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Development of structure-tailored and composite magnetic-fluorescent microspheres through the PRI method

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SUMMARY

Multifunctional micro- and nanoparticles have found their applications in fields like medicine, display materials, cosmetics, and so on. Advances in these fields have been demonstrated to need scalable uniformly sized, mass-produced, and structured spherical particles. In this work, we proposed structure-tailored and multifunctional composite polymeric microspheres with tunable diameter size, by using a versatile and scalable in-fiber particle fabrication through the Plateau-Rayleigh capillary instability method. The results show that the characteristic shapes of the luminescence spectra of $CsPbBr₃$ remained similar before and after embedding in the microspheres. The luminescence intensity was stabilized at 85–90% of their original photoluminescence intensities over an extended period. Moreover, the photoluminescence lifetime of the fluorescent microspheres was increased by 9.03% compared to CsPbBr₃. The X-ray diffraction results revealed that there was no change in the crystal structure of the dopants before and after the encapsulation. Also, precise magnetic manipulation of Janus microspheres was successfully demonstrated.

INTRODUCTION

Multifunctional microspheres have several applications including medicine,^{[1](#page-8-0)} anti-counterfeiting,^{2,[3](#page-8-2)} remote manipulation, and displays.^{4–6} In most of the applications, the fluorescence and magnetization functions have been used more frequently. One type of multifunctional microspheres called Janus is a single particle having two regions with different properties.⁷ Recently, Janus microspheres have gotten great attention because of their asymmetric nature. The ability to integrate tailorable multifunctions in single particle has made them a smart building block for designing the next generation intelligent materials.^{[8](#page-8-5)} Several methods including microfluidic technique, surface modification, electrified co-jetting, and spinning disks technique have been utilized to fabricate Janus particles with different shapes, functionalities, and nature.^{9–11} For example, Li et al.^{[12](#page-8-7)} reported the fabrication of fluorescent-magnetic Janus microspheres by electrospraying. Chen et al.¹³ re-ported the fabrication of magnetic Janus photonic crystal microbeads with multiple fluorescence colors by microfluidic method. Yin et al.^{[10](#page-8-9)} demonstrated the Janus microspheres fabrication with magnetic-fluorescent parts via the microfluidic device. According to literature,^{14,[15](#page-8-11)} particles' application mostly depends on fabrication method and particle size. But, most of these wet methods used to prepare Janus particles have issues like large particle size dispersion,¹⁶ and low yield which prevent the wide use of these methods.¹⁷ So, a reliable and easy-to-use method to fabricate Janus particles with good control of shape, size, composition, and scalability is still considered a major challenge.

To address the challenges mentioned above, a physical top-down in fiber ''Plateau-Rayleigh capillary instability (PRI)'' method, which has several advantages over conventional wet methods, was proposed recently. By using this method, the fabricated particles have a clean surface, high yield as well as Janus structure with a diameter ranging from 100 µm down to 3 µm by optimizing parameters like temperature, preform feed speed, and fiber draw speed. Shabahang and A. F. Abouraddy et al., (2011) reported the first observation of PRI at the corecladding interface in multimaterial fiber.¹⁸ Later, Kaufman and Tao et al., (2012) have shown the ability of this in-fiber PRI method to fabricate the structured particles with uniform size by thermally drawing the multimaterial fibers.^{[16](#page-8-12)} Also, Tao et al., (2016) presented a scalable fabrication approach for digital designing the internal geometry of multimaterial photonic particles.^{[19](#page-8-15)} For magnetic-fluorescent Janus

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Figure 1. In-fiber polymer microspheres fabrication through PRI method

(A) Schematic of the preform-to-fiber thermal drawing process through a fiber drawing tower.

(B) A preform (d \sim 25 mm) has been thermally drawn into a fiber.

(C) Optical side view of the fiber during heat treatment at 380°C from 0 to 3 min.

