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 $\begin{array}{l} \textbf{Citation:} \mbox{ Tan G, Huang Y, Sheng H (2016)} \\ \mbox{Magnetoelectric Response in Multiferroic} \\ \mbox{SrFe}_{12}O_{19} \mbox{ Ceramics. PLoS ONE 11(12): e0167084.} \\ \mbox{doi:10.1371/journal.pone.0167084} \end{array}$ 

**Editor:** Yogendra Kumar Mishra, Institute of Materials Science, GERMANY

Received: September 16, 2016

Accepted: November 9, 2016

Published: December 9, 2016

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**Data Availability Statement:** All relevant data are within the paper and its Supporting Information files.

**Funding:** This work was supported by the Hubei Natural Science Foundation (under the contract no. 2014CFB166) and the Open fund of State Key Laboratory of Advanced Technology for Materials Synthesis and Processing (Wuhan University of Technology) under the contract no. 2016-KF-15. The funders had no role in study design, data collection and analysis, decision to publish, or preparation of the manuscript. **RESEARCH ARTICLE** 

# Magnetoelectric Response in Multiferroic SrFe<sub>12</sub>O<sub>19</sub> Ceramics

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## Abstract

We report here realization of ferroelectricity, ferromagnetism and magnetocapacitance effect in singleSrFe<sub>12</sub>O<sub>19</sub>ceramic at room temperature. The ceramics demonstrate a saturated polarization hysteresis loop, two nonlinear I-V peaks and large anomaly of dielectric constant near Curie temperature, which confirm the intrinsic ferroelectricity of SrFe12O19 ceramicswith subsequent heat-treatment in O2atmosphere. The remnant polarization of the SrFe<sub>12</sub>O<sub>19</sub> ceramic is estimated to be 103µC/cm<sup>2</sup>. The ceramic also exhibits strong ferromagnetic characterization, the coercive field and remnant magnetic moment are 6192Oe and 35.8emu/g, respectively. Subsequent annealing SrFe<sub>12</sub>O<sub>19</sub> ceramics in O<sub>2</sub> plays a key role on revealing its intrinsic ferroelectricity and improving the ferromagnetism through transforming  $Fe^{2+}$  into  $Fe^{3+}$ . By applying a magnetic field, the capacitance demonstrates remarkable change along with B field, the maximum rate of change in  $\varepsilon$  ( $\Delta \varepsilon$ (B)/ $\varepsilon$ (0)) is 1174%, which reflects a giant magnetocapacitance effect in SrFe<sub>12</sub>O<sub>19</sub>. XPS and molecular magnetic moment measurements confirmed the transformation of Fe<sup>2+</sup> into Fe<sup>3+</sup> and removal of oxygen vacancies upon O2 heat treatment. These combined functional responses in SrFe<sub>12</sub>O<sub>19</sub> ceramics opens substantial possibilities for applications in novel electric devices.

### Introduction

Multiferroics is a class of functional materials that simultaneously exhibit ferroelectricity and ferromagnetism in a single structure [1-3]. They can demonstrate not only the magnetic or electric polarization but also the desired magnetoelectric (ME) coupling between the two orders leading to multifunctional performance, such as electric field controlled magnetic data storage or vice versa [4]. This unique coupling feature has a tremendous impact on technology, with potential application for spintronic devices, solid-state transformers, high sensitivity magnetic field sensors, and actuators [5]. As part of the technological drive toward device miniaturization, considerable effort has been devoted to the combination of electronic and magnetic properties into one multifunctional material, i.e., a single device component that can perform more than one task [5–9]. Such idea of combining two orders in one single compound has stimulated a vast research of new multiferroic materials [10–16]. Except the most heavily



**Competing Interests:** The authors have declared that no competing interests exist.

reported multiferroic compounds, such as BiFeO<sub>3</sub> [1, 4, 5], TbMnO<sub>3</sub> [17] and DyMnO<sub>3</sub> [18], some ferrites with hexagonal structures, termed as hexaferrites, have been found to show such ME effects as magnetic field induced ferroelectrics and drawn our attention [19–21]. Although several Y-type and Z-type hexaferrites were reported to demonstrate some ME effects and remarkable changes in polarization upon a magnetic field [22–25], the ME effect in these ferrites is small, their pure electric polarization or ferroelectric features (P-E loops) arestill absent and the magnetism is weak [26]. For applications, however, it will be necessary to generate simultaneously ferroelectricity and ferromagnetism, together with giant ME effects in one single compound at room temperature. Hence, it is a long standing challenge in the research of multiferroics to improve the operating temperature [26] and the ME sensitivity [21, 27].

M-type lead hexaferrite (PbFe<sub>12</sub>O<sub>19</sub>) has demonstrated coexistence of large ferroelectricity and strong ferromagnetism at room temperature [28. 29]. However, lead (Pb) is a kind of toxic element and PbFe<sub>12</sub>O<sub>19</sub> is not an environment-friendly material. SrFe<sub>12</sub>O<sub>19</sub>, instead, is a leadfree M-type hexaferrite and environment-friendly. It has attracted a lot of attention because of its non-toxicity, excellent magnetic properties and wide application in various fieldsuch as magnetic recording and high-frequency devices [30, 31]. Recently, the dielectric and ferroelectric features of M-type hexaferrites, such as BaFe<sub>12</sub>O<sub>19</sub> single crystal, have attracted some attentions [32-34]. However, the authors claimed that M-type barium hexaferrite, belongs to quantum paraelectrics due to the electric dipole of a FeO<sub>5</sub> bipyramid [32,33]. This kind of conclusion conflicts with the reported intrinsic ferroelectricity of PbFe<sub>12</sub>O<sub>19</sub> [29]. After careful analysis of the structure data of the BaFe<sub>12</sub>O<sub>19</sub> and SrFe<sub>12</sub>O<sub>19</sub> single crystals [32-34], we found that the XRD patterns of the  $BaFe_{12}O_{19}$  and  $SrFe_{12}O_{19}$  single crystals are not consistent with that of magnetoplumbite-5H structure for M-type hexaferrites, i.e., the strong diffraction peaks from {110}, {007} and {114} lattice planes are absent. Those single crystals exhibited much higher symmetric structure than M-type hexaferrites. In addition, the single crystals were grown in a sealed furnace, which could result in heavy oxygen deficiency and induce the formation of large amount of oxygen vacancies and  $Fe^{2+}$  inside the crystals. Such crystals could producelarge current leakage during the electronic measurement and would appear a pseudo paraelectric phenomenon. Therefore the conclusion of quantum paraelectrics in those  $BaFe_{12}O_{19}$  and  $SrFe_{12}O_{19}$  single crystals [32–34] are not comparable with the ferroelectric behavior of PbFe<sub>12</sub>O<sub>19</sub> specimen with magnetoplumbite structure. Actually, the doubtful ferroelectric property of SrFe<sub>12</sub>O<sub>19</sub> ceramics with magnetoplumbite structure had already been reported several years ago in our previous study [35]; however, its ferroelectric hysteresis loops differ significantly from classic ferroelectric counterparts and resembled "bananas" due to the current leakage. Its ferroelectricityremains controversial and the banana-shaped P-E loops are not convincing evidence for its ferroelectricity [36]. The ME effect of  $SrFe_{12}O_{19}$  has also not been investigated yet. Under this consideration, we optimized the fabrication process of the specimen by subsequent annealing  $SrFe_{12}O_{19}$  specimen in oxygen atmosphere so as to remove the oxygen vacancies and transform  $Fe^{2+}$  into  $Fe^{3+}$ . In this way, the current leakagewould be greatly reduced and a saturated P-E loop could appear as we did in PbFe<sub>12</sub>O<sub>19</sub> specimens [29]. In this paper, we will then present the improved ferroelectric feature, enhanced impedance property, large dielectric anomaly near the Curie temperature, nonlinear I-V peaks, remarkable ME response, together with strong ferromagnetism in the M-type hexaferrite of  $SrFe_{12}O_{19}$ ceramic specimen with subsequent O<sub>2</sub> annealing process.

