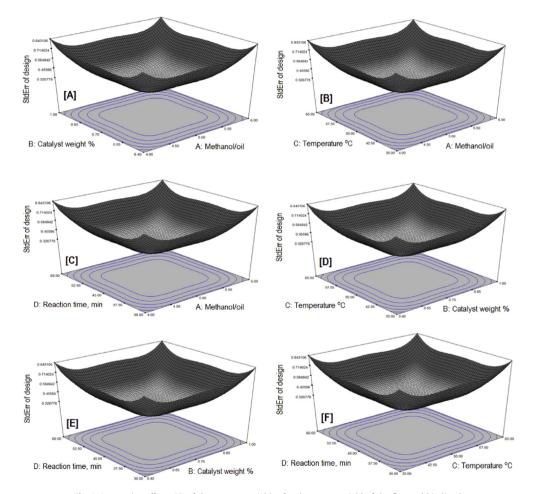


Fig. 1. Interactive effects 3D of the process variables for the percent yield of the flaxseed biodiesel.

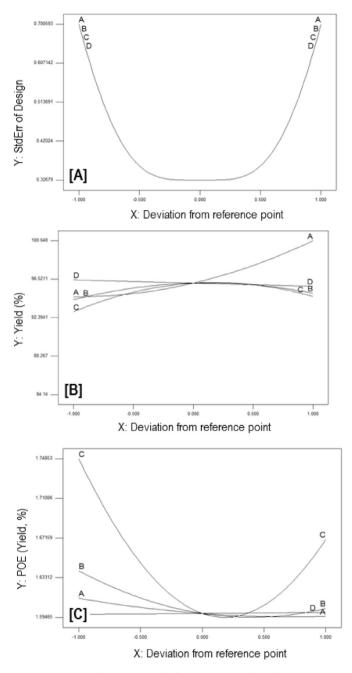


Fig. 2. Deviation of input values of different parameter from Reference point.

Table 5	
Sequential Model Sum of Squares and Lack of Fit test.	

Source	Sum of squares	DF	Mean Square	F Value	Prob>F	
Mean	2.604x10 ⁵	1	2.604x10 ⁵			
Linear	178.93	4	44.73	6.39	0.0012	
2FI	88.30	6	14.72	3.33	0.022	
Quadratic	41.5	4	10.37	3.81	0.0268	Suggested
Cubic	26.45	8	3.31	1.70	0.2670	Aliased
Residual	11.67	6	1.94			
Total	2.604×10^{5}	29	8991.48			
Linear	163.53	20	8.18	7.44	0.0322	
2FI	75.23	14	5.37	4.89	0.0683	
Quadratic	33.73	10	3.37	3.07	0.1455	Suggested
Cubic	7.27	2	3.64	3.31	0.1419	Aliased
Pure Error	4.39	4	1.10			

Table 6

Model summary statistics.

Source	Std. Dev.	R-Squared	Adjusted R-Squared	Predicted R-Squared	Press	
Linear	2.65	0.5159	0.4352	0.1946	279.36	
2FI	2.10	0.7704	0.6429	-0.0112	350.74	
Quadratic	1.65	0.8901	0.7802	0.1915	280.43	Suggested
Cubic	1.39	0.9664	0.8430	-4.1879	1799.46	Aliased

Table 7Adjustment of R-Squared value parameters.

Std. Dev.	1.59	R-Squared	0.8901
Mean	94.76	Adj R-Squared	0.7948
C.V.	1.68	Pre R-Squared	0.2014
Press	277	Adeq Precision	14.274

Table 8

Coefficient estimation for final model equation.

Factor	Coefficient Estimate	DF	Standard Error	95% CI Low	95% CI High	VIF
Intercept	96.10	1	0.52	95	97.19	
Α	3.01	1	0.38	2.21	3.81	1
В	0.35	1	0.38	-0.45	1.15	1
С	0.82	1	0.38	0.015	1.62	1
D	-0.34	1	0.38	-1.14	0.46	1
A ²	1.55	1	0.95	-0.47	3.57	2.41
B ²	-1.43	1	0.95	-3.45	0.59	2.41
C^2	-2.26	1	0.95	-4.28	-0.24	2.41
AB	-0.72	1	0.40	-1.57	0.13	1
AC	-0.96	1	0.40	-1.81	-0.11	1
AD	0.53	1	0.40	-0.32	1.38	1
BC	-1.91	1	0.40	-2.76	-1.06	1
BD	0.40	1	0.40	-0.45	1.25	1
CD	0.081	1	0.40	-0.77	0.93	1

Table 9		
Diagnostics	case	statistics.

