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Article

# High Removal Efficiency of Radioactive Iodine with In Situ-Synthesized Ag<sub>2</sub>O-Mg(OH)<sub>2</sub> Plate Composites

Chunyang Zhang,\* Le Zhang,\* Bowen Zheng, Haoran Chu, Zhaofeng Liu, Yun Bai, Sicheng Chang, Song Yang, Ning Zhao, Qingshan Yang, and Yuheng Ma



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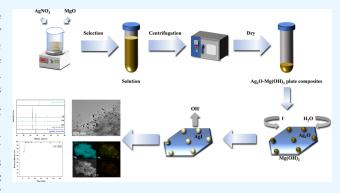
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ABSTRACT: To promote the capacity of adsorbing radioactive iodine (I<sup>-</sup>) in acid and alkaline situations, a high-removal-efficiency adsorbent based on silver oxide (Ag<sub>2</sub>O) and magnesium hydroxide  $(Mg(OH)_2)$  was synthesized by the in situ method. To determine the mechanism of this novel absorbent, batch experiments related to the temperature, pH, competitive ion (Cl<sup>-</sup>), and kinetic analysis were carried out. The results showed that the Ag<sub>2</sub>O-Mg(OH)<sub>2</sub> plate composites had high adsorption capacity and efficiency for I-(409 mg/g, 25 °C) with a wide range of pH values (3-9). In addition, the adsorption time from the initial concentration to Iremoval (97.36%) was only 20 min. Competitive ion experiments depicted that  $Cl^-$  influenced the capacity of adsorbing  $I^-$ . The kvalue of the pseudo-second-order model and regression factor  $R^2$ 



were  $7.86 \times 10^{-3}$  g mg<sup>-1</sup> min<sup>-1</sup> and 0.999 at 25 °C, respectively. The kinetics and XPS results proved that the mechanism of adsorption was chemical adsorption. Compared with other commercial adsorbents, the Ag<sub>2</sub>O-Mg(OH)<sub>2</sub> plate composites had potential for application in nuclear wastewater treatment with low cost and high efficiency.

## 1. INTRODUCTION

Radioactive iodine, produced from human nuclear activities such as nuclear electricity generation and nuclear tests, can be easily dissolved in water. Radioactive iodine mainly contains  $^{129}$ I and  $^{131}$ I, with corresponding half-lives of 1.57  $\times$  10<sup>7</sup> years and 8 days, respectively.2 129I stems from the circulation cooling water of the primary circuit, which would lead to longterm effects when leaked from the nuclear plant. Influences of the leakage accident in Fukushima (Japan) have been aggravated since the beginning of the discharge of radionuclides including radioactive iodine in 2023.<sup>3</sup> In addition, <sup>131</sup>I has been applied as nuclear medicine due to the thyroid's iodine-selective uptake ability.<sup>4</sup> Although its half-life is much shorter than that of  $^{129}$ I, its higher radioactivity (1.5 × 10<sup>17</sup> Bq) causes the risk of cancer, especially for doctors and patients. Radioactive iodine has a high probability of causing harm to the human thyroid directly. Natural aquatic ecosystems can be polluted by radioactive iodine containing nuclear contaminated water, which has a potential influence on the health of people. Therefore, it is imminent to decrease radioactive iodine from wastewater.

Radioactive iodine can be removed by several methods including sorption,<sup>6</sup> ion exchange,<sup>7</sup> membrane separation,<sup>8,9</sup> and chemical precipitation. 10 Among them, sorption has been widely studied owing to its easier processes and lower costs. Activated carbon, 11,12 metal oxides, 13 and metal—organic frameworks (MOFs)<sup>14-17</sup> are the main adsorbents. However, the low adsorption capacity and low selectivity limit the application of activated carbon. Although MOFs exhibit great adsorption performance, their higher cost and poor stability have become limitations in a wide range of applications. Metal oxides such as Ag<sub>2</sub>O, bismuth oxide, and Cu<sub>2</sub>O are potential materials to remove I- attributed to their ability to adsorb iodine ions and form precipitates on the surface. Liu et al. 19 reported that bismuth oxide (Bi<sub>2</sub>O<sub>2,33</sub>) nanoparticles with a flower-like structure showed stability in both acid and alkaline environments and exhibited great selectivity among competitive anions. Zhang et al.<sup>20</sup> found that Bi<sub>2</sub>O<sub>3</sub>/LDHs with sponge-like porous structures can remove 94% of the initial I at near-neutral pH. Jiao et al. 21 obtained block Cu@ Cu<sub>2</sub>O, which reduced 96.65% of I<sup>-</sup> in acid conditions with electrification.

