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Co₃O₄—CeO₂ Nanocomposites for Low-Temperature CO Oxidation

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Abstract: In an effort to combine the favorable catalytic properties of Co₃O₄ and CeO₂, nanocomposites with different phase distribution and Co₃O₄ loading were prepared and employed for CO oxidation. Synthesizing Co₃O₄-modified CeO₂ via three different sol-gel based routes, each with 10.4 wt% Co₃O₄ loading, yielded three different nanocomposite morphologies: CeO₂-supported Co₃O₄ layers, intermixed oxides, and homogeneously dispersed Co. The reactivity of the resulting surface oxygen species towards CO were examined by temperature programmed reduction (CO-TPR) and flow reactor kinetic tests. The first morphology exhibited

the best performance due to its active Co₃O₄ surface layer, reducing the light-off temperature of CeO₂ by about 200 °C. In contrast, intermixed oxides and Co-doped CeO₂ suffered from lower dispersion and organic residues, respectively. The performance of Co₃O₄-CeO₂ nanocomposites was optimized by varying the Co₃O₄ loading, characterized by X-ray diffraction (XRD) and N₂ sorption (BET). The 16–65 wt% Co₃O₄-CeO₂ catalysts approached the conversion of 1 wt% Pt/CeO₂, rendering them interesting candidates for low-temperature CO oxidation.

Introduction

Ceria (CeO₂) has applications in many catalytic reactions, such as methane dry reforming,^[1] hydrocarbon and diesel soot oxidation,^[2] organic synthesis^[3] and especially environmental catalysis.^[4] Ceria is a crucial component of three-way-catalysts (TWCs), serving together with alumina as support for dispersed noble metal (e.g., Pt (or Pd) and Rh) nanoparticles, preventing their sintering at high temperatures. Additionally, ceria regulates the surface oxygen concentration under fuel lean and rich conditions, due to its oxygen buffer (storage/release) capacity (OBC/OSC), associated with the fast Ce⁴⁺/Ce³⁺ redox cycle. Recently, advanced synthesis methods allowed to develop nanostructured ceria of various morphologies (shapes), with high specific surface area (SSA) and improved Ce³⁺/Ce⁴⁺ ratio.^[4a,d,5] Furthermore, noble metals supported on ceria exhibit remarkable catalytic activity in preferential CO oxidation (PROX)^[6] and water gas shift (WGS),^[7] attributed to active sites at the metal/support interface^[8] and the availability of lattice

oxygen (oxygen vacancies).^[9] CeO₂ is thus considered an active (“non-innocent”)^[10] support.

Increasingly stringent emission regulations require continuous innovations, especially regarding engine cold start emissions at temperatures when noble metals are CO-poisoned and inactive.^[11] For noble metals, temperatures around 100–200 °C are typically required to initiate CO oxidation (“ignition”),^[11a,12] which is why ~80% of the emissions result from the cold-start period. Therefore, many studies focused on low-temperature CO oxidation, for example, over Au nanoparticles (2–4 nm size) on reducible oxides (e.g., TiO₂, CeO₂). These are less prone to CO poisoning, but Au nanoparticles tend to sinter. Co₃O₄ has been shown to be very active,^[4b,13] but fully replacing CeO₂ by Co₃O₄ would require substantial modifications of the existing TWC technology, as the CeO₂ support is important for both oxidation and reduction.^[14] However, Co₃O₄-modified CeO₂ nanocomposites may be a compromise,^[15] combining the favorable activity of cobalt oxide with the high oxygen storage capacity of ceria. Most importantly, for such mixed or supported oxides the limitations of availability and costs of noble metals apparently do not apply.

However, apart from the mere basic composition, the performance of Co₃O₄-CeO₂ catalysts strongly depends on the applied synthesis route, which determines the dispersion, morphology/microstructure, surface composition, redox and catalytic properties of the oxides. The materials reported so far in the literature were mainly prepared by conventional impregnation and coprecipitation methods followed by high temperature calcination, which does not yield catalysts with the desired high surface area and high dispersion of oxide phases, which are prerequisites for high catalytic activity in CO oxidation.^[16]

Previously, we have presented a new feasible route for preparation of Co₃O₄-modified CeO₂ catalysts, based on sol-gel

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synthesis combined with solvothermal processing, permitting the direct crystallization of the gel without the need of annealing at high temperatures to induce crystallization.^[17] Using this approach, we have been able to synthesize Co₃O₄-modified CeO₂ nanocomposites with high specific surface area and highly dispersed cobalt oxide nanoparticles. This maximizes the number of accessible active sites and results in high CO oxidation activity of Co₃O₄-modified CeO₂ catalysts, comparable to that of pure Co₃O₄ and, in terms of activation energy, even to Pt/ and Pd/CeO₂.^[18] Au/CeO₂ shows activity at lower temperature, due to lower CO binding energy,^[46,7d,19] but a coinage metal is apparently required.

Based on the effect of different synthesis routes on the structure of Co₃O₄-modified CeO₂ reported previously, herein the available oxygen species, redox properties and catalytic performance are examined in detail. Furthermore, an optimum Co₃O₄ loading of CeO₂ is determined. Pure CeO₂ and Co₃O₄, as well as Pt/CeO₂, are included for comparison. The Co₃O₄-CeO₂ nanocomposites turned out to be promising candidates for low-temperature CO oxidation and could be implemented by moderate modifications of TWC manufacture.