185.8887.54 -1.66 0.658 -1.784 0.437 -1.942 22 296.4095.85 0.55 0.658 0.585 0.047 0.572 5 394.8692.69 2.17 0.658 2.330 0.746 2.819 20 496.8698.12 -1.26 0.658 -1.352 0.251 -1.393 13 596.4894.74 1.74 0.658 1.861 0.476 2.050 24 698.4199.22 -0.81 0.658 -0.872 0.104 -0.865 21 789.3292.26 -2.94 0.658 -3.153 1.366 -5.247 28 895.8893.86 2.02 0.658 -0.747 0.077 -0.736 10 1096.8495.26 1.58 0.658 -0.587 0.047 -0.574 9 1191.0491.59 -0.55 0.658 -0.587 0.047 -0.574 9 1298.7299.13 -0.41 0.658 -0.108 0.002 -0.104 26 1498.1098.95 -0.85 0.658 -0.913 0.114 -0.908 12 1592.2691.48 0.78 0.658 0.325 0.014 0.315 16 1795.9094.64 1.26 0.438 1.058 0.062 1.063 11 1899.54 100.655 -1.11	Standard Order	Actual Value	Predicted Value	Residual	Leverage	Student Residual	Cook's Distance	Outlier t	Run Order
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1	85.88	87.54	-1.66	0.658	-1.784	0.437	-1.942	22
496.8698.12 -1.26 0.658 -1.352 0.251 -1.393 13 596.4894.74 1.74 0.658 1.861 0.476 2.050 24 698.4199.22 -0.81 0.658 -0.872 0.104 -0.865 21 789.3292.26 -2.94 0.658 -3.153 1.366 -5.247 28 895.8893.86 2.02 0.658 2.165 0.644 2.522 2 984.1484.84 -0.70 0.658 -0.747 0.077 -0.736 10 1096.8495.26 1.58 0.658 -0.587 0.047 -0.574 9 1191.0491.59 -0.55 0.658 -0.444 0.027 -0.431 14 1392.2692.36 -0.10 0.658 -0.193 0.114 -0.908 12 1498.1098.95 -0.85 0.658 -0.913 0.114 -0.908 12 1592.2691.48 0.78 0.658 0.325 0.014 0.315 16 1795.9094.64 1.26 0.438 1.058 0.062 1.063 11 1899.54 10.065 -1.11 0.438 -0.928 0.048 -0.923 18 1994.5894.31 0.27 0.438 0.222 0.000 0.230 1 2294.5294.65 -0.13 <td>2</td> <td>96.40</td> <td>95.85</td> <td>0.55</td> <td>0.658</td> <td>0.585</td> <td>0.047</td> <td>0.572</td> <td>5</td>	2	96.40	95.85	0.55	0.658	0.585	0.047	0.572	5
596.4894.741.740.6581.8610.4762.05024698.4199.22 -0.81 0.658 -0.872 0.104 -0.865 21789.3292.26 -2.94 0.658 -3.153 1.366 -5.247 28895.8893.862.020.6582.1650.6442.5222984.1484.84 -0.70 0.6581.6940.3941.82071191.0491.59 -0.55 0.658 -0.587 0.047 -0.736 91298.7299.13 -0.41 0.658 -0.108 0.002 -0.104 261498.1098.95 -0.85 0.658 -0.913 0.114 -0.908 121592.2691.480.780.6580.3250.0140.315161795.9094.641.260.4381.0580.0621.063111899.54100.65 -1.11 0.438 -0.928 0.048 -0.923 181994.5894.310.270.4380.2220.0030.215172094.9095.01 -0.11 0.4380.2380.000 -0.088 42193.3093.020.280.4380.2380.0030.23012294.5294.65 -0.13 0.4380.2160.000 -0.088 42193.3093.020.28 <t< td=""><td>3</td><td>94.86</td><td>92.69</td><td>2.17</td><td>0.658</td><td>2.330</td><td>0.746</td><td>2.819</td><td>20</td></t<>	3	94.86	92.69	2.17	0.658	2.330	0.746	2.819	20
