

# SCIENTIFIC REPORTS



OPEN

## Radial Wettable Gradient of Hot Surface to Control Droplets Movement in Directions

Shile Feng, Sijie Wang, Yuanhao Tao, Weifeng Shang, Siyan Deng, Yongmei Zheng & Yongping Hou

Received: 09 October 2014

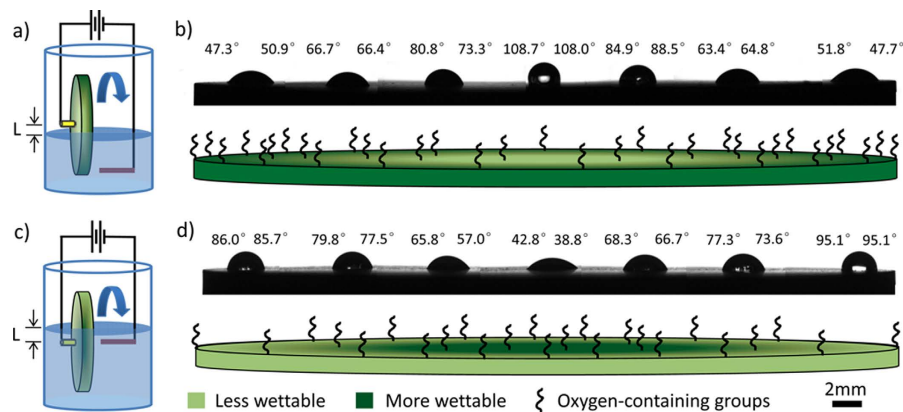
Accepted: 27 March 2015

Published: 15 May 2015

A radial wettable gradient was fabricated on the surface of graphite plate by a simple one-step anodic oxidation process. It was found that the direction and value of the wettable gradient could be easily controlled by adjusting current and oxidation time gradient. With the increase of surface temperature, droplets on surface not only exhibited the transition of boiling mode, but also showed the controlled radial spreading, evaporation and movement behaviors. These phenomena could be attributed to the cooperation of wettability force, hysteresis force and vapor pressure (Leidenfrost effect). Especially, the controlled radial convergence or divergence of droplets with high velocity were realized on the surfaces with either inside or outside radial gradient, which would have crucial applications in the design of microfluidic devices and the exploration of the biotechnology.

The directional movement behaviors of droplets on a surface with wettable gradient exhibit important applications in the design of microfluidic devices and exploration of the biotechnology<sup>1–4</sup>. The different features on wettability at the front and rear of the droplet, which introduces the unbalanced force around the periphery of the droplet,<sup>5</sup> could be achieved via controlling the surface chemical composition and tailoring the surface morphology<sup>6–9</sup>. Chaudhury and Whitesides first created a wettable gradient surface via chemical deposition and further demonstrated that a droplet ran uphill spontaneously on the inclined surface<sup>8</sup>. Ashutosh Shastry *et al.*<sup>10</sup> fabricated a surface with gradient wettability resulted from the solid-liquid contact area fraction, on which droplets motion directionally. Ding-Jun Huang *et al.*<sup>11</sup> described a fabrication process of the surface energy gradient on copper substrate by H<sub>2</sub>O<sub>2</sub> immersion and fluorination with Teflon, which effectively controlled the change of wettability from superhydrophilic to superhydrophobic ones. On the other hand, liquid motion could be controlled by introducing external stimuli such as light<sup>12,13</sup>, heat<sup>14</sup>, vibration<sup>15</sup> and non-equilibrium noise<sup>16</sup>. Kunihiro Ichimura *et al.*<sup>12</sup> modified silica plate with a photoisomerizable azobenzene monolayer and the motion of liquids could be manipulated reversibly by photo irradiation. George Karapetsas *et al.*<sup>14</sup> propelled droplets by a non-uniformly heated substrate. Susan Daniel *et al.*<sup>15</sup> fabricated a surface of relatively high modulus poly-(dimethylsiloxane) (PDMS) on a glass and the droplets were directionally driven by asymmetric lateral vibration. In the previous studies, the fabrication and controlled methods of gradient surface were difficult to implement and the direction of wettable gradient was simple. Although the controlled radial movement of droplets has more important potential applications<sup>4</sup>, few researches have been done due to the difficult fabrication of radial wettable gradient. Therefore, it remains challenging to fabricate gradient at multi-dimensions (e.g., radial direction of gradient on a surface) achieve the controlled radial movement of droplets via a simple, fast and efficient method. Here, we fabricated a radial wettable gradient surface by a simple one-step anodic oxidation process. By controlling the current gradient and oxidation time, the direction and value of the wettable gradient could be easily adjusted. At ambient temperature, droplets on the wettable gradient surface showed radial spreading, and at high temperature, the radial

