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A STELLA simulation model for *in vitro* dissolution testing of respirable size particles

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In vitro dissolution testing is a useful quality control tool to discriminate the formulations and to approximate the *in vivo* drug release profiles. A dissolution apparatus has been custom-made for dissolution testing of dry powder formulations in a small volume of stationary medium (25 μL spread over 4.91 cm^2 area i.e. $\sim 50 \mu\text{m}$ thick). To understand the system and predict the key parameters which influence the dissolution of respirable size particles, a simulation model was constructed using STELLA modeling software. Using this model, the permeation (dissolution followed by diffusion through the membrane) of two anti-tubercular drugs of differing solubilities, moxifloxacin ($17.68 \pm 0.85 \text{ mg mL}^{-1}$) and ethionamide ($0.46 \pm 0.02 \text{ mg mL}^{-1}$), from the respirable size particles and their diffusion from a solution were simulated. The simulated permeation profiles of moxifloxacin from solution and respirable size particles were similar, indicating fast dissolution of the particles. However, the simulated permeation profile of ethionamide from respirable size particles showed slower permeation compared to the solution indicating the slow dissolution of the respirable size particles of ethionamide. The sensitivity analysis suggested that increased mucus volume and membrane thickness decreased the permeation of drug. While this model was useful in predicting and distinguishing the dissolution behaviours of respirable size moxifloxacin and ethionamide, further improvement could be made using appropriate initial parameter values obtained by experiments.

In vitro dissolution testing is a standardized quality control tool in all the pharmacopoeias for immediate and controlled release formulations and it is also used to simulate *in vivo* release profiles¹. However, there is no accepted standardized method to estimate the dissolution profiles of inhaled powder particles; although many dissolution methods (compendial (USP 2) paddle apparatus, flow-through cell apparatus, dialysis bag, Franz diffusion cell, Transwell[®] and DissolvIt[®] systems) for testing aerosols have been described^{2,3}.

Development of an *in vitro* dissolution method which mimics the *in vivo* conditions of the lungs, such as limited volumes of lung fluid (approximately 10–20 $\text{mL}/100 \text{ m}^2$)⁴ is challenging. We have custom-made a dissolution apparatus and evaluated the dissolution behaviour of 1–5 μm drug particles in small volumes (25 μL spread over 4.91 cm^2 area i.e. $\sim 50 \mu\text{m}$ thick) of stationary simulated mucus fluid⁵. The apparatus is similar to the DissolvIt[®] technology⁶. Development of an *in vitro* dissolution method requires a mechanistic understanding of the system and identification of the key variables controlling the rate of dissolution. In this regard, mathematical models are useful in the scientific understanding of a complex system^{7–9}.

Various commercial software packages such as Cloe PK (Cyprotex Ltd., Macclesfield, Cheshire, UK)¹⁰, GastroPlus (Simulations Plus Inc., California, USA)^{11,12}, PulmoSim[™] (Pfizer, New York, USA)¹³, MEDICI-PK (Computing in Technology GmbH, Rastede, Germany)¹⁴, PKSim/MoBi (Bayer Technology Services, Leverkusen, Germany)^{15,16}, SimCyp (Simcyp Ltd., Sheffield, UK)¹⁷, GI-Sim (AstraZeneca, Cambridge, UK)¹⁸, MatLab (MathWorks, Inc., Massachusetts, USA)¹⁹, Berkeley Madonna (University of California, Berkeley, CA, USA)²⁰ and STELLA[®] (Structural Thinking, Experimental learning Laboratory with Animation, isee systems, Lebanon, New Hampshire, USA)⁹ have been used for constructing mathematical models. Among them, PulmoSim[™] (developed from SimCyp[®] by Pfizer) and GastroPlus[™] (developed from Simulations Plus) are the commercially available generic tools used to construct physiologically based pharmacokinetic (PBPK) models for inhalable drugs²¹. They have used pharmacokinetic results from laboratory animal (rat) studies together with drug permeability, mucociliary clearance and pulmonary metabolism data to predict the pharmacokinetics of inhaled drugs in humans²².

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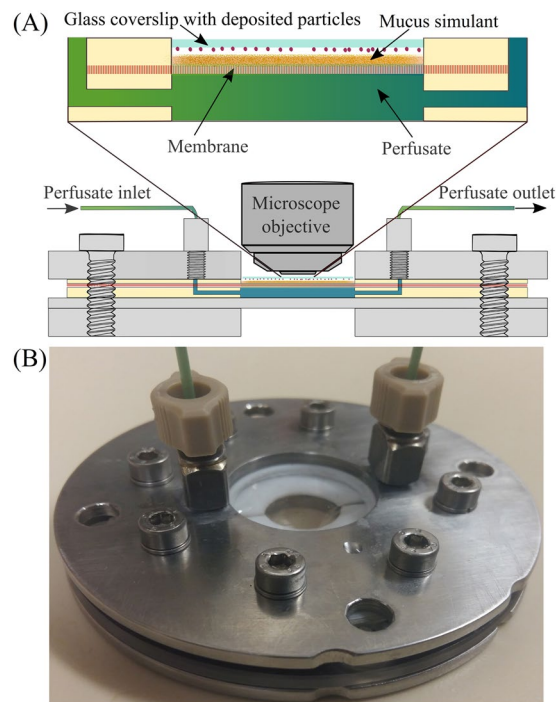


Figure 1. Schematic diagram of the dissolution apparatus (A) and custom-made flow perfusion cell (B). Reproduced with permissions from Eedara et al.⁵

However, the complexity of lung physiology and inhaled delivery complicate the development of PBPK models, and it is challenging to include all the processes in a single model.

In this study we aimed to construct a simple STELLA simulation model to predict the dissolution behaviour of respirable size inhaled dry powder particles in a small volume of mucus simulant and diffusion through a membrane in a custom-made dissolution apparatus. STELLA[®] is user-friendly and icon-based modeling software used to construct a graphical model of a complex system²³. After construction of a model, the program calculates the values of each variable in the model at each successive time increment using a numerical integration using Euler's or a Runge-Kutta method²⁴. STELLA[®] has been used effectively to construct a variety of pharmaceutically-related simulation models for: pharmacokinetics of orally administered drugs^{25–34}, ocular pharmacokinetics³⁵, performance of sustained release dosage forms^{36,37}, prodrug performance³⁸, and gene expression³⁹. The STELLA simulation model described here was used to simulate the permeation (dissolution followed by diffusion through the membrane) of a drug from respirable size particles of two anti-tubercular drugs, moxifloxacin and ethionamide, that have different aqueous solubilities. Further, sensitivity analysis of the model was conducted by varying the volume of the mucus, perfusate flow rate, and membrane thickness to determine their influence on the predicted percentage of drug collected into the collection tubes.

Methods

Materials. Materials (suppliers) were as follows: Moxifloxacin (>98% purity) (Leader Biochemical Group Xi'an Leader Biochemical Engineering Co. Ltd., Xi'an, China); ethionamide (≥99.0% purity) (Hangzhou Dayangchem Co., Ltd., Hangzhou, China); polyethylene oxide (Polyox coagulant, molecular weight 5000 kDa, LR grade) (BDH Chemicals Ltd., Poole, England); phosphate buffered saline (Dulbecco A, pH 7.3 ± 0.2; 0.01 M phosphate buffer, 0.003 M potassium chloride and 0.137 M sodium chloride) tablets (Oxoid Ltd., Basingstoke, UK); and dialysis membrane (molecular weight cut off, MWCO, 12,400 Da) (Sigma-Aldrich New Zealand Ltd., Auckland, New Zealand). Freshly collected and filtered (0.45 μm membrane filter) purified water was used.

In vitro dissolution apparatus and method. The custom made dissolution apparatus and dissolution method have been described previously^{5,40}. In brief, the apparatus (Fig. 1A; schematic diagram of complete setup) consists of a flow perfusion cell (Fig. 1B) connected to a syringe pump, and an optical microscope equipped with a digital camera.