6 98.41 99.22 -0.81 0.658 -0.872 0.104 -0.865 21 7 89.32 92.26 -2.94 0.658 -3.153 1.366 -5.247 28 8 95.88 93.86 2.02 0.658 2.165 0.644 2.522 2 9 84.14 84.84 -0.70 0.658 -0.747 0.077 -0.736 10 10 96.84 95.26 1.58 0.658 -0.687 0.047 -0.574 9 11 91.04 91.59 -0.55 0.658 -0.108 0.002 -0.104 26 14 98.72 99.13 -0.41 0.658 -0.108 0.002 -0.104 26 14 98.10 98.95 -0.85 0.658 -0.913 0.114 -0.908 12 15 92.26 91.48 0.78 0.658 0.833 0.095 0.824 6 16 95.50 95.20 0.30 0.658 0.325 0.014 0.315 16 17 95.90 94.64 1.26 0.438 1.058 0.062 1.063 11 18 99.54 100.65 -1.11 0.438 -0.923 0.215 17 20 94.90 95.01 -0.11 0.438 0.238 0.003 0.230 1 21 93.30 93.02 0.28 0.438 0.238 0.000 -0.048 4 21 9	4	96.86	98.12	-1.26	0.658	-1.352	0.251	-1.393	13
7 89.32 92.26 -2.94 0.658 -3.153 1.366 -5.247 28 8 95.88 93.86 2.02 0.658 2.165 0.644 2.522 2 9 84.14 84.84 -0.70 0.658 -0.747 0.077 -0.736 10 10 96.84 95.26 1.58 0.658 1.694 0.394 1.820 7 11 91.04 91.59 -0.55 0.658 -0.587 0.047 -0.574 9 12 98.72 99.13 -0.41 0.658 -0.444 0.027 -0.431 14 13 92.26 92.36 -0.10 0.658 -0.108 0.002 -0.104 26 14 98.10 98.95 -0.85 0.658 -0.913 0.114 -0.908 12 15 92.26 91.48 0.78 0.658 0.325 0.014 0.315 16 17 95.90 94.64 1.26 0.438 1.058 0.062 1.063 11 18 99.54 100.65 -1.11 0.438 -0.928 0.048 -0.923 18 19 94.58 94.31 0.27 0.438 0.222 0.003 0.215 17 20 94.90 95.01 -0.11 0.438 -0.091 0.000 -0.088 4 21 93.30 93.02 0.28 0.438 0.238 0.003 0.230 1	5	96.48	94.74	1.74	0.658	1.861	0.476	2.050	24
895.8893.862.020.6582.1650.6442.5222984.1484.84 -0.70 0.658 -0.747 0.077 -0.736 101096.8495.261.580.6581.6940.3941.82071191.0491.59 -0.55 0.658 -0.587 0.047 -0.574 91298.7299.13 -0.41 0.658 -0.108 0.002 -0.104 261498.1098.95 -0.85 0.658 -0.913 0.114 -0.908 121592.2691.480.780.6580.3250.0140.315161795.9094.641.260.4381.0580.0621.063111899.54100.65 -1.11 0.438 -0.928 0.048 -0.923 181994.5894.310.270.4380.2220.0030.215172094.9095.01 -0.11 0.438 -0.091 0.000 -0.088 42193.3093.020.280.4380.2380.0030.23012294.5294.65 -0.13 0.438 -0.107 0.001 -0.104 252396.6296.440.180.1600.1250.0000.12032495.6895.75 -0.07 0.160 -0.056 0.000 -0.048 192596.1496.100.04<	6	98.41	99.22	-0.81	0.658	-0.872	0.104	-0.865	21