Key Laboratory of Bio-Inspired Smart Interfacial Science and Technology of Ministry of Education, Beijing Key Laboratory of Bio-inspired Energy Materials and Devices School of Chemistry and Environment Beihang University, Beijing, 100191 (P. R. China). Correspondence and requests for materials should be addressed to Y.Z. (email: zhengym@buaa.edu.cn) or Y.H. (email: houyongpingog@buaa.edu.cn)



**Figure 1. Schematic diagrams of experimental set-up for the fabrication of the wettable gradient and the photographs of the water contact angles.** **a)** Experimental set-up. Electrolyte level is below the center. The point close to the center has a shorter oxidation time and lower current density. A radial wettable gradient is fabricated with the direction from center to periphery. **b)** Photographs of the water contact angles along the graphite surface with wettable direction from center to periphery. More oxygen-containing groups are formed on the periphery. **c)** Electrolyte level is above the center, the radial wettable gradient is in opposite direction, from periphery to center. **d)** Photographs of the water contact angles along the graphite surface with wettable gradient direction from periphery to center. More oxygen-containing groups are formed on the central parts.

evaporation or motion of droplets was realized due to the cooperation between the Leidenfrost effect<sup>17,18</sup> and the wettable gradient driving force. These new phenomena would promote the development of microfluidic device and the design of heat exchanger.

## Results

A circular graphite plate with radial wettable gradient was fabricated by an improved anodic oxidation (see experiment section). As shown in Fig. 1a, when the electrolyte level is below the center for a given distance ( $L$ ), the oxidation time ( $t_{rb}$ ) could be described as:

$$t_{rb} = \frac{\cos^{-1} \frac{L}{r}}{\pi} \times T \quad (1)$$

Where  $t_{rb}$  is the anodic oxidation time at the point away from the center of graphite plate with a distance of  $r$ .  $T$  is the rotation period. We plotted the value  $t_{rb}/T$  as a function of the value of  $L/r$ , which is shown in Figure S1a. For given values of  $L$  and  $T$ , the time of anodic oxidation ( $t_{rb}$ ) is positive correlated with  $r$ . In addition, because of the position relation of the cathode and anode, a current gradient could be formed during the oxidation process<sup>19</sup>. On the binary collaboration effect above (time gradient and current gradient), the radial wettable gradient is gained with the direction from center to periphery (the point close to the center has a shorter oxidation time and lower current density). For Sample-A ( $L=3$  mm,  $T=5$  s), contact angles (CAs) decrease from  $\sim 108.3^\circ$  to  $\sim 47.5^\circ$  with the increase of  $r$ , showing a wettable gradient of  $\sim 4.1^\circ/\text{mm}$  (Fig. 1b). When the electrolyte level is above the center for a given distance ( $L$ ) (Fig. 1c), for each point on the surface of graphite plate, the oxidation time ( $t_{ra}$ ) could be described as:

$$t_{ra} = \left( 1 - \frac{\cos^{-1} \frac{L}{r}}{\pi} \right) \times T \quad (2)$$

Here  $t_{ra}$  is the anodic oxidation time at the point away from center of graphite plate with a distance of  $r$ . For given values of  $L$  and  $T$ , the  $t_{ra}$  could be regarded as a function of the  $r$  (Figure S1b). Clearly, the  $t_{ra}$  decreases gradually with the increase of the  $r$ . Based on the same principle as mentioned above (time gradient and current density gradient), a radial wettable gradient could be fabricated with the direction from periphery to center. For Sample-B ( $L=3$  mm,  $T=5$  s), the CAs could change from  $\sim 40.8^\circ$  to  $\sim 85.8^\circ$  gradually and the average value of wettable gradient achieves  $\sim 3.5^\circ/\text{mm}$ . We also investigated the influence of two parameters, e.g.,  $L$  and  $T$  on the wettable gradient. The results indicate that the value of wettable gradient could be adjusted from  $\sim 2.1$  to  $\sim 4.1^\circ/\text{mm}$  and the  $L$  seemed to have a greater influence

on the wettability gradient (Figure S2). Clearly, the radial wettability gradient on a circular graphite plate could be easily fabricated by an improved anodic oxidation method and both the direction and value of wettability gradient could be controlled via changing the two parameters, i.e.,  $L$  and  $T$ .

