# Effect of Cross-Linking and Surface Treatment on the Functional Properties of Electrospun Polybenzimidazole Separators for Lithium Metal Batteries 

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#### Abstract

In this work, electrospun PBI separators with a highly porous structure and nanofiber diameter of about $90-150 \mathrm{~nm}$ are prepared using a multi-nozzle under controlled conditions for lithium metal batteries. Cross-linking with $\alpha, \alpha$-dibromo-p-xylene and surface treatment using 4 -(chloromethyl) benzoic acid successfully improve the electrochemical as well as mechanical properties of the separators. The resulting separator is endowed with high thermal stability and excellent wettability ( 1080 to $1150 \%$ ) with commercial liquid electrolyte than PE and PP (Celgard 2400) separators. Besides, attractive cycling stability and rate capability in LiFePO $/ 4 / \mathrm{Li}$ cells are attained with the modified separators. Prominently, CROSSLINK PBI exhibits a stable Coulombic efficiency of more than $99 \%$ over 100 charge-discharge cycles at 0.5 C , which is superior to the value of cells using commercial PE and PP (Celgard 2400) separators. The half cells assembled using the CROSSLINK PBI separator can deliver a discharge capacity of $150.3 \mathrm{mAh} \mathrm{g}^{-1}$ at 0.2 C after 50 cycles corresponding to $88.4 \%$ of the theoretical value of $\mathrm{LiFePO}_{4}\left(170 \mathrm{mAh} \mathrm{g}^{-1}\right)$. This work offers a worthwhile method to produce thermally stable separators with noteworthy electrochemical performances which opens new possibilities to improve the safe operation of batteries.


## 1. INTRODUCTION

Rechargeable lithium metal batteries with trustworthy electrochemical performances are considered to be the most promising energy storage devices in portable electronics, electric vehicles, as well as other energy storage devices. ${ }^{1-4}$ A typical lithium metal battery is composed of five parts: electrodes (anode and cathode), current collectors, an electrolyte, a separator, and casing. As a key component of lithium metal batteries, a separator prevents direct contact between the electrodes to avoid internal short circuit while transmitting lithium ions in an efficient manner. Most critically, various characteristics of separators such as mechanical as well as thermal stability, porosity, electrolyte wettability, etc have a significant effect on the comprehensive performance of lithium metal batteries. ${ }^{5,6}$ Currently, microporous membranes made of polyethylene (PE) and polypropylene (PP) are the most commercially used separators owing to their low cost, mechanical and chemical stabilities, electrochemical inertness, and shutdown behavior. However, the biggest shortcoming associated with these separators is their dimensional instability at elevated temperatures due to the inherently low melting point (PE: $130^{\circ} \mathrm{C}$; $\mathrm{PP}: 160^{\circ} \mathrm{C}$ ) which can create severe safety issues during battery operation. ${ }^{7-10}$ Furthermore, poor electrolyte wettability associated with its low porosity as well as low surface energy also
makes commercial PE or PP separators difficult to use in the next-generation lithium metal batteries. ${ }^{11,12}$ These limitations reduce ionic conductivity and battery performance. Therefore, considerable efforts have been devoted to solving these problems. ${ }^{13-17}$ As the brightest strategy, aromatic polymers are widely selected as separators to enhance the safe operation of batteries under harsh conditions. Among the various aromatic polymers, polybenzimidazole (PBI) is a high-temperature and highly durable engineering material. Most PBIs are not easily oxidized and have a decomposition temperature, above 600 ${ }^{\circ} \mathrm{C} .{ }^{18-20}$ Polar nitrogen atoms in its imidazole ring enhance electrolyte wettability, and the rigid backbone structure possesses inherent flame retardancy to the polymer. ${ }^{21}$ For example, Liang's group had studied porous PBI prepared by blending followed by the phase inversion process and reported high conductivity, electrolyte wettability, and thermal stability. ${ }^{22}$

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Figure 1. SEM images and nanofiber diameter distribution of various PBI membranes with different polymer concentrations: (a) $14 \mathrm{wt} \%$, diameter of nanofiber: $60-85 \mathrm{~nm}$, (b) $15 \mathrm{wt} \%$, diameter: $62-85 \mathrm{~nm}$, (c) $16 \mathrm{wt} \%$, diameter: $90-150 \mathrm{~nm}$, (d) $17 \mathrm{wt} \%$, diameter: $110-170 \mathrm{~nm}$, (e) $18 \mathrm{wt} \%$, diameter: 140-240 nm.

Nowadays, electrospun nanofiber membranes owing to their
interconnected and highly porous structure, high surface area, as
well as excellent electrolyte absorption, have become a hot topic of research as high-performance battery separators. For example,
a poly(ether ether ketone) nanofibrous separator fabricated by Li et al. using the electrospinning technique demonstrated an electrolyte uptake of about $524 \%$ and an ionic conductivity of $3.81 \mathrm{mS} \mathrm{cm}{ }^{-1.23}$ Lin et al. also made an electrospun poly(vinylidene fluoride) (PVDF) nanofibrous separator modified by poly(4-styrene sulfonic acid) lithium salt with superior electrochemical performance and durability in comparison to the commercial PP separators. ${ }^{2}$ Lithium-ion battery separators fabricated from poly(vinylidene fluoride) (PVDF) and octyl phenyl polyhedral oligomeric silsesquioxane by electrospinning also exhibited good electrochemical performances and zero-dimensional shrinkage after heat treatment. The membrane exhibited an ionic conductivity of $4.2 \mathrm{mS} \mathrm{cm}^{-1}$, an electrolyte uptake of $912 \%$, and a mechanical strength of 12.7 $\mathrm{MPa} .{ }^{24}$ The electrospun polyimide (PI) and their copolymerbased composite separators possess high thermo-dimensional stability, porosity, as well as excellent electrochemical performance and ideal thermal shutdown function. Moreover, the polyimide separators are of benefit to the compatibility with electrolyte and reduce nucleation and plating overpotentials to form dendrite-like lithium deposit on the electrodes to enhance the cycle life. ${ }^{25-27}$ Polyacrylonitrile (PAN) nanofiber membranes prepared by Dong et al. showed conductivity higher than that of commercial Celgard and a Coulomb efficiency as high as $98.7 \%$ after 50 cycles of battery performance at 0.5 C . ${ }^{3}$ Even though the electrospun separators have an excellent porous structure, the low mechanical strength of various polymeric materials cannot meet the requirement of battery assembly and limits its application as battery separators. ${ }^{28}$