9 84.14 84.84 -0.70 0.658 -0.747 0.077 -0.736 10 10 96.84 95.26 1.58 0.658 1.694 0.394 1.820 7 11 91.04 91.59 -0.55 0.658 -0.587 0.047 -0.574 9 12 98.72 99.13 -0.41 0.658 -0.108 0.002 -0.104 26 14 98.10 98.95 -0.85 0.658 -0.108 0.002 -0.104 26 15 92.26 91.48 0.78 0.658 0.333 0.095 0.824 6 16 95.50 95.20 0.30 0.658 0.325 0.014 0.315 16 17 95.90 94.64 1.26 0.438 1.058 0.062 1.063 11 18 99.54 100.65 -1.11 0.438 -0.928 0.48 -0.923 18 19 94.58 94.31 0.27 0.438 0.222 0.003 0.215 17 20 94.90 95.01 -0.11 0.438 -0.091 0.000 -0.088 4 21 93.30 93.02 0.28 0.438 0.238 0.003 0.230 1 22 94.52 94.65 -0.13 0.43 -0.091 0.000 -0.048 4 23 96.62 96.44 0.18 0.160 0.125 0.000 0.120 3 2	7	89.32	92.26	-2.94	0.658	-3.153	1.366	-5.247	28
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	8	95.88	93.86	2.02	0.658	2.165	0.644	2.522	2
1191.0491.59 -0.55 0.658 -0.587 0.047 -0.574 91298.7299.13 -0.41 0.658 -0.444 0.027 -0.431 141392.2692.36 -0.10 0.658 -0.108 0.002 -0.104 261498.1098.95 -0.85 0.658 -0.913 0.114 -0.908 121592.2691.48 0.78 0.658 0.833 0.095 0.824 61695.5095.20 0.30 0.658 0.325 0.014 0.315 161795.9094.64 1.26 0.438 1.058 0.062 1.063 111899.54 100.65 -1.11 0.438 -0.928 0.048 -0.923 181994.5894.31 0.27 0.438 0.222 0.003 0.215 172094.9095.01 -0.11 0.438 -0.911 0.000 -0.088 42193.3093.02 0.28 0.438 0.238 0.003 0.230 12294.5294.65 -0.13 0.438 -0.107 0.001 -0.104 252396.6296.44 0.18 0.160 0.125 0.000 0.124 32495.6895.75 -0.07 0.160 -0.050 0.000 -0.048 192596.1496.10 0.04 0.105 0.05	9	84.14	84.84	-0.70	0.658	-0.747	0.077	-0.736	10
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10	96.84	95.26	1.58	0.658	1.694	0.394	1.820	7
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	11	91.04	91.59	-0.55	0.658	-0.587	0.047	-0.574	9
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12	98.72	99.13	-0.41	0.658	-0.444	0.027	-0.431	14
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	13	92.26	92.36	-0.10	0.658	-0.108	0.002	-0.104	26
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	14	98.10	98.95	-0.85	0.658	-0.913	0.114	-0.908	12
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	15	92.26	91.48	0.78	0.658	0.833	0.095	0.824	6
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	16	95.50	95.20	0.30	0.658	0.325	0.014	0.315	16
19 94.58 94.31 0.27 0.438 0.222 0.003 0.215 17 20 94.90 95.01 -0.11 0.438 -0.091 0.000 -0.088 4 21 93.30 93.02 0.28 0.438 0.238 0.003 0.230 1 22 94.52 94.65 -0.13 0.438 -0.107 0.001 -0.104 25 23 96.62 96.44 0.18 0.160 0.125 0.000 0.120 3 24 95.68 95.75 -0.07 0.160 -0.050 0.000 -0.048 19 25 96.14 96.10 0.04 0.105 0.029 0.000 0.028 27 26 96.18 96.10 0.76 0.105 0.506 0.002 0.494 23	17	95.90	94.64	1.26	0.438	1.058	0.062	1.063	11