### **Materials and Methods**

We started with the preparation of nano-crystalline SrFe<sub>12</sub>O<sub>19</sub> powders by polymer precursor procedure. Strontium acetate (Sr(CH<sub>3</sub>COO)<sub>2</sub>•3H<sub>2</sub>O) (99.0%, Aladin) and ferric

acetylacetonate (C<sub>15</sub>H<sub>21</sub>FeO<sub>6</sub>)(99.9%, Alfa Aesar) were used as starting material. First of all, 0.2467g strontium acetatewas dissolved in 15 mL glycerin to form a clear solution. The solution was distilled in a rotary evaporator at 120°C for 1 h to remove the water trapped in Sr (CH<sub>3</sub>COO)<sub>2</sub>•3H<sub>2</sub>O. The distilled solution was transferred into a 50 mL flask, which was moved into a glove box. In order to avoid hydrolysis of the  $C_{15}H_{21}FeO_6$  compound in air, the following chemical process was carried out inside a glove box with argonatmosphere. 4.026 g of ferric acetylacetonate was weighed and dissolved in a mixture solution of 100 mL anhydrous ethanol and 70 mL acetone in a 250 mL three-neck flask inside the glove box. The solution was stirred at 70°C for 6 hours to ensure that ferric acetylacetonate was fully dissolved. Subsequently, the strontium and ferric precursor solutions were mixed together. Here, the molar ratio of strontium to iron was set to 1:9.5~10 to balance the Sr loss during the heat treatment process. Afterwards, 45 mL ammonia solution and 15 mL solution of polyethylene glycol were poured into the above mixture solution. The dispersion solution was maintained at 70°C under stirring for 24 hours and then moved out of the glove box. The water and organic molecules were removed by centrifuging the dispersion solutionat 12000 rpm for 30 minutes. The remaining colloid powders were calcined at 450°C for 1 hour. The powders were grinded in a agate mortar for 1 hour and then calcined again at 800°C for another hour to ensure total removal of organic molecules. In this way, pure SrFe<sub>12</sub>O<sub>19</sub> powders in a single phase were obtained. 0.060 g of SrFe<sub>12</sub>O<sub>19</sub> powders were weighed and pressed in a module into a pellet, which was then sintered at 1150°C for 1 hour into a solid ceramic specimen. The ceramic pellet was subsequently annealed in pure O2 at 800°C for 3 hours. Then the ceramic pellet was turned over with upside down and the annealing process was repeated again for another 3 hours. After the furnace was cooling down to room temperature, the ceramic was heat-treated in pure  $O_2$  once more at 700°C for 3 hours. In this way, the oxygen vacancies could be removed and  $Fe^{2+}$  would be fully transformed into  $Fe^{3+}$ , so as to greatly enhance the resistance of the ceramics and reduce the current leakage during the following ferroelectric measurement. Phase identification of the  $SrFe_{12}O_{19}$  powder and ceramic was performed by X-ray powder diffraction (XRD) with Cu-K $_{\alpha}$  radiation. Magnetization was measured using a physical property measurement system (PPMS). For dielectric and ferroelectric measurement, both surfaces of the ceramic pellets were coated with silver paste as electrodes which was heat treated at 820°C for 15 min; the P-E hysteresis loop was measured using a lab-constructed instrument, referred to ZT-IA ferroelectric measurement system. The temperature-dependent dielectric properties were measured by an LCR instrument (HP 8248A). The complex impedance spectrum was measured upon a electrochemical station (Chenghua) within the frequency range of 0.01Hz ~ 1MHz. The magnetocapacitance parameters of the SrFe<sub>12</sub>O<sub>19</sub> pellet were measured using a Wayne Kerr 6500B LCR station by applying a variable magnetic field.

### **Results and Discussion**

### 1. Structure Identification of SrFe<sub>12</sub>O<sub>19</sub> compound

Fig 1a shows the X-Ray diffraction (XRD) pattern of the as-prepared SrFe<sub>12</sub>O<sub>19</sub> specimen, the underneath lines in red color are the standard diffraction spectrum of SrFe<sub>12</sub>O<sub>19</sub> (PDF#33–1340). The single-phase SrFe<sub>12</sub>O<sub>19</sub> powders has been fabricated by sintering at 1150°C for 1h and subsequently annealed in O<sub>2</sub> by 3 steps for a total duration of 9 hours with 3 steps wise.

It can be seen from Fig 1 that all the diffractions peaks of the oxygen annealed specimen match well with the corresponding ones from the standard cards (*PDF#33–1340*), indicating the formation of pure  $SrFe_{12}O_{19}$ . No diffraction peaks from any second ferrite phases or impurity compounds have been indexed in the pattern, revealing the stability of the magnetoplumbite structure  $SrFe_{12}O_{19}$  being sintered at 1150°C. This diffraction pattern is completely



Fig 1. (a) XRD pattern of  $SrFe_{12}O_{19}$  with  $O_2$  annealing process. (b) the standard diffraction pattern of the  $SrFe_{12}O_{19}$ (PDF#33–1340) being marked by discrete red lines.

different from that of reported  $SrFe_{12}O_{19}$  single crystals [32–34], which exhibit much higher symmetry and is lacking the strongest diffraction peaks form {110}, {007} and {114} lattice planes of typical M-type hexaferrites. Since the structure of our fabricated  $SrFe_{12}O_{19}$  ceramics is different from those  $SrFe_{12}O_{19}$  crystals reported in the literatures [32–34], the symmetry and electric properties should also differ significantly.