Ag<sub>2</sub>O is demonstrated as a significant ingredient for I<sup>-</sup> adsorption, which can be precipitated more easily compared with Cl<sup>-.22</sup> Thus, the reaction can generate a high removal

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efficiency in a short period.<sup>23</sup> Nevertheless, the removal ability is poor when Ag<sub>2</sub>O has a low specific surface area. In addition, large particles of Ag<sub>2</sub>O will lead to a reduction of the removal efficiency. Meanwhile, trace amounts of I- make the sorption process difficult. Thus, the above problems can be resolved by choosing a support that has a substantial void ratio and a large specific surface area, anchoring target metal-oxide nanocrystals on its surface to obtain uniform dispersion.<sup>24</sup> Titanate, <sup>2,25,26</sup> natural minerals<sup>27</sup> and zeolites<sup>28–31</sup> are favorable materials that prevent the aggregation of Ag<sub>2</sub>O, increasing its surface contact area are favorable materials that prevent aggregation of metaloxide nanocrystals when increasing its surface contact area. Recently, silver-based materials fabricated by simplified chemical synthesis have gained considerable attention. 32 The literature shows that water-stable MOFs, zeolites, and cuprous oxide loading with Ag nanoparticles enhance the I- removal efficiency.<sup>33</sup> However, higher costs and lower stability limit the application of these supports. Meanwhile, Mg(OH)<sub>2</sub> shows great economic advantages as a support for silver oxide nanoparticle loading. Most importantly, the Mg(OH)<sub>2</sub> support maintains its stability in high-radiation situations, and considerable research has been conducted on it. However, the aforementioned materials are limited due to the deactivation in strong acid and alkaline situations.<sup>28</sup> At present, there is an urgent need to seek a simplified synthesis process and low-cost way to overcome these problems.

In this study, we developed a new type of adsorbent with a high I<sup>-</sup> removal efficiency, which has strong stability in a wide range of pH values by using only the stirring method at room temperature with AgNO<sub>3</sub> and MgO as precursors. Experiments are systematically implied with the following characteristics: reaction time, pH values, temperatures, and competitive ion (Cl<sup>-</sup>). The adsorption mechanism and kinetic analysis were researched in detail.

# 2. MATERIALS AND METHODS

**2.1. Materials.** NaI was purchased from the Beichenfangzheng Chemical Reagent Factory, Tianjin, China. NaCl was purchased from Tianjin Zhiyuan Reagent Co., Tianjin, China. AgNO<sub>3</sub> was purchased from Sinopharm Chemical Reagent Co. Ltd, Shanghai, China. MgO was purchased from Bikeman Bio Co., Changde, China. Mg(OH)<sub>2</sub> was purchased from Damao Chemical Reagent Factory, Tianjin, China. These reagents were all of analytical grade purity and used as received without further purification. Also, nitric acid solution and NaOH (99% pure, Oubokai Chemical Engineering Co., Tianjin, China) were used to adjust the pH values of the solution. Experiments were all conducted with deionized water.

**2.2. Synthesis of the Adsorbent.** The synthesis process can be described as an in situ-synthesis. At room temperature, certain amounts of  $AgNO_3(2.94 \text{ mmol})$  and MgO (9.92 mmol) were added into deionized water (50.0 mL). Then, the solution was stirred with a magnetic rotor in a heating magnetic stirrer for 2 h. After stirring, the sediments were obtained through three cycles of centrifugation. The final precipitates were collected after drying at 60 °C for the whole night. For comparison, the same method was used to synthesize other samples with stirring periods of 12 and 24 h, respectively. Otherwise, single-phase  $Ag_2O$  was synthesized by the method described in the literature. To compare with in situ-synthesis,  $Ag_2O$  and  $Mg(OH)_2$  were mixed in a quartz mortar for 30 min directly to form composites.

**2.3. Characterization.** Crystalline structures of the adsorbents were characterized by using the powder X-ray diffraction (XRD) technique (DX2700, HAOYUAN INSTRU-MENT, China). The diffractometer was equipped with copper target K $\alpha$ , the scanning rate was 5°/min, and the scanning range was 10-80°. The phase composition and chemical state of the adsorbents before and after adsorption were determined by X-ray photoelectron spectroscopy (XPS) technology (Thermo SCIENTIFIC ESCALAB 250Xi, American). Fieldemission scanning electron microscopy (FE-SEM, JEOL, JSM-7800F Prime, Japan; EDS, Thermo Scientific NORANTM System 7, American) and transmission electron microscopy (TEM, JEOL, JEM2100F, Japan) were performed to observe and analyze the micromorphology and composition of the samples. N2 adsorption and desorption was performed by a porous physical adsorption instrument (QUANTACHROME, American), and the surface area was calculated by the Barrett-Emmett-Teller (BET) calculation.