20 94.90 95.01 -0.11 0.438 -0.091 0.000 -0.088 4 21 93.30 93.02 0.28 0.438 0.238 0.003 0.230 1 22 94.52 94.65 -0.13 0.438 -0.107 0.001 -0.104 25 23 96.62 96.44 0.18 0.160 0.125 0.000 0.120 3 24 95.68 95.75 -0.07 0.160 -0.050 0.000 -0.048 19 25 96.14 96.10 0.04 0.105 0.029 0.000 0.028 27 26 96.18 96.10 0.08 0.105 0.056 0.000 0.054 29 27 96.86 96.10 0.76 0.105 0.506 0.002 0.494 23	18	99.54	100.65	-1.11	0.438	-0.928	0.048	-0.923	18
21 93.30 93.02 0.28 0.438 0.238 0.003 0.230 1 22 94.52 94.65 -0.13 0.438 -0.107 0.001 -0.104 25 23 96.62 96.44 0.18 0.160 0.125 0.000 0.120 3 24 95.68 95.75 -0.07 0.160 -0.050 0.000 -0.048 19 25 96.14 96.10 0.04 0.105 0.029 0.000 0.028 27 26 96.18 96.10 0.08 0.105 0.506 0.002 0.494 23	19	94.58	94.31	0.27	0.438	0.222	0.003	0.215	17
22 94.52 94.65 -0.13 0.438 -0.107 0.001 -0.104 25 23 96.62 96.44 0.18 0.160 0.125 0.000 0.120 3 24 95.68 95.75 -0.07 0.160 -0.050 0.000 -0.048 19 25 96.14 96.10 0.04 0.105 0.029 0.000 0.028 27 26 96.18 96.10 0.08 0.105 0.056 0.000 0.054 29 27 96.86 96.10 0.76 0.105 0.506 0.002 0.494 23	20	94.90	95.01	-0.11	0.438	-0.091	0.000	-0.088	4
23 96.62 96.44 0.18 0.160 0.125 0.000 0.120 3 24 95.68 95.75 -0.07 0.160 -0.050 0.000 -0.048 19 25 96.14 96.10 0.04 0.105 0.029 0.000 0.028 27 26 96.18 96.10 0.76 0.105 0.506 0.002 0.494 23	21	93.30	93.02	0.28	0.438	0.238	0.003	0.230	1
24 95.68 95.75 -0.07 0.160 -0.050 0.000 -0.048 19 25 96.14 96.10 0.04 0.105 0.029 0.000 0.028 27 26 96.18 96.10 0.08 0.105 0.056 0.000 0.054 29 27 96.86 96.10 0.76 0.105 0.506 0.002 0.494 23	22	94.52	94.65	-0.13	0.438	-0.107	0.001	-0.104	25
25 96.14 96.10 0.04 0.105 0.029 0.000 0.028 27 26 96.18 96.10 0.08 0.105 0.056 0.000 0.054 29 27 96.86 96.10 0.76 0.105 0.506 0.002 0.494 23	23	96.62	96.44	0.18	0.160	0.125	0.000	0.120	3
26 96.18 96.10 0.08 0.105 0.056 0.000 0.054 29 27 96.86 96.10 0.76 0.105 0.506 0.002 0.494 23	24	95.68	95.75	-0.07	0.160	-0.050	0.000	-0.048	19
27 96.86 96.10 0.76 0.105 0.506 0.002 0.494 23	25	96.14	96.10	0.04	0.105	0.029	0.000	0.028	27
	26	96.18	96.10	0.08	0.105	0.056	0.000	0.054	29
28 94.22 96.10 -1.88 0.105 -1.244 0.013 -1.269 8	27	96.86	96.10	0.76	0.105	0.506	0.002	0.494	23
	28	94.22	96.10	-1.88	0.105	-1.244	0.013	-1.269	8
29 96.66 96.10 0.56 0.105 0.374 0.001 0.363 15	29	96.66	96.10	0.56	0.105	0.374	0.001	0.363	15