### 2. Electric Properties of SrFe<sub>12</sub>O<sub>19</sub> Ceramics

In order to check out if oxygen annealing process could remove the oxygen vacancies and transform  $Fe^{2+}$  into  $Fe^{3+}$ , we measured the complex impedance spectrum of the  $SrFe_{12}O_{19}$  ceramics with and without  $O_2$  annealing by an electrochemical station. The annealing process was carried out in 3 steps, firstly the sintered ceramic was heat treated in  $O_2$  atmosphere in a sealed tube furnace at 800°C for 3 hours, then the specimen was turning over with upside down and once again annealed at the same temperature for another 3 hours, finally the annealed specimen was heat treated at 700°C for 3 hours. The complex impedance of PbFe<sub>12</sub>O<sub>19</sub> can be expressed as follows:

$$Z = Z' + jZ' = \frac{R}{1 + (\omega RC)^2} - j\frac{\omega R^2 C}{1 + (\omega RC)^2}$$
(1)

and the module of the complex impedance is expressed as:

$$|\mathbf{Z}| = \sqrt{\mathbf{Z}'^2 + \mathbf{Z}''^2} \tag{2}$$



Fig 2. Modules of the complex impedance for (a) the conventional  $SrFe_{12}O_{19}$  ceramics being sintered at 1150°C in air only, (b) the sintered ceramic was subsequently annealed in pure oxygen atmosphere at 800°C for 3 hours, (c) the annealed ceramic was flipping over and once again heat treated in O<sub>2</sub>at 800°C for another 3 hours.

Then we measured the complex impedance spectra of the specimens at each annealing step to show how the properties continually improve as the  $Fe^{2+}$  transforms to  $Fe^{3+}$ . Fig 2 exhibits the modules of complex impedance for the  $SrFe_{12}O_{19}$  ceramics without and with oxygen heattreatment, respectively. The modules represents the magnitude of the impedance or electric resistance, which reflects concentration of oxygen vacancies and  $Fe^{2+}$  in  $SrFe_{12}O_{19}$  ceramics. The higher is the module, the lower is the concentration of these charge carriers.

The impedance module or electric resistance of the specimen with  $O_2$  heat-treatment is much higher than that of the ceramic without  $O_2$  treatment within the whole frequency region. The electric resistance (impedance module) of the SrFe<sub>12</sub>O<sub>19</sub> ceramic without  $O_2$  annealing process is only  $1.8 \times 10^3 \Omega$ , which is enhanced to  $1.82 \times 10^5 \Omega$  after first step  $O_2$  treatment. The electric resistance is further promoted to  $7.9 \times 10^6 \Omega$  at a frequency of 0.01 Hz after the second step  $O_2$  annealing process. The third step annealing process didn't change the module of impedance very much. The total electric resistance (impedance module) of the SrFe<sub>12</sub>O<sub>19</sub> ceramic was enhanced by a factor of 4389 after annealing in  $O_2$  in 3 steps wise. The great enhancement of the resistance reveals the drastic reduction of the concentration of the oxygen vacancies and full conversion of Fe<sup>2+</sup> into Fe<sup>3+</sup>, since the current leakage from oxygen vacancies and electronic hopping between Fe<sup>2+</sup> and Fe<sup>3+</sup> has been precluded.

Fig 3a represents the complex impedance spectrum of  $SrFe_{12}O_{19}$  ceramic without subsequent  $O_2$  annealing process. The spectrum is composed of a small Cole circle with a diameter of 215 and a large Cole one with a diameter of 1627. Each circle represents a circuit composed of a capacitor and a resistor which are connected in parallel. The two linked Cole circles could



Fig 3. Complex impedance spectrum of the SrFe<sub>12</sub>O<sub>19</sub> ceramic within the frequency range of 0.01 Hz to 1 MHz, (a) for the ceramic being sintered at 1150°C in air only; (b) for the sintered ceramic with subsequent annealing in O<sub>2</sub>.

then be expressed as two such equivalent series connected circuits, as being shown in Fig 4. The small Cole circle contributes from the grain boundaries and the large one from the grains in  $\text{SrFe}_{12}\text{O}_{19}$  ceramics. Fig 3(b) demonstrates a more complicated impedance spectrum for  $\text{SrFe}_{12}\text{O}_{19}$  ceramics after O<sub>2</sub> annealing process. The equivalent circuitfor the spectrum could also be expressed as two series linked circuits, each one is composed of a capacitor and a resistor being parallel connected (Fig 4). Each Cole circle corresponds to one individual circuit, one for grains and the other one for grain boundaries. Similarly, the spectrum is composed of a small Cole circle and a big half Cole circle, the diameter of the small one is estimated to be  $9.0 \times 10^5$  and that of large one is  $9.8 \times 10^6$ . Obviously, the contribution of the impedance from both grain boundaries and grains in  $\text{SrFe}_{12}\text{O}_{19}$  ceramics with subsequent O<sub>2</sub> heat-treatment have been greatly enhanced in comparison with that without O<sub>2</sub> annealing process. Both real and imaginary parts of the impedance have been promoted more than 1000 times after O<sub>2</sub> heat-treatment.



Fig 4. The equivalent circuit for the complex impedance of SrFe<sub>12</sub>O<sub>19</sub> ceramics, the scheme is composed of two series linked subcircuits with a capacitor and a resistor parallelly connected.

doi:10.1371/journal.pone.0167084.g004

### 3. The Impact of O<sub>2</sub> Treatment on Charge Transfer by XPS

The heat treatment of the sintered  $SrFe_{12}O_{19}$  ceramics in oxygen atmosphere plays a key role on enhancement of their electric resistance through removal of oxygen vacancies and transformation of  $Fe^{2+}$  into  $Fe^{3+}$ . The change in concentration of these charge carriers could be detected by X-ray photoemission spectrum (XPS). We collected XPS data for two specimens, one is sintered  $SrFe_{12}O_{19}$  ceramic without  $O_2$  heat treatment, the other one is the  $SrFe_{12}O_{19}$ ceramic with subsequent  $O_2$  heat treatment at 3 steps wise. We did analysis on Fe 2p energy levels and shallow region of the valence bands for the two specimens.