A membrane is used as a diffusion barrier which allows the transfer of dissolved drug from donor (mucus simulant) to receiver (perfusate) compartment⁴¹. Ideally, a membrane for *in vitro* dissolution testing of respirable particles should possess the same resistance to drug permeation as the lung epithelium. However, practically, the membrane should not be highly resistive and so that the permeation of dissolved drug becomes the limiting step. It should allow the diffusion of dissolved drug molecules through membrane to evaluate the dissolution rate of respirable size drug particles. In this study, a dialysis membrane (MWCO = 12,400 Da) was selected as this is less resistive and commonly used in drug diffusion studies^{42–44}. The thickness of the hydrated dialysis membrane is ~60 μm which is comparable to the thickness of the ciliated cells in the upper airway region (tracheobronchial region) of the lung⁵.

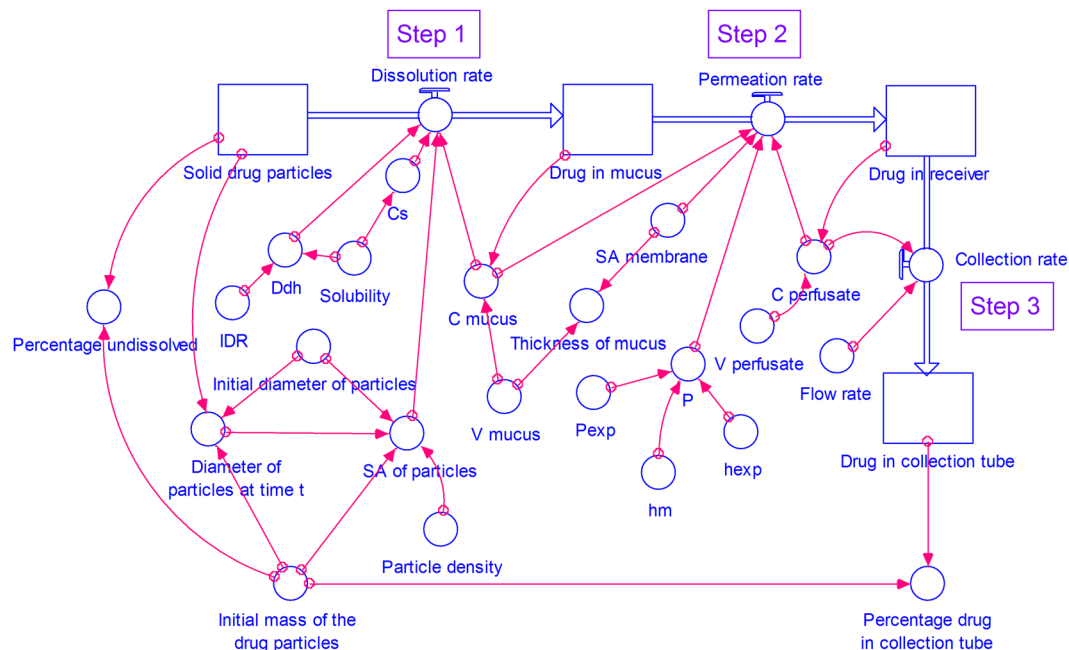


Figure 2. A STELLA model for dissolution of drug from respirable size particles at small volume of mucus simulat under well-stirred conditions. (C - concentration, C_s - saturation concentration, Ddh - D/h , h_{exp} - thickness of the membrane used in the experimental study, h_m - thickness of the membrane, IDR - intrinsic dissolution rate, P - permeability coefficient at time t , P_{exp} - experimental permeability coefficient, SA - surface area, V - volume).

Phosphate buffered saline (PBS, pH 7.4, 37 °C) was pumped on the blood side of the membrane using the syringe pump. A mucus simulat i.e. polyethylene oxide (PEO) with a MWCO of 5000 kDa was dissolved in PBS (pH 7.4) and used as a dissolution medium as reported by Shah *et al.*⁴⁵. An aliquot of mucus simulat (1.5% w/v polyethylene oxide in PBS, pH 7.4) was uniformly spread over the membrane. The respirable fraction of supplied moxifloxacin and ethionamide particles were collected onto the glass coverslips using a modified Twin Stage Impinger (mTSI; Supplementary Figure S1) and brought into the contact of the mucus simulat applied on the membrane. The particle disappearance was observed using a recording optical microscope. The perfusate samples were collected continuously into the tubes over 120 min, and drug concentrations were quantified by validated HPLC assays as described in our previous publication Eedara *et al.*⁵.

A STELLA simulation model for *in vitro* dissolution testing of respirable size dry powder particles. The model consists of four stocks (compartments) (Figs. 2 and 3) representing drug in solid particulate form, dissolved drug in mucus simulat, permeated drug in receiver and collection tube. All the compartments are connected in a stepwise manner as follows:

- Step 1. Dissolution of respirable size dry powder particles in a small volume of mucus simulat.
- Step 2. Permeation of dissolved drug from mucus simulat through the dialysis membrane representing the lung epithelial membrane into the perfusate in the receiver.
- Step 3. Collection of the perfusate with permeated drug into a collection tube.

These steps are described in detail in the following paragraphs.

Step 1. Dissolution of respirable size dry powder particles

In this step (Figs. 2 and 3), the respirable size particles undergo dissolution in the mucus simulat applied on the membrane.

The dissolution rate of the drug particles in the mucus simulat is calculated using the Noyes-Whitney equation⁴⁶ as shown in Fig. 4A.

$$\frac{dM}{dt} = \frac{DS}{h}(C_s - C) \quad (1)$$

In which M is the mass of drug dissolved in time t , dM/dt is the mass rate of dissolution (mass/time), D is the diffusion coefficient of the drug in mucus, S is the total surface area of the particles at time t , h is the thickness of the mucus unstirred diffusion layer, C_s is the solubility of the drug i.e. concentration of a saturated solution of the drug at the surface of the solid particle at a given temperature, and C is the concentration of the drug in mucus simulat at time t .

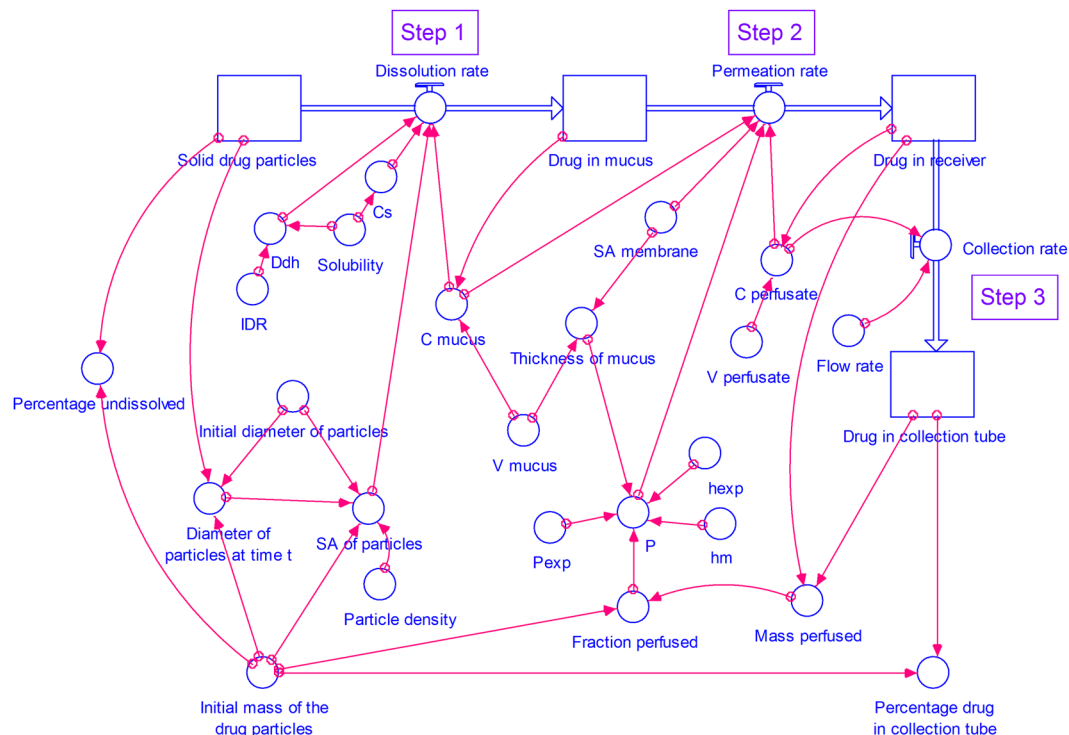


Figure 3. A STELLA model for dissolution of drug from respirable size particles at small volume of mucus simulant under unstirred conditions. (C- concentration, C_s - saturation concentration, Ddh - D/h , h_{exp} - thickness of the membrane used in the experimental study, h_m - thickness of the membrane, IDR- intrinsic dissolution rate, P- permeability coefficient at time t , P_{exp} - experimental permeability coefficient, SA- surface area, V- volume).