2.4. Iodine Ion Removal Experiments. All experiments were conducted with nonradioactive iodine as a substitute to avoid the toxicity of radioactive iodine. A certain amount of iodine ion (10-100 mg<sub>Nal</sub>/L) solution was prepared by dissolving NaI in 1 L of deionized water. A series of experiments were carried out with the mixture of 20 mg of adsorbent and 1 L of iodine solution in a beaker under a magnetic stirrer. The pH value was adjusted by NaOH and HNO<sub>3</sub> solutions. The effects of the equilibrium concentration of I<sup>-</sup>, pH value, temperature, and competitive ions (Cl<sup>-</sup>) on the removal rate of I- were studied. Samples were taken from the solution through a needle and separated from the liquidsolid phase by a PES syringe filter. The residual concentration of I was determined by using a UV-Vis spectrophotometer (PE Company, Lambda750, American) at 226 nm. The coefficient of determination value R<sup>2</sup> calculated from the calibration line is 0.9987. The removal efficiencies were calculated according to the following three equations:

$$Q_{t} = \frac{C_{i} - C_{t}}{m}V \tag{1}$$

$$Q_{\rm e} = \frac{C_{\rm i} - C_{\rm e}}{m} V \tag{2}$$

$$A_{\rm t} = \frac{C_{\rm i} - C_{\rm t}}{C_{\rm i}} \times 100\% \tag{3}$$

where  $C_i$ ,  $C_e$ , and  $C_t$  are the concentrations of dissolved I<sup>-</sup> (mg/L) initially, at equilibrium, and at time t, respectively. m is the weight of the adsorbent (g), and V is the volume of the solution (L).  $Q_t$  and  $Q_e$  are the amounts of I<sup>-</sup> removed at time t and equilibrium, respectively.  $A_t$  is the removal efficiency at time t.

**2.5.** Adsorption Kinetics of the Adsorbent. The experiments of adsorption kinetics were conducted at room temperature in a neutral solution. 20 mg of adsorbent and 10 mg of NaI were added in 1 L of deionized water. Samples were taken from the solution at specific timepoints including 5, 10, 25, 20, 30, 60, 90, and 120 min. After filtration, the concentration of  $I^-$  was determined via UV—vis spectroscopy to calculate the  $Q_t$  of every sample according to eq 1. Considering further analysis of the behavior of the adsorbent in the iodine solution, the pseudo-first-order and pseudo-second-order models were applied to disclose the kinetics of adsorption. The first model was based on the physical

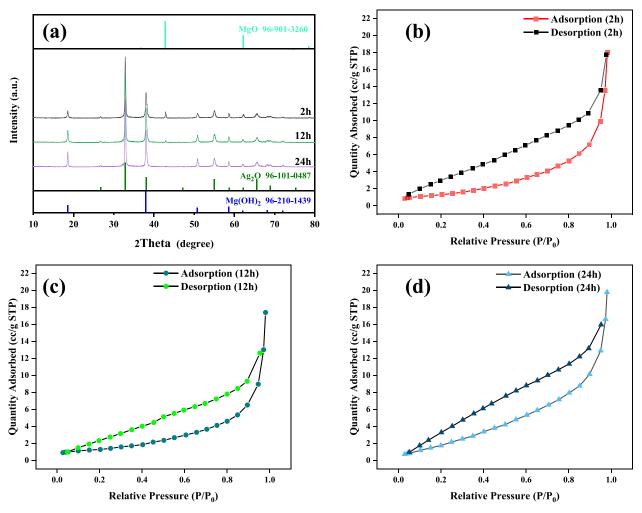


Figure 1. XRD patterns of the adsorbent with different times (a).  $N_2$  adsorption and desorption isotherms of  $Ag_2O-Mg(OH)_2$  plate composites with times of 2 h (b), 12 h (c), and 24 h (d).

absorption theory, while the other was chemisorption involving electron sharing and transfer between the adsorbent and adsorbate. The equations of linear expression of the pseudo-first-order and pseudo-second-order models were as follows:

$$\ln(Q_e - Q_t) = \ln Q_e - k_1 t \tag{4}$$

$$\frac{t}{Q_{t}} = \frac{1}{Q_{e}}t + \frac{1}{k_{2}Q_{e}^{2}} \tag{5}$$

where  $k_1$  and  $k_2$  are constants that represent the first-order and second-order rate coefficients, respectively.

**2.6.** Determination of the Removal Efficiency in the Presence of Competitive lons. To investigate the influence of competitive ions on the removal efficiency of I<sup>-</sup>, 10 mg of NaI was put into 1 L of deionized water with a certain content of NaCl to obtain a solution for competitive experiments. The adsorbents were stirred with the solution for 20 min. Then, the residual content of iodine was determined by UV—vis spectroscopy.

