




## PAPER

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## Flexible and transparent electrodes imprinted from metal nanostructures: morphology and opto-electronic performance†

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We directed the self-assembly of nanoscale colloids *via* direct nanoimprint lithography to create flexible transparent electrodes (FTEs) with metal line widths below 3  $\mu\text{m}$  in a roll-to-roll-compatible process. Gold nanowires and nanospheres with oleylamine shells were imprinted with soft silicone stamps, arranged into grids of parallel lines, and converted into metal lines in a plasma process. We studied the hierarchical structure and opto-electronic performance of the resulting grids as a function of particle geometry and concentration. The performance in terms of optical transmittance was dominated by the line width. Analysis of cross-sections indicated that plasma sintering only partially removed the insulating ligands and formed lines with thin conductive shells and a non-conductive core. We provide evidence that the self-assembly of high-aspect nanowires can compensate for defects of the stamp and substrate irregularities during imprinting, while spheres cannot. The wire-based electrodes thus outperformed the sphere-based electrodes at ratios of optical transmittance to sheet resistance of up to  $\approx 0.9\% \Omega_{\text{sq}}^{-1}$ , while spheres only reached  $\approx 0.55\% \Omega_{\text{sq}}^{-1}$ .

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## 1 Introduction

Solar cells, light-emitting diodes, and other devices that convert between photons and excitons require transparent conductive electrodes. They are often based on thin films of noble metals, indium tin oxide, semiconductor polymers or hybrids, networks of graphene or carbon nanotubes, metal nanowires, or metal grids.<sup>1,2</sup> All of them can be used to create flexible transparent electrodes (FTEs) on thin, flexible and transparent polymer substrates, with performances that depend on the material and the layer morphology.

Metal grids are particularly cost-effective transparent electrodes that can be customized:<sup>3</sup> their sheet resistance and optical transmittance are defined by the chosen grid geometry and vary with pattern, pitch, conductor width, and conductor thickness.<sup>4</sup> Foldable high resolution displays, for instance, require FTEs with a large density of separate, parallel conductors to control the individual pixels. This can be realized with a dense grid of very narrow lines that provide high optical transmittances. The thickness of the lines can be tuned to achieve a conductive cross section that yields an acceptable

sheet resistance. Both requires a process that can pattern dense, narrow lines.

E-beam lithography offers the necessary resolution but has a low throughput.<sup>5</sup> Printing techniques have been reported to improve fabrication speed. Many are limited to line widths above several micrometers, requiring large pitches to attain transparency. Zhu *et al.*<sup>6</sup> combined an electric-field-driven microscale 3D printing technique with a hybrid hot-embossing process to fabricate Ag-based square grid FTEs with sheet resistances of  $0.75 \Omega_{\text{sq}}$  and optical transmittances of  $T_{500} \approx 85.79\%$  at a line width of 10  $\mu\text{m}$  and a pitch of 1000  $\mu\text{m}$ . Wang *et al.*<sup>7</sup> report sheet resistances of  $0.86 \Omega_{\text{sq}}$  and optical transmittances of  $T_{500} \approx 91.26\%$  at a line width of 18  $\mu\text{m}$  and a pitch of 800  $\mu\text{m}$  for their Ag-based square grid FTEs fabricated *via* ultra-fast laser direct writing. Le Zhao *et al.*<sup>8</sup> demonstrate FTEs based on Cu/Ni square grids, fabricated using lithography and electroplating. They achieved sheet resistances of  $0.13 \Omega_{\text{sq}}$  and optical transmittances of  $T_{500} \approx 86\%$  at a line width of 8  $\mu\text{m}$  and a pitch of 170  $\mu\text{m}$ . Zhou *et al.*<sup>9</sup> inkjet printed Ag-based square grid FTEs with sheet resistances of  $9.56 \Omega_{\text{sq}}$  and optical transmittances of  $T_{500} \approx 64.05\%$  at a line width of 46.2  $\mu\text{m}$  and a pitch of 200  $\mu\text{m}$ . Li *et al.*<sup>10</sup> screen printed Ag-based honeycomb FTEs with sheet resistances of  $27 \Omega_{\text{sq}}$  and optical transmittances of  $T_{500} \approx 67\%$  at a line width of 200  $\mu\text{m}$  and a pitch of 1040  $\mu\text{m}$ . Scraping is an alternative 5-step process where the electrode material is spread across a previously prepared substrate pre-patterned with recesses and can yield 3  $\mu\text{m}$  wide lines, for example.<sup>11</sup>

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Nanoimprinting combined with self-assembly provides an efficient 2-step route to grids of sub-micron metal lines.<sup>12–18</sup> Dispersions of metallic nanocolloids (colloidal inks) can be imprinted under ambient conditions in a roll-to-roll compatible process with a patterned polymer stamp that is being rolled over the substrate.<sup>19,20</sup> The colloidal ink is confined in the stamps' cavities and the solvent permeates through the polymer. The dispersed particles self-assemble into features defined by the stamp. Particle geometry and concentration can be tuned to affect self-assembly and the resulting structures.<sup>20</sup> Metallic nanocolloids often carry organic ligand shells that prevent agglomeration and have to be removed after imprinting, for example in a plasma.<sup>21</sup>

Maurer *et al.*<sup>19</sup> nanoimprinted self-assembling Au nanowires with a core diameter of 1.6 nm, an aspect ratio on the order of  $10^3$ , and an oleylamine ligand shell. The wires self-assembled into bundles inside the square grid defined by the stamp. The resulting grid was sintered using a low-pressure, room temperature plasma treatment that retained the overall geometry and did not damage the thin polymer substrate. The resulting FTEs had sheet resistances of  $128 \Omega_{\text{sq}}/196 \Omega_{\text{sq}}$  (in printing direction/perpendicular) and optical transmittances of  $T_{500} \approx 86\%$  at line widths of  $1.41 \mu\text{m}/0.91 \mu\text{m}$  and a pitch of  $19.5 \mu\text{m}$ .<sup>19</sup> Kister *et al.* imprinted Au nanospheres with a core diameter of 3.2 nm and C4-, C8- or C12-thiols or amines. Both reports used the same printing method that we study here, but different process parameters and particle ligands. The best-performing FTEs formed from particles with dodecylamine ligand shells and had sheet resistances of  $150 \Omega_{\text{sq}}$  and optical transmittances of  $T_{500} \approx 91\%$  at line widths  $< 1 \mu\text{m}$  and a pitch of  $19.5 \mu\text{m}$ .<sup>20</sup> The basic functionality of such nanoimprinted electrodes was demonstrated by integrating them into capacitive and resistive touch devices.<sup>19</sup> Other examples for the integration of nanoimprinted electrodes into functional devices include organic field effect transistors,<sup>13,15</sup> nanobatteries<sup>22</sup> and flexible organic light-emitting devices.<sup>23</sup>