In Eq. 1, the quantity D/h may be referred to as a dissolution rate constant, k can be determined from the intrinsic dissolution rate and the solubility of the drug as:

$$\frac{D}{h} = k = \frac{\text{Intrinsic dissolution rate (IDR) of drug}}{\text{Solubility of drug } (C_s)} \quad (2)$$

The concentration of drug in solution in mucus (C) is calculated by

$$C = \frac{\text{Drug in solution in mucus}}{\text{Volume of mucus}} \quad (3)$$

The total surface area of the powder at time t , $S_{t(\text{total})}$ is calculated by

$$\begin{aligned} \text{Total surface area of powder at time } t, S_{t(\text{total})} &= S_{t(\text{particle})} \\ &\times \text{Number of particles} = \pi d_t^2 \\ &\times \frac{6M_0}{\pi d_0^3 \rho} = \frac{6M_0 d_t^2}{d_0^3 \rho} \end{aligned} \quad (4)$$

$$\text{Diameter of the particle at time } t, d_t = \sqrt[3]{\frac{M_t d_0^3}{M_0}} \quad (5)$$

In which M_0 and M_t are the masses of the powder at time 0 and t , d_0 and d_t are the diameters of a particle at time 0 and t , and ρ is the density of the powder. In the model, all particles are assumed to be smooth, spherical and of the same size.

Step 2. Permeation of dissolved drug through the membrane. In this step, the dissolved drug in the mucus simulant, diffuses through the membrane. We have simulated two models: 1. with a well-stirred mucus phase (See Figs. 2) and 2. an unstirred (See Fig. 3) mucus phase i.e. donor compartment.

Diffusion of drug molecules into the receptor phase is a combination of diffusion through mucus simulant, the membrane, and the unstirred water layers (UWLs, assumed to be of negligible thickness compared to the mucus and membrane) which are present on both sides of the membrane. In a well-stirred system (Fig. 4B), the drug in

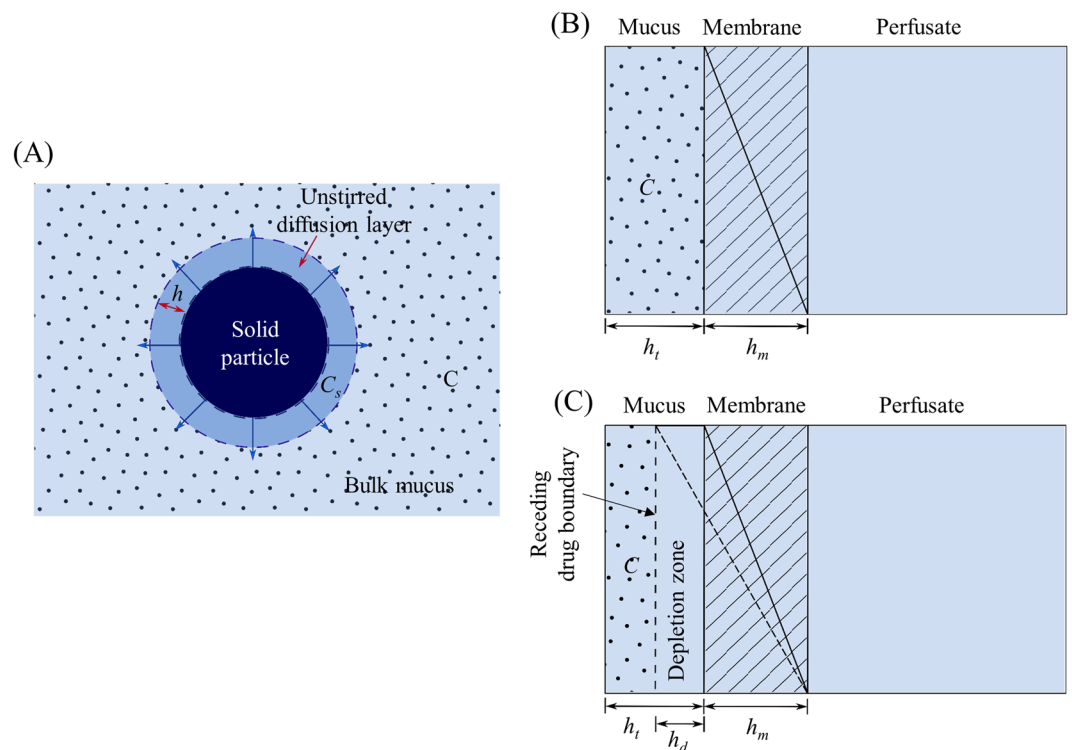


Figure 4. Dissolution of drug particle, showing the unstirred diffusion layer between the particle surface and bulk solution (A), and schematic of drug diffusion from mucus through the membrane at well-stirred (B) and unstirred condition (C) at pseudo steady state. (C - concentration of the drug in mucus simulant at time t , C_s - concentration of a saturated solution of the drug, h - thickness of the mucus unstirred diffusion layer around each particle, h_d - thickness of a depletion zone in the unstirred mucus phase at time t , h_m - thickness of the membrane, and h_t - thickness of mucus).

mucus is homogeneously distributed. Thus, membrane of thickness h_m is the only barrier for diffusion of drug from mucus in a well-stirred system i.e. total diffusion barrier thickness $h_T = h_m$. In an unstirred system (Fig. 4C), as drug passes out of homogeneous mucus, the boundary of drug (dotted line in Fig. 4C) moves towards the left and forms a depletion zone of a thickness h_d .

Thickness of depletion zone $h_d = \text{fraction of drug in the receptor } (f_d) \times \text{thickness of mucus } (h_t)$ (6)

Thickness of depletion zone increases with increasing drug diffusion. The total diffusion barrier thickness in an unstirred system is the thickness of membrane (h_m) and depletion zone (h_d) i.e. $h_T = h_m + h_d = h_m + f_d \times h_t$.

The permeation rate of the drug through a well-stirred or unstirred system was calculated as follows

$$\text{Permeation rate} = PS(C_{\text{mucus}} - C_{\text{perfusate}}) \quad (7)$$

Where permeability coefficient P (cm s^{-1}) is defined as the diffusion coefficient D multiplied by the partition coefficient K , and divided by the diffusional thickness, h and S is the surface area of the membrane. There is no partitioning of drug involved in the case of drug diffusion through the mucus and membrane with aqueous pathways. Thus, P can be expressed as

$$P = \frac{D}{h} \quad (8)$$

In general, it is difficult to determine the D and h independently in order to calculate P . However, permeability coefficient can be measured experimentally (P_{exp}) by measuring the rate of permeation and knowing S , concentration of drug in the donor phase (mucus) C_d and volume of donor phase (mucus) V_d . It can be obtained from the slope of $\ln C_d$ versus time t :

$$\ln C_d = \ln C_{d0} - \frac{PSt}{V_d} \quad (9)$$

$$P_{\text{exp}} = \frac{D}{h_{\text{exp}}} \quad (10)$$

Where h_{exp} is the thickness of the membrane used in the experimental study.

In a well-stirred system, the thickness of the diffusion barrier remains constant throughout the diffusion process. Thus, the permeability coefficient also remains constant (P_{exp}).

In a well-stirred system, at all times, $h_T = h_m$

$$P = \frac{D}{h_T} = \frac{D}{h_m} \quad (11)$$

By substituting the experimental permeability coefficient (i.e. Eq. 10) in Eq. 11

$$P = \frac{P_{exp} h_{exp}}{h_m} \quad (12)$$

In an unstirred system the thickness of the diffusion barrier increases with increasing diffusion due to formation of the depletion zone; hence the permeability coefficient varies with time.