### 3. RESULTS AND DISCUSSION

**3.1. Phase Structure.** To determine the phase structure of the adsorbent, the XRD patterns were measured. Figure 1 displays the XRD patterns and  $N_2$  adsorption and desorption isotherm of the adsorbent under different synthesis times. As

shown in Figure 1a, the highest intensity peak appeared at a distinct diffraction angle  $2\theta = 32.87^{\circ}$ , corresponding to the interplanar phase of Ag<sub>2</sub>O (1 1 1), indicating that Ag<sub>2</sub>O was successfully formed during the stirring synthesis process. It can also be seen from Figure 1a that the diffraction peak of MgO gradually becomes weakened with the stirring time increasing, and the Mg(OH)<sub>2</sub> diffraction peak becomes stronger. At 24h, the diffraction peak of MgO disappeared, which indicated that the Ag<sub>2</sub>O-Mg(OH)<sub>2</sub> composites were successfully synthesized. The results of N<sub>2</sub> adsorption and desorption experiments of Ag<sub>2</sub>O-Mg(OH)<sub>2</sub> composites are shown in Figure 1b-d with synthesis times of 2, 12, and 24 h. According to the figures, all of these three samples showed type IV isotherms and H3 hysteresis loops, which suggested that mesoporous materials were obtained. The pore sizes of Ag<sub>2</sub>O-Mg(OH)<sub>2</sub> composites were 3.432 nm (2 h), 3.430 nm (12 h), and 3.097 nm (24 h) by the BJH adsorption method, respectively. Theoretically, the smaller pore size and the larger BET surface area were beneficial to the adsorption property. Based on the XRD analysis, it can be concluded that the Ag<sub>2</sub>O-Mg(OH)<sub>2</sub> composites were successfully synthesized at 24h. Thus, the following experiments would be conducted with the material synthesized at 24 h.

Figure 2 shows the microstructure and element mapping distribution of  $Ag_2O-Mg(OH)_2$  composites. It can be seen

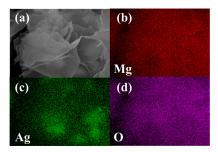


Figure 2. Microstructure and elemental mapping analyses of Ag<sub>2</sub>O–Mg(OH)<sub>2</sub> plate composites before the reaction (a–d).

that  $Ag_2O-Mg(OH)_2$  composites have plate-like structures. According to the literature, <sup>35</sup> this space construction was  $Mg(OH)_2$ , which was beneficial to form a mesoporous structure. To some extent, the plate-like structure promoted the dispersion of  $Ag_2O$ . The mapping results demonstrated that  $Ag_2O$  was dispersed on the  $Mg(OH)_2$  plate uniformly. This phenomenon would encourage the adsorption of  $I^-$ . This clearly proved that the plate-like  $Mg(OH)_2$  was an ideal carrier for  $Ag_2O$ . According to the analysis of Figure 1 and the literature, <sup>35</sup> the mesopores can be attributed to the fact that the MgO crystals were dissolved in water and hydroxylated into  $Mg(OH)_2$  primary particles and then aggregated to produce large plate-like materials through oriented attachment.

Figure 3 shows the respective typical TEM images of the adsorbent. It can be seen that many nanoparticles were well-

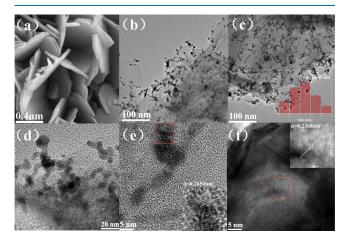


Figure 3. SEM image of  $Ag_2O-Mg(OH)_2$  plate composites (a). TEM images of the adsorbent (b-d). Inset in (c): statistics of particle size distribution in (c) in 100 nm staff. Interplanar spacings of  $Ag_2O$  (e) and  $Mg(OH)_2$  (f).

distributed on the plate. The nanoparticle size was about 6.46  $\pm$  0.05 nm. The interplanar phases of the particles were 0.265 and 0.236 nm corresponding to the (1 1 1) plane of Ag<sub>2</sub>O and (1 0 1) plane of Mg(OH)<sub>2</sub>, <sup>36,37</sup> respectively. This clearly illustrates that Ag<sub>2</sub>O nanoparticles were loaded on the Mg(OH)<sub>2</sub> plate successfully. Similarly, it is certain that the composites would be beneficial for NaI adsorption.

**3.2.** Properties of Ag<sub>2</sub>O–Mg(OH)<sub>2</sub> Plate Composites. Figure 4 shows the I<sup>-</sup> removal efficiency of the Ag<sub>2</sub>O–Mg(OH)<sub>2</sub> composites. Figure 4a shows that the synthesis temperature has a significant influence on the removal efficiency. With a higher synthesis temperature, the composites showed a lower removal efficiency. When the reaction

temperature was 25 °C, the removal efficiency reached 97.36% of the initial concentration within 10 min, while the efficiency was only 65% at 45 °C. This result indicated that the optimal reaction adsorption temperature was 25 °C. However, the adsorption efficiency at the equilibrium of the three temperatures reached up to 97%, suggesting that the material has good thermal stability. According to the results above, considering that the time at which the adsorbent reached the equilibrium adsorption was 20 min, subsequent experiments would be conducted in the same time.