Fig 5 shows the spectra of Fe 2p energy levels for sintered  $SrFe_{12}O_{19}$  ceramics with and without subsequent O2 annealing process. The Fe 2p3/2 peaks are centered at 710.4 eV and 709.68 eV for O<sub>2</sub> treated specimen and non-O<sub>2</sub> treated specimen, while that of Fe 2p1/2 peaks are positioned to 723.84 eV and 723.09 eV for O2 and non-O2 treated specimens, respectively. There appear chemical shifts of 0.72eV and 0.75 eV for Fe 2p3/2 and 2p1/2 lines between the two specimens, respectively. Both Fe 2p1/2 and 2p3/2 spectra are asymmetric and could be fitted into two symmetric peaks (Fig 5). The binding energies of the upper Fe 2p3/2 and 2p1/2lines are fitted to be 711.41 eV and 710.5 eV, while that of lower fitting lines are positioned to 709.94 eV and 709.4 eV for O2 and non-O2 treated specimens, respectively. The chemical shifts of the fitting Fe 2p lines are displayed in the insets of Fig 5. Usually, the binding energies of 2p states of  $Fe^{2+}$  are lower than that of  $Fe^{3+}$ . For example, the binding energy of Fe 2p3/2 in FeCl<sub>3</sub> was measured to be 711.3 eV [37], while that in FeCl<sub>2</sub> was 710.6 eV [37]. There was a chemical shift of 0.7 eV for the Fe 2p3/2 state between  $\text{FeCl}_3$  (Fe<sup>3+</sup>) and Fe Cl<sub>2</sub> (Fe<sup>2+</sup>). In our case, the binding energy of upper Fe 2p3/2 lines hifts from 710.5 eV to 711.41 eV after SrFe<sub>12</sub>O<sub>19</sub> ceramic was heat treated in O<sub>2</sub>. The chemical shift of 0.91 eV appears between two specimens. The binding energy of upper Fe 2p3/2 line at 711.41 eV for O<sub>2</sub> treated specimen is consistent with the value of Fe  $2p_3/2$  line in FeCl<sub>3</sub> (Fe<sup>3+</sup>) compound [37], indicating the existence of full Fe<sup>3+</sup> in O-treated specimen. The lower binding energy of upper Fe 2p3/2 line at 710.5 eV indicates the existence of  $Fe^{2+}$  in non-O<sub>2</sub> treated specimen. Both upper and lower Fe 2p3/2 and 2p1/2 states in non-O<sub>2</sub> treated SrFe<sub>12</sub>O<sub>19</sub> ceramic specimen indicates the existence of Fe<sup>2+</sup> due to the chemical shifts. The binding energies of Fe 2p3/2 and 2p1/2 states shift toward higher energy side after the SrFe<sub>12</sub>O<sub>19</sub> ceramics were subsequently annealed in O<sub>2</sub> atmosphere, indicating the transformation of  $Fe^{2+}$  ions into  $Fe^{3+}$  ions with O<sub>2</sub> treatment.

Such charge transfer in Fe ions could be further confirmed by the Fe 3d states within the valence band region. Fig 6 shows valence band structure of  $SrFe_{12}O_{19}$  ceramic with and without  $O_2$  treatment. There is large difference between the two spectra either in peak positions or the density of states. There are 7 peaks being marked by A, B,...,G in Fig 6. The binding energies and attribution of each peak are summarized in Table 1. Considering calculated electron density of states (DOS) of BiFeO<sub>3</sub> and SeFe<sub>12</sub>O<sub>19</sub> [38,39], we may assign both peaks A and B to the hybridized Fe 3d-O 2p states, peaks C and D to O 2p levels, peaks E, F and G to O 2s state which splits into 3 sub-energy levels. By comparing with the two valence band spectra, we could find that the density of hybridized Fe 3d-O 2p states (peaks A&B) has been enhanced after the specimen was  $O_2$  heat treated. The increment in density of Fe 3d state indicates more Fe<sup>3+</sup> ions existing in the  $O_2$  treated specimen than that in non- $O_2$  treated one, since Fe<sup>3+</sup> ions have one more unpaired 3d electron to be hybridized with O 2p electrons than Fe<sup>2+</sup> ions. Both Fe 2p and 3d states in XPS spectra of  $SrFe_{12}O_{19}$  ceramics confirmed the transformation of Fe<sup>2+</sup> into Fe<sup>3+</sup> after the ceramics were subsequently annealed in pure  $O_2$  atmosphere.

It can be seen from Fig <u>6</u> that there appear full O 2p and 2s states in O<sub>2</sub>-treated SrFe<sub>12</sub>O<sub>19</sub> ceramic, while two O 2p states of peaks C and D are absent in non-O<sub>2</sub> treated SrFe<sub>12</sub>O<sub>19</sub> ceramic. The density of O 2s states (peaks E, F and G) in O<sub>2</sub>-treated specimen are much higher





Fig 5. XPS spectrum for Fe 2p energy levels of the sintered  $SrFe_{12}O_{19}$  ceramics (a) with  $O_2$  treatment and (b) without  $O_2$  treatment. The insets display the upper Fe2p1/2 and Fe 2p2/3 lines for the two specimens, respectively.

than that of  $SrFe_{12}O_{19}$  ceramic without  $O_2$  heat treatment, the intensity of peaks E and F increases from around 8306 (Fig 6b) for the non- $O_2$  treated specimen to around 18922 (Fig 6a) for the  $O_2$  treated specimen. The great enhancement of density of O 2s and O 2p states indicates largely reduction of oxygen vacancies for the  $SrFe_{12}O_{19}$  ceramics after  $O_2$  heat





Fig 6. Valence band spectra of  $SrFe_{12}O_{19}$  ceramics (a) with  $O_2$  heat treatment and (b) without  $O_2$  heat treatment. The dotted lines marked the top of the valence band.

treatment. When the  $SrFe_{12}O_{19}$  pellet was sintered inside a sealed furnace into ceramics, large numbers of  $Fe^{2+}$  would be formed and the excess oxygen would exist in the form of oxygen vacancies due to oxygen deficiency. The oxygen vacancies, however, are positively charged only and have no such 2s and 2p electrons as those around the atomic nucleus in oxygen ions. Therefore the density of O 2s and 2p states are much more depressed in the valence spectrum (Fig 6b) of non-O<sub>2</sub> treated  $SrFe_{12}O_{19}$  ceramics due to the appearance of high concentration of oxygen vacancies. The higher is the content of oxygen vacancies, the lower is the valence electron density. After the  $SrFe_{12}O_{19}$  ceramics are subsequently heat treated in pure O<sub>2</sub> atmosphere,  $Fe^{2+}$  ions are oxidized to  $Fe^{3+}$  and oxygen vacancies could be greatly reduced and be replaced by oxygen ions, as such the density of O 2s and 2p states are greatly improved. Therefore, the appearance of additional two O 2p states (peaks C and D) as well as the great enhancement of the density of O 2s states confirm the removal or great reduction of oxygen vacancies after the specimen was annealed in O<sub>2</sub> atmosphere. This result is consistent with the

#### Table 1. Valence band states assignment.

Peak	Α	В	С	D	E	F	G
Binding Energy	4.18(eV)	6.22(eV)	10.06(eV)	13.27(eV)	20.32(eV)	22.37(eV)	25.73(eV)
Assignment	Fe3d+O2p	Fe3d+O2p	O 2p	O 2p	O 2s	O 2s	O 2s

doi:10.1371/journal.pone.0167084.t001



Fig 7. Plot of dielectric constant as a function of temperature for SrFe<sub>12</sub>O<sub>19</sub> ceramics w treatment at frequencies of (a) 1kHz, (b) 10kHz and (c) 100 kHz.

enhancement of electric resistance after the specimen was heat treated in  $O_2$ . Meanwhile, the valence band edge of  $SrFe_{12}O_{19}$  shifts upwards 0.39 eV after it was annealed in  $O_2$  atmosphere.