The purpose of this study is to develop a mechanically as well as thermally stable PBI separator with high porosity and electrolyte uptake through electrospinning followed by chemical treatment techniques. In this work, electrospinning using multinozzles was employed instead of a single nozzle which improves the consistency of fiber production, reducing spinning time and density of aggregation built up in one location. ${ }^{29-31}$ Herein, electrospun PBI nanofibers are used as film-forming material and $\alpha, \alpha^{\prime}$-dibromo-m-xylene (DBX) as the cross-linking agent. The cross-linked membranes were also treated with 4(chloromethyl) benzoic acid (CMBA) to improve the electrolyte wettability. The effects of the DBX crosslinker and CMBA modifier on electrospun PBI separators prepared using multinozzles are yet to be reported to the best of our knowledge. The developed CROSSLINK PBI separator demonstrated excellent electrochemical performance and thermal stability in comparison to the commercial PE and PP (Celgard 2400) separators.

## 2. RESULTS AND DISCUSSION

2.1. Optimization of PBI Solution Concentration. The selection of the PBI solution concentration has a vital role in the spinning process and fabrication of the separators. The homogeneity has a pronounced impact on the successful performance of a separator and the composition as well as microstructure should be as uniform as possible throughout the material. ${ }^{7}$ In this study, different PBI membranes using solutions of different concentrations ( $14,15,16,17$, and 18 wt $\%$ ) were fabricated using the electrospinning process and their morphologies were observed using SEM analysis. Figure 1 shows the morphology and nanofiber diameter distribution of the prepared membranes. Fibrous structures with beads are formed at 14 and $15 \mathrm{wt} \%$ concentrations, and comparatively, more bead-like structures are observed at $14 \mathrm{wt} \%$. On the other hand, all PBI concentrations of $16 \mathrm{wt} \%$ and more produced
stable fibers, and the diameter of the fiber became larger with an increase in concentration and viscosity of the polymer solution. The formation of beads at low concentrations and increase in the diameter of fibers at high concentrations are related to the viscosity of the solution. The extent of polymer chain entanglement within the solution resulted in the variation of solution viscosity. Increase in the number of polymer molecules results in the increase in polymer chain entanglement and thereby viscosity. At low solution concentration and viscosity, the solution possesses a low viscoelastic force that is not capable of matching the electrostatic as well as Columbic repulsion force that stretch the electrospinning jet during the process, which results in a partial breakup of the jet. Furthermore, the greater number of free solvent molecules at low concentrations owing to the effect of surface tension comes together into a spherical shape, producing the formation of beads. Increase in polymer chain entanglement as well as improvement in viscoelastic force at high solution concentration prevents the breakup of jet and enables the solvent molecules to be distributed over the polymer molecules, leading to the smooth fiber formation with improved uniformity. The gradual increase in viscoelastic force with increase in solution concentration limits the stretching effect of the electrostatic as well as Columbic repulsion forces and increase the fiber diameter and its uniformity. The fine morphology and uniform nanofiber diameter distributions ( $90-150 \mathrm{~nm}$ ) exhibited by PBI membranes at a concentration of $16 \mathrm{wt} \%$ realized their better fiber-forming performance. Therefore, the separators used in this study are fabricated with modified and pristine PBI solutions of $16 \mathrm{wt} \%$ concentration.
2.2. Morphology and Structure of Separators. Figure 2 shows the SEM images and photographs of the different


Figure 2. SEM images of surface of different separators: (a) PLAIN PBI, (b) CROSSLINK PBI, (c) CROSSLINK PBI-CMBA, and (d) Commercial PE.
separators. It is off-white and opaque across its surface. All PBIbased separators have a highly porous structure (see Table 1) than the commercial PE separator. In the case of the PLAIN PBI separator, the nanofibers formed are straight and smooth. However, after modification, the nanofiber structure became

Table 1. Porosity (P), Electrolyte Uptake (EU), and Mechanical Properties of the PBI Separator and Commercial PE Separator

| property | PLAIN PBI | CROSSLINK PBI | CROSSLINK PBI-CMBA | commercial PE | Celgard 2400 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| P (\%) | $87 \pm 3$ | $70 \pm 4$ | $78 \pm 3$ | $40 \pm 2$ | $41 \pm 340$ |
| EU (\%) | $912 \pm 4$ | $1087 \pm 4$ | $1151 \pm 3$ | $49.5 \pm 340$ |  |
| tensile strength (MPa) | $3.61 \pm 0.8$ | $10.77 \pm 1.2$ | $8.91 \pm 0.5$ | $32.16 \pm 1.2$ | 12844 |
| elongation at break (\%) | $36.11 \pm 1.8$ | $78.51 \pm 2.2$ | $53.17 \pm 1.5$ | 7644 |  |
| modulus (MPa) | $22.25 \pm 1.2$ | $36.33 \pm 2.4$ | $23.74 \pm 1.5$ | $55.03 \pm 2.5$ |  |




Figure 3. (a) FT-IR spectra and (b) TGA curves of electrospun PBI (PLAIN PBI), crosslinked electrospun PBI (CROSSLINK PBI), and cross-linked-CMBA-treated (CROSSLINK PBI-CMBA) electrospun PBI-based separators.