To investigate the influence of pH values at 25 °C, the results are shown in Figure 4b. It can be seen that the composites retained high removal efficiency over wide pH values (3–9). According to the literature,  $^{38}$  this work shows a strategy in acid and alkaline conditions and can be used in practical applications. To be noticed, the pH values of the solution increased under acidic conditions, which may suggest that the composites had a certain buffer to acidic conditions. The increase in pH value can be attributed to the fact that the  $Mg(OH)_2$  nanoplate participated in the reaction with hydrions more frequently due to its large specific surface area and alkalinity in acid situation. However, the pH value barely changed in the alkaline situation because the alkaline condition was beneficial to keep the  $Mg(OH)_2$  nanoplate structure stable.

Considering the future application of the material to cope with complex aqueous situations, experiments were performed to explore the performance of the material mainly against chloride ions.  $Cl^-(NaCl)$  was used as a competitive ion. The result is depicted in Figure 4c. It can be seen that with a higher  $Cl^-$  concentration, the removal efficiency of  $I^-$  would decrease to 60% even at a concentration of 200 mg/L. This confirmed that the  $Ag_2O-Mg(OH)_2$  plate composites had a certain anticompetitive ion ability.

Figure 4d shows the influence of the adsorbent concentration on the I removal efficiency. It can be seen that the removal efficiency was lower with an adsorbent content below 30 mg/L. However, with a high concentration of adsorbent, the removal efficiency of I- was stable. Moreover, when the adsorbent content increased to 30 mg/L, the removal efficiency of I- reached 90%, which effectively alleviated the influence of coprecipitation<sup>39</sup> between the target ions and competing ions. Then, the removal efficiency of I- returned to a high performance as the adsorbent concentration continued to increase. These results proved that the method of increasing the adsorbent would be a response to a high concentration of Cl<sup>-</sup> in the removal of I<sup>-</sup>. Although the ability to absorb I<sup>-</sup> was actually affected by Cl<sup>-</sup>, considering the balance between the I<sup>−</sup> removal efficiency and the cost of the adsorbent, the Ag<sub>2</sub>O− Mg(OH)<sub>2</sub> plate composites can be suggested as an effective method. Thus, the concentration of 20 mg/L adsorbent was acceptable to remove I<sup>-</sup>.

In practical applications, medical wastewater usually contains a high concentration of NaCl. In order to ensure that the adsorbent shows favorable performance, the concentration of NaCl was fixed as 100 mg/L. To determine the influence of the mass ratio between NaCl and NaI (Figure 4e), the concentration of I<sup>-</sup> was increased to explore the adsorption capacity of the adsorbent (20 mg) under a fixed NaCl concentration (100 mg/L). With an increase in I<sup>-</sup>, the adsorption saturation phenomenon occurred when the content of the adsorbent was fixed. The capacity of the saturation adsorption of I<sup>-</sup> under interference was calculated. When the

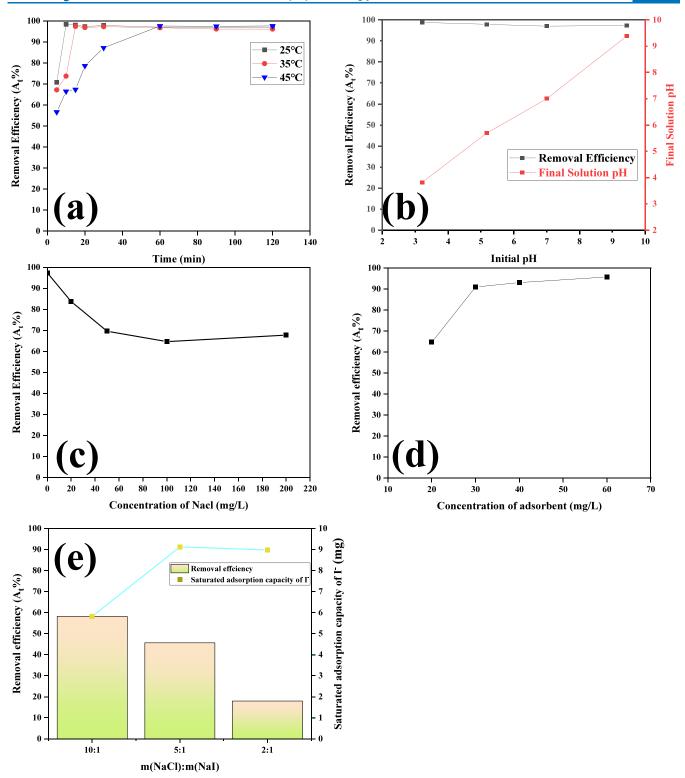


Figure 4. Removal efficiency of  $I^-$  by the  $Ag_2O-Mg(OH)_2$  plate composite at different temperatures (a) and pH values (b). Removal efficiency of  $I^-$  in the presence of the competitive ion  $Cl^-(c)$ . Effects of the adsorbent concentration on the  $I^-$  removal efficiency (d). Effects of  $I^-$  concentration on the  $I^-$  removal efficiency (e).

mass ratio changed from 10:1 to 2:1, the adsorption capacity first increased and then slightly decreased with increasing  $I^-$ . It can be inferred that the maximum saturation adsorption capacity was maintained at about 9 mg/L of NaI in the presence of a higher concentration of  $I^-$ . It is suggested that a higher concentration of  $I^-$  facilitated the adsorption capacity of  $I^-$ . To some extent, the removal efficiency of  $I^-$  by  $Ag_2O-$ 

 $Mg(OH)_2$  plate composites would be affected by the presence of competitive ions (Cl<sup>-</sup>).