Energy dispersive spectrometer (EDS) experiment of Sample-A was shown in Figure S3 and Table S1. The ratio of O/C increases gradually from 0.0448 to 0.3467 with the increase of distance away from the center. Due to the fact that the C content can be considered as a constant on the surface of graphite plate, a gradient of O content is formed during the anodic oxidation process and more oxygen-containing surface groups (C–OH, C=O, COOH) are formed on the periphery of graphite plate<sup>19</sup>. In addition, scanning electron microscope (SEM) observations show that the surface is very rough and the change of morphology at different areas is little (Figure S4). It has been recognized that the topographic structures and the surface chemical compositions are crucial to surface wettability. In our experiments, all of the results indicate that the wettability gradient on graphite plate is mainly controlled by the gradient of chemical composition, and the value of wettability gradient is amplified by the roughness of surface (i.e., from hydrophilic to more hydrophilic ones, or from hydrophobic to more hydrophobic ones<sup>20</sup>).

Although a large wettability gradient is already realized ( $\sim 4.1^\circ/\text{mm}$ ), the water droplets could only exhibit directional spreading at room temperature (shown in Figure S5 and Figure S6). On both surfaces (Sample-A and Sample-B), when a water droplet comes in contact with the surface, it spreads along the wettability gradient immediately and shows an asymmetric shape due to large wettability gradient forces and high hysteresis force<sup>21</sup>.

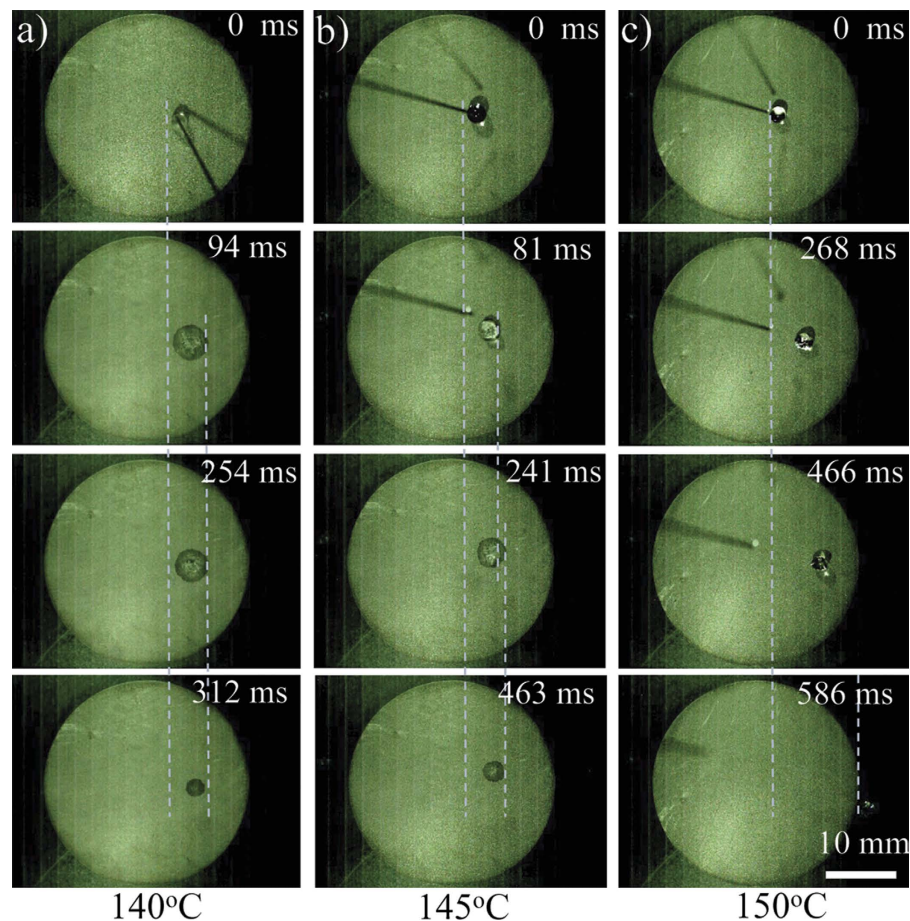
It is well known that a liquid would levitate on a cushion of its own vapor when it contacts with a hot solid (Leidenfrost effect). Linke *et al.*<sup>17</sup> used the effect to reduce the hysteresis forces and realized the self-propulsion of droplets on the asymmetric topology surface. Ali Hashmi *et al.*<sup>18</sup> demonstrated that a small cart could be levitated by Leidenfrost vapor to reduce the friction. The cart could be propelled not only by gravitational force over a slanted flat surface, but also self-propelled over a ratchet shaped horizontal surface. Here, we also heated the graphite plate to reduce the hysteresis forces to control the motion of droplets. When a liquid droplet is dripped on a surface heated above its boiling point, three typical cases are formed, nucleate boiling (the droplet boils immediately when it contacts the heated surface), gentle film boiling (the droplet floats on its own vapor called Leidenfrost vapor layer without any contact with the surface), and spraying film boiling (both Leidenfrost vapor layer and sputtering tiny droplets). The critical temperature for the formation of Leidenfrost vapor layer is defined as Leidenfrost temperature ( $TL$ )<sup>22</sup>. Figure S7 shows the negative correlation of the Leidenfrost temperature and CAs at different positions of Sample-A<sup>23</sup>. With the decrease of CAs (Fig. 1b, S7), Leidenfrost temperature increases from  $\sim 143.2^\circ\text{C}$  to  $\sim 149.7^\circ\text{C}$  due to the fact that hydrophobic surface performs more favorable conditions for the formation and growth of bubbles than hydrophilic surface and the generated bubbles are easier to merge to vapor blanket<sup>23</sup>.