In an unstirred system, at time 0, $h_T = h_m$

$$P_0 = \frac{D}{h_T} = \frac{D}{h_m} \quad (13)$$

At time t , $h_T = h_m + f_d \times h_t$

$$P_t = \frac{D}{h_T} = \frac{D}{h_m + f_d h_t} \quad (14)$$

By substituting experimental permeability coefficient (i.e. Eq. 10) in Eq. 14 the permeability coefficient at time t is:

$$P_t = \frac{P_{exp} h_{exp}}{h_m + f_d h_t} \quad (15)$$

Step 3. Collection of the perfusate containing permeated drug into a collection tube. In this step (See Figs. 2 and 3), perfusate is continuously removed from the receiver into the collection tubes. Thus, the drug permeated into the perfusate in the receiver compartment is transferred into the collection tubes at a rate calculated using Eq. 16.

$$\text{Collection rate} = \text{Concentration of drug in perfusate} \times \text{Perfusate flow rate} \quad (16)$$

The components of the model. Step 1 - dissolution of respirable size dry powder particles in small volume of mucus simulant, Step 2 - permeation of dissolved drug from mucus through the dialysis membrane, and Step 3 - collection of the perfusate with permeated drug into a collection tube are linked to construct a model for dissolution of drug from respirable size particles at small volume of mucus simulant under well-stirred (Fig. 2) or unstirred (Fig. 3) conditions. Various equations and assumptions that were made in the construction of the simulation models are described in the Supplementary information (Sections S1 and S2).

Simulation of the percentage cumulative drug permeated versus time profiles using STELLA simulation model. The simulations for the permeation (dissolution followed by diffusion of drug) of anti-tubercular drugs, moxifloxacin and ethionamide from respirable size particles were conducted using the initial parameter values shown in Table 1. The parameter values used were obtained from the experimental results shown in Eedara *et al.*⁵. The moxifloxacin and ethionamide respirable size particles were assumed to possess a particle density of 1.0 g cm^{-3} ⁴⁷.

Sensitivity analysis of the model. Sensitivity analyses of the models were conducted by varying the volume of the mucus (25, 50, and $100 \mu\text{L}$), perfusate flow rate ($0.2, 0.4, \text{ and } 0.8 \text{ mL min}^{-1}$) and membrane thickness (experimental membrane thickness (h_{exp}) 60, 80, $100 \mu\text{m}$, and membrane thickness used in the simulation (h_m) 30, 60 and $90 \mu\text{m}$). The parameters were varied one at a time while keeping others fixed to determine the influence of the parameters on the predicted percentage drug collected into the collection tubes.

Results and Discussion

Permeation of drug from solution through the membrane. STELLA models were constructed for permeation of the drug from a solution (only diffusion of drug) through the membrane under well-stirred (Supplementary Figure S2) or unstirred conditions (Supplementary Figure S3). Various equations and assumptions that were made in the construction of the simulation models (Supplementary Figures S2 and 3) are described in the Supplementary information (Sections S3 and S4). The simulations for the permeation of moxifloxacin and ethionamide from solutions were conducted using the initial parameter values shown in Supplementary Table S1.

The experimental permeability coefficient calculated from data covering over 80% permeation for ethionamide ($5.3 \times 10^{-4} \text{ cm min}^{-1}$) is three times higher than that of higher molecular weight moxifloxacin ($1.8 \times 10^{-4} \text{ cm min}^{-1}$)⁵. The simulation profiles (Fig. 5) also show the faster permeation of ethionamide compared to moxifloxacin at both well-stirred and unstirred conditions. Ethionamide showed complete permeation by 60 min at

Parameters	Moxifloxacin	Ethionamide
Drug solubility (at donor medium pH) [*]	$17.70 \times 10^{-3} \text{ g cm}^{-3}$	$0.46 \times 10^{-3} \text{ g cm}^{-3}$
Intrinsic dissolution rate (at donor medium pH)	$0.50 \times 10^{-3} \text{ g cm}^{-2} \text{ min}^{-1}$	$0.06 \times 10^{-3} \text{ g cm}^{-2} \text{ min}^{-1}$
Diameter of particles	$2.9 \times 10^{-4} \text{ cm}$	$3.6 \times 10^{-4} \text{ cm}$
Particle density (assumed)	1.0 g cm^{-3}	1.0 g cm^{-3}
Experimental permeability coefficient (P_{exp})	$1.8 \times 10^{-4} \text{ cm min}^{-1}$	$5.3 \times 10^{-4} \text{ cm min}^{-1}$
Mucus simulant	1.5% w/v PEO in PBS, pH 7.4	
Mucus simulant volume	$25 \times 10^{-3} \text{ cm}^3$	
Perfusate, its pH and flow rate	PBS, pH 7.4, $0.4 \text{ cm}^3 \text{ min}^{-1}$	
Perfusate volume in the receptor	$500 \times 10^{-3} \text{ cm}^3$	
Area of the membrane	4.91 cm^2	
h_{exp} [†]	$62.5 \times 10^{-4} \text{ cm}$ (hydrated membrane)	
h_m (assumed) [†]	$62.5 \times 10^{-4} \text{ cm}$	

Table 1. Initial parameter values used for simulation. *Drug solubility was measured in PBS, pH 7.4 and we assumed the same solubility in mucus simulant (1.5% w/v polyethylene oxide (PEO) in PBS, pH 7.4) used in the experimental study. [†] h_{exp} - thickness of the membrane used in the experimental study, h_m - thickness of the membrane used in the STELLA simulations.

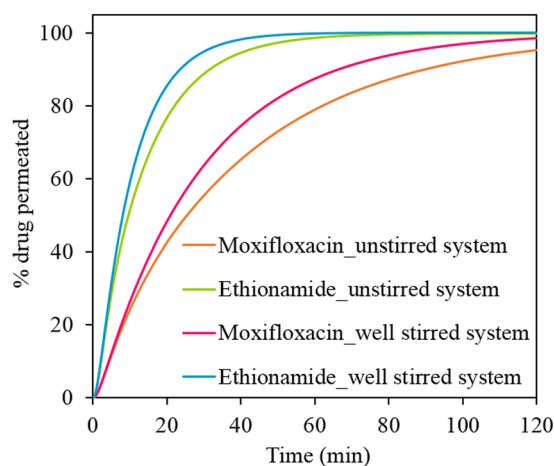


Figure 5. STELLA simulated permeation profiles of moxifloxacin and ethionamide from the solutions (only diffusion of drug) at $25 \mu\text{L}$ of mucus assuming a homogenous (well-stirred) donor and an unstirred donor with a developing depletion zone.

both well-stirred and unstirred conditions. However, moxifloxacin showed slower permeation taking more than 120 min to completely permeate the drug through the membrane. The slower permeation of both moxifloxacin and ethionamide at unstirred condition was due to an increased diffusion barrier thickness with a depletion zone (Fig. 4C).

Dissolution of drug from the respirable size particles. Figure 6 shows the simulated permeation profiles of moxifloxacin and ethionamide from solutions of the drugs and from suspensions of respirable size particles using $25 \mu\text{L}$ of mucus simulant and 0.4 mL min^{-1} perfusate flow rate. The permeation profiles of moxifloxacin from the suspension (dissolution followed by diffusion) and a solution (only diffusion) were superimposable at both well-stirred and unstirred conditions indicating rapid dissolution of the moxifloxacin particles with permeation rate being controlled by the diffusion through the membrane. Overall, ethionamide permeated faster than moxifloxacin; however, the ethionamide respirable particles showed a significant decrease in the permeation of drug compared to the solution at well-stirred and unstirred conditions due to the slow dissolution of poorly water-soluble (0.46 mg mL^{-1})⁵ ethionamide particles in the small volume ($25 \mu\text{L}$) of mucus simulant. Both moxifloxacin and ethionamide respirable particles showed a faster permeation of drug under the well-stirred condition compared to the unstirred condition as expected.