(D) COC microspheres' ($d \sim 3$ to 30 μ m) SEM images.

microspheres fabricated by the in-fiber PRI method, we doped superparamagnetic Fe₃O₄ in one semi-sphere to get magnetic functionality, whereas for the other semi-sphere the CsPbBr₃ Perovskite quantum dots (PQDs) has been used for fluorescent functionality. Although most of the researchers have used fluorescent dye molecules to prepare composite fluorescence microspheres,^{[20](#page-8-16),[21](#page-8-17)} they have issues like unstable optical properties, narrow excitation, and wide emission wavelength.^{[22](#page-8-18)} To avoid these problems, we have selected CsPbBr₃ PQDs because they have exceptional photovoltaic and optoelectronic properties.^{[23–25](#page-8-19)} However, when exposed to light, heat or moister these PQDs show poor stability which limit their potential applications.^{[26–28](#page-8-20)} One way to overcome this issue is polymer encapsulation of these PQDs to make them more resistant against environmental factors.

In this work, structure-tailored and composite magnetic-fluorescent microspheres have been fabricated by using an efficient and versatile in-fiber PRI method.^{29–31} Here we are reporting the synthesis of composite magnetic-fluorescent microspheres from 100 µm down to 3 µm. The microspheres have been developed under the influence of surface tension, so their surface was extremely smooth. We have used a stackand-draw approach to put multiple cores in a single fiber to induce PRI simultaneously for mass production. It makes them highly suitable and potential candidates for many applications.

RESULTS AND DISCUSSION

We have used the in-fiber particle fabrication through the PRI method to prepare microspheres with tunable diameter as shown in [Figure 1.](#page-2-0) In this method, a centimeter-scaled model called ''preform'' is heated at a specific temperature to get a viscous state, and then stretched to get fibers. Multimaterial fibers have been realized using this technique during the last several years.^{32–36} The schematic of the preform-to-fiber drawing process is shown in [Figure 1A](#page-2-0), whereas [Figure 1](#page-2-0)B illustrates a section of fiber formed by thermal drawing and a conical-shaped preform obtained after melting. During this process, the temperature of the furnace was set around the softening temperature of the cladding material to maintain the continuity of the fiber and the intrinsic dimensional proportionality between the core and cladding.^{[16](#page-8-12)} The fibers after getting out of the heating zone were rapidly cooled to room temperature to prevent any axial instability phenomena. Typical prefabricated rods are shown in [Figure S1](#page-7-0). SEM of the cross-section show that the fibers retain the same core/cladding structure as the preform, and the dimensional ratios are consistent ([Figure S2](#page-7-0)).

The PRI was induced in the fiber by thermal treatment,^{[18](#page-8-14)} and the dynamics of heat treatment over time for breakup process has been shown in [Figure 1C](#page-2-0). At the low temperature the viscosity is large which keeps the core intact, but with the increase in temperature the viscosity decreased, and surface tension reduces the inertial viscous forces causing the instability growth until cylindrical fluid converted into droplets. A sinusoidal modulation emerges at the interface and the depth of this modulation continue to increase until the core converted into droplets.

The "mother" droplets were connected by a bridge until they detached and left small "satellite" microspheres in the middle.^{18,[37](#page-9-0)} These microspheres remain steady in the cladding after cooling down to room temperature. The N, N-dimethylacetamide solution (DMAC) has been used to dissolve the PSU, to release these microspheres.

This in-fiber PRI approach has several key benefits. First, the spherical microspheres with uniform and tunable diameters as well as with a wide diameter range can be prepared. Second, it has ability for mass production/scalability. A large number of microspheres can be fabricated by using stack-and-draw method, in which several cores in the same fiber breakup simultaneously. Third, the ability of this approach to fabricate microspheres with complex structures (core-shell, Janus, and beach ball) by designing and preparing the macroscopic preform with the required structure. The fluid instability theory describes that when a cylindrical fluid is encased in another fluid, a sinusoidal wave (wavelength: λ) will emerge at the liquid surface because of difference in materials' surface tensions, as shown in [Figure 1C](#page-2-0). The PRI process can be explained by the equation given below:

$$
\Delta P = \gamma \left(\frac{1}{R_1} + \frac{1}{R_2} \right) \tag{Equation 1}
$$

here R₁, and R₂ are the radius of curvature, surface tension coefficient is represented by γ , and ΔP describes the pressure difference. From two factors we can determine the diameter of spherical microspheres: (i) instabilities wavelength (λ) and (ii) rate of perturbations (τ). The perturbation rate " τ " can be calculated using the Tomotika's linear theory: $38,39$ $38,39$

$$
\tau = D_0 \mu_{\text{clad}} / \left[\gamma_i (1 - \eta^2) \Phi(\eta, \mu_{\text{core}} / \mu_{\text{clad}}) \right]
$$
 (Equation 2)