**3.3. Kinetics of Adsorption.** Figure 5 shows the curves obtained by fitting two equations through calculations. Relevant statistics are also displayed in Table S1. The regression factor  $(R^2)$  values were all less than 0.900 under the pseudo-first-order kinetic equation and decreased with

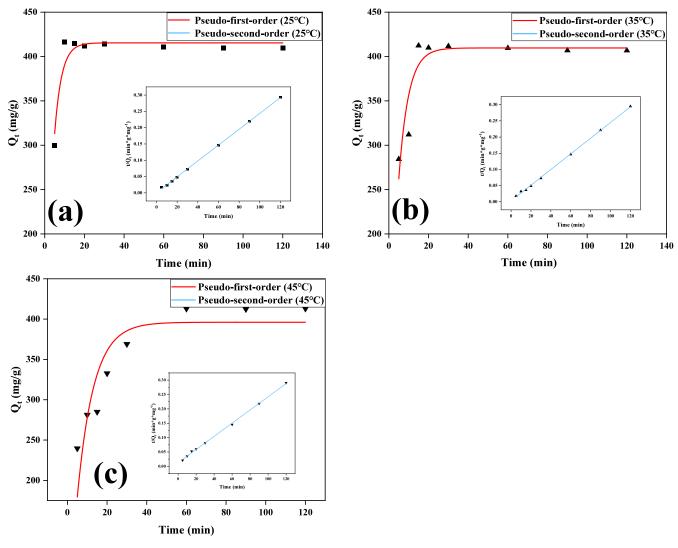


Figure 5. Adsorption kinetic curves of iodine by Ag<sub>2</sub>O-Mg(OH)<sub>2</sub> plate composites at temperatures of 25 (a), 35 (b), and 45 °C (c).

increasing temperature. Fitting the pseudo-second-order kinetic equation,  $R^2$  values reached 0.999 under all temperatures, which was closer to 1 than that of the pseudo-first-order kinetic equation. The I<sup>-</sup> adsorption results obtained by experiments  $(Q_{\rm exp})$  were quite similar to that obtained by calculation  $(Q_{\rm cal})$ . These results indicated that the  ${\rm Ag_2O-Mg(OH)_2}$  plate composites fit better with the pseudo-second-order kinetics. This also meant that the adsorption of I<sup>-</sup> uniformly occurred at various adsorption sites on  ${\rm Ag_2O}$  nanoparticles that were loaded on  ${\rm Mg(OH)_2}$  plates. Meanwhile, this phenomenon was also consistent with the TEM and SEM results. As discussed above, it can be considered that the adsorption process was chemisorption.

**3.4. Adsorption Mechanism.** After reaction with NaI, the element mapping results are displayed in Figure 6. Compared with Figure 2, the mapping of silver content decreased in a small range. However, the I element appeared, and the distribution of Ag and I elements highly coincided. This was also consistent with the analysis results of the kinetics. This demonstrated that AgI was formed in the process of contact and adsorbed on the surface of adsorbents. The fact that the morphology of the sample changed can be attributed to the fact that the composites used for characterization were collected after the reaction. The literature <sup>40</sup> shows that

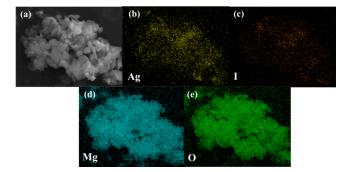


Figure 6. Elemental mapping analyses (a-d) and microstructure (e) of  $Ag_2O-Mg(OH)_2$  plate composites after the reaction.

 $Mg(OH)_2$  nanoplates may be dissolved in deionized water due to their solubility (9 mg/L) at 18 °C, and a higher temperature (25 °C) would aggravate the dissolution and result in shape change.