Figure 2 shows the movement behaviors of droplets on the surface of Sample-A heated at different temperatures. When the temperature varies from  $\sim 140^\circ\text{C}$  to  $\sim 150^\circ\text{C}$ , only nucleate boiling and gentle film boiling modes are observed. At  $\sim 140^\circ\text{C}$ , since the temperature of the whole graphite plate is lower than Leidenfrost temperature ( $\geq 143.2^\circ\text{C}$ ), the boiling mode is nucleate boiling. When a droplet is dripped on the heated surface, it spreads along the wettability gradient direction at  $\sim 94$  ms, exhibiting directional spreading and then evaporates extremely fast in  $\sim 94$ – $312$  ms, showing directional evaporation (Fig. 2a). At  $\sim 150^\circ\text{C}$ , as the temperature is higher than Leidenfrost temperature ( $\leq 149.7^\circ\text{C}$ ), boiling mode changes to gentle film boiling on the whole surface. When a droplet is dripped on the heated surface, it keeps ball shape and slides off the horizontal surface fast along the wettability gradient direction only at  $\sim 586$  ms (Fig. 2c). At  $\sim 145^\circ\text{C}$ , initially, the droplet moves along the wettability gradient at 81 ms, just as that at  $\sim 150^\circ\text{C}$  because the temperature is larger than Leidenfrost temperature and the boiling mode is gentle film boiling. The increase of hydrophilicity induces the increase of Leidenfrost temperature. At the sites with the Leidenfrost temperature of above  $145^\circ\text{C}$ , the boiling mode changes to nucleate boiling. The droplet exhibits directional spreading in  $\sim 81$ – $241$  ms and then directional evaporation in  $\sim 241$  to  $\sim 463$  ms (Fig. 2b), just as at  $\sim 140^\circ\text{C}$ . The similar movement behaviors can also be observed on Sample-B. Clearly, not only the change of boiling mode, but the radial directional spreading, evaporation and sliding behaviors are observed in our work and the movement behaviors are controlled easily via temperature.

All the observations result from the nucleation, growth and departure of bubbles on wettability gradient surface. The bubble emission frequency is defined as<sup>24</sup>:

$$f = \frac{1}{\tau_{gt} + \tau_{wt}} \quad (3)$$

Here  $f$  is the bubble emission frequency,  $\tau_{gt}$  is the growth time (the duration of the growth of bubbles) and  $\tau_{wt}$  is the waiting time (the duration between the departure of the former bubble and the appearance of the current bubble). Hai Trieu Phan *et al.*<sup>24</sup> demonstrated that the bubble emission frequency decreased with the rise of surface hydrophilicity and the decrease of temperature. At low superheat (below Leidenfrost temperature,  $\sim 140^\circ\text{C}$ ), the boiling mode is nucleate boiling. Due to the fact that the drop tends to create nearly equal contact angles at both edges under effect of the Laplace pressure within the



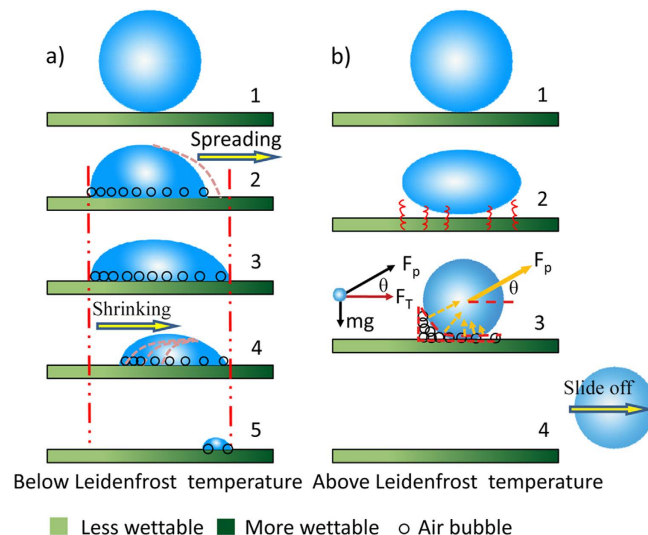
**Figure 2. Movement behaviors of droplets on surface of Sample-A heated at different temperature.**

