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OPEN Stiffness gradient of the beetle penis facilitates propulsion in the spiraled female spermathecal duct

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It is well known that sexual selection is the main driving force of substantial diversity of genitalia found in animals. However, how it facilitates the diversity is still largely unknown, because genital morpho/ physical features and motions/functional morphology of the structures in sexual intercourse are not linked for the vast majority of organisms. Here we showed the presence of material gradient and numerically studied an effect of stiffness gradient of the beetle penis during its propulsion through the female duct. We found that stiffness gradient on the penis essentially affects its propulsion. Microscopic investigation suggests the possibility that the tip of the hyper-elongated penis is softer than the rest of it, and our numerical model confirms that this type of distribution of stiffness gradient aids in faster propulsion than other types. This result indicates that previously ignored physical properties of genital materials are of crucial importance in evolutionary studies of genitalia.

Male and female genitalia evolve more quickly and yield remarkable diversity in comparison with other characters¹⁻⁵. This phenomenon has previously attracted attention of evolutionary biologists, and its mechanisms have been intensively investigated by sophisticated experiments^{4,6-15}. It is widely accepted that the immense diversity of genital structures is driven by sexual selection in general^{1,2,5,16}. Moreover most researches in this field were focused on the male genitalia¹⁷, however, it has been recently uncovered that females play an active role in sexual selection by active choice of males^{18,19} and that interactions between sexes are very important factors for genital evolution of both sexes^{20,21}.

Knowledge of how male and female genital properties affect physical interaction during sexual intercourse is essential in the evolutionary studies of genital structures. Since natural selection does not act directly on shapes, but rather influences shapes indirectly through functions, links between genital morpho-physical features and their functional significance are critically important to understand evolutionary mechanisms of diversification. Nevertheless biomechanics which challenges comprehensive understanding of kinematics and dynamics of movements in relation to the structural features have been largely ignored in this field, but recently this topic started to contribute more to our knowledge due to modern experimental techniques, elaborate modeling tools, and by increasing number of interdisciplinary studies^{15,22–27}.

Hereby we numerically modeled hyper-elongated male and female genitalia especially focusing on physical properties observed in cassidine beetles, to gain insights about how genital features affect penile propulsion that is an initial and vital process of male and female physical interactions during copulation. In these beetles, the male penises represent an elongated cuticular flagellum, transferring sperm, and female genitalia where the flagellum is inserted represent a partly cuticular and helical spermathecal duct including some reversal turns²⁸ called knots (Fig. 1). Recently impacts of the shapes of the female spermathecal duct on male penile propulsion were numerically evaluated in this system²⁴. Moreover for insect cuticular and fibrous structures, tenent setae of beetle tarsi were demonstrated to have longitudinal material and stiffness gradients²⁹, which result in specific mechanical behavior of the entire attachment system³⁰. Therefore, stiffness properties of the male flagellum and female spermathecal duct were hypothesized to be an important parameter, which might influence flagellum motion within the female spermathecal duct.

In order to test this hypothesis, we analyzed the autofluorescence composition of the genitalia based on the differences of different biopolymers using confocal laser scanning microscopy³¹. This method provides indications

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Figure 1. Schematics of female ducts (blue), male flagella (red) and male flagella guiding structures (green). Spheres on the male flagella show the tips of the male flagella. For simplicity, reversal turns (knots) are not depicted. (a) Mating is just stated; the tip of male flagella guiding structure is inserted to the female duct. (b) The male flagellum is fully inserted into the female duct.

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for the material composition of arthropod cuticle structures³¹. The effect of the estimated properties on the genitalia propulsion was then evaluated using the numerical model previously established by Filippov *et al.*²⁴ with certain modifications. The question of this study is how the male-female interactions during copulation are affected by the material properties of the genitalia. In the present paper we report on the stiffness gradient of the male flagellum along the duct, whereas no gradient was observed in the internal wall of the female spermathecal duct. This type of material distributions in the male and female genitalia showed the highest velocity in the numerical simulation, if compared to other variants of distributions of material properties.