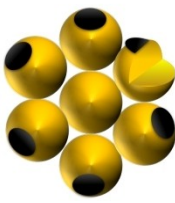
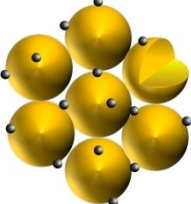

Results and Discussion

Table 1 summarizes the three synthesis routes and the different resulting structures of the Co₃O₄ modified CeO₂ catalysts, as reported previously.^[17] Herein, the focus is on their reduction by CO, reflecting the active oxygen species and ability for oxygen vacancy formation, which are important for the catalytic flow reactor performance. Then, the Co₃O₄ loading is tuned, including further characterization and activity measurements. The catalytic performance of the Co₃O₄-CeO₂ nanocomposites is finally contrasted to those of the pure oxides and Pt/CeO₂.

CO-TPR of pure CeO₂ and Co₃O₄

First, the pure oxides were characterized by CO temperature programmed reduction, with the results being in line with the literature.^[4d,15a,20] For pure CeO₂, prepared by the combination of sol-gel and solvothermal methods in ethanol (STE), and further air calcined (AC) at 500 °C (i.e., STE-AC),^[4d] the CO₂ evolution in CO-TPR occurs in three regions (Figure 1a, red line): (I) 250–425 °C, due to removal of surface lattice oxygen (O_{SL}); CO + O_{SL} → CO₂; (II) 425–625 °C, due to water gas shift (WGS) between CO and surface OH groups (CO + OH → CO₂ + 1/2 H₂); (III) >

Table 1. Overview of three different sol-gel routes for synthesis of Co₃O₄-CeO₂ nanocomposites and of corresponding structures (details please see the Supporting Information).

Route	Procedure	Structure ^[17]
1	<p>4 mmol CeB 8 mmol AO 0.025 mmol F127 20 mL DME</p> <p>dry on glassplate → 1-gel (Ce)</p> <p>transfer gel into autoclave → 1-gel (Ce) 1mmol Co(OAc)₂ 30 mL EtOH</p> <p>200 °C 6h ↓</p> <p>1-STE ← muffle furnace 500 °C 2h</p> <p>1-STE-AC</p>	 <p>small (3–5 nm) Co₃O₄ particle aggregation (black), forming layers on the surface of larger (10–20 nm) agglomerated CeO₂ particles (yellow): “supported Co₃O₄”</p>
2	<p>4 mmol CeB 8 mmol AO 0.025 mmol F127 20 mL DME 1 mmol Co(OAc)₂</p> <p>dry on glassplate → 2-gel (Ce+Co)</p> <p>transfer gel into autoclave → 2-gel (Ce+Co) 30 mL EtOH</p> <p>200 °C 6h ↓</p> <p>2-STE ← muffle furnace 500 °C 2h</p> <p>2-STE-AC</p>	 <p>coexisting (3–5 nm) Co₃O₄ (grey) and (20–30 nm) CeO₂ nanoparticles (yellow): “intermixed oxides”</p>
3	<p>1 mmol CeB 2 mmol POBC 1 mmol Co(OAc)₂ 5 mL DME</p> <p>dry on glassplate → 3-gel (Ce+Co)</p> <p>transfer gel into autoclave → 3-gel (Ce+Co) 30 mL EtOH</p> <p>200 °C 6h ↓</p> <p>3-STE ← muffle furnace 500 °C 2h</p> <p>3-STE-AC</p> <p>Mixing ↑ 3 mmol CeB 6 mmol AO 0.025 mmol F127 15 mL DME</p>	 <p>homogeneous distribution of cobalt within CeO₂ (via Co–O–Ce network): “Co-doped CeO₂”</p>

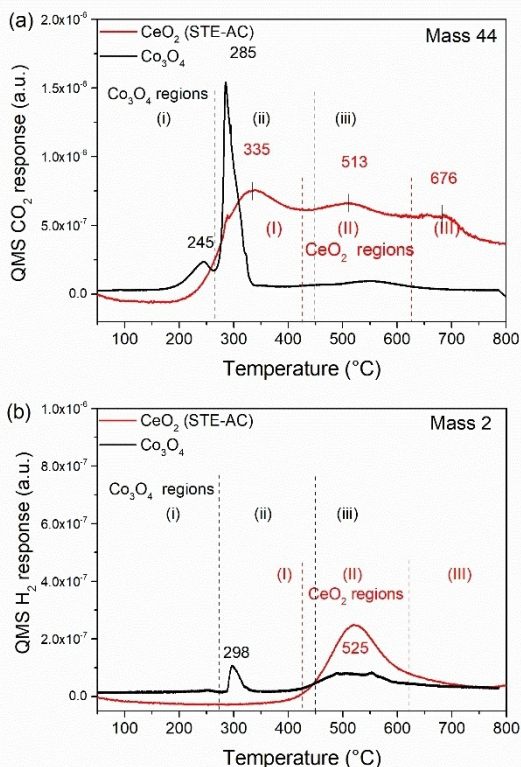


Figure 1. CO-TPR of pure CeO₂ (STE-AC) and commercial Co₃O₄: (a) CO₂ and (b) H₂ evolution.

625 °C, due to extraction of bulk lattice oxygen (O_{BL}). Accordingly, due to WGS the H₂ evolution on CeO₂ exhibits a main peak in region II (Figure 1b). Still, the reducibility of ceria is much lower than that of Co₃O₄.