**a)** The movement behaviors of droplet on the surface at  $\sim 140^\circ\text{C}$ . The droplet spreads along the wettability gradient direction at  $\sim 94$  ms, and exhibits directional evaporation in  $\sim 94$ – $312$  ms. **b)** The movement behaviors of droplet on the surface at  $\sim 145^\circ\text{C}$ . Initially, the droplet moves along the wettability gradient direction at  $\sim 81$  ms and then exhibits directional spreading in  $\sim 81$ – $241$  ms. Finally, it exhibits directional evaporation in  $\sim 241$ – $463$  ms. **c)** The sliding behavior of droplet at  $\sim 150^\circ\text{C}$ . The droplet keeps ball shape and slides off the horizontal surface fast along the wettability gradient direction at  $\sim 586$  ms. The volume of droplet is  $10\ \mu\text{L}$ . The scale bar, 10 mm.

drop<sup>25</sup> and the unbalanced wettability force points to the more wettable side, the droplet initially spreads along wettability gradient, exhibiting directional spreading (Fig. 3a, Frame 2, 3). Subsequently, since the hydrophobic surface performs more favorable conditions for the formation and growth of bubbles than hydrophilic surface (the evaporation velocity on relative hydrophobic sites is larger) and wettability force points to the more wettable side, the less wettable side shrinks and the more wettable side is pinned until the whole droplet disappears, exhibiting directional evaporation (Fig. 3a, Frame 4, 5). At high superheat (above Leidenfrost temperature), the boiling mode is gentle film boiling. The decrease of waiting time induces a larger bubble emission frequency and the generated bubbles are easier to merge to vapor blanket (Fig. 3b, Frame 2). So, the droplet would keep a ball shape (Fig. 3b, Frame 3). More bubbles are generated at the hydrophobic site and a vapor pressure gradient is introduced. Due to the high pressure at the hydrophobic site, the total pressure could be written as  $F_p$ , which points to the more wettable side and has an angle  $\theta$  with horizontal plane. Under the effect of pressure and gravity ( $mg$ ) ( $m$  is the mass of droplet,  $g$  is the acceleration due to gravity), a horizontal total force  $F_T$  is generated. Due to the Leidenfrost effect<sup>17</sup>, hysteresis force ( $F_H$ ) becomes much smaller than total force  $F_T$ . Therefore, above Leidenfrost temperature, a droplet keeps ball shape with high CA and slides off the horizontal surface fast along the wettability gradient direction (Fig. 3b, Frame 4), corresponding to the observation at  $\sim 150^\circ\text{C}$ . At  $\sim 145^\circ\text{C}$ , due to the different boiling modes on the different sites, all of the directional spreading, evaporation and movement are observed.

We surveyed the directional movement behaviors of droplets on different points of the graphite plates on Sample-A and Sample-B at  $\sim 150^\circ\text{C}$ . For Sample-A, when a droplet is dripped near to the center of the surface, it can slide along the outside radial direction (i.e., wettability gradient direction) and slide off





**Figure 3. Schematic diagrams for the mechanism of directional droplet motion on over-heated wettable gradient surface.** **a)** The directional spreading and evaporation behaviors of droplet on wettable gradient surface. The droplet initially spreads directionally along wettable gradient (Frame 2, 3). With lower superheat, the evaporation velocity of droplet at relative hydrophobic site is larger. The less wettable side shrinks and the more wettable side is pinned until the whole droplet disappears, exhibiting directional evaporation (Frame 4, 5). **b)** The directional sliding behaviors of droplets on wettable gradient surface with gentle film boiling mode. At higher superheat, the decrease of waiting time induces a larger bubble emission frequency and the generated bubbles are easier to merge to vapor blanket (Frame 2). It induces the droplet in a ball shape (Frame 3). More bubbles at the hydrophobic site induce vapor pressure gradient. Droplets slide off the graphite plate quickly under effects of pressure and gravity (Frame 4).

the surface in less than  $\sim 500$  ms with a velocity of  $\sim 40$  mm/s (Fig. 4 a-d,i). Otherwise, when a droplet is dripped at the periphery of the Sample-B surface, it could also slide along the inside radial direction (i.e., wettable gradient direction) with the velocity of  $\sim 30$  mm/s (Fig. 4 e-h,j). After the droplet passes the center, the direction of wettable gradient force reverses, which would hinder the movement of droplet. Therefore, the velocity slows down gradually until the droplet slides off the surface (Figure S8). Clearly, controlled radial spreading or convergence and divergence of droplets on the graphite plate at high temperature are realized for the first time by a one-step anodic oxidation method.