where D_0 is core diameter, μ is viscosity of the material, γ_i is interfacial surface tension, Φ is a defined function, 38 and $\eta = \frac{\pi D_0}{\lambda}$. When the heat-
ing time is greater than the a then conillans ing time is greater than the τ , then capillary instability has enough time to shrink the steady fluid to break-up into spherical microspheres. By controlling the core diameter " D_{o} " we can tune the final particle diameter "D" as illustrated below:^{[40](#page-9-3)}

$$
D = \sqrt[3]{3\pi/2\eta} D_o
$$
 (Equation 3)

Considering excellent thermal stability and exceptional optical properties of the COC, it has been selected as core material in this work.^{[41](#page-9-4)} Also, after fiber drawing, we need to remove the cladding material using selective solvent. Thus cladding materials should have opposite dissolution properties as compared with core material to ensure that the dissolution will not cause any loss of the core material. Furthermore, in PRI approach the heat treatment requires that the softening temperature of the cladding material should be higher than that of the core material. Considering this, polysulfone (PSU) was selected as the cladding material.

After getting expertise in fiber drawing process,^{42–47} we have analyzed and optimized different parameters like temperature, feed speed, and draw speed, to study their effect on the fiber diameter, which has linear relation with particle diameter [\(Equation 3\)](#page-3-0). The particle size con-trol was confirmed by SEM images of some selected samples shown in [Figure 1D](#page-2-0), with diameter range from \sim 30 µm to \sim 3 µm, highlighting the flexibility of the in-fiber PRI method in tuning particle size. This excellent tunability of diameter size from several millimeter to several nanometers is a key benefit of this approach which is difficult to realize by using the conventional wet methods. Also, we can control the particle size by optimizing the inner and outer diameters of preform.

The scalability of in-fiber particle fabrication through PRI using stack-and-draw approach was demonstrated as shown in [Figure 2](#page-4-0). We have integrated 200 COC rods in PSU cladding to create a preform, which was thermally drawn to get a fiber with 200 cores as shown in [Figures 2](#page-4-0)A and 2B. Then, this fiber was used to obtain polymer microspheres with uniform size after heat treatment at 380°C to induce PRI as shown in [Figure 2C](#page-4-0).

SEM images have shown that the microspheres had clean surfaces and were not adherent to each other ([Figures 2D](#page-4-0) and 2E). For particle size analysis, we used the previously reported method of calculating 100 microspheres in SEM images by the ImageJ software.⁴⁸ The size results of the distribution are shown in [Figure 2](#page-4-0)F. It showed that the distribution was very narrow, with an average D \sim 3.15 \pm 0.16 µm. This stack-and-draw approach significantly increased the yield of microspheres by several orders of magnitude. Additionally, the optical transmission microscopy images revealed that due to the barrier of the cladding material between the cores, despite the close proximity of the cores to each other $(\sim20 \text{ }\mu\text{m})$, they remain in place after heat treatment in the form of regularly arranged three-dimensional arrays.

We have fabricated the fluorescent composite microspheres CsPbBr₃@COC through PRI approach as shown in [Figure 3](#page-5-0). The solution blending method was used to mix a 10% doping ratio of inorganic CsPbBr₃ with the COC matrix. After optimizing the parameters like composition, mixing time, and temperature, the enhanced doping effect has been achieved. The cores with fluorescence function ([Figure S3\)](#page-7-0) were integrated with the cladding to form the preform. Then the fiber drawing and particle processing were conducted similarly as has been done for undoped samples. The photograph of the fluorescent polymeric microspheres under ambient light and UV excitation, fabricated through PRI method, was shown in [Figure S4](#page-7-0).

The confocal laser scanning microscopy (CLSM) luminescence images of two representative microspheres (size \sim 100 µm) have been shown in [Figures 3A](#page-5-0) and 3B, and the fluorescence results demonstrated that the CsPbBr₃ microspheres have been effectively encapsulated within the polymer microspheres. To explore the spatial distribution of CsPbBr₃ in the composite microspheres, we scanned a randomly selected fluorescent microsphere using the z stack mode of the CLSM. As shown in [Figure 3](#page-5-0)C, the CsPbBr3@COC displayed uniform and bright fluorescence in every randomly selected focal plane, indicating uniform dispersion of the fluorescent substance throughout the microspheres. Additionally, as revealed by the X-ray diffraction (XRD) results in [Figure 3](#page-5-0)D, typical crystal diffraction peaks were observed alongside the amorphous structure corresponding to the polymer matrix, which closely match the structure of CsPbBr₃ (PDF No. 18–0364).