Co₃O₄ is reduced at lower temperature and several studies^[20] reported a two-step process: Co³⁺ → Co²⁺ → Co⁰. This was confirmed by CO-TPR of commercial Co₃O₄, as evident from Figure 1 (black lines). The CO₂ evolution (Figure 1a) occurs in three stages: (i) < 270 °C, via O_{SL} removal; CO + O_{SL} → CO₂; Co³⁺_{SL} → Co²⁺_{SL}; (ii) 270–450 °C, O_{BL} removal of bulk lattice oxygen (CO + O_{BL} → CO₂), causing Co³⁺_{BL} → Co²⁺_{BL}, and further reduction of Co²⁺ → Co⁰.^[21] In the 450–670 °C region, CO disproportionation (2CO → CO₂ + C) or CO dissociation (CO → C + O) may occur on Co⁰, resulting in minute CO₂ desorption.^[22] Additionally, some H₂ evolution (Figure 1b) is detected around 300 °C, pointing to WGS of CO with surface OH groups.^[23] Some OH groups only react around 500 °C. Both for CeO₂ and Co₃O₄ mass 18 was also recorded, but no water desorbed over the entire temperature range. CO-TPR spectra (mass 44 and 2) of a 1:1 physical mixture of CeO₂/Co₃O₄ were simply a superposition of the spectra of the individual oxides, indicating that oxide/oxide interactions were absent in this case.

CO-TPR of 10 wt% Co₃O₄-modified CeO₂ synthesized via routes 1–3

For Co₃O₄-modified CeO₂ different and more complex CO- and H₂-TPR profiles were obtained, that were not just a sum of the profiles of the individual oxides. First, new low temperature peaks indicate additional surface oxygen species and, second, the “individual oxide peaks” are shifted by 20 or more degrees to higher temperature. Both indicate synergistic interfacial interactions between cobalt oxide and ceria, affecting the Co³⁺/Co²⁺ and Ce⁴⁺/Ce³⁺ redox properties, which seems to promote the reactive oxygen species. This also holds true for H₂ evolution.^[20b,24]

Accordingly, CO-TPR was performed for all six samples (three STE (Figure 2) and the corresponding STE-AC (Figure 3) samples). The different profiles clearly show that the interaction with CO/reducibility (CO₂ evolution) strongly depends on the preparation route and the heat-treatment (calcination), as both affect the Co distribution. Based on the CO-TPR results in Figure 1 and the literature,^[20c,24a,c,25] the peaks of all synthesized nanocomposites, except from 3-STE, can be assigned to five regions:

1. Region I (< 240 °C): Reaction of CO with reactive oxygen species, very likely on Co₃O₄, present after the oxidative pretreatment. Molecularly adsorbed oxygen on Co²⁺ dissociates to atomic oxygen (O–), transforming Co²⁺ to Co³⁺. CO

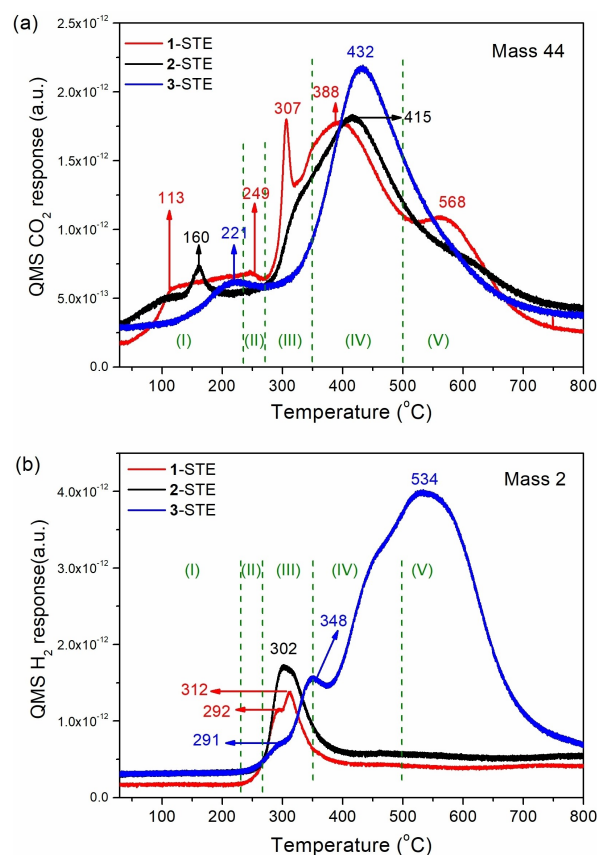


Figure 2. CO-TPR of 10.4 wt.% Co₃O₄ modified CeO₂ STE samples: (a) CO₂ and (b) H₂ evolution.