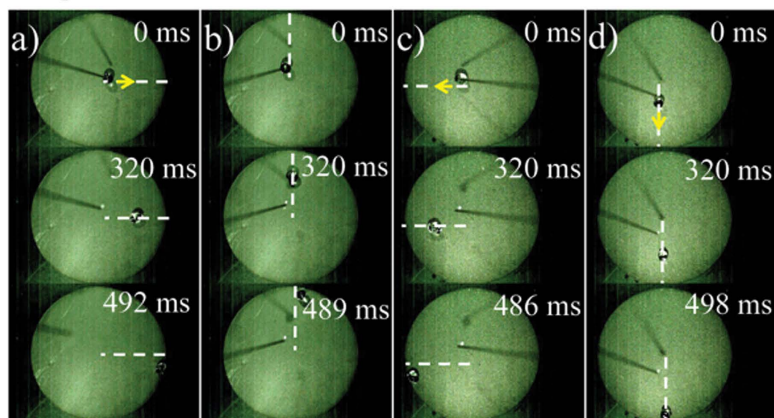
In conclusion, radial wettable gradient with direction toward the periphery or the centre of graphite plate was easily achieved by a one-step anodic oxidation method. At room-temperature, droplets on such kind of surface could exhibit controlled radial spreading behaviors. At higher temperature, due to the wettable gradient, not only the transition of boiling mode, but also the directional spreading, evaporation and movement behaviors of the droplets were observed. The radial convergence and divergence of droplets were controlled effectively on the graphite plate at high temperature, which can be extended to realm of micro-fluidics and the exploration of the biotechnology.

## Methods

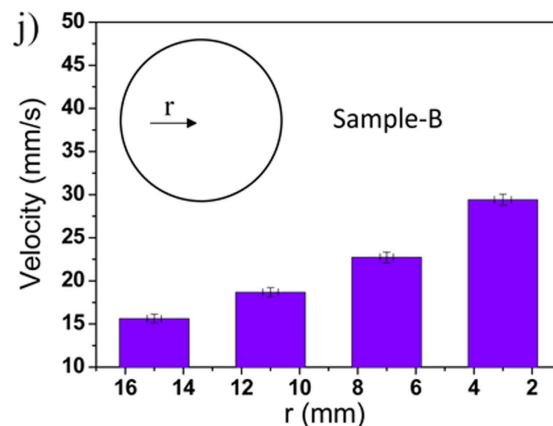
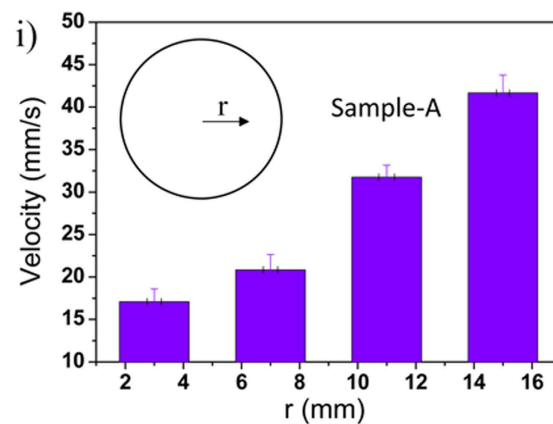
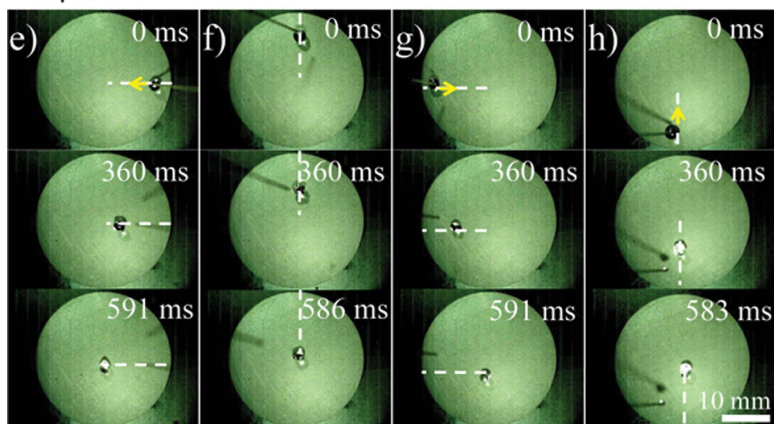
**Preparation of a circular graphite plate with radial wettable gradient.** A circular graphite plate (diameter: 30 mm, thickness: 3 mm, manufactured by Ji Xing Sheng, in Co. of Beijing, China) with no visible scratches were rinsed thoroughly with ethanol and deionized water for following use. The radial wettable gradient on a circular graphite plate was fabricated by an improved anodic oxidation with 0.05 M sodium hydrate (NaOH) electrolyte solution and a constant current of 0.5 A. The electrolyte level is set above or below the center of the circular graphite plate with a certain distance ( $L$ ) to control the direction of wettable gradient. During the anodic oxidation process, the circular graphite plate was rotated uniformly for a cycle with a constant period ( $T$ ). The schematic diagram of experimental set-up was shown in Fig. 1a,c. The center of circular graphite plate is zero point position.