Comparison of the experimental permeation profiles with STELLA simulated permeation profiles. The experimental permeation profiles of moxifloxacin (Fig. 7A) from its solution and respirable particles were not significantly ($p > 0.05$) different which indicates rapid dissolution of moxifloxacin, and its permeation was limited by diffusion through the membrane. The experimental permeation profile (solid lines with markers and error

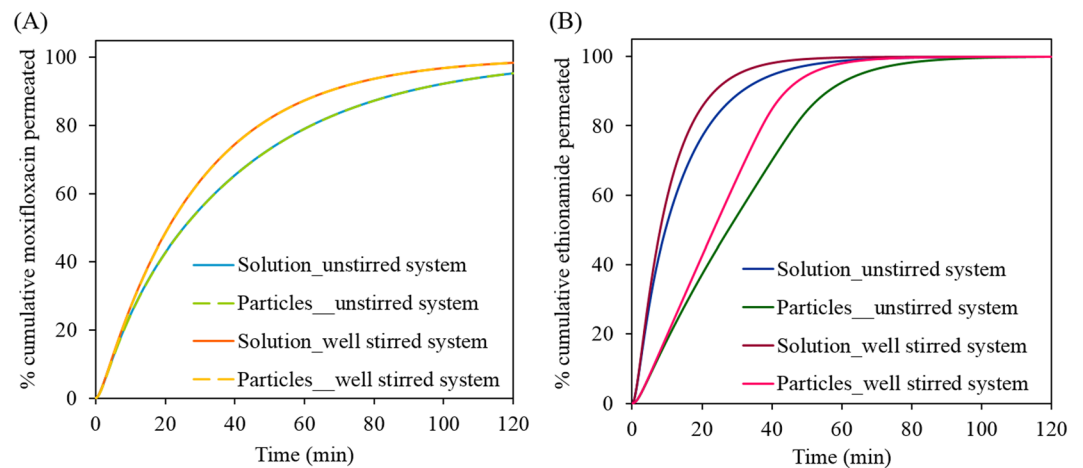


Figure 6. STELLA simulated permeation profiles of moxifloxacin (A) and ethionamide (B) from the solutions (50 μg in 25 μL of mucus simulant) and respirable size particles (50 μg) under well-stirred and unstirred conditions. The mucus simulant volume and perfusate flow rate were 25 μL and 0.4 mL min^{-1} , respectively. In figure (A), the moxifloxacin permeation profiles from solution and respirable size particles were superimposed with each other at both well-stirred and unstirred conditions.

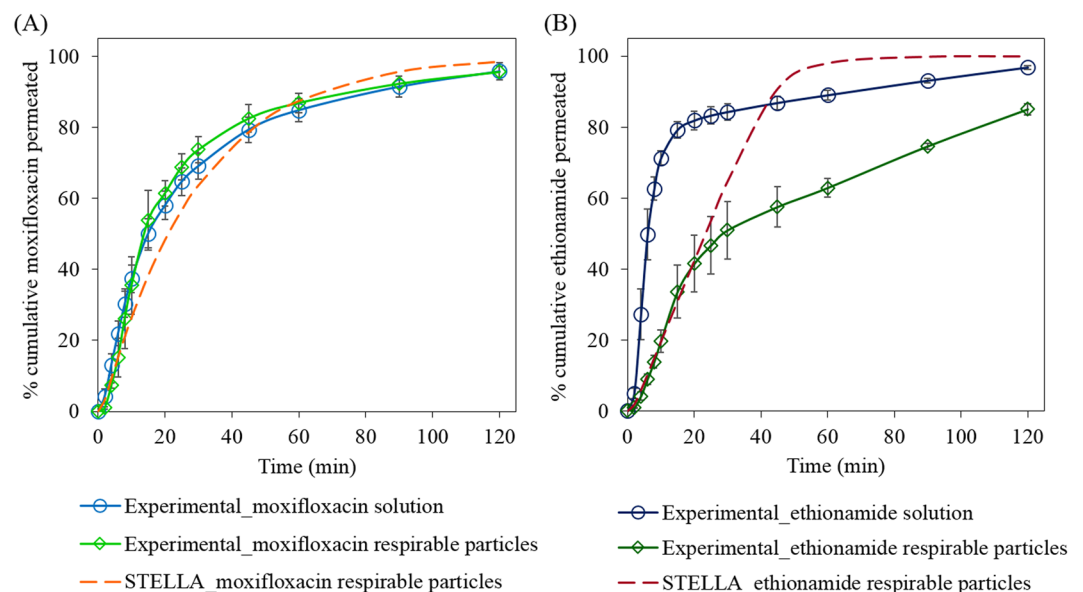


Figure 7. Experimental permeation profiles (solid lines with markers and error bars) of moxifloxacin (A) and ethionamide (B) from the solutions and respirable size particles ($\sim 50 \mu\text{g}$) in comparison to the simulation permeation profiles (dashed lines) from respirable size particles under well-stirred condition. The mucus simulant (1.5% w/v PEO in PBS) volume and perfusate (PBS, pH 7.4) flow rate were 25 μL and 0.4 mL min^{-1} , respectively. Data are means \pm SD ($n = 3$).

bars in Fig. 7A) of moxifloxacin from respirable size particles approximately fits with the simulated permeation profiles at well-stirred condition (dashed lines in Fig. 7A). In the case of ethionamide (Fig. 7B), the experimental permeation profile from respirable size particles only fits with the well-stirred STELLA simulated permeation profile over initial 30 min, followed by a slower permeation of the drug.

The differences between the STELLA simulations and the experimental data exemplify the value of simulations, since they indicate that the mechanism incorporated into the existing STELLA model are insufficient to describe the dissolution. Thus, the differences stimulate creative thinking about other factors that may influence drug delivery rate from respirable drug particles. Some possible reasons for the differences in the simulated and experimental permeation profiles of ethionamide are:

1. In the STELLA simulation, the particles are assumed to be smooth, spherical and of uniform size, but the experimental ethionamide powder particles were broken, non-spherical and with a size distribution of 1.5 to 8 μm .

- The intrinsic dissolution rate (IDR) of the drug used in STELLA simulation was determined in PBS, pH 7.4 as dissolution medium using a compressed disc (1.3 cm²) of powder by the rotating disc method. However, during the experimental dissolution study for the respirable size particles, the particles collected using the mTSI are well-separated and smaller in size compared to the compressed powder disc used in IDR study and might possess the unstirred diffusion layer of varying thickness compared to the compressed disc used in the IDR study. Further during the experimental dissolution study, a viscous mucus simulant composed of PEO and PBS, pH 7.4 was used as a dissolution medium in which the diffusion of the dissolved drug might be slower compared to the PBS, pH 7.4 alone used in the IDR study.

These possible reasons provide the basis for other experiments as well as modifications to the STELLA model to achieve a closer agreement between the simulation profiles and the experimental results.

Sensitivity analysis. Sensitivity analyses of the simulations to the changes in the mucus simulant volume, perfusate flow rate and membrane thickness are shown in following sections.

Sensitivity to the change in mucus simulant volume. Figure 8 shows the simulated permeation profiles of moxifloxacin and ethionamide with increasing mucus simulant volumes (25, 50 and 100 μL) at 0.4 mL min⁻¹ perfusate flow rate under well-stirred and unstirred conditions. The permeation of both the drugs decreased with increasing mucus simulant volume at well-stirred and unstirred conditions.

For moxifloxacin all three volumes (25, 50 and 100 μL) of the mucus simulant can solubilize the mass of the moxifloxacin (50 μg) completely, so the concentration of the moxifloxacin in mucus simulant decreases with increasing volumes (25 μL - 2.0 mg mL⁻¹ > 50 μL - 1.0 mg mL⁻¹ > 100 μL - 0.5 mg mL⁻¹). Thus the driving concentration in the donor decreases so the permeation rate reduces. For ethionamide, the situation is more complex. The solubility of ethionamide in PBS (0.46 \pm 0.02 mg mL⁻¹) is much lower than that of moxifloxacin and there is excess undissolved ethionamide in all three volumes of mucus simulant tested (25 μL - 11.5 μg , 50 μL - 23.0 μg , 100 μL - 46 μg) at earlier times. Eventually, sufficient ethionamide has permeated such that there is no excess undissolved drug in the donor. This occurs at an earlier time when the donor volume is large. Hence the driving concentration decreases leading to a fall in the permeation rate at earlier times as the donor volume is increased. This result has implications for understanding the absorption rate of drug from the lungs. As for the biopharmaceutical classification system for orally administered drugs, a similar system can be envisaged for the pulmonary route in which drug dose, drug solubility and volume of lung fluid will influence absorption rate.