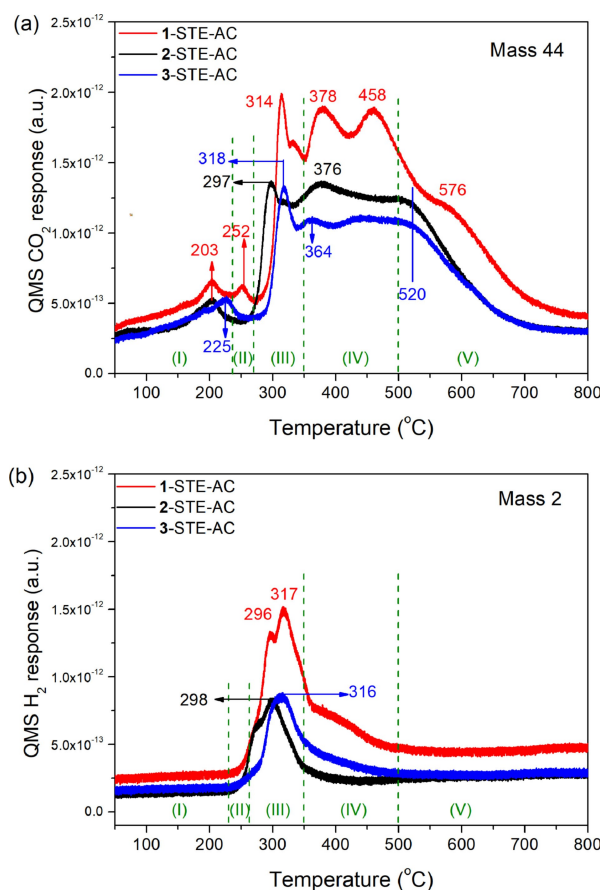


Figure 3. CO-TPR of 10.4 wt.% Co_3O_4 modified CeO_2 STE-AC samples: (a) CO_2 and (b) H_2 evolution.

may also react with this oxygen species to carbonates, that decompose below 200°C .^[4b]

2. Region II ($240\text{--}270^\circ\text{C}$): Reaction of O_{SL} at $\text{Co}_3\text{O}_4/\text{CeO}_2$ interfaces and reduction of $\text{Co}^{3+} \rightarrow \text{Co}^{2+}$: $\text{CO} + \text{O}_{\text{SLCo}_3\text{O}_4} \rightarrow \text{CO}_2$;
3. Region III ($270\text{--}350^\circ\text{C}$): Reaction of O_{BL} near $\text{Co}_3\text{O}_4/\text{CeO}_2$ interfaces: $\text{CO} + \text{O}_{\text{BLCo}_3\text{O}_4} \rightarrow \text{CO}_2$; $\text{Co}^{3+} \rightarrow \text{Co}^{2+}$. Reaction of O_{BL} of CoO , interacting with CeO_2 , producing Co^0 : $\text{CO} + \text{O}_{\text{BLCoO}} \rightarrow \text{CO}_2$; $\text{Co}^{2+} \rightarrow \text{Co}^0$. WGS reaction of OH on Co_3O_4 , including both isolated Co_3O_4 (at slightly lower temperature) and the $\text{Co}_3\text{O}_4/\text{CeO}_2$ interface (at slightly higher temperature): $\text{CO} + \text{OH} \rightarrow 1/2 \text{H}_2 + \text{CO}_2$;
4. Region IV ($350\text{--}500^\circ\text{C}$): removal of O_{SL} of CeO_2 interacting with Co_3O_4 ; $\text{CO} + \text{O}_{\text{SL}} \rightarrow \text{CO}_2$;
5. Region V ($> 500^\circ\text{C}$): Reaction of O_{BL} of CeO_2 : $\text{CO} + \text{O}_{\text{BLCeO}_2} \rightarrow \text{CO}_2$; $\text{Ce}^{4+} \rightarrow \text{Ce}^{3+}$.

The CO_2 evolution in region III is related to Co_3O_4 surface patches, from which the surface abundance of the modified Co_3O_4 phase can be deduced. For STE samples, only sample 1-STE has a sharp peak in this region (Figure 2a), while sample 2-STE has a weak shoulder and sample 3-STE has no peak. This indicates that the amount of the available Co_3O_4 on or near the ceria surface is $1\text{-STE} > 2\text{-STE} > 3\text{-STE}$ (in line with HRTEM results).^[17] For sample 3-STE, the intense peak of CO_2 evolution (432°C ; Figure 2a) is caused by the decomposition of the POBC

ligand, which is still present after the solvothermal treatment. This is reflected in the lower temperature shoulder of the 534°C peak of H_2 evolution (Figure 2b). The latter peak and the one at 348°C once more indicate WGS of CO with surface OH groups.

To examine how high temperature calcination influences reactivity/reducibility, the STE samples were air-calcined at 500°C for 2 h (STE-AC). After calcination, all STE-AC samples showed low temperature peaks in region I, and especially sharp peaks in region III. The different intensities in region III indicate that part of the Co in sample 2-STE-AC and 3-STE-AC sintered and/or segregated to the surface (Figure 3). The higher temperature peaks are related to ceria. Once more, the intensity of the peaks in regions I–III indicates the amount of Co oxide that is available for CO oxidation. Compared to pure Co_3O_4 (Figure 1) and uncalcined nanocomposites (Figure 2), the peaks in region III are even more shifted to higher temperature, indicating an increased interaction with CeO_2 . For 2-STE-AC and 3-STE-AC, though some Co aggregated, some Co is still in the bulk of CeO_2 , and may thus not participate in CO oxidation. The H_2 evolution of STE-AC samples in region III (Figure 3b), due to WGS, showed a similar trend. Sample 1-STE-AC formed the most H_2 , while 2-STE-AC and 3-STE-AC produced only half the H_2 amount. Thus, it can be deduced that 1-STE-AC exhibited most active Co_3O_4 interacting with CeO_2 , while the other two samples had only about half the amount of available Co_x/CeO_2 . This is consistent with high-resolution transmission electron microscopy (HR-TEM) micrographs of the AC samples.^[17]

Catalytic performance of 10 wt % Co_3O_4 -modified CeO_2 synthesized via routes 1–3

The catalytic activity of the six samples (three STE samples by different routes and the corresponding STE-AC samples) in CO oxidation (5% CO, 10% O_2 , He balance) was evaluated at different temperatures (Figure 4). Trends were tabulated previously;^[17] herein, more detailed catalytic tests are contrasted to the characterization discussed above. For practical applications, apart from the catalytic activity, the thermal stability of catalysts is most crucial. To detect a potential loss of catalytic activity, the CO conversion was thus recorded upon heating, upon subsequent cooling and upon re-heating, *without* intermittent catalyst reactivation. Catalysts that underwent such cycling are stable in isothermal reactions up to 200°C , typically over hundreds of hours.