Figure 4. Thermal shrinkage (photographs before and after heat treatment) of (a) PLAIN PBI separator: $150^{\circ} \mathrm{C}$ for 30 min , (b) CROSSLINK PBI at $150^{\circ} \mathrm{C}$ for $30 \mathrm{~min},(\mathrm{c})$ CROSSLINK PBI-CMBA at $150^{\circ} \mathrm{C}$ for 30 min , (d) commercial PE separator at $120^{\circ} \mathrm{C}$ for 10 min , and (e) commercial PE at $150^{\circ} \mathrm{C}$ for 1 min .
slightly curvy and rough. This may be due to the contraction of the film during drying after being treated with $\alpha, \alpha^{\prime}$-dibromo-mxylene (DBX) and 4 -(chloromethyl) benzoic acid (CMBA). The increase in roughness over time after being treated with sulfuric acid is also reported elsewhere. ${ }^{32}$ With an increase in the exposure time and concentration of sulfuric acid, swelling and hence increase in fiber thickness and loosening were noticed in their work. The commercial PE separator possesses a porous microstructure with a thick tree-branch-like polymer phase, which may be dependent on the wet process conditions. ${ }^{33}$ The cross-sectional morphology of PBI and the modified separator (Figure S 1 ) also supported a typical nanofiber microstructure without any beads. The cryo-fractured cross-sectional morphology of CROSSLINK PBI exhibits a mechanically stable
networked structure than that of PLAIN PBI. The pristine PBI and modified PBI separators in this work exhibit a random orientation of fibers that form a weblike interwoven network, and the gap between fibers may facilitate the film to possess better wettability and ion movement than the commercial PE separator. ${ }^{23}$

The chemical structure of the separators is confirmed by the FTIR spectra (Figure 3a). Typical PBI bands are noticed for the pristine PLAIN PBI membrane, including $\mathrm{N}-\mathrm{H}$ stretching at $3600-3000 \mathrm{~cm}^{-1}$ and the $\mathrm{C}=\mathrm{N}$ stretching vibration at 1613 $\mathrm{cm}^{-1} .^{22}$ After cross-linking, the $\mathrm{N}-\mathrm{H}$ and $\mathrm{C}=\mathrm{N}$ peak intensities are decreased, indicating that these functional groups act as cross-linking sites in the reaction. The cross-linking mechanism is shown in Figure S2. ${ }^{34}$ Moreover, after hydrophilization with

CMBA, the presence of the $\mathrm{O}-\mathrm{H}$ band could be verified in the vicinity of $3600-3200 \mathrm{~cm}^{-1}$, and the $\mathrm{C}=\mathrm{O}$ band stretching is identified at around $1700 \mathrm{~cm}^{-1}$, suggesting a successful modification of cross-linked PBI with CMBA.
2.3. Thermal Stability of Separators. The thermal stability of the separator is a property to guarantee safety especially for high-power batteries. ${ }^{35}$ No significant weight loss is noticed up to $200{ }^{\circ} \mathrm{C}$ in the TGA thermogram of the separators (Figure 3b). The first weight loss observed between 200 and $450^{\circ} \mathrm{C}$ is attributed to the loss of residual solvent and additives present in the system. ${ }^{36,37}$ The main polymer starts to decompose as the temperature exceeds $450{ }^{\circ} \mathrm{C}$ because of its rigid molecular structure and high thermal stability and the weight retention of the separators is about 70 to $80 \%$ at 700 ${ }^{\circ} \mathrm{C} .{ }^{36}$ The CROSSLINK PBI separator shows more weight loss due to the degradation of cross-linking agent ( $\alpha, \alpha$ '-Dibromo-mxylene, bp: $140{ }^{\circ} \mathrm{C}$ ) and solvent (acrylonitrile, bp: $300{ }^{\circ} \mathrm{C}$ ) present. Furthermore, the melting point of CMBA and sodium persulfate are at $201-202^{\circ} \mathrm{C}$ and $180^{\circ} \mathrm{C}$ in the CROSSLINK PBI-CMBA separator, respectively. ${ }^{37}$ Commercial Celgard 2400 reported by Liang et al., however, showed comparatively lower main chain decomposition temperature ( $\sim 400{ }^{\circ} \mathrm{C}$ ) and complete degradation as the temperature increased to $500^{\circ} \mathrm{C}$, indicating that PBI-based membranes have much better thermal stability than Celgard $2400 .{ }^{22}$
The thermal shrinkage of the separators was determined by measuring their dimensional change after storage at $150{ }^{\circ} \mathrm{C}$ for 30 min , and the photographs of the samples are shown in Figure 4. There is no significant change in the dimension and color observed in all the PBI-based separators expressed their outstanding thermal stability up to $150^{\circ} \mathrm{C}$, which is attributed to the superior thermal stability of imidazole groups and strong skeleton provided by PBI fibers. However, an apparent tendency in the reduction of dimensional stability with temperature is noticed in the commercial PE separator. The PE separator exhibits a remarkable shrinkage after heating at $120^{\circ} \mathrm{C}$ for 10 min and totally melted even before one minute as the temperature increased to $150^{\circ} \mathrm{C}$. A shrinkage of about $10 \%$ at $150^{\circ} \mathrm{C}$ and complete melting at $200{ }^{\circ} \mathrm{C}$ with Celgard 2400 reported by Liang et al. demonstrates comparatively excellent dimensional thermostability in PBI-based separators mainly due to the aromatic structure of the membrane. ${ }^{22}$ Moreover, the thermal shrinkage of PBI separators at $150{ }^{\circ} \mathrm{C}$ is significantly lower than that of high-density polyethylene (HDPE)/alumina nanocomposites fabricated using the extrusion process that can avoid the internal short circuits between two electrodes during battery operation and reduce the risk of thermal runway. ${ }^{38}$
2.4. Porosity and Electrolyte Wettability. The wettability of separators toward the electrolyte has a great influence on the ion conductivity as well as efficient functioning of a battery. ${ }^{39}$ The membranes with high porosity $(P)$ can successfully attain high electrolyte uptake and consequently elevated electrochemical performances. The PLAIN PBI separator displays a porosity of about $87 \%$ (Table 1). After cross-linking, the porosity $(P)$ has been decreased owing to the chemical bond formed between DBX and PBI. By sharp contrast, the commercial PE separator possesses the lowest porosity of about $40 \%$. To further confirm the wettability of the present membranes, the contact angle toward water and liquid electrolyte is also measured and the results are shown in Figure S3. The PE separator and Celgard 2400 exhibit a relatively high electrolyte contact angle of about $42.8^{\circ}$ and $61^{\circ}$, respectively, whereas PBI-based membranes rapidly absorb the electrolyte
and exhibit a contact angle between $11^{\circ}$ and $14^{\circ} .{ }^{40}$ As expected from high porosity, the pristine PBI membrane shows an electrolyte uptake of $912 \%$ owing to the good compatibility between polar nitrogen in PBI and the electrolyte (Table 1). ${ }^{41}$ The cross-linked membranes after CMBA treatment exhibit a high affinity toward both water and electrolyte due to the presence of polar functional groups (carboxyl, -NH). ${ }^{42}$ The high electrolyte affinity is an indication of the high $\mathrm{Li}^{+}$ion conductivity of the separator. ${ }^{43}$ The good electrolyte absorption behavior can also facilitate interfacial compatibility and $\mathrm{Li}^{+}$ion diffusion at the electrode/electrolyte interface, which will endow the battery with a poor Ohmic polarization phenomenon and improve cell performance. ${ }^{40}$ Moreover, the contact angle of water above $90^{\circ}$ on pristine PBI and cross-linked PBI is due to their hydrophobicity, while CMBA treatment supports the hydrophilicity owing to the presence of carboxyl functional groups. The contact angle results confirmed that, regardless of hydrophobicity, the plentiful hydrophilic carboxyl groups and porous structures of CROSSLINK PBI-CMBA could facilitate the absorption and spreading of the liquid electrolyte.