Surface analysis of Ag<sub>2</sub>O-Mg(OH)<sub>2</sub> composites was carried out by XPS before and after the I<sup>-</sup> reaction. As shown in Figure 7a, there were obviously different signals before and after the reaction. The I signal appeared after the reaction, which further demonstrated that I<sup>-</sup> was successfully adsorbed

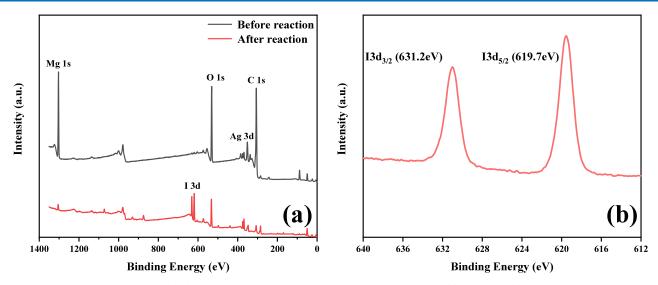


Figure 7. XPS spectra of Ag<sub>2</sub>O-Mg(OH)<sub>2</sub> plate composites before and after iodine adsorption (a) and I 3d (b).

on the composites. According to Figure 7b, the shape analysis revealed that the peaks at 619.7 and 631.2 eV corresponded to I  $3d_{3/2}$  and I  $3d_{5/2}$  peaks of AgI, <sup>41</sup> respectively, indicating that the reaction process of Ag2O–Mg(OH)<sub>2</sub> plate composites with NaI was a chemical adsorption reaction. The reaction equation of Ag2O–Mg(OH)<sub>2</sub> plate composites and I<sup>-</sup> can be described as below:

$$Ag_2O + 2I^- + H_2O = AgI + 2OH^-$$
 (6)

To compare the performance of the composites synthesized by the ex situ method,  $Ag_2O$  and  $Mg(OH)_2$  were ground in a quartz mortar at 25 °C for 30 min with a mass ratio of the two components identical to that used in the in situ method. Figure 8 shows the removal efficiencies of the two methods. As can be seen from Figure 8, the composites prepared by the ex situ method displayed a lower removal rate and lower removal efficiency even at a time of 120 min. The final adsorption efficiency was less than 60%, which confirmed that the ex situ method did not promote the capacity of the adsorbent. The ingredients of this adsorbent prepared by the ex situ method

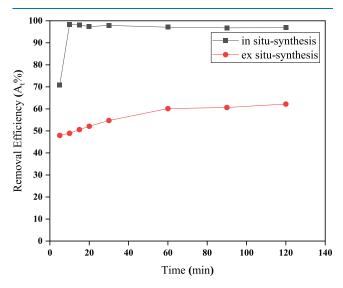


Figure 8. Removal efficiencies of the in situ and ex situ synthesis methods.

were used to conduct this experiment (Figure S1). SEM images of the ex situ ingredient materials are displayed in Figure S3. It can be seen that the synthesized Ag<sub>2</sub>O spherical nanoparticles aggregated as shown in Figure S3a, which reduced their removal efficiency on I<sup>-</sup>. Compared with the ex situ method, Ag<sub>2</sub>O particles and Mg(OH)<sub>2</sub> nanoplates were observed by fitting together morphologically, as shown in Figure S3b. The TEM image of the ex situ-synthesized adsorbent further confirmed that Ag<sub>2</sub>O particles cannot be anchored uniformly on the Mg(OH)<sub>2</sub> plate, which reduced its specific surface area and hindered the I<sup>-</sup> removal ability. Hence, this confirmed that the in situ method had a high removal efficiency of I<sup>-</sup>, and the composites had a wide potential for application in nuclear medical wastewater.

3.5. Cost Comparison of Ag<sub>2</sub>O-Mg(OH)<sub>2</sub> Plate **Composites.** To evaluate the cost, the commercial adsorbents were compared with Ag<sub>2</sub>O-Mg(OH)<sub>2</sub> plate composites. As can be seen from Figure S2, the composites had a much higher removal efficiency of I<sup>-</sup> compared with activated carbon(AC), XAD-4 resin, and 251  $\times$  8Cl resin. However, the 201  $\times$  7Cl resin represented nearly the same efficiency in 24 h contact. Hence, aiming at the cost and efficiency of the 201 × 7Cl resin and Ag<sub>2</sub>O-Mg(OH)<sub>2</sub> plate composites, further research was carried out. The cost comparison studies are shown in Table S2. It is clearly demonstrated that the  $Ag_2O-Mg(OH)_2$  plate composites exhibited excellent performance and outstanding efficiency in I- removal in the initial 60 min even with low adsorbent concentration (20 mg/L). The removal efficiency was 10 times higher than that of  $201 \times 7Cl$  resin (200 mg/L). Comprehensively, it is certain that the composites have the advantage of low cost for I removal and the potential for commercial application.