### 4. Dielectric Relaxation of O2-Treated SrFe12O19 Ceramics

We then measured the dielectric relaxation behavior of  $O_2$  treated SrFe<sub>12</sub> $O_{19}$  ceramicsby a HP4284A LCR instrument. Fig 7 shows the temperature-dependent dielectric constants of the specimen at different frequencies of 1kHz, 10kHz and 100 kHz. At 1kHz, there appear three peaks, locating at 174°C, 368°C and 490°C (Fig 7a), the first two peaks are similar to that of PbFe<sub>12</sub> $O_{19}$  corresponding to two kinds of phase-transitions [29]. Similarly, the first peak  $T_d$  could be assigned to the ferroelectric to anti-ferroelectric phase transition, while the second one ( $T_m$ ) to the anti-ferroelectric to para-electric phase transition. The maximum dielectric constant at  $T_d$  is 2621. The third peak is attributed from a complicated phase transition. Since the dielectric constant ( $\epsilon$ ) becomes negative when temperature is higher than 527°C (Fig 7), the phase structure could then be assigned to a so-called "left hand materials (LHM)" whose dielectric constant is less than 0. Therefore the third peak ( $T_1 = 527°C$ ) is proposed to be the phase transition from para-electric phase to LHM.

The first transition peak is sensitive to the frequency, the larger is the frequency, the higher is the transition temperature. When the frequency increases from 1 kHz to 10 kHz, the first transition peak shifts from 174°C to 199°C and the maximum dielectric constant drops from 2261 to 1394. Further increasing the frequency from 10 kHz to 100 kHz, this peak shifts to



**Fig 8.** Modified Curie-Weiss law calculation. (a) Logarithm of  $(1/\epsilon - 1/\epsilon_d)$  as a function of logarithm of  $(T-T_d)$  at 10 kHz. and (b) logarithm of  $(1/\epsilon - 1/\epsilon_m)$  as a function of logarithm of  $(T-T_m)$  at 100 kHz for the SrFe<sub>12</sub>O<sub>19</sub> ceramic being sintered at 1150°C for 1 hour and subsequently annealed in O<sub>2</sub> for 9 hours with 3 steps wise.

239°C and the maximum dielectric constant decreases from 1394 to 847. However, the second transition peaks didn't move accordingly, while the third peak ( $T_1$ ) moves to the opposite direction, the higher is the frequency, the lower is the transition temperature.

The temperature of the first dielectric constant peak show large shifts with frequencies, suggesting that  $SrFe_{12}O_{19}$  is a relaxor ferroelectric compound with a diffuse phase transition. At 1kHz, the maximum  $\varepsilon$ -T peak (490°C) demonstrates a strong ferroelectric to antiferroelectric phase transition, associated with a broad  $\varepsilon$  (*T*) anomaly near the vicinity of the transition temperature. These kinds of dielectric anomalies at different frequencies provides additional evidence for the ferroelectricity of SrFe<sub>12</sub>O<sub>19</sub>.

Upon the anomalies of the dielectric constants, we then made the calculation of the reciprocal dielectric constants as a function of temperature using modified Curie-Weiss law, being expressed as follows:

$$\frac{1}{\varepsilon} - \frac{1}{\varepsilon_{\rm m}} = C(T - T_{\rm m})^{\gamma} \tag{3}$$

where  $\gamma$  is the critical exponent, representing the degree of diffuseness of the transition, and *C* is a Curie–Weiss-like constant.  $\varepsilon_m$  is the maximum dielectric constant at temperature of transition peak T<sub>m</sub>. For a sharp transition,  $\gamma = 1$ , the materials are called normal ferroelectrics. Diffuse transitions lie in the range  $1 < \gamma < 2$  [40], whereas at  $\gamma = 2$  the materials correspond to a so-called "complete" diffuse phase. When  $\gamma > 2$ , the materials would take a diffuse phase transition from ferroelectrics to anti-ferroelectrics or antiferroelectrics to paraelectricity [29].



Fig 9. (a) The saturated ferroelectric polarization hysteresis (P-E) loop, and (b) a plot of current as a function of voltage (I-V curve) of  $SrFe_{12}O_{19}$  ceramic. The ceramic has been sintered at 1150°C for 1 hour and subsequently annealed at 800°C in pure oxygen for a total duration of 9 hours in 3 steps wise. The measurement was made at a frequency of 33Hz and room temperature (300K).

Fig 8 shows plots of Ln(1/ $\varepsilon$ -1/ $\varepsilon_d$ ) as a function of Ln(T-T<sub>d</sub>) at 10 kHz and Ln(1/ $\varepsilon$ -1/ $\varepsilon_m$ ) as a function of Ln(T-T<sub>m</sub>) at 100kHz for SrFe<sub>12</sub>O<sub>19</sub> ceramic, respectively. Linear fitting to the experimental datausing Curie-Weissformula derives out the slope of the fitting lines, which were determined to be  $\gamma = 2.3$  and 2.2 at frequencies of 10 KHz and 100kHz, respectively. The calculated lines following Curie-Weiss formula fit well with the experimental data points. The linear relationship between Ln(1/ $\varepsilon$ -1/ $\varepsilon_m$ ) and Ln(T-T<sub>m</sub>) reveals that the temperature dependence of the dielectric constant obeys the Curie–Weiss law, providing additional evidence for the relaxor ferroelectric feature of the SrFe<sub>12</sub>O<sub>19</sub> ceramics.

### 5. Ferroelectric Polarization of SrFe<sub>12</sub>O<sub>19</sub> Ceramics

The ferroelectric P-E loop of the SrFe<sub>12</sub>O<sub>19</sub> ceramics without O<sub>2</sub> heat-treatment was looking like a "banana" (Figure E in S1 File) [35], which had drawn lots of doubts on the validity of its ferroelectricity. Considering that the "banana" shaped P-E loop (Figure E in S1 File) could be induced by current leakage and the necessity of confirming the validity of its ferroelectricity, we then heat treated the SrFe<sub>12</sub>O<sub>19</sub> ceramics in pure oxygen atmosphere for total duration of 9 hours with 3 steps wise, so as to greatly enhance its resistance through reducing the concentration of charge carriers. The great reduction of the concentration of charge carriers, such as oxygen vacancies and Fe<sup>2+</sup> by annealing the ceramics in oxygen, could dramatically reduce the current leakage and thus saturate the ferroelectric hysteresis loop of the SrFe<sub>12</sub>O<sub>19</sub> ceramics.

Fig.9 shows a fully saturated ferroelectric hysteresis (P-E) loop of the  $SrFe_{12}O_{19}$  ceramic with  $O_2$  annealing process. A drastic variation of the polarization appears in the vicinity of the

specimen's coercive field at around 10 kV/m. Further increasing the applied field up to 25 kV/ m, the polarization of the ceramic gradually approaches to saturation along with a concave arc line (Fig 9a).