The structure–property relations between the morphology of metal conductors formed during nanoimprinting and the optoelectronic electrode performance are not fully understood. There are, however, some studies on spin-coated, inkjet-printed and drop-casted nanoparticle assemblies and the effect of plasma sintering on their morphology and/or sheet resistance. Shaw *et al.*<sup>24</sup> investigated crack formation in spin-coated assemblies of ligand-capped colloids (varying in composition, shape, size and ligand as well as the used solvent) on Si substrate during drying,  $\text{O}_2$  plasma-induced ligand removal, and thermal sintering. They found that close-packed and ordered particle packing always led to cracking, while disordered particle films with thicknesses up to 440 nm remained crack-free. Reinhold *et al.*<sup>25</sup> studied the effect of Ar plasma sintering on the morphology and resistivity of inkjet printed tracks (Ag nanoparticles with a diameter of 5 to 10 nm in tetradecane) on polymer substrates. They report the formation of a conductive Ag skin layer and a non-conductive core. The skin layer thickness was independent of the printed layer thickness and increased with plasma treatment time before saturating. Ma *et al.*<sup>26</sup> investigated the effect of Ar plasma sintering on the

morphology of drop-casted layers of Ag nanoparticles (gum arabicum capped, 23 nm and 77 nm in diameter, dispersed in DI water) on glass and the resulting sheet resistance. Plasma sintering converted discrete particles to a more continuous film with time, and increasing RF power accelerated this transition. A simple parallel circuit model was formulated based on a fully sintered skin layer and a less or non-conductive core. Assuming a non-conductive core, the calculated skin layer resistivities matched the morphological development with increasing plasma sintering time and increasing RF power well.

Here, we study the effects of particle shape and superstructure formation on the conductor morphology and optoelectronic performance. Au nanowires (wires) and Au nanospheres (spheres) were imprinted as grids of parallel lines with a width of about  $1.6 \mu\text{m}$  and a pitch of  $19.5 \mu\text{m}$  at different Au concentrations  $c_{\text{Au}}$  on polyethylene terephthalate (PET) foil. The lines underwent  $\text{H}_2/\text{Ar}$  plasma sintering. We quantified the performances of the resulting transparent electrodes using a figure of merit (FOM) and compared them to the electrode morphologies before and after plasma sintering. We found that wires form lines with a coarse surface microstructure and pronounced bleeding, while spheres form smooth lines with less bleeding. The plasma formed a conductive shell and a non-conductive core for both particle types, with the thicker shell in case of the spheres. Electrode performance was dominated by defect densities, where wires outperformed spheres because they better bridged stamp and substrate irregularities during imprinting. The FOM always increased with increasing  $c_{\text{Au}}$ , but the FOM with wires was at least 3.4 times higher at any given  $c_{\text{Au}}$ .

## 2 Materials and methods

### 2.1 Synthesis of Au nanowires/-spheres

**2.1.1 Chemicals.** Tetrachloroauric(III) acid trihydrate ( $\text{HAuCl}_4 \cdot 3\text{H}_2\text{O}$ ) was synthesized according to Schubert *et al.*,<sup>27</sup> oleylamine (Acros Organics, C18 content of about 80–90%) was purchased from Fisher Scientific GmbH (Schwerte, Germany) and filtered with a  $0.45 \mu\text{m}$  Rotilabo-PTFE syringe filter from Carl Roth GmbH + Co. KG (Karlsruhe, Germany) prior to each usage to remove any oxidized residues, triisopropylsilane (95%) and *n*-hexane (at least 99% p.a.) were obtained from abcr GmbH (Karlsruhe, Germany), pentane (Sigma Aldrich, for HPLC,  $\geq 99\%$ ) and borane *tert*-butylamine complex (Sigma Aldrich, 97%) were obtained from Merck KGaA (Darmstadt, Germany), cyclohexane (ROTISOLV  $\geq 99.9\%$ , GC Ultra Grade) was bought from Carl Roth GmbH + Co. KG (Karlsruhe, Germany) and absolute ethanol (99.8%, analytical reagent grade) was procured from Fisher Scientific GmbH (Schwerte, Germany). All chemicals were used without further purification unless explicitly mentioned.

**2.1.2 Syntheses.** Ultrathin nanowires (AuNW) with a gold (Au) core and an oleylamine (OAm) ligand shell were synthesised according to Nough *et al.*,<sup>28</sup> a route based on the original research by Feng *et al.*<sup>29</sup> Nanospheres (AuNP) with Au cores and OAm ligand shells were synthesised according to Kister *et al.*,<sup>20</sup> a route based on the original research by Wu *et al.*<sup>30</sup>

In a typical AuNW synthesis, 60 mg of  $\text{HAuCl}_4 \cdot 3\text{H}_2\text{O}$  (10 mM) were weighed into a disposable 50 mL glass snap-on vial from Carl Roth GmbH + Co. KG (Karlsruhe, Germany). Then, 9.9 mL of *n*-hexane and 2.04 mL of oleylamine (400 mM) were added. The mixture was vortexed for 1 min to fully dissolve the Au acid. Then, 3.06 mL (1 M) of triisopropylsilane (TIPS) were added as reducing agent. The solution was vortexed for 30 s and kept in an oven at 25 °C for 24 h without any mechanical agitation.

The highly hygroscopic  $\text{HAuCl}_4 \cdot 3\text{H}_2\text{O}$  was weighed in dry in a glove box from SylaTech GmbH (Walzbachtal, Germany) because the presence of water results in shorter wires.<sup>31</sup> The reaction vessel was filled with dry Ar. OAm acts both as ligand and as reducing agent, albeit weaker than TIPS. OAm and TIPS were added in that order using a 5 mL pipette. The interval between injections was minimized to avoid reduction in the absence of TIPS.

In a typical AuNP synthesis, 200 mg of  $\text{HAuCl}_4 \cdot 3\text{H}_2\text{O}$  were weighed into a disposable 100 mL glass snap-on vial from Carl Roth GmbH + Co. KG (Karlsruhe, Germany) under ambient conditions because the synthesis is less water sensitive. Then, 16 mL of pentane and 16 mL of OAm were added. The mixture was stirred at 500  $\text{rad min}^{-1}$  and room temperature for 45 min (solution A). In the meantime, 80 mg of tert-butylamine borane were dissolved in a mixture of 4 mL pentane and 4 mL OAm (solution B). After precisely 45 min (the waiting time determines the sphere diameter), solution B was added to solution A and the color turned immediately dark brown. Then the mixture was stirred for another 60 min with a loose lid.

**2.1.3 Purification, dilution, and storage.** After synthesis, AuNW were purified by adding twice the reaction volume of absolute ethanol and shaking the snap-on vial. Sedimentation occurred in a Rotanta 460 RS centrifuge from Andreas Hettich GmbH & Co. KG (Tuttlingen, Germany) with a swing-out rotor at 110 rcf for 2 min and the slowest possible deceleration. The supernatant was discarded and the wires were re-dispersed in an amount of *n*-hexane corresponding to the original reaction volume. The purification procedure was repeated before re-dispersing the wires in cyclohexane to obtain a stock dispersion of  $c_{\text{Au}} \approx 10 \text{ mg mL}^{-1}$  (estimated based on  $\text{HAuCl}_4 \cdot 3\text{H}_2\text{O}$  weighed in and 100% yield).

The purification of AuNP was similar, but with centrifugation at 3435 rcf and 5 min for the first and 3435 rcf and 60 min for the second step. The AuNP were re-dispersed to  $c_{\text{Au}} \approx 30 \text{ mg mL}^{-1}$ .

Other ink concentrations were produced through dilution of the respective stock dispersion. AuNW inks were stored in a fridge at 5 °C, AuNP inks were stored at room temperature for 16 h before usage.