# 4. CONCLUSIONS

In this work, we successfully synthesized  $Ag_2O-Mg(OH)_2$  plate composites through an in situ synthesis method. The TEM and SEM test results confirmed that  $Ag_2O$  nanoparticles were uniformly distributed on the surface of the  $Mg(OH)_2$  plate. Due to the high selective absorption of  $Ag_2O$  and the large specific surface area of  $Mg(OH)_2$ , the adsorbent had a high removal efficiency for  $I^-$  (97.36%) during the adsorption process. The mechanism of the adsorbent was chemical

adsorption. Meanwhile, the composites maintained a high removal efficiency in a wide range of pH values (3–9) at room temperature. Compared with the ex situ-synthesized materials, the in situ synthesis process promoted the  $\rm I^-$  removal performance. In conclusion,  $\rm Ag_2O-Mg(OH)_2$  plate composites can be used as candidate materials for nuclear medical wastewater treatment.

#### ASSOCIATED CONTENT

## **Supporting Information**

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acsomega.4c09661.

Additional experimental details, comparison of adsorbents and simulated kinetic parameters (PDF)

#### AUTHOR INFORMATION

## **Corresponding Authors**

Chunyang Zhang — Department of Radioactive Waste Management, China Institute for Radiation Protection, Taiyuan 030006 Shanxi, P.R. China; Shanxi Provincial Engineering Research Center of Nuclear Facilities Decommissioning and Radioactive Waste Management, Taiyuan 030006 Shanxi, P.R. China; orcid.org/0009-0005-0376-0456; Email: 18984342715@163.com

Le Zhang — Department of Radioactive Waste Management, China Institute for Radiation Protection, Taiyuan 030006 Shanxi, P.R. China; Shanxi Provincial Engineering Research Center of Nuclear Facilities Decommissioning and Radioactive Waste Management, Taiyuan 030006 Shanxi, P.R. China; Email: lezhang95@163.com

# **Authors**

Bowen Zheng — Department of Radioactive Waste Management, China Institute for Radiation Protection, Taiyuan 030006 Shanxi, P.R. China; Shanxi Provincial Engineering Research Center of Nuclear Facilities Decommissioning and Radioactive Waste Management, Taiyuan 030006 Shanxi, P.R. China

Haoran Chu — Department of Radioactive Waste Management, China Institute for Radiation Protection, Taiyuan 030006 Shanxi, P.R. China; Shanxi Provincial Engineering Research Center of Nuclear Facilities Decommissioning and Radioactive Waste Management, Taiyuan 030006 Shanxi, P.R. China

Zhaofeng Liu — Department of Radioactive Waste Management, China Institute for Radiation Protection, Taiyuan 030006 Shanxi, P.R. China; Shanxi Provincial Engineering Research Center of Nuclear Facilities Decommissioning and Radioactive Waste Management, Taiyuan 030006 Shanxi, P.R. China

Yun Bai — Department of Radioactive Waste Management, China Institute for Radiation Protection, Taiyuan 030006 Shanxi, P.R. China; Shanxi Provincial Engineering Research Center of Nuclear Facilities Decommissioning and Radioactive Waste Management, Taiyuan 030006 Shanxi, P.R. China

Sicheng Chang — Department of Radioactive Waste Management, China Institute for Radiation Protection, Taiyuan 030006 Shanxi, P.R. China; Shanxi Provincial Engineering Research Center of Nuclear Facilities Decommissioning and Radioactive Waste Management, Taiyuan 030006 Shanxi, P.R. China Song Yang — Department of Radioactive Waste Management, China Institute for Radiation Protection, Taiyuan 030006 Shanxi, P.R. China; Shanxi Provincial Engineering Research Center of Nuclear Facilities Decommissioning and Radioactive Waste Management, Taiyuan 030006 Shanxi, P.R. China

Ning Zhao — Department of Radioactive Waste Management, China Institute for Radiation Protection, Taiyuan 030006 Shanxi, P.R. China; Shanxi Provincial Engineering Research Center of Nuclear Facilities Decommissioning and Radioactive Waste Management, Taiyuan 030006 Shanxi, P.R. China

Qingshan Yang — Department of Radioactive Waste Management, China Institute for Radiation Protection, Taiyuan 030006 Shanxi, P.R. China; Shanxi Provincial Engineering Research Center of Nuclear Facilities Decommissioning and Radioactive Waste Management, Taiyuan 030006 Shanxi, P.R. China

Yuheng Ma — Department of Radioactive Waste Management, China Institute for Radiation Protection, Taiyuan 030006 Shanxi, P.R. China; Shanxi Provincial Engineering Research Center of Nuclear Facilities Decommissioning and Radioactive Waste Management, Taiyuan 030006 Shanxi, P.R. China

Complete contact information is available at: https://pubs.acs.org/10.1021/acsomega.4c09661

#### **Author Contributions**

C.Z. conducted the experiments, analyzed/collected the data, and wrote and revised the manuscript. L.Z. provided the idea and designed the experiments. B.Z. and Z.L. revised the manuscript. H.C. provided project support. Y.B., S.C., and S.Y. gave valuable advice to prepare the manuscript. N.Z., Q.Y., and Y.M. collected data. This manuscript was written through contributions of all authors. All authors have given approval to the final version of the manuscript.

#### Notes

The authors declare no competing financial interest.

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