Figure 2. Scalable in-fiber polymer microspheres fabrication

(A) Schematic diagram of a multicore preform thermally drawn into fiber, then the cores were annealed to form spherical droplets and released from the cladding by selective dissolution.

(B) Optical image of fiber cross-section with 200 COC cores in the PSU cladding.

(C) Fiber side view optical transmission image after inducing PRI.

(D) SEM image of 3 µm (average diameter) COC microspheres in good number.

(E) Zoomed-in SEM image of some microspheres from (D) exhibiting clean and smooth surface.

(F) The size distribution of COC microspheres.

The optical properties of the fluorescent microspheres were also characterized. [Figure 3](#page-5-0)E shows the normalized fluorescence excitation and emission spectra of CsPbBr₃@COC microspheres and CsPbBr₃. The results reveal that the characteristic shapes of the luminescence spectra of CsPbBr₃ remained similar before and after embedding in the microspheres. However, its photoluminescence (PL) peaks were blue shifted from 520 nm to 515 nm compared to the CsPbBr₃. This indicates that the size of the PQDs decreased after being doped into the COC.^{[49](#page-9-7)[,50](#page-9-8)} To observe the stability of CsPbBr₃@COC microspheres' fluorescent property, PL intensity spectra has been recorded after every 24 h for seven days. [Figure 3F](#page-5-0) displays that all emission peaks for the fluorescent microspheres were stabilized at 515 nm. The luminescence intensity had a decay phenomenon (~15%) in the first 1–2 days, and then the green samples were stabilized at 85–90% of their original PL intensities in the subsequent time.

Also, the UV-Vis spectra has been shown in [Figure S5](#page-7-0), CsPbBr₃ has a characteristic absorption peak at 515 nm while the pure COC microspheres have no prominent absorption peak. The combined effect of these two materials has produce an insignificant absorption peak at 515 nm for CsPbBr₃@ COC microspheres. The time-resolved PL spectra of CsPbBr₃ and CsPbBr₃@COC samples were fitted using a tri-exponential function.⁵

$$
I_{(t)} = A_1 \exp\left(-\frac{t}{\tau_1}\right) + A_2 \exp\left(-\frac{t}{\tau_2}\right) + A_3 \exp\left(-\frac{t}{\tau_3}\right)
$$
 (Equation 4)

where $I_{(t)}$ is the emission intensity that changes with time, τ_1 , τ_2 , τ_3 are the lifetimes of different decay processes, and A_1 , A_2 , A_3 are the coefficients at these lifetimes.⁵

Figure 3. In-fiber fluorescent composite microspheres fabrication through PRI

(A and B) Bright-field and fluorescence images (excited by a 405 nm laser) of two fluorescent composite microspheres with diameters of about 100 mm. (C) A series of CLSM luminescence images of sections of a microsphere, going from middle to bottom.

(D) XRD patterns of fluorescent composite microspheres.

(E) Fluorescence emission spectra of CsPbBr₃ and composite microspheres.

(F) PL intensity curves of the fluorescent microspheres dispersed in DMAC for a week.

(G and H) Decay curves and fitting results of CsPbBr₃ measured at 520 nm and composite microspheres measured at 515 nm.

$$
\tau_{\text{avg}} = \frac{A_1 \tau_1^2 + A_2 \tau_2^2 + A_3 \tau_3^2}{A_1 \tau_1 + A_2 \tau_2 + A_3 \tau_3}
$$
 (Equation 5)

The results [\(Figures 3](#page-5-0)G and 3H) show that the average PL lifetime of CsPbBr₃ at 520 nm is 41.29 ns and that of the particles at 515 nm is 45.02 ns, which is an improvement of 9.03%. This means that non-radiative transitions are weakened and energy losses are reduced.⁵² This may be because the surface of CsPbBr₃ is secondarily passivated by the flexible and dense COC polymer chains, which affects the radiative recombination of charge carriers and thus can effectively increase the fluorescence lifetime.