## 2.2 Small-angle X-ray scattering (SAXS)

Sphere diameter and dispersion state were characterized *via* SAXS. The dispersion was transferred to glass mark-tubes from Hilgenberg GmbH (Malfeld, Germany) with an inner diameter of 1.5 mm. The tubes were sealed with a fast-curing two-component epoxy from R&G Faserverbundwerkstoff GmbH (Waldenbuch, Germany) to prevent solvent evaporation.

The scattering setup, a Xeuss 2.0 HR SAXS/WAXS instrument from Xenocs SAS (Grenoble, France) used a Cu  $K\alpha$  source and a detector PILATUS3 R 1 M from DECTRIS AG (Baden, Switzerland) at a distance of about 550 mm from the samples. The distance was calibrated with a Ag behenate sample before each measurement. Each sample was measured for a total of 30 min. The two-dimensional scattering images were azimuthally integrated with the software Foxtrot from Synchrotron SOLEIL (Saint-Aubin, France) to obtain the scattering curves. The solvent background was measured separately and subtracted. To determine the average sphere diameter, fitting of the scattering curves was performed with the software SASfit from the Laboratory for Neutron Scattering at Paul Scherrer Institute (Villigen, Switzerland).

## 2.3 Nanoimprinting

**2.3.1 Substrate cleaning.** PET substrates of type Melinex 401 CW from DuPont Teijin Films UK Ltd (Redcar, United Kingdom) with a thickness of 0.75  $\mu\text{m}$  were cleaned using an ultrasonic bath in a custom-made cleaning rack using the following sequence of solvents: 5 min acetone, 5 min ethanol, and 5 min Milli-Q ultrapure water. The substrates dried for 30 min at 60 °C, just below their glass transition temperature of 70–80 °C. Acetone removed any grease residues, ethanol and the ultrapure water removed acetone and increased polarity, the ultrapure water dried without residues.

**2.3.2 Polydimethylsiloxane (PDMS) imprinting stamp fabrication.** PDMS imprinting stamps were fabricated in a two-step-moulding process. First, a PDMS master was moulded off a silanized silicon master from AMO GmbH (Aachen, Germany) with a pattern of parallel line channels (patterned area  $A \approx 7 \text{ cm} \times 7 \text{ cm}$ , pitch  $p \approx 19.5 \mu\text{m}$ , channel width  $w_c \approx 1.6 \mu\text{m}$  and channel depth  $d_c \approx 4.2 \mu\text{m}$ ). The imprinting stamp was moulded off the silanized master stamp.

Silanization was performed directly on the silicon master and after plasma activation of the PDMS master for 1.5 min using an oxygen plasma at 0.3 mbar in a low pressure plasma reactor of type Pico from Diener electronic GmbH & Co. KG (Ebhausen, Germany). Silanization took place inside a conventional glass desiccator with a snap-on vial cap containing 30  $\mu\text{L}$  of (tridecafluoro-1,1,2,2-tetrahydrooctyl)trichlorosilane from abcr GmbH (Karlsruhe, Germany). The vial was shielded from the masters to increase uniformity. The desiccator was flushed with Ar, evacuated to 3 mbar, and disconnected from the vacuum pump. After 30 min, the desiccator was slowly ventilated with air.

PDMS base and curing agent, Sylgard 184 from Dow Inc. (Midland, USA), were mixed in a 10 : 1 (w/w) ratio and degassed in a Speedmixer DAC 600.2 VAC-P from Hauschild GmbH & Co. KG (Hamm, Germany) at a speed of 2350 rpm and a pressure of 1 mbar for 3 min. The mixture was poured onto the respective master with a Teflon spacer ring (2 mm thick) and a glass plate as top sealing. The PDMS was fully cured at 80 °C for 3 h and the replica were carefully peeled off along the stamp channels.

Imprinting stamps were cut into two parts with an area of 3.5 cm  $\times$  8 cm of which 3.5 cm  $\times$  7 cm were patterned. Larger

areas can be printed using the complete imprinting stamp.<sup>19</sup> The flat 3.5 cm × 0.5 cm at either end of the stamp served as run-in and run-out areas during imprinting.

**2.3.3 Nanoimprinting.** Nanoimprinting was carried out using a modified TQC Sheen automatic film applicator from Industrial Physics Inks & Coatings GmbH (Hilden, Germany), equipped with a custom-made 3 kg steel cylinder (8 cm in diameter and height) that was moved at a constant speed of 4 mm s<sup>-1</sup>. The PDMS stamps were attached to the steel cylinder using a double-sided tape from tesa SE (Norderstedt, Germany). Immediately before imprinting, 60 μL of ink were injected directly into the gap between the PDMS imprinting stamp and the PET substrate using a pipette. Continuous processing is possible *e.g.* using a syringe pump for the ink. After imprinting, ink residues on the PDMS stamp were removed using Scotch Magic Tape from 3 M Deutschland GmbH (Kleinostheim, Germany). There was no degradation of the stamps apparent from the geometry of the prints after using the same stamp for 60 prints. A detailed, illustrated description of the nanoimprinting process is included in Section 1 of the ESI.† Note that nanoimprinting is sensitive to humidity and has to be carried out well above the dew point to avoid capillary condensation. We typically imprinted at 22 °C and 55% *rH* at a dew point of 12.5 °C.

## 2.4 Plasma sintering

Plasma sintering was performed in a low pressure 13.56 MHz RF plasma reactor of type Pico from Diener electronic GmbH & Co. KG (Ebhausen, Germany) immediately after nanoimprinting. Ar/H<sub>2</sub> (95% Ar and 5% H<sub>2</sub>) was used as process gas. The procedure was carried out at room temperature and ≈ 0.3 mbar for 20 min with 100 W RF power.

## 2.5 Sheet resistance measurements

Sheet resistances were determined in a 2-point-probe configuration using a multi-channel multi-meter (DAQ6510 data acquisition logging multi-meter system) equipped with multiplexer cards (7702 40-channel differential multiplexer module with screw terminals) from Keithley Instruments GmbH (Germaring, Germany). The electrodes were contacted using a fast drying Ag paste ACHESON Ag DAG 1415 from Plano GmbH (Wetzlar, Germany) and AGF 1 miniature crocodile clamps from SKS Kontakttechnik GmbH (Niederdorf, Germany). Ag paste was applied in two parallel lines, each 1.5 cm long and spaced 1.5 cm apart, resulting in a square measurement field. The determined resistances corresponded directly to the desired sheet resistances.

## 2.6 UV-vis spectroscopy

The optical transmittance of the electrodes was determined with a Cary 5000 UV-vis-NIR spectrophotometer from Agilent Technologies Deutschland GmbH (Waldbronn, Germany) with a tungsten halogen light source for the visible range and a deuterium arc light source for the UV range. The samples were mounted behind blackened metal masks with circular apertures (5 mm in diameter). Measurements were performed in

double-beam mode against air at scan rates of 600 nm min<sup>-1</sup>. The samples were placed such that the blank sides were in contact with the mask to prevent any damage to the electrodes on the other side. Baselines of bare PET substrates were recorded as references.