Results

Autofluorescence composition along the flagellum. The confocal laser scanning microscopy analysis revealed a gradient in the autofluorescence composition along the flagellum (Fig. 2). Except for the apical regions, the flagellum exhibited strong green and red autofluorescences. The tips (nearly 1% of the total length: ca. $82 \mu m$, $97 \mu m$, $127 \mu m$) of the flagellum showed mainly blue autofluorescence inside the curve and green autofluorescence on another side (Fig. 2d,f). In the material of the spermathecal ducts of the females no longitudinal gradient in the autofluorescence composition (Fig. 2h). The internal wall showed mainly orange to green autofluorescence and the external layer shows the dominance of the blue autofluorescence. The duct showed blue autofluorescence in the outer part of the duct wall and mainly green and partially red autofluorescence in the inner part of the wall (Fig. 2g,h). Same tendency was observed, when we analyzed male and female structures simultaneously, but the females showed stronger intensity of green and red autofluorescence in comparison to that of the male (Supplementary Fig. 1).

Numerical simulation. We hereby applied the previous numerical model²⁴ in which we numerically created the fibrous male flagellum as an elastic uncompressible fiber and the highly helical spermathecal duct as an elastic channel (Figs 3 and 4; females: blue lines, males: red lines). Although the female spermathecal duct is not only helical but also the whole helical duct is convoluted in reality, not straightened²⁴, we created the female model excluding the convoluted shape of the whole helical duct as shown in Figs 3 and 4. For females, we included the knots on the duct, which were demonstrated to increase the male energy expenditure for penile propulsion in the previous study²⁴ (Figs 3 and 4). The end of the male flagellum was just pushed to propel it into the female spermathecal duct to imitate the genital motion during penile penetration.

Results of the simulations for the flagellum with uniform and gradient of rigidity (Figs 3 and 4) are summarized in Figs 5 and 6. Because the longitudinal material gradient was found only in the male flagellum and the inner wall of the female spermathecal duct showed constantly green to red autofluorescence, we focused on the analysis of the material gradient of the male flagellum below. First of all we analyzed the local deviation of the flagellum from the intact female duct axis along the x-coordinate of the duct for 4 cases: constantly soft, constantly hard, almost constantly soft with the hard end, and almost constantly hard with the soft end (Fig. 5). Each curve in Fig. 5 corresponds to the flagella rigidity distribution depicted in the Figs 3 and 4. There is a clear difference between the curves obtained for the female systems without and with the knots. This difference between them is mainly due to the various degrees of oscillations caused by the phase shift of the knots between segments of the flagellum and female duct having the same index *j*, which is produced by the phase shift around every knot *j*.

A correlation between maxima of the absolute tip velocity along the female duct and positions of the knots is presented in Fig. 6. Using Eq. 2 in the materials and methods, instant velocity of the flagellums' tip was calculated for each case as a function of time. However, for the comparison, this velocity is plotted here as a function of the tip coordinate x(1). Every curve here presents the velocity averaged over moving time window with the width comparable to the time interval between neighboring minima. The averaging makes the maxima in velocity more



Figure 2. Confocal laser scanning micrographs of flagella (for two individuals **a,b**, respectively) and spermathecal duct (**g**) of *Cassida rubiginosa*. (**c**-**f**) The details of the base (**c,e**) and the tips (**d,f**) of the flagella are digitally enlarged from the original images (**a,b**), respectively. The stripes are artifacts of image processing. (**g**) The spermathecal duct, the left end corresponds to the beginning of the spermatheca and the right end corresponds to the beginning of the vagina. (**h**) The details of the duct. We visualized the emitted wavelengths $420-480, \geq 490, \geq 560$, and ≥ 640 with blue, green, red and red, respectively.



Figure 3. 3D scheme of numerical experiments. Two extreme cases of the male flagellum stiffness are presented. (**a**) continuously soft. (**b**) continuously hard. The central axis of the female duct is shown by the blue line, the male flagellum is shown by the red line. The entire flagellum is inserted in the female spermathecal duct.







Figure 5. Local deviation distances of a male flagellum from a female duct axis along the x-coordinate of the channel for four cases presented in Figs 3 and 4. Corresponding cases are marked by arrows. Smooth curves represent cases for the channels without knots. Oscillating curves show the distances for the cases when male flagella had gradient and female channels had four knots.