Electrospun PBI separators in this study showed 2 to 2.6 times higher electrolyte uptake than the commercial PE membrane and 10 to 12.8 times than Celgard 2400 reported by Zhu et al., ${ }^{40}$ suggesting that the PBI-based separators could offer more lithium-ion migration during charge/discharge reaction and thereby corresponding battery performance. ${ }^{12}$ The CROSSLINK PBI-CMBA exhibits higher electrolyte uptake followed by CROSSLINK PBI and pristine PBI separators. The electrolyte uptake value for PBI-based membranes are similar to that of polyimide (PI) and poly (ethylene-co-vinyl acetate) (EVA)/ polyimide (PI)/EVA (PIE) tri-layer membranes (700-1052\%) reported by Kim et al. ${ }^{8}$ All the above results have unambiguously confirmed superior liquid electrolyte wettability of modified PBI membranes.
2.5. Mechanical Property. The separator must be strong enough to withstand the tension during battery assembly or at unexpected collisions taking place. ${ }^{12,44}$ Table 1 and Figure S4 present the mechanical performances of PBI-based and commercial PE separators. The mechanical strength and elongation at break of the PE separator are 32.16 MPa and $174.1 \%$, respectively, suggesting a physical state of the strong and flexible separator. A good separator membrane should have sufficient strength to hinder the Li dendrites and appropriate strain to guarantee flexibility. The PLAIN PBI separator exhibits tensile strength and modulus of 3.61 and 22.25 MPa , respectively. After cross-linking, both the strength and modulus were increased up to 10.77 and 36.33 MPa , respectively, due to the strong chemical network formed among PBI chains through DBX. However, the highly porous structure formed after CMBA modifications leads to the deterioration in the mechanical property of the cross-linked PBI membrane. ${ }^{23}$ The tensile strength value achieved is similar to the porous PBI-based separator reported by Liang et al. ${ }^{22}$ Furthermore, the PBI separators are mechanically weaker than the commercial PE due to the difference in the manufacturing process. PE film used in this study was manufactured by an optimized wet process, including an extrusion step, two axis elongation, and a pore generation step via solvent extraction to control thickness, pore structure, as well as mechanical strength. ${ }^{33,45}$ Even though the mechanical properties are relatively lower than those of the commercial PE separator and Celgard $2400,{ }^{22}$ the present membranes can be randomly stretched and folded, which can still meet the requirements for commercialization.


Figure 5. Electrochemical impedance spectra of $(a, b)$ the $\mathrm{SS} /$ separator/SS cell and (c) the $\mathrm{Li} /$ separator/Li cell with different separators: PLAIN PBI, CROSSLINK PBI, CROSSLINK PBI-CMBA, commercial PE, and Celgard 2400.
2.6. Electrochemical Performances. 2.6.1. Ionic Conductivity. The ionic conductivity of the separator has a significant role in achieving high rate capability and battery reversibility performances. ${ }^{3,46}$ According to the Nyquist plot obtained in Figure 5a,b, the bulk resistance (intercept of the Xaxis of the plot) and ionic conductivity of all the PBI-based membranes are calculated and the values are illustrated in Table 2. It can be noticed that the maximum ionic conductivity of 0.86

Table 2. Electrochemical Performances of Different Separators

| separator <br> designation | thickness <br> $(\mathrm{mm})$ | bulk <br> resistance <br> $(\Omega)$ | ionic conductivity <br> $(\sigma)\left(\mathrm{mS} \mathrm{cm}^{-1}\right)$ | tortuosity <br> $(\tau)$ |
| :--- | :---: | :---: | :---: | :---: |
| PLAIN PBI | 0.058 | 11.30 | 0.654 | 3.61 |
| CROSSLINK <br> PBI | 0.025 | 3.70 | 0.860 | 2.82 |
| CROSSLINK | 0.032 | 102.92 | 0.396 | 4.39 |
| PBI-CMBA <br> commercial PE <br> Celgard 2400 | 0.025 | 14.52 | 0.228 | 4.15 |