When the applied field decreases, the polarization remains at the value of saturation because most of the ceramic's domains still align themselves along the electric field's direction. The spontaneous polarization, which is equal to the saturation value of the electric displacement extrapolated to the zero-field strength, remains almost constant with external field variations. This result reveals that all the electric displacement dipoles have aligned themselves along the direction of the external field until the external field was less than the negative coercive field of the ceramics. When the applied field switched to the reversal direction, the spontaneous polarization demonstrated a hysteresis and changedthe direction suddenly at the position of negative coercive field. The polarization voltage changes signs to be negative and approaches to the negative saturated value along with a reversal concave arc line (Fig 9a) within the field range of -10 kV/m to -25 kV/m. The remnant polarization in this classic hysteresis loop is estimated to  $be103\mu C/cm^2$ , which is around 8.3 times higher than that  $(15\mu C/cm^2)$  $cm^2$ ) of SrFe<sub>12</sub>O<sub>19</sub> ceramics without subsequent heat treatment in O<sub>2</sub> [35]. Therefore subsequent annealing  $SrFe_{12}O_{19}$  ceramics in oxygen not only saturated the hysteresis loop, but also greatly improved the remnant polarization value through reducing the current leakage, which results from the removal of oxygen vacancies and the transformation of  $Fe^{2+}$  to  $Fe^{3+}$  [28, 29]. Similar ferroelectric hysteresis loops being measured on different SrFe<sub>12</sub>O<sub>19</sub> ceramic specimens are supplied in the S1 File (Supplementary Materials), so as to confirm the reliability and repetitiveness of ferroelectric data.

The last evidence for the validity of ferroelectricity for SrFe<sub>12</sub>O<sub>19</sub> ceramics would be attributed from the appearance of two current peaks at I-V plot (Fig 9b) along with the polarization switching. When the ferroelectric polarization is switching, the screening surface charges flow from one electrode to the other one and create momentarily a sudden change of current. In the current versus voltage plot, this will result in two peaks with reversal directions as being shown in Fig 9(b). The two nonlinear I-V peaks show very clearly the switching phenomenon of the polarization and does not present any linear current component (or current leakage component). The two I-V peaks are similar to that of typical ferroelectric compounds (Pb  $(Zr_{0.4}Ti_{0.6})O_3$  and LiNbO<sub>3</sub>) [41] and could convince us that the P-E hysteresis loop indeed origins from the ferroelectric polarization instead of current leakage. The origin of the ferroelectricity of  $SrFe_{12}O_{19}$  ceramics is similar to that of  $PbFe_{12}O_{19}$  and has been discussed in detail in our previous literatures [28, 29], since both compounds share the same crystal structure. The off-center shift of the Fe<sup>3+</sup> ions and the displacement of O<sup>2-</sup> ions from its original corner positions in the FeO<sub>6</sub> octahedron are supposed to be the origin of electric polarization in SrFe<sub>12</sub>O<sub>19</sub> too [28, 29]. The saturated ferroelectric hysteresis loop, two peaks in the I-V curve, the giant anomalies of the dielectric constant in the vicinity of the transition temperatures ( $T_m$ and  $T_d$ ) as well as the comply of the reciprocal dielectric constant with modified Curie Weiss law provide us with enough evidences to prove the intrinsic ferroelectricity of  $SrFe_{12}O_{19}$ ceramics.

This result is quite different from that reported M-type hexaferrtie single crystals, which were claimed to be a new family of magnetic quantum paraelectrics and retained paraelectric symmetry down to zero temperature [32-34]. Actually those crystals showed different crystal structure with higher symmetry and were grown in a sealed furnace without subsequent heat-treatment in oxygen atmosphere. There would be high concentration of oxygen vacancies and Fe<sup>2+</sup> ions inside the crystals. These kinds of carrier charges would reduce the electric resistance of the crystals and induce large current leakage during the electric measurement. As such no saturated polarization hysteresis loop could be observed in these crystals. Both different crystal

structure and low concentration of carrier charges make our ceramic specimens differ significantly from those crystals in ferroelectric and dielectric properties.

### 6. Magnetic Properties of SrFe<sub>12</sub>O<sub>19</sub> Compound

For magnetic measurement, the  $SrFe_{12}O_{19}$  powders were prepared with the same heat-treatment history as that of above ceramics. The magnetic measurement was made upon  $SrFe_{12}O_{19}$ powders by the Physical Property Measurement System (PPMS) at room temperature. Fig 10 exhibits the ferromagnetic hysteresis loops of  $SrFe_{12}O_{19}$  powders with and without  $O_2$  heattreatment. It can be seen that magnetic properties of  $SrFe_{12}O_{19}$  have been greatly improved by annealing the powders in oxygen atmosphere. The coercive fields of the  $SrFe_{12}O_{19}$  powders with  $O_2$  treatment reaches as high as 6192 Oe, while that of the same powders without  $O_2$  treatment is 4111 Oe. The coercive field has been promoted 2081 Oe through  $O_2$  heat-treatment. The remnant magnetic moment has also been enhanced from 33.5 emu/g to 35.8 emu/g after annealing the  $SrFe_{12}O_{19}$  powders in oxygen atmosphere. The increase in remnant magnetization is quite modest since the applied magnetic field is not high enough to have all of the domains align themselves parallelly to the external field. Such promotion of magnetic polarization was also observed in M-type lead hexaferrite (PbFe\_{12}O\_{19}) after annealing in  $O_2$  atmosphere [29].

The heat-treatment in oxygen atmosphere transformed  $Fe^{2+}$  into  $Fe^{3+}$ , which provides one more unpaired electron spin for magnetic polarization of  $SrFe_{12}O_{19}$ . The existence of more  $Fe^{3+}$  in  $SrFe_{12}O_{19}$  would promote its magnetic properties. On the other hand, a certain content of  $Fe^{2+}$  existing in  $SrFe_{12}O_{19}$  which results from sintering the ceramics in a oxygen deficient





doi:10.1371/journal.pone.0167084.g010

atmosphere, such as a sealed air furnace, would reduce its ability for magnetic polarization and degrade its magnetic properties since  $Fe^{2+}$  contains one less electron spins than  $Fe^{3+}$ .

The evidence for increment of  $Fe^{3+}$  content in  $SrFe_{12}O_{19}$  ceramics after  $O_2$  treatment is the great promotion of the coercive magnetic field in the M-H loop of Fig 10. The coercive field is the intensity of the applied magnetic field required to reduce the magnetization of that material to zero after the magnetization of the sample has been driven to saturation. This value reflects the ability of spontaneous magnetic polarization of the magnetic materials. All the magnetic dipoles or spins are aligned anti-parallelly to the external magnetic field at the coercive point, whose value equals to the full magnetization in the opposite direction to withstand an external magnetic field without becoming demagnetization. The more is the content of  $Fe^3$ <sup>+</sup> in  $SrFe_{12}O_{19}$  compound, the higher is the concentration of unpaired electron spins and thus the larger is the ability of its full spontaneous magnetic polarization, which would need higher external magnetic field to balance the anti-parallelly aligned magnetic dipoles or spins. Therefore the coercive field would be promoted if there are more  $Fe^{3+}$  ions than  $Fe^{2+}$  ions in  $SrFe_{12}O_{19}$  compound. When the dipoles or spins are all anti-parallelly aligned to the external field at the coercive point of -4154 Oe with 0 magnetization in  $SrFe_{12}O_{19}$  ceramics without  $O_2$ treatment (Fig 10a), there are still many parallelly aligned dipoles or spins in the  $O_2$  treated SrFe<sub>12</sub>O<sub>19</sub> ceramics, whose net magnetization still remains at 21.05 emu/g at this point (Fig 10b & Figure A in S1 File). By comparing the increase of Bohr magnetrons at this field point (-4154 Oe) between the two samples, we are able to estimate the number of Fe<sup>2+</sup> that converts to Fe<sup>3+</sup>.