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variables and residual variation plots for normal and predicted value along with run and reaction time are shown in Fig. 4 and Fig. 5, respectively. The Residual variation plots with different process variables and variation in run number for the diagnostics case statistics are elaborated in Figs. 6 and 7. The criteria for desirability for constraints is shown in Fig. 8. The point prediction and optimization of independent variables for maximum biodiesel yield from the flaxseed oil are tabulated in Tables 10 and 11 respectively.

2. Experimental design, materials, and methods

2.1. Materials

The flaxseed oil was collected from the local market of Bale-Robe, Ethiopia. Methanol (CH₃OH, 99.8% purity), sulfuric acid (H₂SO₄, 98%), and KOH were bought from Sigma Aldrich and were of analytical grade. During experiment 0.1 N sulfuric acid solution was used. All chemicals consumed during the biodiesel synthesis were of analytical grade.

2.2. Methods

Biodiesel from flaxseed oil was produced in a batch experiment. The biodiesel produced in the laboratory from flaxseed oil involved a two-step transesterification reaction accompanied with product separation, washing, and drying. The process flow chart for the biodiesel production from flaxseed oil shown in Fig. 9. A fixed quantity (50 g) of the oil was measured and poured into a conical flask. The

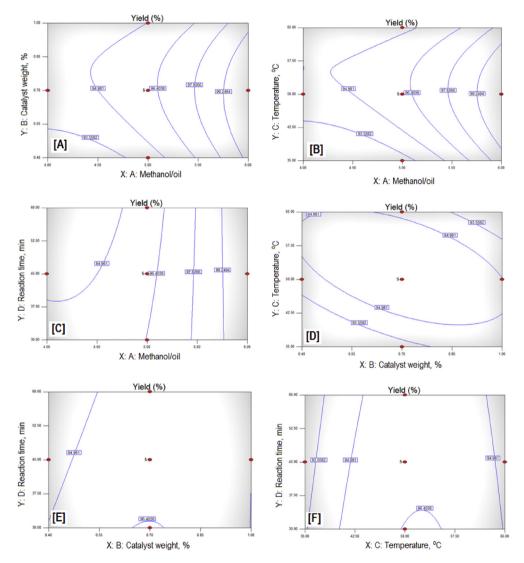


Fig. 3. Standard Error of Design at different parameters for the percent yield of the flaxseed biodiesel.

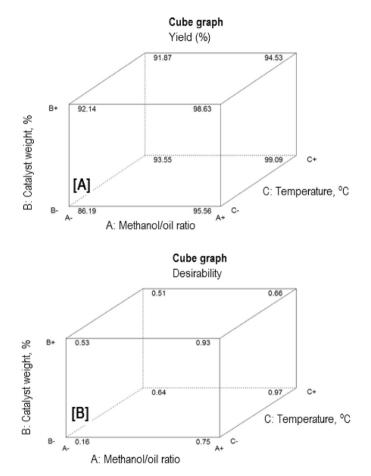


Fig. 4. Cube graph for the maximum percent yield of the flaxseed biodiesel at different parameters.

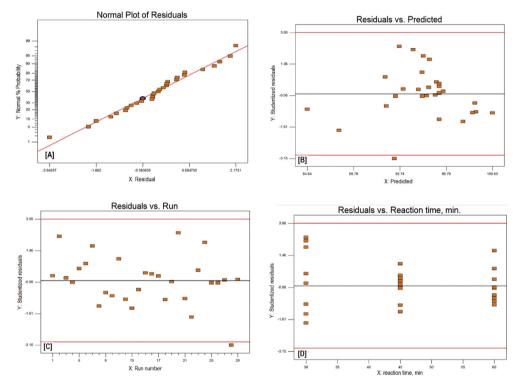


Fig. 5. Residual variation Plots for normal and predicted value along with run and reaction time.

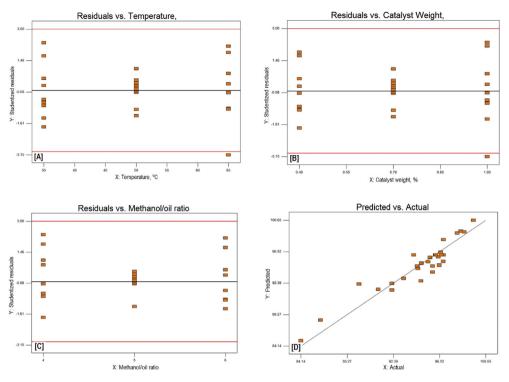


Fig. 6. The Residual variation Plots with different process parameters.

flaxseed oil was pre-heated at 110 °C for 30 min to remove the moisture content in oil. The process involves the catalyst KOH in different weight percentage of oil (0.40, 0.70, and 1.0%), methanol at various molar ratios of methanol/oil (4:1, 5:1, and 6:1) under different temperature (35, 50, and 65 °C) and reaction time (30, 45, and 60 min). The water washing method was used for further purification of FAME (biodiesel). The mixture was stirred gently to avoid foam formation. The mixture was left overnight to settle into two phases: a water-impurity phase and a biodiesel phase. Separating funnel was used to separate the FAME (biodiesel) from the water-impurity phase. This process was repeated three times to ensure the removal of most impurities from the biodiesel fraction. The washed biodiesel fraction was then reheated at 100 °C for 1 h to evaporate the residual water. The titration of biodiesel fraction with sulfuric acid (0.1 N) was used for the quantification of the FAME [6]. The percentage yield of flaxseed biodiesel was determined by comparing biodiesel weight with flaxseed oil weight used initially.