Under unstirred condition, not only do the above factors operate, but in addition there is an increase in the diffusion (depletion layer) thickness that further slows the permeation of both moxifloxacin and ethionamide with increasing mucus simulant volumes.

Influence of perfusate flow rate. Figure 9 shows that there was no significant change in the simulated permeation profiles of moxifloxacin and ethionamide from respirable size particles in 25 μL of mucus simulant at increasing perfusate flow rates (0.2, 0.4 and 0.8 mL min⁻¹) under well-stirred and unstirred conditions.

The perfusion flow rate could potentially affect permeation rate for two reasons: (i) Its effect on the concentration in the receptor phase and (ii) Its effect on the thickness of the static diffusion layer on the receptor side of the membrane.

Passive diffusion of drug molecules from a solution through the membrane occurs from the region of higher to the lower concentration and is directly proportional to the concentration difference ($C_{\text{mucus}} - C_{\text{perfusate}}$) between the donor (mucus) and receptor (perfusate). The calculated concentrations of moxifloxacin and ethionamide in mucus and perfusate at various perfusate flow rates (0.2, 0.4, and 0.8 mL min⁻¹) in the STELLA simulation under well-stirred and unstirred condition are presented in Supplementary information (moxifloxacin: at well-stirred condition- Supplementary Table S2, at unstirred condition- Supplementary Table S3, ethionamide: at well-stirred condition- Supplementary Table S4, at unstirred condition- Supplementary Table S5). The perfusate concentrations of both the drugs at all the perfusate flow rates under well-stirred and unstirred conditions were negligible compared with the mucus concentration ($C_{\text{perfusate}} \ll C_{\text{mucus}}$ i.e. $(C_{\text{mucus}} - C_{\text{perfusate}}) \approx C_{\text{mucus}}$). Thus, the diffusion rate is proportional to the concentration of the drug in the mucus, C_{mucus} and thus the perfusate flow rate has no significant effect on the permeation rates of moxifloxacin and ethionamide.

The diffusion barrier consists of mucus simulant, the membrane and the unstirred water layers which are present on both sides of the membrane⁴⁸. The thickness of the unstirred water layers is unknown and might be small compared to the mucus simulant and membrane thickness. Thus, we assumed the thicknesses of mucus simulant and hydrated membrane as the diffusion barrier thickness in the STELLA simulation model. However, with increasing perfusate flow rate, the thickness of the unstirred water layer present beneath the membrane towards the receptor compartment might decrease leading to faster permeation of drug⁴⁹ but this was not built into the model.

Influence of the membrane thickness. The thickness (h_{exp}) of the hydrated membrane used in the experimental drug permeation study was measured using a micrometer. However, the permeation barrier consists of the hydrated membrane plus unstirred water layers on each side of the membrane so the exact thickness of the diffusion barrier is unknown. Thus, we have simulated the permeation profiles (Fig. 10) of moxifloxacin and ethionamide from the solutions (50 μg of the moxifloxacin or 10 μg of ethionamide in 25 μL of mucus simulant, 0.4 mL min⁻¹ perfusate flow rate) for a range of experimental membrane thicknesses ($h_{\text{exp}} = 60, 80$ and 100 μm), and compared the results with the experimental permeation profile to estimate the thickness of the unstirred

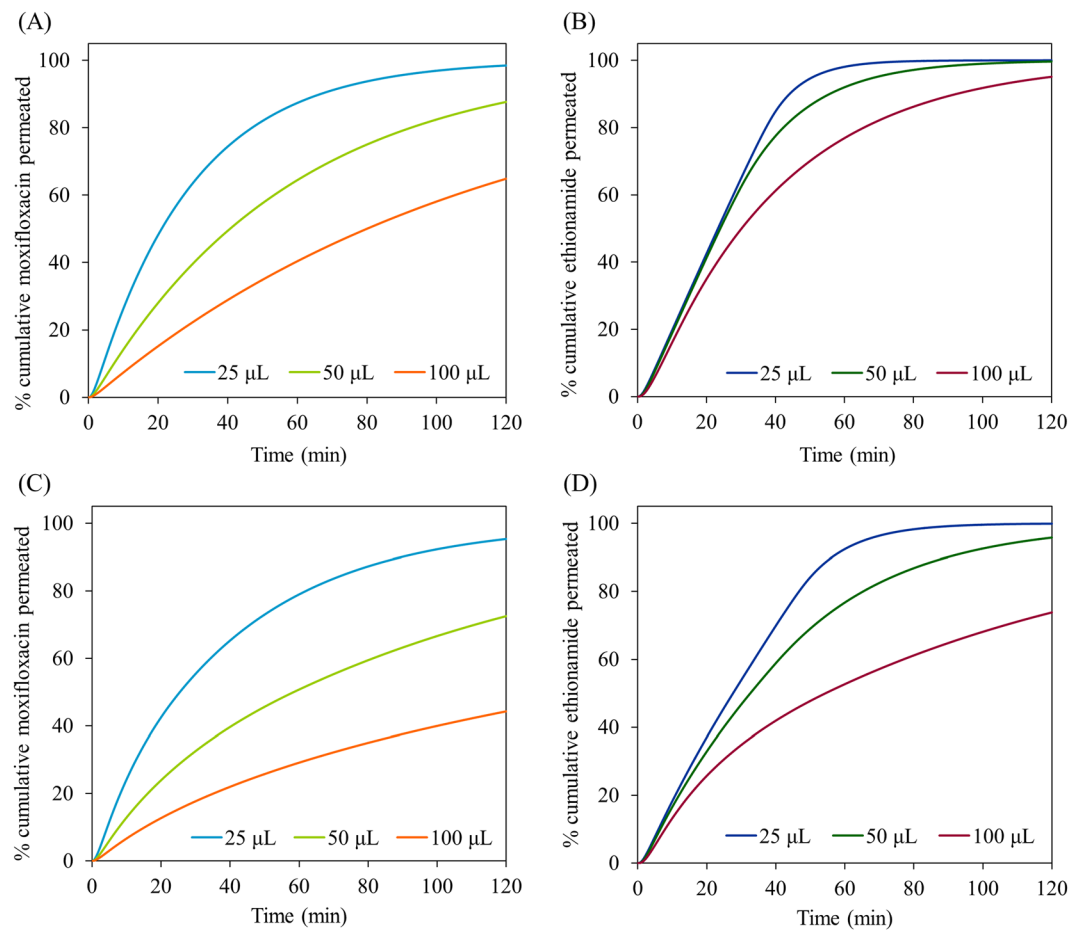


Figure 8. Influence of mucus simulant volume (25, 50 and 100 μL) on the simulated permeation (dissolution followed by diffusion) of mofloxacin (A- well-stirred condition; C- unstirred condition) and ethionamide (B- well-stirred condition; D- unstirred condition) from the respirable size particle suspensions at 0.4 mL min^{-1} perfusate flow rate under well-stirred condition and unstirred conditions.

water layer thickness. As expected, increasing h_{exp} increase the permeation rate (see Eq. 15) and the simulation profile at $h_{exp} = 100 \mu\text{m}$ for both mofloxacin and ethionamide closely matched the experimental permeation profile over 80% of drug permeation. This suggests that the thickness of the unstirred water layer in the receptor was approximately $40 \mu\text{m}$.

The simulated and experimental permeation profiles (Fig. 10) of mofloxacin and ethionamide show an initial near linear steady state permeation followed by a falling permeation rate over 80% drug release due to the decreasing concentration of drug in the donor compartment. However, the experimental permeation profiles of ethionamide show significantly slower permeation after 80% drug release compared to the simulated permeation profiles. The possible reason for the slower permeation of ethionamide might be due to the slower dissolution of larger particles (size distribution of 1.5 to $8 \mu\text{m}$) of ethionamide during experimental study.