Under this consideration, we calculated the molar susceptibility from the measured B-H datasets of both samples through the equation:

$$\chi_m = \chi M/w \tag{4}$$

where  $\chi = B/H$  (B = magnetic moment in emu, H = external field in Oe), M is the molar mass of SrFe<sub>12</sub>O<sub>19</sub>, *w* is the weight of the sample. Afterwards, the molar susceptibility is converted to molecule magnetic moments by the equation:

$$\mu_m = \sqrt{3\chi_m kT/L\mu_0} \tag{5}$$

where L =  $6.022 \times 10^{23}$  mol<sup>-1</sup> (Avogadro's number), k =  $1.380 \times 10^{-23}$  J·K<sup>-1</sup> (Boltzmann constant),  $\mu_0 = 4\pi \times 10^{-7}$ N·A<sup>-2</sup> (vacuum permeability), T = temperature. The field dependent molecule magnetic moments are displayed in the (Figure A in <u>S1 File</u>). Upon the value of molecule magnetic moments, the unpaired electron numbers could then be calculated through the equation of  $\mu_B = \mu_m \sqrt{n(n+2)}$ , where  $\mu_B = eh/2m = 9.274 \times 10^{-24}$  J·T<sup>-1</sup> (Bohr magnetron, h is the Planck constant), n is the number of unpaired electrons,  $\mu_m$  is molecule magnetic moments. In this way,  $\mu_m$  is calculated to be  $0.9285 \times 10^{-23}$  J·T<sup>-1</sup> and  $3.3759 \times 10^{-23}$  J·T<sup>-1</sup> for the non-O<sub>2</sub> treated and O<sub>2</sub> treated SrFe<sub>12</sub>O<sub>19</sub> ceramics at point of -4154 Oe, which is the coercive field of the non-O<sub>2</sub> treated sample (Fig 10a & Figure A in <u>S1 File</u>). Finally, the number of unpaired electrons is determined to be  $n_1 = 0.414$  and  $n_2 = 2.772$  for the non-O<sub>2</sub> treated and O<sub>2</sub> treated SrFe<sub>12</sub>O<sub>19</sub> ceramic, respectively. Therefore, the difference of the unpaired electron numbers between two samples is  $\Delta n = n_2 - n_1 = 2.358$ . At this point of view, The second sample (O<sub>2</sub> treated SrFe<sub>12</sub>O<sub>19</sub> ceramic) has around 2.4 Fe<sup>2+</sup> ions convert to Fe<sup>3+</sup> ions after the SrFe<sub>12</sub>O<sub>19</sub> ceramic), indicating that around 2.4 Fe<sup>2+</sup> ions convert to Fe<sup>3+</sup> ions after the SrFe<sub>12</sub>O<sub>19</sub> ceramic was heat treated in O<sub>2</sub> atmosphere.

Therefore heat-treatment of  $SrFe_{12}O_{19}$  in oxygen would not only improve the ferroelectric polarization performance but could also enhance the ferromagnetic properties through transforming  $Fe^{2+}$  into  $Fe^{3+}$ . The large hysteresis loop reflects the strong magnetic feature of

 $SrFe_{12}O_{19}$ . The above combined results demonstrate the simultaneous occurrence of large ferroelectricity and strong ferromagnetism in the single  $SrFe_{12}O_{19}$  compound at room temperature. It allows us to expect a new generation of electronic devices being made of such a practicable multiferroic candidate, in which large ferroelectricity and strong ferromagnetism coexist.

### 7. Magnetocapacitance Effect of SrFe<sub>12</sub>O<sub>19</sub> Ceramics

Previous studies on certain rare-earth manganites [6, 42] suggested that materials having long wavelength magnetic structures often exhibit a strong interplay between magnetic ordering and ferroelectricity, which makes the capacitance of the manganites [43] and Y-type hexaferrites exhibit great response to the B field [44]. In order to check out if the M-type strontium hexaferrite (SrFe<sub>12</sub>O<sub>19</sub>) could also generate such coupling response upon an external magnetic field, we set up a simple system for the ME coupling measurement, which was performed by measuring the capacitance as a function of the magnetic field (B). The SrFe<sub>12</sub>O<sub>19</sub> ceramic was coated with silver electrodes on both sides and then placed in a space between two electromagnets. Upon the application of the magnetic field, the Wayne Kerr 6500B LCR Precision impedance analyzer, which was linked with the electrodes on both surfaces of the ceramic, would output the variable capacitance with the external magnetic field B. The B-field-dependent relative magnetic permeability was calculated using a defined formula, which can be expressed as follows [45]:

$$\mu_r = \frac{Z(T) - Z(0)}{if\mu_0 h \ln \frac{c}{h}} + 1 = \left[\frac{Z''(T) - Z''(0)}{f\mu_0 h \ln \frac{c}{h}} + 1\right] - i\left[\frac{Z'(T) - Z'(0)}{f\mu_0 h \ln \frac{c}{h}}\right]$$
(6)

where Z(T) is the complex impedance when magnetic field B = T, Z(0) the impedance for B = 0;  $\mu_0$  is the vacuum permeability, h is the space between two magnets, c and b are the inner and outer radius of the ring magnets. Fig 11 displays the dependence of the relative magnetic permeability ( $\mu_r$ ) on B and the change in  $\epsilon$  (or magnetocapacitance) along with B field. It can be seen from Fig 11a that  $\mu_r$  increases in a stepwise fashion, which is attributed to the evolution in magnetic structures. Five successive magnetoelectric phases could be thus mapped out: the first terrace (0<B<55mT) for modified helix, the ramp (55mT<B<150mT) for intermediate I, the second terrace (140mT<B<480mT) for intermediate II and III. The collinear ferrimagnetic phase is assigned to the region (480mT<B<883mT) with a rather large slope in  $\mu_r$ . These magnetic phases has been delimited by yellow dot lines (Fig 11a).