We have prepared the magnetic-fluorescent Janus microspheres by using this efficient and versatile in-fiber PRI method as illustrated in [Figure 4](#page-6-0). A magnetic-fluorescent composite COC cylindrical rod has been designed and fabricated. This rod has two-halves which were obtained by using a homemade customized mold. The one-half of the cylinder was doped with CsPbBr₃, while the other half was doped with $Fe₃O₄$ nanoparticles. Then this rod has been integrated with PSU cladding and thermally drawn to get the fiber. To obtain the magnetic-fluorescent Janus microspheres, the fiber drawing and particle processing were conducted in a similar way as has been done for undoped samples.

Fluorescent and magnetic functionalities of the Janus core was shown in [Figures 4](#page-6-0)A, 4B and 4C. The photograph of the core rod has been shown in [Figure 4A](#page-6-0). The fluorescence properties of the half-cylindrical core containing CsPbBr₃ has been shown in [Figure 4](#page-6-0)B, emitting bright

Figure 4. In-fiber fluorescent-magnetic Janus microspheres fabrication through PRI

(A–C) The Janus core of the preform processed through the customized mold, demonstrates dual functionality.

(D–F) CLSM luminescence images of the Janus particles, show clear hemispheric division.

(G) XRD patterns of Fe₃O₄, CsPbBr₃, and Janus particles.

(H) Fluorescence emission spectra of CsPbBr₃ and Janus particles.

(I) Hysteresis loop of Janus microspheres.

(J and K) Schematic and optical images showing the rotational motion of Janus particles under an external magnetic field.

green fluorescence under UV light, while the other half shows no response to UV light excitation. And the [Figure 4](#page-6-0)C demonstrates the magnetic properties of the semi-cylindrical core containing $Fe₃O₄$ nanoparticles. It can be seen that the core rod is attracted in mid-air by an external magnetic field (generated by a ferromagnet). The CLSM was used to examine the distribution of the fluorescent material in the Janus microspheres. [Figures 4D](#page-6-0), 4E and 4F revealed that CsPbBr₃ is uniformly distributed on the fluorescent half of the microspheres. Whereas the other half containing Fe₃O₄ nanoparticles produced no fluorescence. Moreover, consistent with the earlier description, the images exhibit clear boundaries between the two hemispheres, mirroring the structure prior to the induction of PRI by heat treatment. This characteristic offers a novel approach for the future digital design of the multifunctional structured polymer microspheres. The XRD results for magnetic-fluorescent Janus microspheres [\(Figure 4G](#page-6-0)) proves that the composite particles were successfully prepared because the diffraction peaks of composite Janus particles coincide with those of Fe₃O₄ as well as CsPbBr₃, demonstrating that before and after the encapsulation there is no variation in the crystal structure of the dopants.

We have also investigated the optical properties of the magnetic-fluorescent Janus microspheres, the normalized fluorescence excitation and emission spectra of Janus microspheres and CsPbBr₃ were shown in [Figure 4H](#page-6-0). Similar to the fluorescent microspheres mentioned above, the PL emission peak of Janus microspheres undergoes a 5 nm blue-shift phenomenon. The Janus microspheres' magnetic properties were also characterized by using vibrating sample magnetometer (VSM). The results in [Figure 4](#page-6-0)I show that the magnetic induction intensity of the microspheres is estimated to be \sim 1.5 emu g $^{-1}$, which makes them good candidate for potential applications like magnetic separation and display.

Remote manipulation of these Janus microspheres has been demonstrated and full dynamics were captured as shown in [Figures 4J](#page-6-0) and 4K. The movement and orientation of the Janus microspheres can be manipulated by the external-magnetic field, thus making them useful for

fluorescent switching and displays. Given the superparamagnetic property of the doped iron oxide nanoparticles, we used two ferromagnets to manipulate Janus microspheres dispersed in DMAC and captured the dynamic process by the fluorescence microscope with a camera. It has been discovered that when the magnet is placed in such a way that its rotation axis is parallel to the substrate [\(Figure 4J](#page-6-0)), the rotation of the magnet causes the Janus particles to form multiple angles and ranges of the fluorescent face, and when the magnet is placed in such a way that its rotation axis is perpendicular to the substrate [\(Figure 4K](#page-6-0)), the Janus structured microspheres follow the magnet in the in-situ rotation.