Samples 1-STE (Figure 4a) and 2-STE (Figure 4b) (prepared by two individual precursors) did not show any hysteresis or loss of activity within several test cycles. In contrast, for sample 3-STE (Figure 4c) the CO conversion upon heating and subsequent cooling do not coincide anymore. Interestingly, the CO conversion at a given temperature became apparently higher upon cooling and then remained the same during re-heating. This behavior of 3-STE (for which a single source precursor was used) can be explained by the decomposition of residual organics (e.g., POBC ligand) upon heating to $\sim 250^\circ\text{C}$ in oxidative atmosphere (which is supported by previous ther-

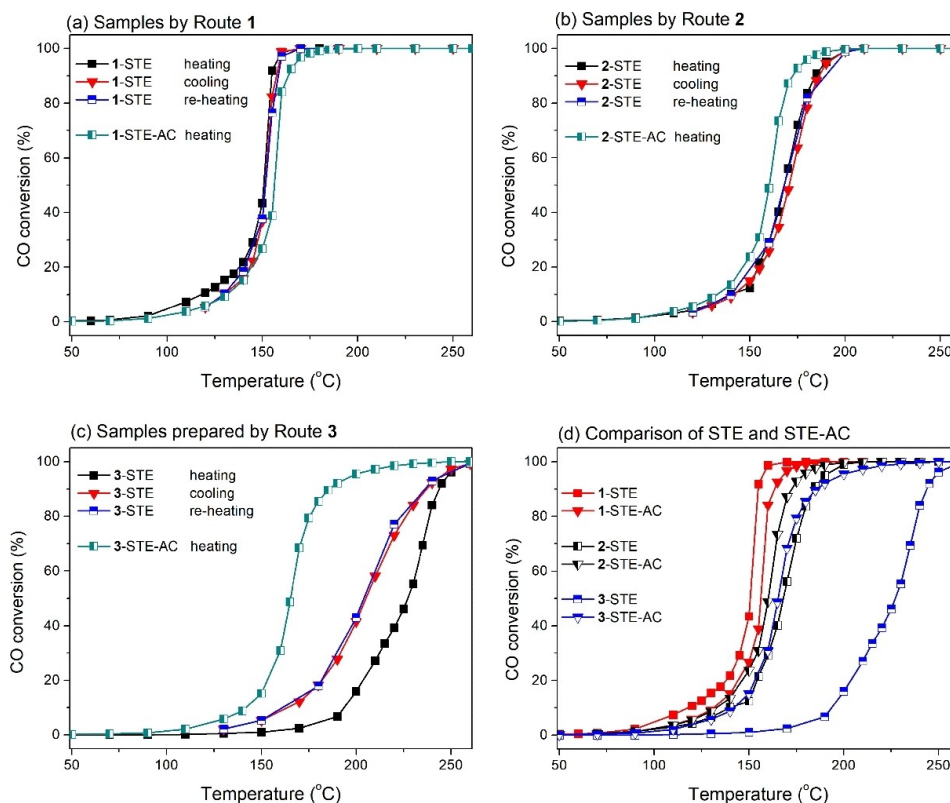


Figure 4. CO oxidation over 10.4 wt% Co_3O_4 modified CeO_2 samples. (a) route 1, (b) route 2, (c) route 3 and (d) direct comparison of 1st heat-up.

mogravimetric analysis (TGA)).^[17] The highest activity (at a given temperature) of the catalyst prepared by route 1 can be explained by the more active and more abundant Co_3O_4 on the CeO_2 surface (layer structure).^[17]

In order to determine the effect of calcination, the STE-AC samples were also tested in CO oxidation (Figure 4). 1-STE-AC exhibited somewhat lower CO conversion than its STE pendant (Figure 4a). In contrast, when comparing the other STE samples with the corresponding STE-AC samples (Figure 4b, c), at a given temperature 2-STE-AC and especially 3-STE-AC had a higher CO conversion than the related STE samples. Apparently, the significant amount of organic residues, which had remained after solvothermal treatment, blocked reaction sites, resulting in lower activity. Thus, the high temperature calcination is beneficial for 2-STE and 3-STE to remove organic residues. Nevertheless, the high temperature calcination also caused a structure collapse and reduction in surface area (from 216~217 m^2g^{-1} to 25~96 m^2g^{-1}),^[17] which is why annealing of 1-STE (with the smallest amount of organic residues) resulted in somewhat lower catalytic activity of 1-STE-AC. Therefore, for 1-STE the post-synthesis calcination should be avoided. The performance of all catalysts in the first heating cycle is directly compared in Figure 4d.