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pronounced. Thick lines in the figure show the velocities calculated for the same systems without knots. The propulsion velocity strongly depends on the stiffness of the flagellum. The velocity for the rigid flagellum with





soft end is much higher than the same value for all other cases. Accelerated flagellum propulsion was observed at the knot sites.

Discussion

The CLSM results of the present study indicate longitudinal gradient in the material composition of the flagellum and the absence of such a longitudinal gradient in the female spermathecal duct. According to Michels and Gorb³¹, orange (which is a mixture of the green and red) to green autofluorescence and no autofluorescence gradient along the female spermathecal duct, observed in the inner wall, suggest that the inner wall is almost homogeneously composed of sclerotized cuticle. On the contrary, the observed autofluorescence compositions of the flagellum suggest that larger parts of the flagellum are mainly composed of sclerotized cuticle, while the flagellum tip contains mainly non-sclerotized cuticle and relatively high proportions of the rubber-like protein resilin, whose concentration increases towards distal end. For other cuticular outgrowths, such as hairy attachment pads reported for many insects^{32,33}, correlations between material and stiffness gradients were demonstrated recently^{25,29}. A simulation showed that such a stiffness gradient, found in the hairy attachment system, affects the mechanical behavior of the hairs during contact formation/breakage²⁴. In addition to it, the female structures, which we have analyzed simultaneously in the same CLSM scan with the male structures, had generally stronger intensity of green to red autofluorescence, which suggests larger thickness of the cuticular wall in females. These results inspired us to hypothesize that the beetle flagellum also may have a stiffness gradient and the inner wall of the spermathecal duct is constantly stiffer than the flagellum. Our model implemented those male and female genital properties clearly demonstrated that the stiffness gradient along the flagellum impacts flagellum's penetration in the relatively stiff helical-like counterpart of the female.

The flagellum that is equally stiff along its length results in a greater deformation between the original and penetrated positions of the female duct (Fig. 5). It means the flagellum simply "ignores" the duct's shape and its resultant mechanical disturbance which was demonstrated in Filippov *et al.*²⁴. Nevertheless, the absolute velocity of the flagellum is the slowest in this condition (Fig. 6). Contrary to these results, the hard flagellum with the soft tip, possibly reflecting the real beetle system, shows quite different results (Figs 5 and 6), especially the velocity. It seems that the soft end of the flagellum is flexible enough to quickly adjust small curvature in the duct, and at the same time, it is strongly pushed by the rigid basal part. In reality, not only the longitudinal stiffness gradient, but also a transverse stiffness gradient observed in the apical region of the flagellum, i.e. the relatively soft inner curve and the rigid outer curve, would aid the flagellum tip to adjust to the small curvature of the female duct. Interestingly, the uniform soft flagellum with the soft end, i.e. very big deformation of the female duct and/ or much slower velocity of the male flagellum (Figs 5 and 6). It is conceivable that a flagellum with lower transversal stiffness strongly absorbs propulsion forces that in turn decrease the degree of further propulsion. Thus, the results obtained from our simulations, strongly support the hypothesis that the stiffness gradient in the beetle flagellum facilitates penile propulsion.

In our previous study²⁴, the effects of variable shapes of female ducts on the penile propulsion were analyzed. It was found that certain parameters of the female duct, such as the presence of knots and the small curvature of the

duct, affect the velocity decrease of the penile propulsion or the increase of the energy expenditure for propulsion. Because sexual intercourses in the field can be disrupted by other males or by natural enemies, it is highly likely that males inserting a penis and ejaculating quickly can be preferred in the course of sexual selection. Therefore, the stiffness gradient of the flagellum capable of quick penetration of the female duct can be selected as a favorable structure for both males and females, even if it could increase the energy expenditure for male penile propulsion which was demonstrated in the previous study²⁴.