## 2.7 Confocal laser scanning microscopy (CLSM)

The electrodes' surface topographies were characterized using a MarSurf CM explorer from Mahr AG (Thalwil, Switzerland) at 100-fold magnification, which corresponded to a measuring field of about 161 μm by 161 μm. The vertical resolution was 2 nm, the lateral resolution 320 nm, effectively allowing for data points every ≈ 130 nm. For a single topography map, 1240 equidistant height traces across eight parallel conductor segments were acquired. Data analysis was performed with Python (Anaconda distribution) as described below. Note that CLSM overestimates the height of the material at the edge of the lines, blurring the edge. We thus detected the edge with a slope-based (*m*) termination criterion (absolute values of *m*:  $|m_{\text{wires}}| \leq 0.03$  and  $|m_{\text{spheres}}| \leq 0.06$ ) for both S-shaped sides of the Gaussian conductor profile.

## 2.8 Cross-sectioning *via* focused ion beam (FIB)

The conductor cross sections were prepared using a FEI Versa 3D DualBeam from Thermo Fisher Scientific GmbH (Schwerte, Germany). The conductors were protected by subsequently deposited layers of Pt using the electron beam first, then the ion beam.

## 2.9 Transmission electron microscopy (TEM)

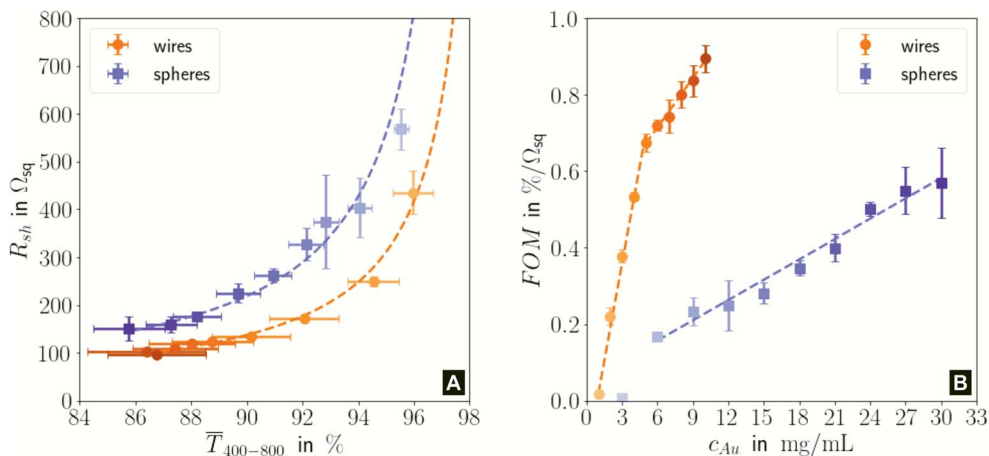
Dry particle samples were prepared by diluting AuNW and AuNP dispersions to concentrations of approximately 0.1 mg mL<sup>-1</sup> and drop-casting 3 μL on a carbon-coated copper grid from Plano GmbH (Wetzlar, Germany). All samples were characterized at an acceleration voltage of 200 kV in a JEM 2010 from JEOL GmbH (Freising, Germany).

## 2.10 Scanning electron microscopy (SEM)

Scanning electron micrographs were recorded using either a FEI Quanta 400 ESEM or a FEI Versa 3D DualBeam from Thermo Fisher Scientific GmbH (Schwerte, Germany) with secondary electron detectors. The electrodes for SEM were imprinted onto polished, p-type silicon wafers from Siebert Wafer GmbH (Aachen, Germany).

# 3 Results and discussion

Fig. 1 illustrates the trade-off between electrical resistance *R* and optical transmittance *T* of metal grid-based FTEs. We prepared grids of parallel lines using gold nanosphere (AuNP) and gold nanowire (AuNW) colloids with increasing concentration *c*<sub>Au</sub> (three samples per concentration), plasma-sintered them, and compared their average transmittances  $\bar{T}_{400-800}$  in the visible range (from 400 nm to 800 nm) to their sheet resistances *R*<sub>sh</sub>. It



**Fig. 1** (A): Sheet resistances  $R_{sh}$  and optical transmittances  $\bar{T}_{400-800}$  for wire- and sphere-based electrodes directly after plasma sintering. Data for electrodes with  $R_{sh}$  that exceeded the scale are not included (Section 2 of the ESI† has the complete data set). (B): Dependence of  $FOM = \bar{T}_{400-800} \cdot R_{sh}^{-1}$  with concentration  $c_{Au}$ . All graphs show average values from three measurements, the standard deviation, and a fit (dashed lines). Light colours represent the lowest and dark colours the highest Au concentrations in the printed colloids.

is convenient to express the overall performances using the Figure of Merit developed by Fraser and Cook,<sup>32</sup>

$$FOM = \bar{T}_{400-800} \cdot R_{sh}^{-1}, \quad (1)$$

that compares the ratio of the mean optical transmittance  $\bar{T}_{400-800}$  and the sheet resistance  $R_{sh}$ .

The concentrations of the colloids were varied in the range of 1–10  $mg mL^{-1}$  for the wires and 3–30  $mg mL^{-1}$  for the spheres. The lower limit was set by percolation; the upper limit was set by requiring a minimum optical transmission of 85%. Darker colors in the plots indicate larger concentrations.

Sheet resistance and optical transmittance decreased with increasing  $c_{Au}$  for both wires and spheres, but wires always had lower  $\bar{T}_{400-800}$  and  $R_{sh}$  for a given concentration. Functional electrodes could be made from both wires and spheres in the range  $c_{Au} \in 3$  to 10  $mg mL^{-1}$ . The FOM for wire-based electrodes in this range was at least 3.4 times larger than that of sphere-based electrodes. Resistances were more sensitive to  $c_{Au}$  than transmittances, and the FOM increased with  $c_{Au}$  for both nanocolloids. FTEs with the same optical transmittance always had lower  $R_{sh}$  when made from wires. Interestingly,  $\delta FOM/\delta c_{Au}$  for wire-based electrodes abruptly decreased at  $c_{Au} \approx 5$   $mg mL^{-1}$  to 75%. The highest FOM  $\approx 0.9\% \Omega_{sq}^{-1}$  of all FTEs in this study was for AuNW at  $c_{Au} = 10$   $mg mL^{-1}$ .