The apparent activation energy (E_a) of all STE and STE-AC samples was calculated from Arrhenius-type plots using kinetic rates below 30% conversion (Figure 5). 1-STE has the lowest E_a of 47.4 kJ mol^{-1} , while 3-STE shows the highest E_a of

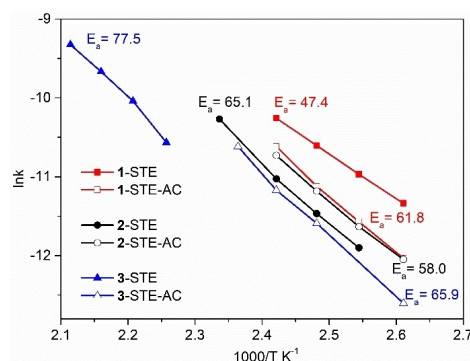


Figure 5. Arrhenius-type plots for CO oxidation over STE and STE-AC samples (error: $\pm 2 \text{ kJ mol}^{-1}$).

77.5 kJ mol^{-1} . The E_a of 1-STE is similar to that of noble metals supported on ceria, such as 0.5 wt% Pd/ CeO_2 (48–52 kJ mol^{-1}),^[9b] 1 wt% Pd/ CeO_2 (40 kJ mol^{-1}),^[26] 0.5 wt% and 1 wt% Pt/ CeO_2 (42–63^[9b] and 44 kJ mol^{-1}),^[27] respectively) and Au/ CeO_2 (46–56 kJ mol^{-1}).^[28] Thus, the combination of sol-gel and solvothermal methods allows obtaining very active cobalt oxide-modified ceria nanocomposites, which could be used as a low-temperature-active additive to noble metal loaded CeO_2 .

The promising activity of 10.4 wt% Co_3O_4 - CeO_2 catalysts (route 1) is attributed to the favorable phase distribution, i.e., a high dispersion and small crystallite size of the active Co_3O_4 phase on CeO_2 .^[29] The oxygen availability seems promoted by

synergetic interfacial interactions between cobalt and ceria (Co–O–Ce bonds), modifying the $\text{Co}^{2+}/\text{Co}^{3+}$ and $\text{Ce}^{3+}/\text{Ce}^{4+}$ redox properties and producing more active oxygen species.^[20b,30] Along these lines, the Co_3O_4 loading on CeO_2 catalysts was varied, as described in the following.

Optimizing the Co_3O_4 loading on CeO_2 (via route 1)

To further improve the performance of Co_3O_4 -modified CeO_2 , the number of Co_3O_4 surface sites accessible to the reaction was optimized via the Co_3O_4 loading. As route 1 produced the material with the highest CO oxidation activity, additional catalysts were prepared following this route, but with different amounts of cobalt precursor. The molar percentage of $\text{Co}(\text{Oac})_2/(\text{CeB} + \text{Co}(\text{Oac})_2)$ used for all samples was 10, 20, 30 and 80%, translating to $\text{Co}_3\text{O}_4/(\text{Co}_3\text{O}_4 + \text{CeO}_2)$ wt.% ratios of 4.9, 10.4, 16.6 and 65.1 wt%, respectively.

The 1-STE samples with different Co_3O_4 loading were characterized by X-ray diffraction (XRD) and N_2 sorption (Figure 6). The XRD of 4.9 wt% $\text{Co}_3\text{O}_4/\text{CeO}_2$ showed only diffraction peaks of CeO_2 , as Co was highly dispersed.^[31] The higher loadings exhibited features characteristic of both Co_3O_4 and CeO_2 , with the intensity of the Co_3O_4 diffraction peaks increasing with Co loading. The CeO_2 crystals were in the size

range of 2.5–3.5 nm, whereas that of Co_3O_4 was about 25 nm (similar to commercial Co_3O_4).

The textural properties of the differently loaded 1-STE catalysts were characterized by N_2 adsorption. Adsorption-desorption isotherms, the resulting specific surface area (SSA) and the pore size distributions are plotted in Figure 6 b,c. The specific surface area (S_{BET}) decreased with increasing loading. While S_{BET} was about 220 m^2/g for 4.9 wt% $\text{Co}_3\text{O}_4/\text{CeO}_2$, it was only $\sim 120 \text{ m}^2/\text{g}$ for 65.1 wt% $\text{Co}_3\text{O}_4/\text{CeO}_2$. Nevertheless, this is still large compared to the SSA of commercial Co_3O_4 ($37 \text{ m}^2/\text{g}^{-1}$). Up to 16.6 wt% $\text{Co}_3\text{O}_4/\text{CeO}_2$, the isotherms indicate mainly mesopores and a small proportion of macropores, with narrow pore size distributions. In contrast, the 65.1 wt% $\text{Co}_3\text{O}_4/\text{CeO}_2$ sample is mostly macroporous with a small amount of mesopores. Thus, a suitable ratio between Co_3O_4 and CeO_2 is crucial to preserve mesoporosity and to obtain a high specific surface area with a high dispersion of Co_3O_4 on CeO_2 . The structural data are summarized in Table 2.