Figure 11 shows the simulated permeation profiles of mofloxacin and ethionamide from respirable size particles in $25 \mu\text{L}$ of mucus simulant at increasing membrane thickness (h_m) (30 , 60 , and $90 \mu\text{m}$) and 0.4 mL min^{-1} perfusate flow rates under well-stirred and unstirred conditions. With increasing membrane thickness, the diffusional length for the solute molecules increases and leads to a slower permeation. Accordingly, the permeation of both the drugs decreased with increasing membrane thickness (h_m) at well-stirred and unstirred conditions. However, the simulated permeation profile of ethionamide was not a close fit to the experimental permeation profile.

Conclusions

A STELLA simulation model was constructed for *in vitro* dissolution testing of respirable size particles in a custom-made dissolution apparatus. Both the simulations and the experimental data stimulate thinking on operative mechanisms involved in drug delivery via the lungs. The simulated permeation profile of ethionamide from a solution (only membrane diffusion) showed faster permeation compared to mofloxacin under well-stirred and unstirred conditions. However, the permeation of both the drugs was slower in the model which assumed unstirred conditions as the diffusion layer thickness increases by the formation of a depletion zone under unstirred conditions. The simulated permeation profiles of mofloxacin from solution (only diffusion) and respirable size particles (dissolution followed by the diffusion through the membrane) were similar, indicating fast

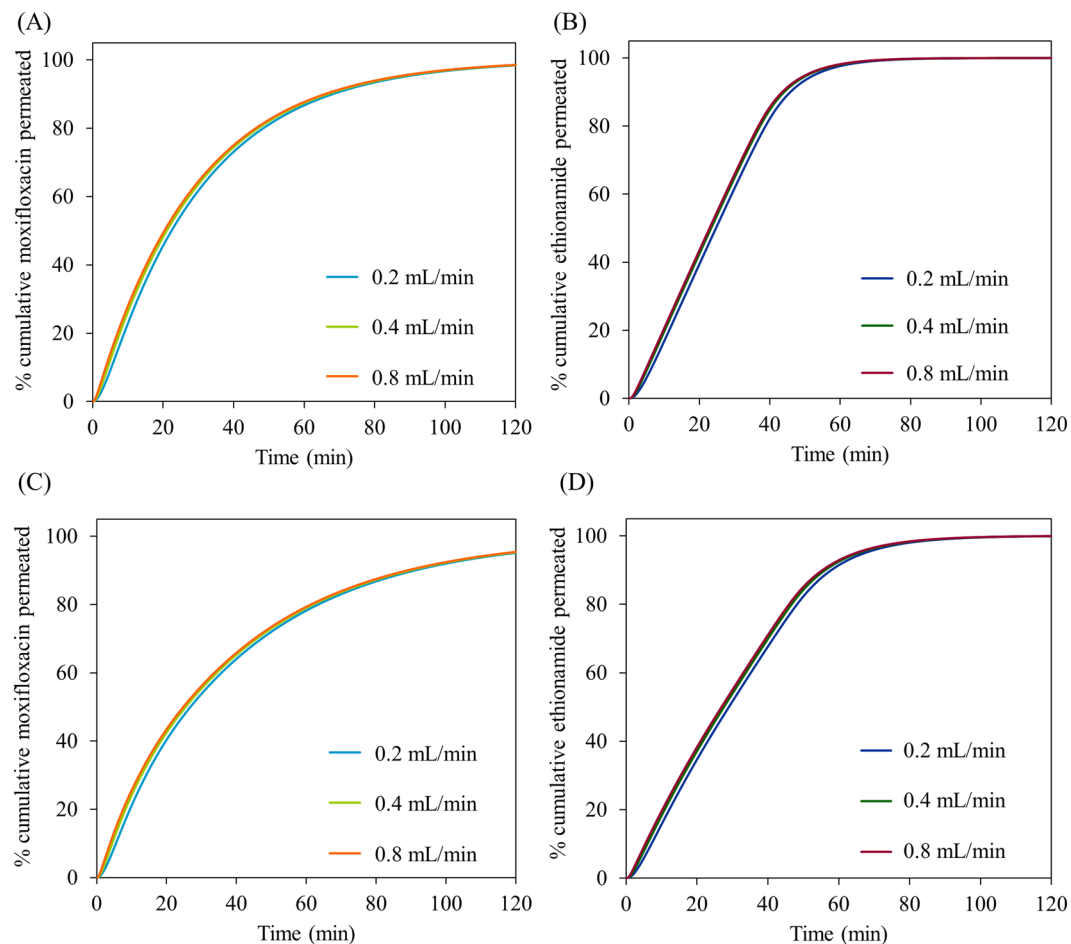


Figure 9. Influence of perfusate flow rate (0.2, 0.4 and 0.8 mL min⁻¹) on the simulated permeation (dissolution followed by diffusion) of moxifloxacin (A- well-stirred condition; C- unstirred condition) and ethionamide (B- well-stirred condition; D- unstirred condition) from the respirable particles using 25 μ L of mucus.

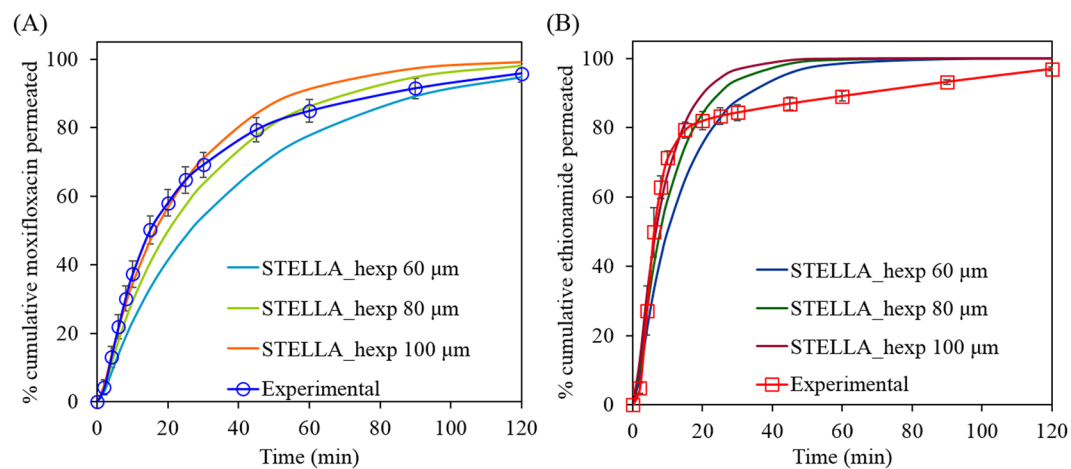


Figure 10. Comparison of the simulated permeation profiles of moxifloxacin (A) and ethionamide (B) from the solutions (50 μ g of moxifloxacin or 10 μ g of ethionamide in 25 μ L of mucus simulant, 0.4 mL min⁻¹ perfusate flow rate) at an experimental membrane thickness (h_{exp}) of 60, 80, and 100 μ m under unstirred conditions with the experimental permeation profiles.