In the following, we analyze the effect of particle shape on grid morphology, starting with nanowires. The wires (Fig. 2A) had a core diameter  $d_w$  of 1.7 nm<sup>28</sup> and lengths  $l_w$  between 2  $\mu m$ <sup>33</sup> and 6.4  $\mu m$ <sup>34</sup> (aspect ratio on the order of 10<sup>3</sup>). Previous studies have shown that 70% of the wires at the concentrations used here are part of dispersed bundles.<sup>35</sup>

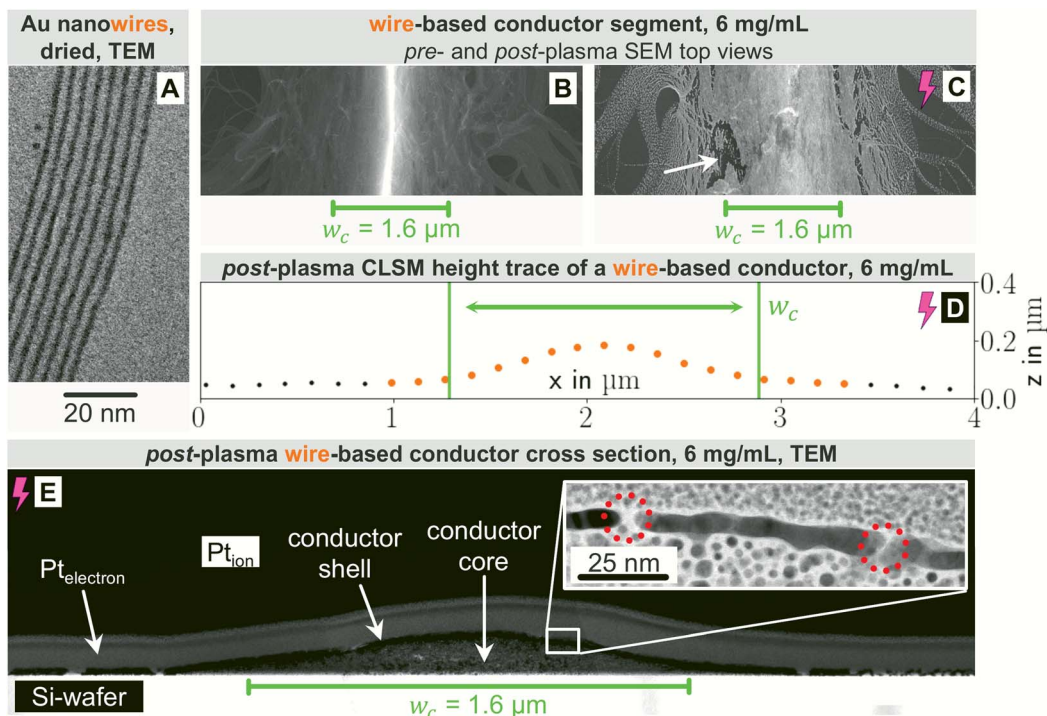
Fig. 2 shows top-view electron micrographs of grids imprinted from wire dispersions with  $c_{Au} = 6$   $mg mL^{-1}$  on doped Si before (B) and after (C) plasma sintering. Approximately 90% of the wires were concentrated and aligned in lines of width  $w_c$ , the rest exceeded the boundaries (bleeding) and was only partially aligned. A sharp ridge formed in the center of

the line. Plasma sintering partially removed the oleylamine and blunted the ridge. The wires in particularly thinly covered areas of the bled part fragmented, rendering them non-conductive. Fig. 2D shows the profile of a plasma-sintered line on PET foil obtained from CLSM. The wires formed a flat, Gaussian profile that was wider than the stamp feature, probably because the material flowed when the stamp was removed.

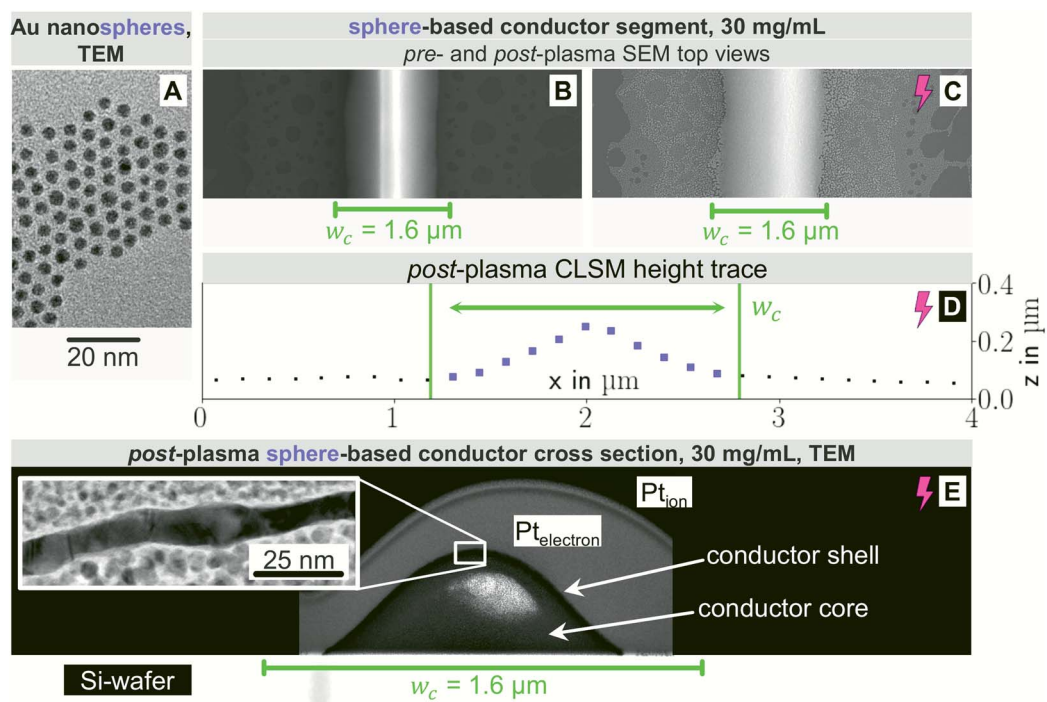
Bundling wires form extended networks.<sup>12,19,36</sup> We propose that they are gel-like and cannot be easily displaced by the stamp, which causes further bleeding (Fig. 2B and C). Defects in the conformal stamp-substrate contact due to edge imperfections and reduced contact pressure around the channel edges aggravate the effect.<sup>37</sup>

Fig. 2E is a transmission electron micrograph of a plasma-treated line on a silicon substrate. The change of the cross-sectional profile during plasma sintering was minor. Only the outermost part of the conductor was fully sintered, resulting in a structure with a metallic Au shell (average thickness  $t_{shell} = 5.7 \pm 1.1$  nm) and a hybrid, probably less conductive core. The plasma did not fully penetrate the deposited material, probably because shell formation is self-limiting. This explains why extended plasma sintering barely lowered  $R_{sh}$ . The cross section confirms that material beyond  $w_c$  contributes to conductivity and suggests that CLSM overestimates the height of the non-conductive areas next to the conductor. The shell of the center part was porous as marked in Fig. 2E, probably due to the AuNW bundle superstructure.

Compare, now, the wire-derived lines to samples formed from spheres. We imprinted Au cores with diameters  $d_{sp}$  of about 3.7 nm that were coated with a dense shell of OAM (shell thickness approximately 2 nm) as seen in Fig. 3A. They were fully dispersed according to Small Angle X-ray Scattering (Fig. S3 of the ESI†). Fig. 3 shows top-view electron micrographs of imprinted grids formed at  $c_{Au} = 30$   $mg mL^{-1}$  on doped silicon before (B) and after (C) plasma sintering. The lines were sharply delineated with little bleeding and a homogeneous surface



**Fig. 2** Typical morphological features of lines printed from AuNW at  $c_{Au} = 6 \text{ mg mL}^{-1}$  before and (purple flash) after plasma. (A): TEM image of dried and self-assembled wires. (B): SEM image (top-view) of a printed line. (C): SEM image (top-view) of a printed, plasma-sintered line; the white arrow indicates one of the typical crack-like defects which start forming at  $6 \text{ mg mL}^{-1}$  in the bled parts. (D): Height trace of a printed, plasma-sintered line. (E): TEM image of a cross-section of a printed, plasma-sintered line. Inset: A shell formed by the plasma. The red dashed circles indicate gaps within the shell.