Catalytic performance of different Co_3O_4 loadings on CeO_2 (via route 1)

The different 1-STE nanocomposites (without air-calcination) were subsequently tested in CO oxidation, and contrasted to

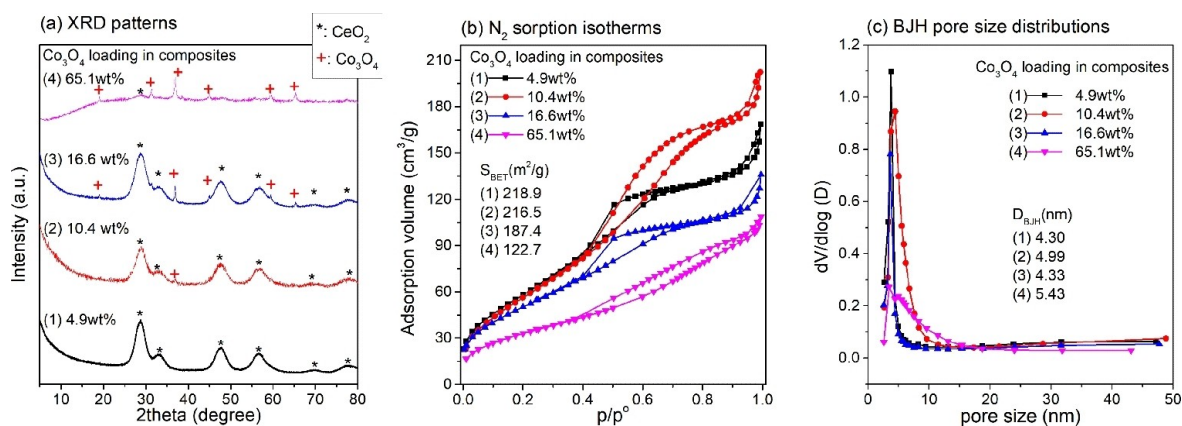


Figure 6. (a) XRD patterns, (b) N_2 adsorption-desorption isotherms, and (c) pore size distributions of Co_3O_4 - CeO_2 nanocomposites (1-STE). The data of the 10.4 wt% sample were adapted with permission from ref. [17]. Copyright 2015, Wiley.

Co_3O_4 loading [wt %]	P_{CeO_2} ^[a] [nm]	$P_{\text{Co}_3\text{O}_4}$ ^[b] [nm]	S_{BET} ^[c] [$\text{m}^2 \text{g}^{-1}$]	$T_{10\%}$ ^[d] [$^{\circ}\text{C}$]	$T_{90\%}$ ^[e] [$^{\circ}\text{C}$]	$r_{100^{\circ}\text{C}}$ ^[f] [$\text{mol s}^{-1} \text{g}^{-1}$]	$R_{100^{\circ}\text{C}}$ ^[g] [$\text{mol s}^{-1} \text{m}^{-2}$]	$R_{\text{Co}100^{\circ}\text{C}}$ ^[h] ($\text{mmol CO}/\text{mmol Co h}^{-1}$)
0 (Ceria)	< 3	/	277.0	253	398	/	/	/
4.9	3.0	/	218.9	138	197	3.90×10^{-6}	1.78×10^{-8}	22.9
10.4	3.5	/	216.5	117	155	7.78×10^{-6}	3.59×10^{-8}	21.6
16.6	2.5	27.5	187.4	105	148	1.23×10^{-5}	6.56×10^{-8}	21.4
65.1	3.3	23.7	122.7	105	134	1.21×10^{-5}	9.87×10^{-8}	7.4
100 (Co_3O_4)	/	28	37	84	114	4.14×10^{-5}	1.12×10^{-6}	11.9
0 (Pt/ CeO_2)	13.5	/	43.2	100	124	1.15×10^{-5}	2.68×10^{-7}	/

[a] CeO_2 crystal particle size calculated by Scherrer equation from XRD (JCPDS card number of CeO_2 : 34-0394) [b] Co_3O_4 crystal particle size calculated by Scherrer equation from XRD (JCPDS card number of Co_3O_4 : 42-1467) [c] BET surface area from N_2 sorption [d] Reaction temperature for 10% CO conversion [e] Reaction temperature for 90% CO conversion [f] Reaction rate of CO oxidation at 100°C per gram [g] Normalized specific reaction rates of CO oxidation on a unit surface area at 100°C [h] Reaction rates per unit amount of Co at 100°C .

pure CeO₂, pure Co₃O₄ and 1 wt.% Pt/CeO₂ (the latter with a mean Pt particle size of 1.7 nm, according to CO chemisorption). Figure 7 shows the temperature-dependent CO conversion of the different pretreated 1-STE samples and pretreated reference catalysts (10 mg each). The temperatures of 10% CO conversion ($T_{10\%}$) for 1 STE samples are: 138 °C (4.9 wt%) > 117 °C (10.4 wt%) > 105 °C (16.6 wt%) = 105 °C (65.1 wt%) > 100 °C (1 wt% Pt/CeO₂) > 84 °C (Co₃O₄); the temperatures of 90% CO conversion ($T_{90\%}$) are: 197 °C (4.9 wt%) > 155 °C (10.4 wt%) > 148 °C (16.6 wt%) > 134 °C (65.1 wt%) > 124 °C (1 wt% Pt/CeO₂) > 114 °C (Co₃O₄).