$\mathrm{mS} \mathrm{cm}{ }^{-1}$ is obtained for CROSSLINK PBI membrane, 1.2 times more than that of Celgard $2400\left(0.687 \mathrm{mS} \mathrm{cm}^{-1}\right)$ and 3.8 times more than that of the commercial PE separators $(0.228 \mathrm{mS}$ $\mathrm{cm}^{-1}$ ), assigned to its higher porosity and electrolyte uptake. The strong interaction of the electron-rich imidazole ring on PBI with lithium ions also aids the lithium salt dissociation into $\mathrm{Li}^{+}$ ions by strong conjugated interactions and more easy ion transmission. ${ }^{36,41}$ Even though the CMBA-treated membranes
exhibited higher porosity and wettability with liquid electrolytes, the CROSSLINK PBI membrane shows comparatively high conductivity due to the higher flexibility and the presence of $\mathrm{Br}^{-}$ ions in its structure, which facilitate easy $\mathrm{Li}^{+}$ion conduction. The polarizability of the anion ( $\mathrm{Br}^{-}$) allows for the hopping-site environment to reduce the activation barriers and facilitate easy ion conduction. Kraft et al. have shown the influence of anion polarizability on the lattice stiffness and the associated $\mathrm{Li}^{+}$ion migration in their studies. ${ }^{47}$

The high ionic conductivity may improve the chargedischarge capacity and thus decrease the rate of increase of the transfer resistance in the cycle test. ${ }^{3,48}$ To study the impact of membranes' internal pores connectivity on conductivity, tortuosity values are calculated, and the values are illustrated in Table 2. Even though numerous pores are present in the membranes, the interconnectivity of pores is necessary for good Li-ion passage. CROSSLINK PBI shows that the lowest proper tortuosity (2.82) among other PBI-based membranes revealed its applicability to the energy storage devices. ${ }^{36}$ CROSSLINK PBI-CMBA exhibited a maximum tortuosity value of about 4.39 and showed the prolonged lithium-ion path through the membrane. Tortuosity, membranes' internal pore connectivity, is a diffusional parameter describing the complexity of mass or ionic transport that affects transport parameters, liquid-phase diffusivity, and conductivity. The $\mathrm{Li}^{+}$ion transportation path will be extended with an increase in tortuosity. If the pore size and connectivity of a nonwoven separator are not sufficiently controlled, critical problems such as nonuniform current acceleration, internal short circuit, mitigation of liquid electrolyte leakage, and self-discharge of the batteries may occur. ${ }^{33,49,50}$


Figure 6. Cyclic stability of batteries with different separators at (a) 0.2 C and (b) 0.5 C ; (c) comparison of rate performance of batteries with different separators.

The interfacial compatibility between the electrode and the polymer separator was also measured using ac impedance spectroscopy of the $\mathrm{Li} /$ separator/ Li cell and the results are displayed in Figure 5c. A small semicircle related to the solid electrolyte interphase (SEI)-derived resistance and a clear decrease for the second semicircle that relates to charge transfer resistance can be observed for the CROSSLINK PBI separatorbased cell. The charge transfer resistance deduced from the semi-circle in the high-frequency region is about $106.5 \Omega$ and $120.7 \Omega$ for CROSSLINK PBI and Celgard-2400, respectively. The lower interfacial impedance that existed between the CROSSLINK PBI separator and the lithium electrode reflects the interfacial compatibility between the separator and the Li metal electrode, which is ascribed to the good electrolyte absorption behavior of the separator that can facilitate $\mathrm{Li}^{+}$ diffusion at the separator-electrode interface and greatly help improve the overall cell performance. ${ }^{40,51,52}$
2.6.2. Battery Performance. The cell performance of the separators using $\mathrm{LiFePO}_{4} / \mathrm{Li}$ half-cells at 0.2 and 0.5 C rates at room temperature is illustrated in Figures S5 and 6a,b. All the cells assembled with different separators display stable chargedischarge platforms, indicating its remarkable reversibility. ${ }^{53}$ The battery with the CROSSLINK PBI separator has the best cycling performance among all the other PBI separator-based batteries. The cell with the PLAIN PBI separator reveals an initial charge capacity of $158.3 \mathrm{mAh} \mathrm{g}^{-1}$, a discharge capacity of $155.2 \mathrm{mAh} \mathrm{g}^{-1}$, and a Coulombic efficiency of $98.04 \%$ at 0.2 C rate. After 50 cycles, the cell maintained a Coulombic efficiency of $99.8 \%$ (charge and discharge capacities of 139.0 and 138.7 $\mathrm{mAh} \mathrm{g}{ }^{-1}$ ). As observed in Figures 6a and S5, the 0.2 C discharge capacities of the battery assembled with CROSSLINK PBI as
well as CMBA-treated CROSSLINK PBI are 151.4 and 147.8 $\mathrm{mAh} \mathrm{g}^{-1}$ respectively. CROSSLINK PBI exhibits a Coulombic efficiency of $99.8 \%$ even after 50 charge-discharge cycles, which is superior to the value of the cell using commercial PE and Celgard 2400 separators. The discharge capacity after 50 cycles of charging and discharging corresponds to $88.4 \%$ of the theoretical value of $\mathrm{LiFePO}_{4}\left(170 \mathrm{mAh} \mathrm{g} \mathrm{g}^{-1}\right){ }^{12}$ As the C rate increases to 0.5 , the PLAIN PBI membrane maintained a Coulombic efficiency of $96.5 \%$ (charge capacity: $120.7 \mathrm{mAh} \mathrm{g}^{-1}$; discharge capacity: $116.5 \mathrm{mAh} \mathrm{g}^{-1}$ ) and $99 \%$ (charge capacity: $94.0 \mathrm{mAh} \mathrm{g}^{-1}$; discharge capacity: $93.1 \mathrm{mAh} \mathrm{g}^{-1}$ ), respectively, after the first and the 100th cycle of charging-discharging. CROSSLINK PBI exhibits a maximum efficiency of about $99 \%$ after the 100th charge-discharge cycle, which is superior to the commercial PE and Celgard 2400 separators. A fast capacity decay while cycling at 0.5 C rate is observed for the CROSSLINK PBI-CMBA separator (Figure 6b) as a result of low ionic conductivity and high tortuosity values. ${ }^{36}$ The remarkable cycling performance of the CROSSLINK PBI separator is attributed to the synergistic effects of its excellent electrolyte uptake, flexibility, and electrochemical stability, which could facilitate easy ion migration, electrolyte retention, and reduction in interfacial resistance while cycling.