Fig 11b displays great response of the capacity (or  $\varepsilon$ ) to the applied magnetic field (B). The dramatic variation of dielectric constant with B field is similar to that of M-type BaFe<sub>12-x</sub>Sc<sub>x</sub>O<sub>19</sub> [42] and Y-type hexaferrite Ba<sub>0.5</sub>Sr<sub>1.5</sub>Zn<sub>2</sub>(Fe<sub>1-x</sub>Al<sub>x</sub>)<sub>12</sub>O<sub>22</sub> [20], and is associated with the magnetic phase transition along with B field. Within helix and intermediate I phases in range of 0~150 mT, the dielectric constant displays a downward slope line with small declining value (from 208.2 to -134.5). However, when B comes into the Intermediate II phase, the dielectric constant increases rapidly from -134.5 to 2650. The great change in  $\varepsilon$  is expressed as two remarkable peak structures centered in the middle of Intermediate II phase (254 mT) and III phase (363 mT), respectively (Fig 11b). The maximum dielectric constants show rapid drops at the magnetic boundary between Intermediate II and III (254 mT<B<300mT) and that between Intermediate III and collinear phases (300 mT<B<48 mT). The valley bottom ( $\varepsilon$  = 66) between the two peaks locates at 300 mT, which could be assigned to the borderline between intermediate II and III magnetic phases.

When B comes across into ferrimagnetic collinear phase (B>480), the dielectric constant remains almost as a flat line ( $\epsilon$ ~-730) with little fluctuation, whose amplitude is less than 90.





Fig 11. Giant magnetocapacitance effect: (a) B-dependent magnetic permeability ( $\mu_r$ ) and delimited magnetic phase profile; (b) variable dielectric constant as a function of B field for the O<sub>2</sub> treated SrFe<sub>12</sub>O<sub>19</sub> ceramics at a frequency of 100Hz and room temperature (300K).

The maximum relative change in  $\varepsilon$  ( $\Delta\varepsilon(B)/\varepsilon(0) = [\varepsilon(B)-\varepsilon(0)]/\varepsilon(0)$ , where B = 254mT) is 1174%, which reflects a giant magnetocapacitance effect of SrFe<sub>12</sub>O<sub>19</sub> ceramics. This magneto-capacitance order is much higher than that of YMnO<sub>3</sub> thin films with a magnitude of only 5.5% at 3T [46]. Thus, the hexaferrite with long-wavelength magnetic structures exhibits remarkable ME responses at low B fieldand roomtemperature, which opens substantial possibilities for applications of ME systems.

The magnetic phase within the B region of 450 mT < B < 800 mT could also referred to the so called "left hand materials" with negative capacitance (dielectric constants). Although negative capacitance is known to exist in semiconductors [47] and ferroelectrics, where it has been predicted theoretically [48], its direct measurement has been elusive so far [49]. Sayeef Salahuddin and colleagues has reported that negative capacitance in ferroelectrics can be directly measured by putting a large resistance between the voltage supply and the electrodes of the ferroelectric capacitor [50], such a negative capacitance is just a transient phenomenon and is intrinsically unstable because it exists only around the tipping point between the two thermodynamically stable polarization states [49, 50]. This complicates practical implementation. Here, we happened to observe the negative capacitance (or dielectric constant) in  $O_2$  treated SrFe<sub>12</sub>O<sub>19</sub> ceramicsbeing stimulated by low magnetic field. The negative capacitance could remain stable under application of low B field (450mT<B<800mT). Such low B-field induced negative capacitance was also experimentally measured in another M-type Hexaferrite  $(La_{0.2}Pb_{0.7}Fe_{12}O_{19})$ , whose lowest dielectric constant reaches as small as -84866.2 at the B field of 700 mT [51]. The negative capacitance of ferroelectrics could offer a solution to a bottleneck in transistor miniaturization: transistors are becoming too small and clock-speed too fast to remove the heat generated during switching, resulting in increased power dissipation and over heating [49]. Amplification of low gate voltage using negative capacitance would enable lowpower operation and could overcome such bottleneck problem in transistor miniaturization process.

In brief, large ferroelectricity and strong ferromagnetism are naturally merged together in one single  $SrFe_{12}O_{19}$  compound, due to the coexistence of the off-centered FeO<sub>6</sub> octahedron in its sub-unit cell and electron spins in partially filled 3d orbits of the Fe<sup>3+</sup> ions. Thus, the mutually exclusive electric and magnetic orders are naturally integrated in one single  $SrFe_{12}O_{19}$  compound. Therefore, large ferroelectricity, strong ferromagnetism and giant ME coupling effect are all synchronously realized in one single phase of  $SrFe_{12}O_{19}$  at room temperature (300K).

### Conclusion

In summary, our work directly demonstrates the coexistence of large ferroelectricity and strong ferromagnetism in M-type strontium hexaferrite ( $SrFe_{12}O_{19}$ ) at room- temperature (300K). We not only merge together the electric and magnetic orders, but also realize the giant magnetocapacitance effect in one single  $SrFe_{12}O_{19}$  compound at room temperature. The  $SrFe_{12}O_{19}$  ceramic displays a classical polarization hysteresis loop (P-E) with full saturation, two particular nonlinear I–V peaks, and dielectric anomalies near the Curie temperature, all of which verify its intrinsic ferroelectricity. Subsequent annealing the  $SrFe_{12}O_{19}$  ceramic in oxygen atmosphere greatly enhance its electric resistance through removal of oxygen vacancies and transformation of  $Fe^{2+}$  into  $Fe^{3+}$ , leading to the full saturation of the P-E loops. XPS spectra revealed the experimental evidences for great reduction of oxygen vacancies and transformation of  $Fe^{2+}$  into  $Fe^{3+}$  in  $SrFe_{12}O_{19}$  ceramics upon annealing in  $O_2$ . The remnant polarization of the  $SrFe_{12}O_{19}$  ceramics is  $103\mu C/cm^2$ . Large magnetic hysteresis loop was also observed in  $SrFe_{12}O_{19}$  due to its strong ferromagnetism. Furthermore, the capacitance (or

dielectric constant) exhibits dramatic variation along with B field. The magnetic structure profile has been mapped out upon the relative magnetic permeability. Two remarkable peak structures of  $\varepsilon$  appeared at the centers of Intermediate II and III magnetic phases, respectively. The maximum relative change in  $\varepsilon$  is 1174%, which reflects a giant magnetocapacitance effect of SrFe<sub>12</sub>O<sub>19</sub> ceramics. Low B-field induced negative capacitance was also observed in this compound.

### **Supporting Information**

**S1 File. SFO19 Supplementary File.** (DOCX)

### Acknowledgments

The authors acknowledge the financial support from Hubei Natural Science Foundation under the contract No. 2014CFB166; Open fund of State Key Laboratory of Advanced Technology for Materials Synthesis and Processing (Wuhan University of Technology) under the contract No. 2016-KF-15.

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Formal analysis: GT YH HHS.

Funding acquisition: GT.

**Investigation:** YH HHS.

Methodology: GT.

**Project administration:** GT.

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Supervision: GT.

Validation: YH.

Visualization: YH.

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