Conclusions

In this work, a versatile, flexible, and scalable in-fiber microspheres fabrication through PRI method has been used to prepare undoped COC, CsPbBr₃ doped COC, and magnetic-fluorescent Janus (CsPbBr₃//Fe₃O₄@COC) microspheres with diameter size ranging from ~100 µm down to \sim 3 µm. By optimizing the temperature, preform feed-speed and fiber draw-speed, we have fabricated the microspheres with smooth surface and narrow size distribution ($C_V < 5\%$). Also, the stack-and-draw approach enabled us to increase the microspheres' yield by several orders of magnitude by placing 200 fibers in preform core to induce the PRI simultaneously. The CsPbBr₃@COC microspheres' fluorescence lifetime was enhanced by 9% and the fluorescence intensity remained stable around 90% of the initial intensity, whereas the Janus microspheres have demonstrated good response to external magnetic field for remote manipulation in both parallel and perpendicular directions of rotation. This work will be a key addition toward fabricating multifunctional polymeric particles with tunable size and complex structures.

Limitations of the study

Although the present work has played a significant role in the large-scale preparation of functional and/or complex structured microspheres, we found nonuniform doping of functional materials for microspheres with small diameter (\sim 3 µm). This is due to the fact that when doping has been done using the solution mixing method, the functional materials are agglomerated and thus their sizes are usually beyond the submicron range and some of the dopant material escapes from the substrate when the core breaks up. More efforts are needed to improve the doping for smaller diameter particles. One possible way is to use surface modification to enhance the binding capacity of the dopant to the matrix material.

STAR+METHODS

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SUPPLEMENTAL INFORMATION

Supplemental information can be found online at [https://doi.org/10.1016/j.isci.2024.110407.](https://doi.org/10.1016/j.isci.2024.110407)

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AUTHOR CONTRIBUTIONS

H.Y. and K.J. investigated, designed, and conducted the experiments. H.Y. and X.L. fabricated the fibers and tested the particles. H.Y., K.J., X.L., Y.Z., X.D., H.H., X.Q., and G.T. wrote the manuscript with contributions from all authors. All authors discussed the results. X.Q. and G.T. supervised the research.

DECLARATION OF INTERESTS

The authors have no relevant financial interests in this article and no potential conflicts of interest to disclose.

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STAR+METHODS

KEY RESOURCES TABLE

RESOURCE AVAILABILITY

Lead contact

Further information and requests for resources and reagents should be directed to and will be fulfilled by the lead contact, Xvsheng Qiao (qiaoxus@zju.edu.cn)

Materials availability

This study did not generate new unique reagents.

Data and code availability

- All data reported in this paper will be shared by the [lead contact](#page-10-4) upon request.
- This article does not report original code.
- Any additional information required to reanalyze the data reported in this article is available from the [lead contact](#page-10-4) on request.

EXPERIMENTAL MODEL AND STUDY PARTICIPANT DETAILS

This study does not use experimental methods typical in the life sciences.

METHOD DETAILS

COC/PSU preform fabrication

(i) The pellets (millimeter-sized, 8007, Zeon Corporation, Japan) were purchased to the obtain a cylindrical rod of COC with diameter \sim 2 mm and length $~60$ mm by thermally pressing them at 240°C using a customized mold between the thermos-compressor. (ii) Purchased PSU (P-1700, Solvay, USA) pellets were placed into a mold measuring 70 mm in length, 27 mm in width, and 27 mm in height, then they were transformed into a cuboid rod by using the hot press at 290°C. Next, the cuboid PSU rod was processed into a round rod (diameter ~25 mm, Length ~70 mm) through a table-top lathe. Several parallel straight holes slightly larger than COC cylinders were drilled in the PSU section by using a bench top drill. (iii) Inserted the COC rods into the PSU holes for a monolithic preform. Then, the core/cladding structured preform was consolidated at 200°C for 1h in a vacuum oven.

CsPbBr3 preform fabrication with fluorescent function

(i) The cyclohexane solution (Sigma-Aldrich) has been used to dissolve the COC pellets and stirring was done for 1h (600 rpm, 70°C) to obtain pure and transparent COC/cyclohexane solution. (ii) Then, the CsPbBr₃ phosphors with doping ratios ranging from 1%–10% were mixed into the above solution and stirred at 600 rpm for 12 h. (iii) To completely dry the compound the evaporation has been in a vacuum furnace. (iv) Then, the compound was thermally pressed at 240°C through a customized mold between the thermos-compressor to form cylindrical rods with diameter \sim 2 mm and length \sim 60 mm. Then, these rods were inserted into the PSU tube for a fluorescent preform.