2.3. Design of experiment

The face-centered central composite design (FCCD) was applied to optimize the biodiesel yield. This design is most suitable approach to optimize such processed which have a quantitative independent variable, and its response can also be observed quantitatively experimental matrix. The FCCD have sufficient tool to find the optimum values of independent variables within the selected range. Two levels and four factors with five center point values were considered for this experiment, the total number of experiments suggested through this method was $(2^4 + 2 \times 4 + 5)$ 29 batch experiments. The independent variables selected for optimization were methanol/oil molar ratio (A), catalyst weight percent (B), reaction temperature (D) and reaction time (E). The response chosen was the biodiesel yields produced through KOH catalyzed transesterification reaction of flaxseed oil. The actual values of

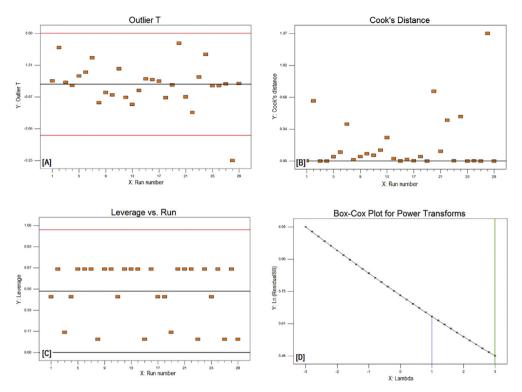


Fig. 7. Variation in run number for Diagnostics Case Statistics.

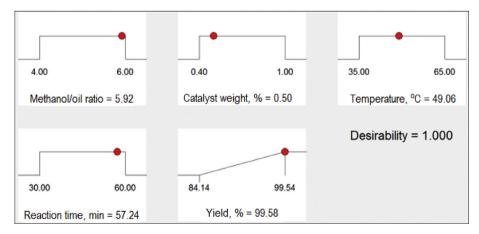


Fig. 8. Criteria for desirability for Constraints.

Factor	Name		Level	Low level	High Level		Std. Dev.	
Α	Methanol to o	il ratio	5	4	6		1x10-2	
В	Catalyst Weight		0.7	0.4	1		1×10^{-2}	
С	Temperature		50	35	65		2	
D	Reaction Time		45	30	6	0	1	
	Prediction	SE Mean	95% CI low	95% CI high	SE Pred	95% PI low	95% PI high	
Yield (%) POE (Yield (%))	96.096 1.59845	0.52	95	97.19	1.68	92.52	99.67	

Table 10 Point prediction for yield of the flaxseed biodiesel.

Table 11

Optimal processing conditions from numerical optimization.

Parameter				Yield (%)		Desirability
X ₁	X ₂	X3	X4	Predicted	Experimental	
5.90:1	0.51	59.19	32.83	99.56	98.60	1.000

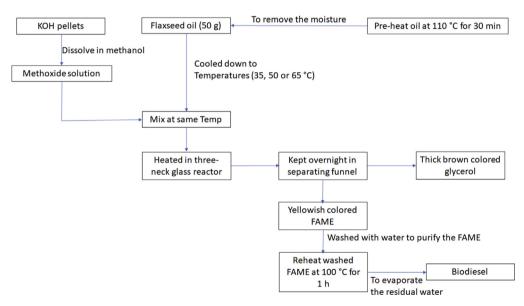


Fig. 9. Flow chart for biodiesel production from flaxseed oil.

the independent variables are listed in Table 1. The biodiesel synthesis was conducted in batch, and each set of experimental conditions were selected randomly to minimize systematic error. All statistical parameters including analysis of variance (ANOVA) and figures were plotted with the help of Design-Expert 6.0.6 (Stat-Ease, Inc., Minneapolis, USA) [7].

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Conflict of Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Appendix A. Supplementary data

Supplementary data to this article can be found online at https://doi.org/10.1016/j.dib.2020.105225.

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