**Fig. 3** Typical morphological features of lines printed from AuNP at  $c_{Au} = 30 \text{ mg mL}^{-1}$  before and (purple flash) after plasma. (A): TEM image of dried and self-assembled spheres. (B): SEM image (top-view) of a printed line. (C): SEM image (top-view) of a printed, plasma-sintered line. (D): Height trace of a printed, plasma-sintered line. (E): TEM image of a cross-section of a printed, plasma-sintered line. Inset: A shell formed by the plasma.

microstructure. The difference to wires is probably due to the spheres' excellent dispersion state even at high  $c_{\text{Au}}$  towards the end of the printing process. A ridge formed along the centre that was blunted by the plasma sintering and is no longer visible after plasma sintering. The center line microstructure remained homogeneous after plasma; coalescence and island formation beyond the defined feature did not contribute to conductivity.

Fig. 3D shows the CLSM profile of a plasma-sintered line on PET with a similar Gaussian profile as for nanowires above. Fig. 3E depicts the core-shell structure with a shell thickness  $t_{\text{shell}} = 8.1 \pm 1.4$  nm, slightly above that for wires, and a non-porous structure. Lines printed at  $c_{\text{Au}} = 12$  mg mL<sup>-1</sup> had similar features. At lower concentrations, closer to the percolation threshold, pores and disconnected segments formed (Fig. S7 in the ESI†).

In the following, we analyze the effect of particle concentration on the geometry of the printed, plasma-sintered grids. Confocal metrology provided a total of twenty height profiles measured on PET – one at each of the respective ten  $c_{\text{Au}}$  for both wires and spheres. Fig. 4A and B show topography maps of selected conductor segments, Fig. S4 and S5 of the ESI† show larger areas for the lowest and highest  $c_{\text{Au}}$ . We detected the edges of printed lines using a slope-based termination criterion (see Materials & Methods Section on CLSM). The cross sections of the shells were calculated by multiplying the average  $t_{\text{shell}}$

(Section S6 in the ESI†) with the outer contour length. The mean values of  $w$ ,  $h_{\text{max}}$  and  $A_{\text{shell}}$  as a function of gold concentration are shown in Fig. 4C, D and E.

The width and height of wire-derived imprinted lines increased with  $c_{\text{Au}}$  (Fig. 4A). The height of sphere-derived imprinted lines increased with  $c_{\text{Au}}$ , while their width was maximal at the lowest concentration and minimal at 12 mg mL<sup>-1</sup>. The difference between wires and spheres is likely due to the different agglomeration mechanisms. A considerable fraction of wires at  $c_{\text{Au}} = 1$  mg mL<sup>-1</sup> is bundled,<sup>35</sup> while spheres are still well dispersed at 30 mg mL<sup>-1</sup> (Fig. S3 in the ESI†).

The variation of  $\delta w/\delta c_{\text{Au}}$  for spheres is likely connected to ink viscosity and agglomeration. Low-concentration inks tend to have low viscosities, low contact angles, and longer drying times. They can easily migrate beyond  $w_c$  before complete solvent evaporation. Higher concentrations increase the viscosity and agglomeration rate, reducing  $w$  to below  $w_c$ . A small fraction of the ink still bleeds, and the highest concentration leads to a perceptible amount of metal deposited beyond  $w_c$ .

For wires,  $\delta h_{\text{max}}/\delta c_{\text{Au}}$  showed an increase at 3 mg mL<sup>-1</sup> which roughly coincided with  $w$  reaching  $w_c$ . This suggests that at lower concentrations, particles can freely assemble into increasingly wide lines. When  $w$  reaches  $w_c$ , additional particles add to the thickness or cause bleeding, and  $w/h_{\text{max}}$  drops

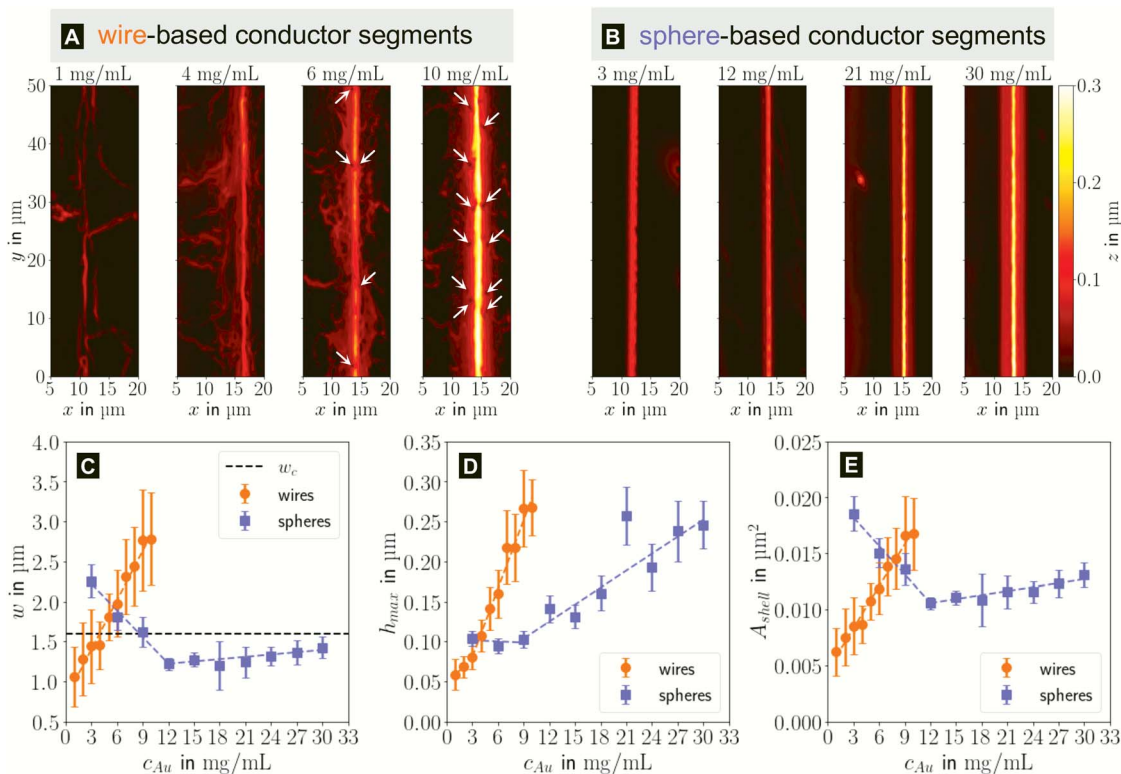


Fig. 4 Topography maps of (A) wire- and (B) sphere-based printed lines after plasma sintering. White arrows indicate defects similar to those in Fig. 2C. (C) Average conductor width  $w$ , (D) maximum conductor height  $h_{\text{max}}$  and (E) cross-sectional area  $A_{\text{shell}}$  as a function of gold concentration  $c_{\text{Au}}$ . Standard deviations are indicated as error bars, the dashed lines are fits by linear regression to better illustrate the (piece-wise) linear behaviour.

steadily at  $4 \text{ mg mL}^{-1}$  and above (Fig. S9 in the ESI†). A similar change of  $\delta h_{\text{max}}/\delta c_{\text{Au}}$  for spheres at  $9 \text{ mg mL}^{-1}$  coincided with the  $w = w_c$ , too, suggesting the same mechanism.