There are several sophisticated experimental studies investigating driving and stabilizing mechanisms of hyper-elongation^{7,13,15,28,34,35}. However, neither of the authors took into account the material properties of genitalia. It has been recently shown that the males with the cut off tip of the flagellum in bugs acquired lower paternity¹⁵. This result might be partly explained by the results of our simulation. It is likely that the absence of the softer tip causes troubles for sexual behavior, because of a less effective propulsion, although the question why the slower insertion causes lower paternity in the lab condition must be considered in further details. As Dougherty *et al.*¹⁵ pointed out, the functional morphology has been largely ignored in the studies of genital evolution. The hyper-elongated genitalia are ubiquitous in animals, not only in insects but also in vertebrates like ducks³⁶, and it is very interesting to broaden studying taxa for comparing the mechanical properties among animals. Our approach shed light on the importance of studying materials' properties with the combination of experimental and numerical approaches for better understanding evolutionary mechanisms of genitalia.

Materials and Methods

Autofluorescence composition of the male flagellum and female spermathecal duct. The autofluorescence composition of the flagellum was investigated with the confocal laser scanning microscope Zeiss LSM 700 (Zeiss, Germany). For this purpose, beetles *Cassida rubiginosa* (Chrysomelidae) were collected in Jena (Germany) in May 2014 and in June 2015, kept in plastic jars with fresh leaves of thistles *Cirsium* spp., (Asteraceae) and grew to the next generation of adults. The shape and measurements of the male flagellum and female spermathecal duct of this species had reported in Filippov *et al.*²⁴. Four males and three females were analysed. Of the treated samples, one male and female were analysed simultaneously to compare the intensity of autofluorescences between them. The flagella and spermathecal ducts were freshly dissected in the $1 \times$ phosphate butter solution (pH 7.4) (Carl Roth, Germany), and embedded in glycerine overnight. Subsequently, they were mounted on glass slides, and their autofluorescences were visualized, as described by Michels and Gorb³¹. The wave lengths of lasers 405, 488, 555, and 639 nm laser lines were used, and we applied a band-pass emission filter 420–480 and long pass emission filters transmitting light with wavelengths of \geq 490, \geq 560, and \geq 640, respectively. Then we visualized the emitted wavelengths 420–480, \geq 490, \geq 560, and \geq 640 with blue, green, red and red, respectively. All samples were observed using 10-fold objective lens with different digital zoom.

Numerical model. Here we have developed further a numerical model previously proposed in Filippov *et al.*²⁴. The model basically consists of two conceptual components: an elastic uncompressible fiber (flagellum), which can move inside an elastic channel. The transversal rigidity of the fiber and elasticity of the channel are adjustable. The flagellum motion is generated by pushing on its base by an external force. In the previous model, it was supposed that the female duct is generally stiffer than the flagellum, as it is suggested by our analysis of autofluorescence composition.

The flagellum was numerically constructed from a big number N (up to $N=10^5$) of elastically connected discrete segments. In the present study, we needed more accurate calculation than before and created more segments in comparison with the previous model²⁴. Each segment has a length of $dr \le 1 \mu m$ defined by a total length of the system L = 10 mm measured from the microscopic images for our model beetle, *Cassida rubiginosa*.

The flagellum model is provided with strong longitudinal stiffness k^{\parallel} which prevents extension and compression of the practically rigid segments and two components of elastic forces $\vec{f}^{elastic} = \{f^{\parallel}, f^{\perp}\}$: $\vec{f}_{jj\pm 1}^{\parallel} = k^{\parallel}(\vec{r}_j - \vec{r}_{r\pm 1})[1 - ((\vec{r}_j - \vec{r}_{r\pm 1})/dr)^2]$, and $\vec{f}_j^{\perp} = k^{\perp}(2\vec{r}_j - \vec{r}_{j+1} - \vec{r}_{j-1})$, acting between the neighboring nodes \vec{r}_j . Longitudinal force, $\vec{f}_{jj\pm 1}^{\parallel}$ tends to conserve a distance between the nodes \vec{r}_j and $\vec{r}_{j\pm 1}$ close to the equilibrium dr. Like in the previous model²⁴, we supposed that the transverse stiffness $k^{\perp} = const$ is much weaker $k^{\parallel} \gg k^{\perp}$