Apparently, pure CeO₂ is the least active (30% conversion at 300 °C), but already adding ~4.9 wt.% Co₃O₄ drastically increased activity. This trend continued for 10.4, 16.6, and 65.1 wt%, the latter approaching the activity of Pt/CeO₂. Clearly, the higher the Co percentage in the synthesis and thus the final Co₃O₄ loading are, the higher the resulting catalytic activity is. Pure Co₃O₄ is the most active, but for possible TWC-applications, ~16–65 wt% Co₃O₄-modified CeO₂-based catalysts seem the best. This agrees with a similar higher activity of Co₃O₄ catalysts impregnated by 10 wt.% CeO₂ in preferential CO oxidation.^[15a]

To compare the different samples, the catalytic activity/rate of the catalysts at 100 °C was normalized by weight ($r_{100^\circ\text{C}}$), by specific surface area ($R_{100^\circ\text{C}}$) and by the unit amount of Co ($R_{\text{Co}100^\circ\text{C}}$), as listed in Table 2 (the CO conversion at 100 °C was below 20% for all samples). Up to 16.6 wt% Co₃O₄, the values of $r_{100^\circ\text{C}}$ and $R_{100^\circ\text{C}}$ increased almost in direct proportion to the Co₃O₄ loading. For example, the $r_{100^\circ\text{C}}$ and $R_{100^\circ\text{C}}$ values of 4.9% Co₃O₄ are $3.90 \times 10^{-6} \text{ mol s}^{-1} \text{ g}^{-1}$ and $1.78 \times 10^{-8} \text{ mol s}^{-1} \text{ m}^{-2}$, respectively. The corresponding values of 10.4% Co₃O₄ are $7.78 \times 10^{-6} \text{ mol/s g}$ and $3.59 \times 10^{-8} \text{ mol/s m}^2$, i.e., each almost exactly double.

This is consistent with the $R_{\text{Co}100^\circ\text{C}}$ values, as up to 16.6 wt% Co₃O₄ the samples have almost the same $R_{\text{Co}100^\circ\text{C}}$ value of $22 \pm 1 \text{ mmol CO/mmole Co-h}$ (Table 2). This indicates that Co₃O₄ is well dispersed, forming increasingly larger islands on the CeO₂ surface. Further increasing the Co₃O₄ loading to 65 wt% hardly increased the specific activity and even decreased the rate

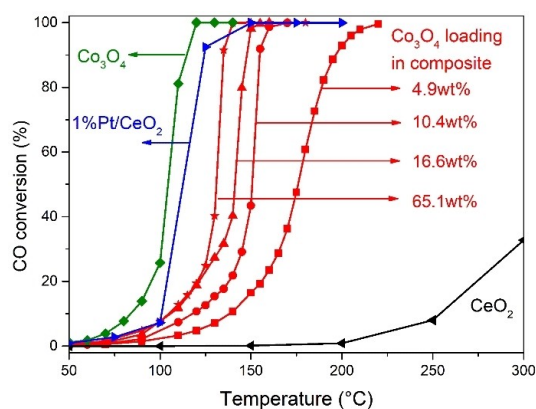


Figure 7. CO conversion vs. temperature of Co₃O₄-modified CeO₂ (STE) for different loadings. CeO₂, Co₃O₄, and Pt/CeO₂ serve as reference. Conditions: 5% CO, 10% O₂, He balance; 10 mg catalyst.

normalized by the Co amount to 7.4 mmol CO/mmol Co-h, as agglomerated particles or thicker layers have less dispersion. This is clearly evident from the low temperature range (Figure 7), with the conversion of the 16.6 and 65 wt% samples being almost the same. Pure Co₃O₄ nanoparticles are characterized by a similar value (11.9 mmol CO/mmol Co-h), as the Co₃O₄ dispersion is lower than that of thin Co₃O₄ layers.

Even though Co₃O₄ is known for high CO oxidation activity at low temperature, the use of pure Co₃O₄ in catalytic converters is not feasible, as ceria has oxygen storage/release (buffer) capacity, in addition to preventing sintering. It is thus important to preserve the main CeO₂ phase, but its low-temperature activity could be boosted by well-dispersed Co₃O₄ overlayers. As modern engines run under oxygen-rich conditions to increase mileage, the exhaust gas is oxygen rich too, which stabilizes the Co₃O₄ phase, so that no reduction would occur (deactivation by adsorbed water may be a problem at lowest temperatures, though). The re-oxidation of (metallic) cobalt starts above 200 °C, at 300 °C it is oxidized to CoO and Co₃O₄, and at 400 °C Co₃O₄ is the most stable phase.^[13b] Clearly, operando examination of the nanocomposites would add to the mechanistic understanding^[32] and Co₃O₄ may also be beneficial for NO_x reduction.^[33]

Conclusions

The current results demonstrate that the sol-gel synthesis of Co₃O₄-CeO₂ nanocomposites, in combination with solvothermal treatment, allows obtaining well-dispersed cobalt oxide nanoparticles on high surface area CeO₂. The obtained materials are thermally more stable and very active in CO oxidation, and are comparable to supported Pt-, Pd- and Au-CeO₂ catalysts. The catalytic performance of Co₃O₄-modified CeO₂ strongly depends on the number of the Co₃O₄ surface sites accessible for the CO oxidation reaction, which is controlled by the route of introducing Co cations and by the Co loading. Considering the high activity of the presented catalysts in CO oxidation, with that of 16 wt% Co₃O₄-CeO₂ approaching that of Pt/CeO₂, it is anticipated that further optimization of the layered CeO₂-Co₃O₄ nanocomposites may allow obtaining prototypes with even better low-temperature TWC performance. In terms of a practical application in TWCs, the long-term stability and activity in hydrocarbon oxidation and NO_x reduction in realistic exhaust gas feeds should also be investigated.

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Conflict of Interest

The authors declare no conflict of interest.

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