**Characterization.** Water contact angles (CAs) were measured by the optical contact angle meter system (OCA40Micro, Dataphysics Instruments GmbH, Germany) and the static CAs were determined by the averages of at least five measurements. The volume of the droplet is  $5 \mu\text{L}$ . The directional movement behaviors of droplets were observed by a high speed CCD (HSCCD, V9.1, PHANTOM, America). The temperature was controlled by heating stage (IKA C-MAG HS7). Scanning electron microscope (SEM, Quanta FEG 250, FEI) was employed for the surface micro-structure analysis of graphite plate.

## Sample-A: 150°C



## Sample-B: 150°C



**Figure 4. Outside radial movement of droplet on surface of Sample-A at ~150°C.** a) Droplet moves from center to right periphery. b) Droplet moves from center to top periphery. c) Droplet moves from center to left periphery. d) Droplet moves from center to bottom periphery. When the droplet is dripped beside the center of the surface, it slides along the outside radial direction (i.e., wettable gradient direction) and sliding off the surface in less than ~500 ms. **Inside radial movement of droplet on surface of Sample-B at ~150°C.** e) Droplet moves from above periphery to center. f) Droplet moves from left periphery to center. g) Droplet moves from right periphery to center. h) Droplet moves from bottom periphery to center. When the droplet is dripped at the periphery of the Sample-B surface, it could slide along the inside radial direction (i.e., wettable gradient direction) and move to the center of graphite plate in less than 600 ms. i) Sliding velocities of droplets on different points on surface of Sample-A at ~150°C. j) Sliding velocities of droplets on different points on surface of Sample-B at ~150°C ( $r$  is the distance to center of graphite plate). The volume of the droplet is 10  $\mu$ L. The scale bar, 10 mm.

The chemical composition was measured by field emission scanning electron microscopy (FESEM) with energy dispersive spectrometer (EDS) (JSM-7500 F, JEOL, Japan).

## References

- John, K., Bar, M. & Thiele, U. Self-propelled running droplets on solid substrates driven by chemical reactions. *Soft. Matter* **18**, 183–199 (2005).
- Moumen, N., Subramanian, R. S. & McLaughlin, J. B. Experiments on the motion of drops on a horizontal solid surface due to a wettability gradient. *Langmuir* **22**, 2682–2690 (2006).
- Bardaweel, H. K., Zamuruyev, K., Delplanque, J. & Davis, C. E. Wettability-gradient-driven micropump for transporting discrete liquid drops. *J. Micromech. Microeng.* **23**, 035036 (2013).
- Fang, G., Li, W., Wang, X. & Qiao, G. Droplet motion on designed microtextured superhydrophobic surfaces with tunable wettability. *Langmuir* **24**, 11651–11660 (2008).
- Daniel, S. & Chaudhury, M. K. Rectified motion of liquid drops on gradient surfaces induced by vibration. *Langmuir* **18**, 3404–3407 (2002).
- Suzuki, A., Maeda, S., Hara, Y. & Hashimoto, S. Design and motion control of self-propelled droplets. Micro Electro Mechanical Systems (MEMS): 2014 IEEE 27th International Conference on, San Francisco, CA. Washington, DC, USA: IEEE, Jan. 26–30; DOI: 10.1109/MEMSYS.2014.6765638 (2014).
- Nakata, S., Miyaji, T., Matsuda, Y., Yoshii, M. & Abe, M. Mode-Switching of a Self-Propelled Object Sensitive to the Photo-Isomerization of a Molecular Layer. *Langmuir* **30**, 7353–7357 (2014).