The cross-sectional area  $A_{\text{shell}}$  was almost proportional to  $w$  for both wires and spheres (Fig. 4E). This is because  $t_{\text{shell}}$  is set by the plasma process and practically independent of  $c_{\text{Au}}$ . The conductor width  $w \gg h_{\text{max}}$  dominates the product  $t_{\text{shell}} \cdot w$ .

For wires, percolation and electrical conductivity occurred at  $2 \text{ mg mL}^{-1}$ ; crack-like defects appeared at  $6 \text{ mg mL}^{-1}$  (white arrows in Fig. 4A), and became denser with increasing  $c_{\text{Au}}$ . They did not affect  $w$  and  $A_{\text{shell}}$  but affected the conductivity  $\sigma_{\text{shell}}$ , which changed sign and slope at  $6 \text{ mg mL}^{-1}$  (Fig. 5C).

With CLSM, the sphere-derived lines appeared mostly defect-free (due to the limited resolution and field of vision) as shown in Fig. 4B. A detailed analysis indicated, however, that lines formed at low concentrations (3 to  $9 \text{ mg mL}^{-1}$ ) contained large discontinuous segments and exhibited numerous pores (Fig. S7 of the ESI†). Additionally, we found imprinting defects (Fig. S8 in the ESI†) due to tapered or clogged stamp channels and stamp irregularities. They appear less frequently than the cracks in wire-based lines but reduce  $\sigma_{\text{shell}}$  more drastically because they often affect the entire width of the line and render it non-conductive. We propose that small, dispersed spheres are more susceptible to such defects because their superstructures are more easily disrupted than network-forming, bundling wires. Increasing  $c_{\text{Au}}$  increases the probability that irregularities are bridged by a thicker particle layer.

The measured macroscopic sheet resistance  $R_{\text{sh}}$  of the transparent electrodes is due to the parallel conductivity of 750 parallel printed lines of length  $l = 1.5 \text{ cm}$ . If we assume that only their shells with cross-sectional areas  $A_{\text{shell}}$  conduct, the overall sheet resistance is

$$R_{\text{sh}}^{-1} = R^{-1} = G = \sigma_{\text{shell}} \cdot \frac{750 \cdot A_{\text{shell}}}{l} \Rightarrow \sigma_{\text{shell}} = G \cdot \frac{l}{750 \cdot A_{\text{shell}}}, \quad (2)$$

and we can calculate conductivities of the shell material  $\sigma_{\text{shell}}$  as shown in Fig. 5C. We test this assumption below.

The shell conductivities  $\sigma_{\text{shell}}$  universally increased with increasing  $c_{\text{Au}}$ . They remained below one third that of bulk Au

( $\sigma_{\text{Au}} \approx 4.52 \times 10^7 \text{ S m}^{-1}$ ).<sup>38</sup> The most conductive shells had  $1.39 \times 10^7 \text{ S m}^{-1}$  for wire-based and  $1.02 \times 10^7 \text{ S m}^{-1}$  for sphere-based line arrays, in the range reported for ultra-thin polycrystalline Au films with thicknesses of 5.5 to 8.0 nm,<sup>39</sup> below the electron mean free path of  $\lambda_{\text{Au}} \approx 37.7 \text{ nm}$ .<sup>40</sup> This is consistent with a shell-dominated conductivity.

The change of  $\delta \sigma_{\text{shell}}/\delta c_{\text{Au}}$  at  $5 \text{ mg mL}^{-1}$  for wire-based lines is due to the line width  $w$  that exceeds  $w_c$  (Fig. 4C), accompanied by an increasing number of crack-like defects in the shell as discussed above (Fig. 4A).

The wire-based lines outperformed the sphere-based lines at every  $c_{\text{Au}}$  despite a thinner (5.66 nm vs. 8.07 nm), porous shell. A possible explanation is the increased defect density in sphere-based lines. It does not affect  $w$ ,  $h_{\text{max}}$  and  $A_{\text{shell}}$ , but can render entire lines non-conductive so that they contribute nothing to  $\sigma_{\text{shell}}$ . A second difference are grain boundary densities in the shells. The wires are micrometer-long single crystals<sup>29</sup> and largely oriented in imprinting direction. Their crystallinity may be at least partly retained during plasma sintering,<sup>41</sup> while spheres are likely to create small grains. Thirdly, the likelihood that the only partially sintered line core also contributes to conduction, is higher in case of the high aspect ratio wires than in case of the spheres ( $l_w \gg d_{\text{sp}}$ ).

In summary, the electrical properties of both electrode types were dominated by the core/shell structure of its conductors. Defects within the conductor shell and concentration independent shell thicknesses below  $\lambda_{\text{Au}}$  prevented  $\sigma_{\text{shell}}$  from reaching bulk Au conductivity. The wires' ability to self-assemble into percolating superstructures even at the lowest concentration used is the basis for the superior performance of wire-derived electrodes.

The printed lines reduce the optical transmittance mainly by masking parts of the substrate. The change in optical transmittance  $\delta \bar{T}_{400-800}/\delta c_{\text{Au}}$  was always negative for both wires and spheres (Fig. 6A and B). The value was constant for spheres; it changed at  $6 \text{ mg mL}^{-1}$  for wires, close to where  $w$  exceeded  $w_c$  (Fig. 4C). Wire-based electrodes had lower optical transmittances; all were above  $\approx 85\%$  and thus practically useful.

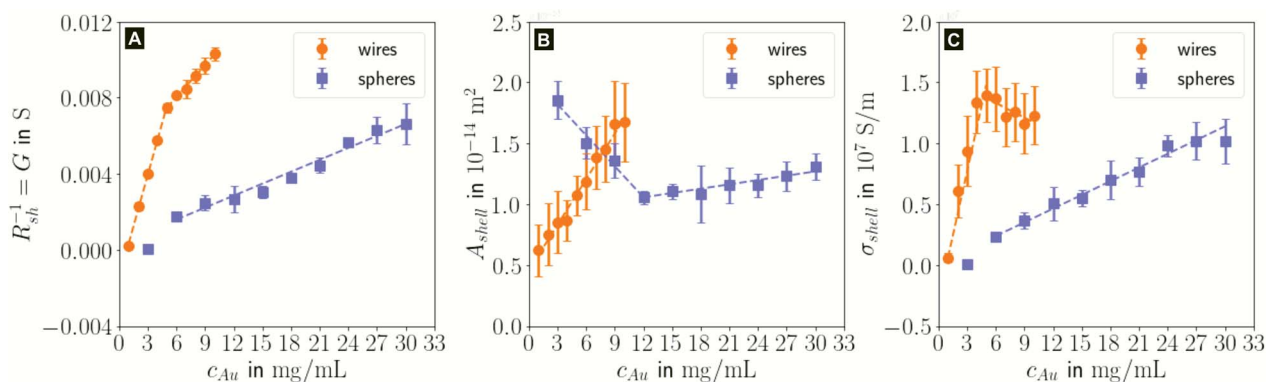


Fig. 5 Effect of particle concentration  $c_{\text{Au}}$  on (A) the conductance  $G$  of a representative square electrode sub-section, (B) the cross-sectional area  $A_{\text{shell}}$  and (C), the shell conductivity  $\sigma_{\text{shell}}$ . Standard deviations are indicated as error bars, the dashed lines are fits by linear regression to better illustrate the piece-wise linear relations.