The rate capability of the cells containing different separators are investigated at room temperature and different chargedischarge current densities from 0.1 to 0.5 C for 20 cycles and the discharge capacities of the cells are shown in Figure 6c. All separators were continuously cycled for five cycles at each rate and the rate was reduced back to 0.1 C . A slow attenuation in the discharge capacities with an increase in current density is observed, attributed to the increase of the Ohmic polarization


Figure 7. Schematic of (a) electrospinning device and (b) multi-nozzle.
effect and overcharging potential at higher current density. ${ }^{12}$ Initially, at very low current density, no significant changes were noticed in the performance of various PBI-based separators. The cell with a CROSSLINK PBI separator shows the highest discharge capacity at the same current density of 0.2 C , attributed to its high ion conductivity and superior compatibility at the electrode/separator interface. ${ }^{54}$ The cell assembled with CROSSLINK PBI yields about $92.4 \%$ of the initial capacity at a high discharge rate ( 0.5 C ). In addition to its improved cycling performance, the CROSSLINK PBI separator also displayed high rate performance with a discharge capacity of $145.2,140.7$, and $133.8 \mathrm{mAh} \mathrm{g}^{-1}$ at $0.1,0.2$, and 0.5 C , respectively. When the battery was cycled back to 0.1 C , a high capacity of 142.2 mAh $\mathrm{g}^{-1}$ was retained ( $97.9 \%$ ), which indicates the high reversibility of the battery. For comparison, PLAIN PBI, CROSSLINK PBICMBA, commercial PE, and Celgard 2400 separators hold 92.6, $95.8,93.0$, and $97.3 \%$, respectively. The outstanding performances of the PBI-based separators are due to their high porosity, electrolyte wettability and ion conductivity.

## 3. SUMMARY AND CONCLUSIONS

Currently, polyolefin as a secondary battery separator is the most commercialized because of its lower price and high mechanical as well as chemical properties. However, the low thermal stability, low porosity, and poor electrolyte uptake limited their applications. To improve these shortcomings, polybenzimidazole, a high-temperature, highly durable super engineering material-based membranes are fabricated using the electrospinning process. A multi-nozzle is used to increase productivity and form a fine porous structure. Good coverage over a large area demonstrates prospects for scale up. Better process controllability in the multi-nozzle design leads to good-quality (size, distribution) fibers which avoid undesired short circuit of cells during charging/discharging. Cross-linking of PBI is done using $\alpha, \alpha^{\prime}$-dibromo-m-xylene (DBX) to improve the mechanical as well as chemical stability and hydrophilization using 4-(chloromethyl) benzoic acid (CMBA) to further improve electrolyte wettability. Compared to the commercial PE separator and Celgard 2400, CROSSLINK PBI and CROSSLINK PBI-CMBA exhibits excellent thermal stability which would help enhance battery safety. More significantly, the introduction of CMBA treatment was found to deliver the enhancement of porosity and electrolyte uptake (1151\%). However, their high tortuosity and low conductivity values adversely affected the battery cycling stability. The CROSS-

LINK PBI membrane exhibits superior ionic conductivity of about $0.860 \mathrm{mS} \mathrm{cm}{ }^{-1}$. Meanwhile, the stable Coulombic efficiency along with high-capacity retention (97.9\%) after being cycled back to lower C rate demonstrates the excellent cyclic stability and high reversibility of battery. Therefore, our study provides an effective strategy to design the thermally stable separator for high-power lithium metal batteries.