8. Chaudhury, M. K. & Whitesides, G. M. How to make water run uphill. *Science* **256**, 1539–1541 (1992).
9. Duncombe, T. A., Parsons, J. F. & Böhringer, K. F. Droplet transport on flat chemically heterogeneous surfaces via periodic wetting barriers and vibration. Micro Electro Mechanical Systems (MEMS): 2010 IEEE 23rd International Conference on, Wanchai, Hong Kong. Washington, DC, USA: IEEE, Jan. 24–28; DOI: 10.1109/MEMSYS.2010.5442388 (2010).
10. Shastry, A., Case, M. J. & Böhringer, K. F. Directing droplets using microstructured surfaces. *Langmuir* **22**, 6161–6167 (2006).
11. Huang, D.-J. & Leu, T. Fabrication of high wettability gradient on copper substrate. *Appl. Sur. Sci.* **280**, 25–32 (2013).
12. Ichimura, K., Oh, S. & Nakagawa, M. Light-driven motion of liquids on a photoresponsive surface. *Science* **288**, 1624–1626 (2000).
13. Yang, D. *et al.* Photon control of liquid motion on reversibly photoresponsive surfaces. *Langmuir* **23**, 10864–10872 (2007).
14. Karapetsas, G., Sahu, K. C., Sefiane, K. & Matar, O. K. Thermocapillary-driven motion of a sessile drop: effect of non-monotonic dependence of surface tension on temperature. *Langmuir* **30**, 4310–4321 (2014).
15. Daniel, S., Chaudhury, M. K. & De Gennes, P. Vibration-actuated drop motion on surfaces for batch microfluidic processes. *Langmuir* **21**, 4240–4248 (2005).
16. Sumino, Y., Magome, N., Hamada, T. & Yoshikawa, K. Self-running droplet: Emergence of regular motion from nonequilibrium noise. *Phys. Rev. Lett.* **94**, 068301 (2005).
17. Linke, H., *et al.* Self-Propelled Leidenfrost Droplets. *Phys. Rev. Lett.* **96**, 154502 (2006).
18. Hashmi, A., *et al.* Leidenfrost levitation: beyond droplets. *Sci. Rep.* **2**, 797 (2012).
19. Feng, S., *et al.* Controlled Directional Water-Droplet Spreading on a High-Adhesion Surface. *Angew. Chem. Int. Ed.* **53**, 6163–6167 (2014).
20. Wenzel, R. N. Surface Roughness and Contact Angle. *J. Phys. Colloid Chem.* **53**, 1466–1467 (1948).
21. Hou, Y., *et al.* Temperature-controlled directional spreading of water on a surface with high hysteresis. *NPG Asia Mater.* **5**, e77 (2013).
22. Tran, T., Staat, H. J., Prosperetti, A., Sun, C. & Lohse, D. Drop impact on superheated surfaces. *Phys. Rev. Lett.* **108**, 036101 (2012).
23. Jo, H., Ahn, H. S., Kang, S. & Kim, M. H. A study of nucleate boiling heat transfer on hydrophilic, hydrophobic and heterogeneous wetting surfaces. *Int. J. Heat Mass Trans.* **54**, 5643–5652 (2011).
24. Phan, H. T., Caney, N., Marty, P., Colasson, S. & Gavillet, J. Surface wettability control by nanocoating: the effects on pool boiling heat transfer and nucleation mechanism. *Int. J. Heat Mass Trans.* **52**, 5459–5471 (2009).
25. Daniel, S., Chaudhury, M. K. & Chen, J. C. Fast Drop Movements Resulting from the Phase Change on a Gradient Surface. *Science* **291**, 633–636 (2001).

## Acknowledgements

This work was supported by the National Key Basic Research Program of China (2013CB933000), the National Natural Science Foundation of China (21234001, 51203006, 21204002, 21004002), the Doctoral Fund of Ministry of Education of China (20121102110035), the Specialized Research Fund for the Doctoral Program of Higher Education (20111102120049) and the Aeronautical Science Foundation of China (2012ZF51065).

## Author Contributions

S. F., Y. T., W. S., S. D., performed all the experiments. S. F., Y. H., Y. Z. wrote the manuscript and Y. H., Y. Z. developed the underlying concepts. Y. H., Y. Z. and S. W. drew graphs and provided comments and S. F., Y. H., Y. Z. modified the paper. All authors reviewed the manuscript.

## Additional Information

**Supplementary information** accompanies this paper at <http://www.nature.com/srep>

**Competing financial interests:** The authors declare no competing financial interests.

**How to cite this article:** Feng, S. *et al.* Radial Wettable Gradient of Hot Surface to Control Droplets Movement in Directions. *Sci. Rep.* **5**, 10067; doi: 10.1038/srep10067 (2015).



This work is licensed under a Creative Commons Attribution 4.0 International License. The images or other third party material in this article are included in the article's Creative Commons license, unless indicated otherwise in the credit line; if the material is not included under the Creative Commons license, users will need to obtain permission from the license holder to reproduce the material. To view a copy of this license, visit <http://creativecommons.org/licenses/by/4.0/>