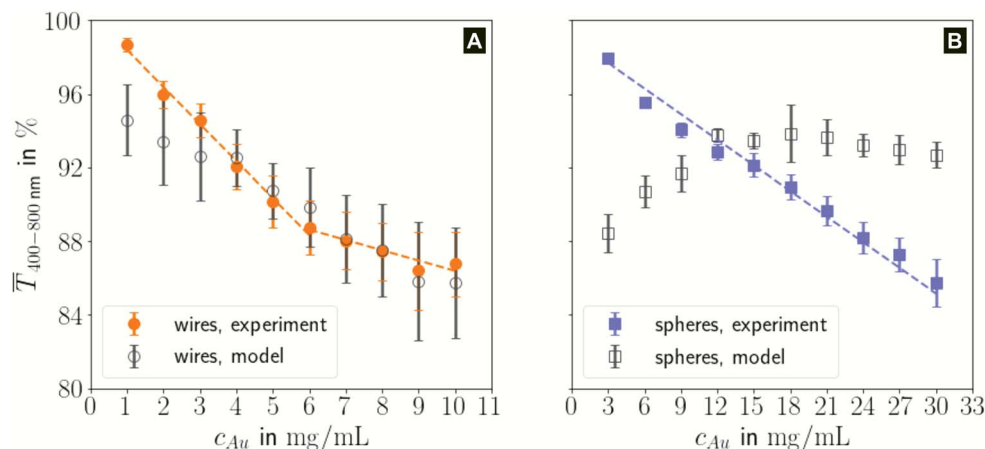


Fig. 6 Development of the optical transmittance  $\bar{T}_{400-800}$  for (A) wire- and (B) sphere-based electrodes (experiment and model) with concentration  $c_{Au}$ , the belonging standard deviation and a data fit (dashed lines).

We approximated the metal lines as rectangles of width  $w$  at pitch  $p$  using data from CLSM measurements (the stamp pitch was  $p = 19.5 \mu\text{m}$ ). The PET substrate was taken to be transparent and the rectangular lines as opaque. This yields a model transmittance  $T_{\text{model}}$  (Fig. S10 of the ESI†) of

$$T_{\text{model}} = \left(1 - \frac{w}{p}\right) \cdot 100\% \quad (3)$$

The experimental  $\bar{T}_{400-800}$  for wire-based lines were above  $T_{\text{model}}$  (Fig. 6A) up to  $c_{Au} = 3 \text{ mg mL}^{-1}$ . The lines at such low concentrations were narrow but thin (Fig. 4C and D) and likely not fully opaque over the entire width. The lines formed above  $4 \text{ mg mL}^{-1}$  had  $w > w_c$  (Fig. 4C) and became increasingly thicker (Fig. 4D and S9 in the ESI†). This increased their opacity and improved the match between model and experiment in the range 4 to  $10 \text{ mg mL}^{-1}$ .

The experimental  $\bar{T}_{400-800}$  for sphere-based lines exceeded  $T_{\text{model}}$  for 3 to  $9 \text{ mg mL}^{-1}$ . The lines were broad (Fig. 4C) and thin in this range, only growing in thickness at  $9 \text{ mg mL}^{-1}$  and above (Fig. 4D and S9 in the ESI†). In contrast to wires, we found that  $T_{\text{model}} - \bar{T}_{400-800} > 0$  above  $12 \text{ mg mL}^{-1}$ , probably because the metal that was deposited beyond  $w$  (Fig. 3C) caused strong diffuse scattering.

In summary, sphere-based outperformed wire-based electrodes in optical transmittance. Lines formed from spheres at low concentrations were more transparent; lines formed at higher concentrations were narrower. This is likely a direct consequence of the bundling wires' lower percolation threshold that enabled significant material deposition beyond  $w_c$ , which more than compensated for the increasing bleeding of spheres at high concentrations.

Considering both optical and electrical properties,  $c_{Au}$  affected optical transmittance much less than  $R_{\text{sh}}$  for both wires and spheres (Fig. 5A). The overall FOM was dominated by the sheet resistance, which explains the better performance of wire-based electrodes (Fig. 1).

## 4 Conclusion

Flexible transparent electrodes were imprinted from AuNP or AuNW at different concentrations and treated with plasma that partially removed the oleylamine ligand. We found strong correlations between the geometry of the nanocolloid, the concentration used for imprinting, the resulting post-plasma grid morphology, and the opto-electronic performances.

Plasma sintering led to a conductor structure with an outer gold shell that covered a hybrid core. The imprinted lines' average conductivity  $\sigma_{\text{shell}}$  depended on the density of defects in the shell that changed depending on concentration and particle type and rendered some lines discontinuous. Wire-based inks were less prone to such discontinuities and thus outperformed the sphere-based inks. The wires' aspect ratios of above 1000 facilitated their self-assembly into percolating superstructures that bridged stamp and substrate irregularities. This result is interesting for industrial processes that require a robust printing of lines. At concentrations  $\geq 6 \text{ mg mL}^{-1}$ , an increasing number of crack-like defects occurred within the bled parts of wire-based conductors and impaired  $\sigma_{\text{shell}}$ .

The optical transmittance of wire-based electrodes made with concentrated inks followed a simple model that assumes opaque lines.  $\bar{T}_{400-800}$  of sphere-based electrodes made with concentrated inks was more strongly affected by bleeding that led to areas of partial transmittance. Nevertheless, sphere-based outperformed wire-based electrodes due to a better definition of geometry at high concentrations ( $7-10 \text{ mg mL}^{-1}$ ) and due to more transparent lines at lower concentrations ( $3-6 \text{ mg mL}^{-1}$ ).

For both wires and spheres, concentration affected  $\bar{T}_{400-800}$  much less than  $R_{\text{sh}}$ . The FOM was thus dominated by  $R_{\text{sh}}$ , and wire-based electrodes that reached significantly lower  $R_{\text{sh}}$  at the same Au content performed better than sphere-based electrodes.

Both wire- and sphere-based electrodes had relatively large non-conductive parts. Their fraction may be reduced by tuning the ligand chemistry and the plasma process. It should be

possible to deposit lines that are thin enough to be entirely converted into metal, for example, if the plasma step is optimized such that it does not degrade their continuity.

An important aspect that has not been covered here is the stability of printed conductors. Thin metal films are prone to slow de-wetting<sup>42</sup> and electromigration.<sup>43</sup> Wire-based electrodes with their pores and large, crack-like defects at higher concentrations are particularly vulnerable to such mechanism. Their relevance will be discussed in a forthcoming manuscript.

## Author contributions

L. F. Engel designed the studies, performed the experiments himself or supervised them, implemented Python code for data analysis and visualization, analysed and visualized all acquired data and wrote the original draft. L. González-García and T. Kraus conceptualized the overarching research goals, acquired funding, administered, and supervised the project. They reviewed, edited and commented on the manuscript drafts.

## Conflicts of interest

There are no conflicts to declare.

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