## 4. EXPERIMENTAL SECTION

4.1. Materials. The materials used for this study included liquid-type polybenzimidazole (S26, PBI advanced materials, Korea), $N, N$-dimethyl acetate (DMAc, Sigma Aldrich), $\alpha, \alpha^{\prime}$ -dibromo-m-xylene (DBX, 97\%, Sigma Aldrich), 4-(chloromethyl) benzoic acid (CMBA, 95\%, Sigma Aldrich), sodium persulfate ( $\geq 98$, Sigma Aldrich), acetone (Sigma Aldrich), acrylonitrile (AN, >99\%; Samchun), and isopropyl alcohol (IPA, $\geq 98 \%$, Sigma Aldrich). All chemicals were used without any further purification. A commercial polyethylene (PE) separator ( $25 \mu$ m thick) supplied by W-Scope Korea Co., Ltd. and polypropylene (PP) (Celgard 2400, USA) membrane were used for comparative study. $N$-methyl pyrrolidone (NMP), lithium iron phosphate $\left(\mathrm{LiFePO}_{4}\right)$, poly(vinylidene fluoride (PVDF), and cathode materials were provided by Sigma Aldrich. Lithium metal (Honjo metal Co., Ltd.) was used as the anode and 1 M lithium hexafluorophosphate solution ( $\mathrm{LiPF}_{6}$ ) in ethylene carbonate/diethyl carbonate (EC/DEC) $(1,1, \mathrm{v} / \mathrm{v})$ (Sigma-Aldrich) was used as the electrolyte. The cell test was conducted using a Swagelok cell (Hi-Touch, Korea).
4.2. Electrospinning Using the Multi-Nozzle. A schematic of the electrospinning device is shown in Figure 7a. The electrospinning device consists of a collector connected to the electric charge supply (Tekham, Korea), a syringe pump (Havard, USA) to control the speed of spinning solution feed, a multi-nozzle connected to the syringe, and 23 gauge needles to the multi-nozzle. Moreover, an infrared (IR) lamp ( $220 \mathrm{~V}, 60$ W ) for controlling temperature and humidity inside the housing and an illuminated lamp for visual inspection of fiber were also used. The collector was wrapped with an aluminum foil or a PTFE nonwoven fabric (Namyang non-woven fabric Co., Ltd) to facilitate the acquisition of electrospun fibers. A male-female fitting metal nozzle-PTFE tube ( $1 / 16^{\prime}$ size) (Nano NC, Korea) was used to inject the spinning solution. The multi-nozzle was divided into a distribution part consisting of 16 holes and an injection part to inject the polymeric solution (Figure 7b). In this experiment, 23 G metal needles were inserted into eight
holes excluding four edges of the multi-nozzle to manufacture PBI fibers. The 8-3 holes on the edges were blocked with Teflon to prevent the solution flow. The injection syringe was connected to the PTFE tube ( $1 / 16$ ' size).
4.3. Preparation of PBI Separators. PBI-based separators were fabricated by the electrospinning method with a steady flow rate of $1.1 \mathrm{~mL} \mathrm{~h}^{-1}$ and a high voltage of approximately 22 kV using the multi-nozzle as per the scheme illustrated in Figure 7. PBI solution with different concentrations ( $14,15,16,17$, and $18 \mathrm{wt} \%$ ) was prepared by dissolving PBI in DMAc by stirring at $80^{\circ} \mathrm{C}$ for 24 h using an oil bath. Then, the resultant solution was loaded into the syringe and vacuum-degassed for about 24 h to remove air bubbles and subjected to IR radiation for 30 to 60 min before electrospinning to maintain a constant temperature $\left(40^{\circ} \mathrm{C}\right)$ and humidity ( $\sim 20 \%$ ) inside the housing. The needle to collector distance was 15 cm . The obtained electrospun membranes were dried in an oven at ambient temperature (25 ${ }^{\circ} \mathrm{C}$ ) for 24 h .
4.4. Modification of the PBI Separator: Cross-Linking and CMBA Hydrophilization. $\alpha, \alpha^{\prime}$-Dibromo-m-xylene (DBX) solution (3 wt \%) in acrylonitrile was used as the cross-linking solution. The PBI membrane was treated with the cross-linking agent by stirring the membrane in solution at $80^{\circ} \mathrm{C}$ for 24 h . Afterward, the cross-linked membrane was immersed in isopropanol (IPA) for about 24 h to remove the residual material followed by drying in a vacuum oven (OV-11, Jeio Tech) at 60 ${ }^{\circ} \mathrm{C}$ for 24 h . The cross-linked membrane was designated as CROSSLINK PBI, and the mechanism of cross-linking is shown in Figure S1. ${ }^{34}$

The cross-linked membrane was then treated with 4(chloromethyl) benzoic acid (CMBA) to activate the surface and improve its electrolyte wettability. CMBA solution ( 0.5 wt $\%)$ in acetone was used as the hydrophilization agent and sodium persulfate as the free radical initiator for CMBA activation. The cross-linked PBI membrane was immersed in sodium persulfate solution ( $1 \mathrm{wt} \%$ in distilled water), and then, CMBA/acetone solution was added slowly. As CMBA is insoluble in water, care should be taken during addition to prevent precipitation. The reaction was then carried out at $40^{\circ} \mathrm{C}$ for 24 h . This temperature was selected to minimize solvent evaporation. ${ }^{55}$ After the reaction, the modified PBI membrane was immersed in acetone for 24 h to remove CMBA and then in deionized water for another 24 h to remove any remaining sodium persulfate and acetone. Finally, the modified membrane was dried at $60^{\circ} \mathrm{C}$ for 24 h using a vacuum oven. The chemical structure of the cross-linked PBI after hydrophilization with CMBA (CROSSLINK PBI-CMBA) is shown in Figure 8. Table 3 presents the designation of three different separators used in this study.


Figure 8. Chemical structure of cross-linked CMBA-treated PBI.

Table 3. Designation of Separators

| sample designation | treatment method |
| :--- | :--- |
| PLAIN PBI | electrospun pristine PBI |
| CROSSLINK PBI | cross-linked electrospun PBI |
| CROSSLINK PBI-CMBA | CMBA-treated cross-linked PBI |