Janus structured preform fabrication with fluorescent-magnetic multifunction

(i) Both the fluorescent and magnetic composites were fabricated by the dispersion of the functional particles in COC matrix through chemical solution. (ii) Two half-cylindrical rods were machined separately using another customized mold with a diameter ~2 mm and length ~60 mm by using two kinds of composites. Then, they were thermally combined into a round rod. (iii) The round rod was inserted into the PSU tube for a fluorescent-magnetic Janus preform.

Fiber thermal drawing

To provide the suitable pull when the bottom of the preform is just starting to soften, a 2 mm diameter hole was drilled horizontally at 5 mm from the bottom of the preform. A stainless-steel wire with 10g weights was passed through the bottom hole. Then, the assemblies formed were fitted to the custom thermal drawing tower, and the preform was thermally drawn into fibers at 260°C. The preform feeding speed was set and maintained at 1 mm/min, the drawing speed was set around 1.5 m/min. To ensure the uniform diameter of fiber with the diameter 600 ± 10 µm the drawing speed was monitored and controlled accordingly.

Particles fabrication through the PRI method

The core/cladding structured fiber was cut into 20 cm long pieces and subsequently fixed on customized glass sheets with length \sim 20 cm and width \sim 2.5 cm with a high temperature tape. Next, these glass sheets were placed in a tube furnace and heat treated at 380°C for 5min. The continuous heat input caused the fibers to soften again and provided the driving force for the core to break into particles by PRI.

Particle release

The PSU cladding has been dissolved with 99.0% DMAC (Sigma-Aldrich) at 100°C for 30–40 min, to release the particles. The washed sample was centrifuged at 15000 rpm for 5min, then the supernatant was removed. After adding DMAC again, the ultrasound was performed for 5min to further dissolve the PSU cladding. This process was repeated five to six times until all the PSU has been removed and the solvent was evaporated, leaving the COC particles on the substrate.

Characterization

Images of the fibers were collected by an optical microscope (OM, CX40M, China) in transmitted light mode. The morphology of particles and the cross-sectional images of the fiber were studied by using a scanning electron microscope (SEM, Zeiss Gemini SEM 360, Germany), and the acceleration voltage was 5 kV. Elemental compositions and distribution of the fiber and the doped material were analyzed via energy dispersive X-ray spectrometer (EDS), during the test, the acceleration voltage was set to 15 kV and the working distance was 8.5 mm. The fluorescence images of CsPbBr₃ in the COC microspheres were captured using a confocal laser scanning microscope (CLSM, Leica TCS SP5 II, Germany) by exciting at 405 nm. The vibrating sample magnetometer (VSM, Lakeshore 7404, USA) was used for room temperature magnetic analysis with a field up to 2.0 T, while the pole head diameter was 5cm, the pole pitch was 16.2 mm, the sensitivity was 5 \times 10⁻⁷ emu, and the measurement ranged from 5 \times 10⁻⁷ emu-10³ emu. X-ray diffraction spectra of Fe₃O₄ nanoparticles, CsPbBr₃ powder, and composite microspheres were obtained with the X-ray diffractometer (XRD, Bruker D8 Advance, Germany) equipped with Cu Ka radiation, and the measured angle ranged from 10° to 80° , the scan speed was $0.14^{\circ}/s$. Photoluminescence emission spectra and decay curves were recorded on an FLSP920 spectrometer (Edinburgh Instrument Ltd., Livingston, UK) with a 405nm EPLED laser. In this process, the fluorescence lifetime monitoring wavelengths of fluorescent microspheres and perovskite samples were 515nm and 520nm, respectively. Optical absorption spectra have been observed by using the ultraviolet-visible-near infrared spectrophotometer (Shimadzu, UV-4100, Japan). The measurement ranged from 700 nm to 250 nm, and the scan speed was 300 nm/min.

QUANTIFICATION AND STATISTICAL ANALYSIS

Data were expressed as mean \pm SEM (standard error of mean).