Like in the previous model²⁴, we supposed that the transverse stiffness $k^{\perp} = const$ is much weaker $k^{\parallel} \gg k^{\perp}$ than the longitudinal one. In the real system, the flagellum seems to have different stiffness along its length (see below), which was taken into account in the current analysis. It means that k^{\perp} varies from segment to segment. From preliminary experiments we expect that k^{\perp} should be a nonlinear function, which is almost constant at the beginning and quickly falls down near the end. For definiteness we apply:

$$k^{\perp} = k_0^{\perp} \left[1 - g \left(\frac{r_j - r_1}{r_N - r_1} \right)^{\alpha} \right]$$
(1)

Here parameters k_0^{\perp} and *g* determine general rigidity and a rigidity gradient along the flagellum. In particular, at g = 0, large/small constant k_0^{\perp} corresponds to the uniform hard/soft flagellum, respectively. If g = 0.99, then the tip of the flagellum is 100 times softer than its base. Using different combinations of the parameters, we analyzed four different variants of the system: constantly soft, constantly hard, almost constantly soft with the hard end, and almost constantly hard with the soft end. To reproduce the two last cases, we had used exponent $\alpha = 5$.

Female duct along the coordinate $X \in [0, L_x]$ was defined by its spiral core:

$$Y = A_0 \sin(2\pi X/\lambda_0) + R \sin(2\pi X/\lambda); \quad Z = Z_0(X) + R \cos(2\pi X/\lambda + \varphi(X))$$
(2)

with the parameters $R = L_x/30$; $\lambda = L_x/40$, $0.1L_x < A_0 < 0.5L_x$ and $0.2L_x < \lambda_0 < 0.4L_x$. It has secondary structure with some number N_{knots} of knot points at positions X_n , where direction of spiral rotation changes to a reverse one. The phase rotations were caused by the phase function $\varphi(X)$ defined as a sum of step-like functions $\varphi(X) = \sum_{n=1}^{N_{kopts}} (-1)^n [\pi/2 + \tan^{-1}((X - X_n)/2\tau)]$ with factors $(-1)^n = \pm 1$ for mutually opposite phase rotations around even and odd nods, respectively.

The female spermathecal duct is not only helical but also convoluted²⁴. However following the former paper²⁴, we concentrated on the role of spiral and knot geometries and neglected all the variations of the spiral core $Y_0 = A_0 \cos(2\pi X/\lambda_0) = 0$ and limited ourselves by the straight spiraled-duct only. Such spirals having four knots $N_{knots} = 4$ and different combinations of the flagellum rigidities are shown in Figs 3 and 4. In each figure, the spiral axis of the female elastic channel is shown by a blue line. The position of the flagellum inside the female channel is shown by red curves and the flagellum tip is marked by a red circle. Numerically, the female duct was defined as an elastic confinement acting on every segment $\{z_j(x_j), y_j(x_j)\}$ of the male flagellum by the returning forces: $f_y^{confinement}(X = x_j) = K(Y(X) - y_j)$; $f_z^{confinement}(X = x_j) = K(Z(X) - z_j)$, which are regulated by the elastic constant K.

For reflecting a probable uniform stiffness which is suggested by CLSM images, we fixed everywhere below, i.e. a general flagellum rigidity $k_0^{\perp} = K$ for the rigid and $k_0^{\perp} = 0.01K$ for the soft uniform flagellum (g=0), respectively. Parameters g = 0.99 and $k_0^{\perp} = K$ are chosen for the rigid gradient flagellum with the soft end and g = -99 and for $k_0^{\perp} = 0.01K$ the soft flagellum with the hard end.

The presence of liquid inside the channel was taken into account by introducing a proportional to the velocity \vec{v}_j damping force: $f_j^{damping} = \gamma \vec{v}_j$. This force was also added to the equations of motion of all the segments, which are the same as in previous study²⁴:

$$\frac{\sigma \bar{v}_j}{\sigma \tau} = f_j^{elastic} + f_j^{confinement} + f_j^{damping}$$
(3)

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Author Contributions

Y.M., S.N.G., A.E.F. and A.E.K. designed the research. A.E.F. established the mathematical model, and A.E.F. and A.E.K. analysed. Y.M. conducted the CLSM analysis. A.E.F., Y.M., S.N.G. and A.E.K. wrote the manuscript.

Additional Information

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