4.5. Characterization. Scanning electron microscopy (SEM, Phillips XL30 S FEG, Netherlands) with an electron beam of accelerating voltage 15 kV was used to investigate the surface morphology of the separators. Before the examination, the samples were sputter-coated (JEOL JFC-110 E) with gold to avoid charge accumulation. The average diameter of the nanofibers was obtained using the ImageJ software (NIH, USA) by counting 50 randomly selected nanofibers from the SEM images. ${ }^{12}$ The chemical structures of different separators were confirmed by using Fourier transform infrared (FTIR) spectroscopy with attenuated total reflectance (Nicolet Impact 400, Thermo Scientific, USA) at room temperature, in the wavenumber range of $600-4000 \mathrm{~cm}^{-1}$ with a resolution of 4 $\mathrm{cm}^{-1}$ and 64 scans. The water and electrolyte ( $1 \mathrm{M} \mathrm{LiPF}_{6}$ in EC/ $\mathrm{DMC}=1 / 1(\mathrm{v} / \mathrm{v}))$ contact angles were determined using a Phoenix 300 Touch contact angle analyzer (Surface ElectroOptics Ltd) at $25^{\circ} \mathrm{C}$. Mechanical properties of the membranes were measured using a universal testing machine (UTM, Zwick Tensile machine) at a cross-head speed of $10 \mathrm{~mm} \mathrm{~min}^{-1}$, and the sample was in the form of a dog bone. The average of three samples was reported. The thermal stability of the membranes from room temperature to $700{ }^{\circ} \mathrm{C}$ was investigated using a thermogravimetric analyzer (TGA, Q50, TA Instruments, USA) at a heating rate of $10{ }^{\circ} \mathrm{C} \mathrm{min}^{-1}$ in a nitrogen atmosphere. Furthermore, the thermal shrinkage of the separators was examined by measuring the dimensional change after placing 16 $\pi$ coin cell samples in an oven at $150^{\circ} \mathrm{C}$ for 30 min .

The porosity $(P)$ of the PBI separator and the commercial PE separator was measured by the n-butanol immersion method. The dry separators $(2 \mathrm{~cm} \times 1 \mathrm{~cm} \times 30 \mu \mathrm{~m})$ were soaked in n butanol for 2 h at room temperature, and porosity was calculated using the following eq 1 :

$$
\begin{equation*}
\operatorname{Porosity,} P(\%)=\frac{W_{\mathrm{w}}-W_{\mathrm{d}}}{\rho_{\mathrm{b}} V_{\mathrm{d}}} \tag{1}
\end{equation*}
$$

where $W_{\mathrm{d}}$ and $W_{\mathrm{w}}$ are the weights of the samples (accuracy: $\pm$ 0.01 mg ) before and after soaking in n-butanol, respectively. $\rho_{\mathrm{b}}$ and $V_{\mathrm{d}}$ are, respectively, the density of $n$-butanol and the volume of the dry sample. An average of three specimens was reported.

The electrolyte uptake (EU) was measured by measuring the weight of the separators ( $2 \mathrm{~cm} \times 2 \mathrm{~cm}$ ) before and after soaking in the liquid electrolyte $\left(1 \mathrm{M} \mathrm{LiPF}_{6}\right.$ in EC/DMC $\left.=1 / 1(\mathrm{v} / \mathrm{v})\right)$ for 2 h . The electrolyte uptake was calculated using the formula 2:

$$
\begin{equation*}
\mathrm{EU}(\%)=\frac{W_{2}-W_{1}}{W_{1}} \times 100 \tag{2}
\end{equation*}
$$

where $W_{2}$ is the weight of the separator after being immersed in the electrolyte and $W_{1}$ is the weight of the dry separator. An average of three specimens was reported.

The electrochemical impedance spectroscopy (EIS) (ZIVE SP2, WonA Tech. Co.) measurements were used to calculate the ionic conductivity by placing the electrolyte-soaked separator between two stainless-steel electrodes. The measurements were
taken at an ac voltage of 5 mV in a frequency range of 2 MHz to 0.1 Hz . The ionic conductivity ( $\sigma$ ) was calculated using eq 3:

$$
\begin{equation*}
\sigma=\frac{d}{R_{\mathrm{b}} \times A} \tag{3}
\end{equation*}
$$

where $A$ and $d$ are the area and thickness (using a Vernier caliper, accuracy: $\pm 0.01 \mathrm{~mm}$ ) of the separator, respectively. $R_{\mathrm{b}}$ is the bulk resistance of the separator determined from the Nyquist plot. In the same way, the Nyquist plot of the Li /separator/ Li cell with Celgard, PE, as well as PBI-based separators and lithium metal as two electrodes in the frequency range of 0.1 Hz to 1 MHz was also gained by using EIS.
The tortuosity of all the membranes was calculated from porosity and conductivity values using eq 4:

$$
\begin{equation*}
\operatorname{Tortuosity}(\tau)=\sqrt{\frac{P \sigma_{0}}{\sigma}} \tag{4}
\end{equation*}
$$

where $P$ is the porosity of the membrane, $\sigma_{0}$ is the conductivity of the pure liquid electrolyte ( $9.8 \mathrm{mS} \mathrm{cm}{ }^{-1}$ ), and $\sigma$ is the conductivity of the separator at room temperature. ${ }^{36,56}$
Battery performance was analyzed using Swagelok cells assembled by sandwiching the liquid electrolyte-soaked separator between the cathode and anode in a glovebox filled with the argon atmosphere. The cathode slurry was prepared by mixing $80 \mathrm{wt} \% \mathrm{LiFePO}_{4}, 10 \mathrm{wt} \%$ poly(vinylidene fluoride) (PVDF), and 10 wt \% super-P (SP) carbon with the NMP solvent. The slurry was uniformly curtain-coated onto the aluminum foil. Lithium metal was used as the anode. The liquid electrolyte consisted of $1 \mathrm{M} \mathrm{LiPF}_{6}$ dissolved in the EC/DEC ( $1: 1$ volume ratio) mixture. For comparison, a cell with the same electrolyte and electrode was also assembled using a commercial PE separator and PP (Celgard 2400). The thickness of the separators and mass loading of the LFP cathode was varied from 0.025 to 0.058 mm and 1.7 to 2.2 mg , respectively. The performance of the membranes as a separator was studied by measuring the rate capability at different charge/discharge current densities ( 0.1 to 0.5 C rate) and cycle performance in the voltage range of 2.0 to 4.2 V under constant current ( 0.2 and 0.5 C).

## - ASSOCIATED CONTENT

## (s) Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acsomega.2c05472.

Cross-linking mechanism; contact angle; stress-strain curves; and battery performance (PDF)

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## Notes

The authors declare no competing financial interest.

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