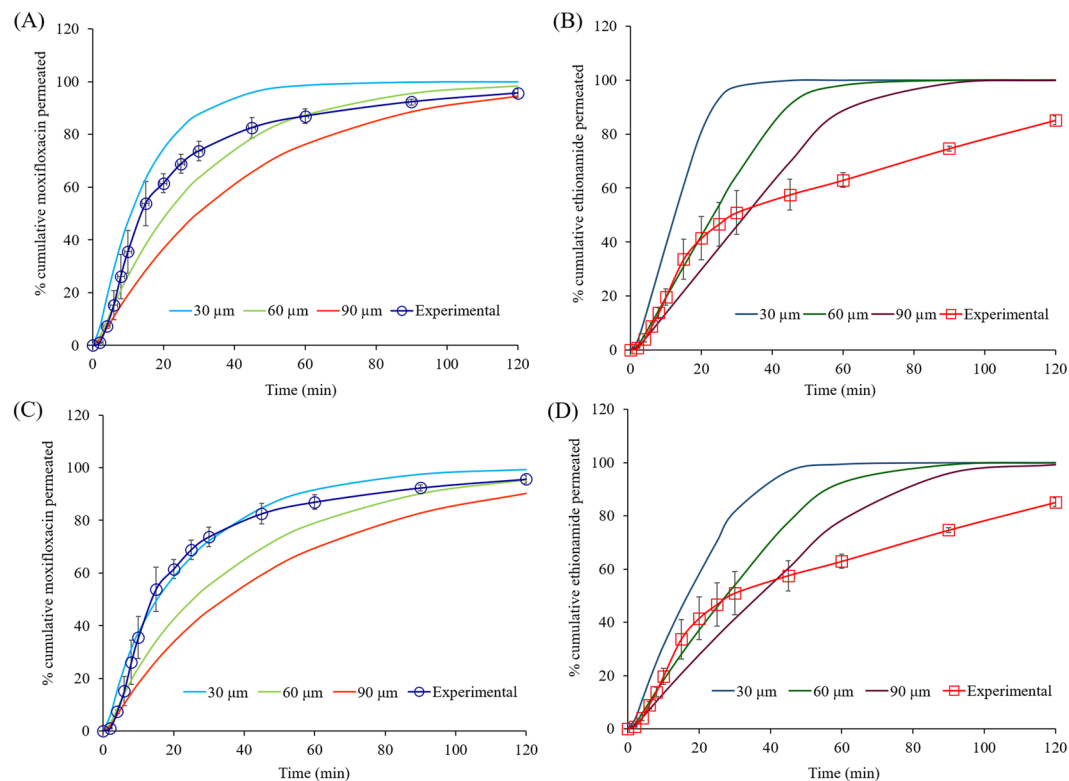


Figure 11. Influence of membrane thickness (30, 60, and 90 μm) on the simulated permeation (dissolution followed by diffusion) of moxifloxacin (A- well-stirred condition; C- unstirred condition) and ethionamide (B- well-stirred condition; D- unstirred condition) from the respirable particles using 25 μL of mucus under well-stirred and unstirred conditions. Experimental permeation profiles (solid lines with markers and error bars) of moxifloxacin and ethionamide from the respirable size particles ($\sim 50 \mu\text{g}$) using 25 μL of mucus at 0.4 mL min^{-1} perfusate flow rate.

dissolution of the particles. However, the simulated permeation profile of the lower soluble ethionamide showed slower permeation compared to the solution indicating that dissolution rate delayed permeation. Increasing the volume of the mucus simulant reduced the permeation rate of moxifloxacin to a greater extent than ethionamide. This suggests the need for a biopharmaceutical classification system for drugs delivered via the lungs and better understanding of lung fluid volumes. Membrane thickness decreased the permeation of drug. This model will be useful to inform understanding of the dissolution behaviour of drug from respirable size particles before proceeding to experimental studies in the custom-made dissolution apparatus.

Received: 13 June 2019; Accepted: 25 November 2019;

Published online: 06 December 2019

References

1. FDA, U. Guidance for Industry: Dissolution testing of immediate-release solid oral dosage forms. Food and Drug Administration, Center for Drug Evaluation and Research (CDER) (1997).
2. Gray, V. A. *et al.* The inhalation ad hoc advisory panel for the USP performance tests of inhalation dosage forms. *Pharma. Forum* **34**, 1068–1074 (2008).
3. Son, Y.-J., Mitchell, J. P. & McConville, J. T. *In vitro* performance testing for pulmonary drug delivery. In *Controlled Pulmonary Drug Delivery* (eds Smyth, H. D. C. & Hickey, A. J.) 383–415 (Springer New York, 2011).
4. Patton, J. S. & Byron, P. R. Inhaling medicines: delivering drugs to the body through the lungs. *Nat. Rev. Drug Discov.* **6**, 67–74 (2007).
5. Eedara, B. B., Tucker, I. G. & Das, S. C. *In vitro* dissolution testing of respirable size anti-tubercular drug particles using a small volume dissolution apparatus. *Int. J. Pharm.* **559**, 235–244 (2019).
6. Gerde, P. *et al.* DissolvIt: an *in vitro* method for simulating the dissolution and absorption of inhaled dry powder drugs in the lungs. *Assay. Drug Dev. Technol.* **15**, 77–88 (2017).
7. Hall, C. A. & Day, J. W. Jr. *Ecosystem modeling in theory and practice: an introduction with case histories* (eds Hall, C. A. & Day, J. W. Jr.) (John Wiley & Sons, Inc., 1977).
8. Costanza, R. & Gottlieb, S. Modelling ecological and economic systems with STELLA: Part II. *Ecol. Modell.* **112**, 81–84 (1998).
9. Costanza, R. & Voinov, A. Modeling ecological and economic systems with STELLA: Part III. *Ecol. Modell.* **143**, 1–7 (2001).
10. Leahy, D. E. Progress in simulation modelling for pharmacokinetics. *Curr. Top. Med. Chem.* **3**, 1257–1268 (2003).
11. Agoram, B., Woltosz, W. S. & Bolger, M. B. Predicting the impact of physiological and biochemical processes on oral drug bioavailability. *Adv. Drug. Deliv. Rev.* **50**, S41–S67 (2001).
12. Abuasal, B. S., Bolger, M. B., Walker, D. K. & Kaddoumi, A. *In silico* modeling for the nonlinear absorption kinetics of UK-343,664: a P-gp and CYP3A4 substrate. *Mol. Pharm.* **9**, 492–504 (2012).

13. Collingwood, S. P., Coe, D., Pryde, D. & Lock, R. Respiratory drug discovery, current developments and future challenges: Highlights from the Society of Medicines Research Symposium, held on June 14th, 2012 - Horsham, UK. *Drugs of the Future* **37**, 619–625 (2012).
14. Huisinga, W., Telgmann, R. & Wulkow, M. The virtual laboratory approach to pharmacokinetics: design principles and concepts. *Drug Discov. Today* **11**, 800–805 (2006).
15. Thelen, K., Jantravid, E., Dressman, J. B., Lippert, J. & Willmann, S. Analysis of nifedipine absorption from soft gelatin capsules using PBPK modeling and biorelevant dissolution testing. *J. Pharm. Sci.* **99**, 2899–2904 (2010).
16. Willmann, S. *et al.* Whole-body physiologically based pharmacokinetic population modelling of oral drug administration: inter-individual variability of cimetidine absorption. *J. Pharm. Pharmacol.* **61**, 891–899 (2009).
17. Heimbach, T. *et al.* Physiologically based pharmacokinetic modeling to supplement nilotinib pharmacokinetics and confirm dose selection in pediatric patients. *J. Pharm. Sci.* **108**, 2191–2198 (2019).
18. Sjögren, E. *et al.* *In silico* predictions of gastrointestinal drug absorption in pharmaceutical product development: application of the mechanistic absorption model GI-Sim. *Eur. J. Pharm. Sci.* **49**, 679–698 (2013).
19. Lindfield, G. & Penny, J. Chapter 1 - An Introduction to Matlab®. In *Numerical Methods (Fourth Edition)* (eds Lindfield, G. & Penny, J.) 1–72 (Academic Press, 2019).
20. Emond, C., Ruiz, P. & Mumtaz, M. Physiologically based pharmacokinetic toolkit to evaluate environmental exposures: Applications of the dioxin model to study real life exposures. *Toxicol. Appl. Pharmacol.* **315**, 70–79 (2017).
21. Borghardt, J. M., Weber, B., Staab, A. & Kloft, C. Pharmacometric models for characterizing the pharmacokinetics of orally inhaled drugs. *AAPS J.* **17**, 853–870 (2015).
22. Radivojević, S., Zellnitz, S., Paudel, A. & Fröhlich, E. Searching for physiologically relevant *in vitro* dissolution techniques for orally inhaled drugs. *Int. J. Pharm.* **556**, 45–56 (2019).
23. Patrick Smith, F., Holzworth, D. P. & Robertson, M. J. Linking icon-based models to code-based models: a case study with the agricultural production systems simulator. *Agric. Syst.* **83**, 135–151 (2005).
24. Wallach, D., Makowski, D., Jones, J. W. & Brun, F. Chapter 3 - Simulation with dynamic system models. In (eds Wallach, D., Makowski, D., Jones, J. W. & Brun, F. B. T.-W. with D. C. M. (Third E.)) 97–136 (Academic Press, 2019).
25. Fei, Y., Kostewicz, E. S., Sheu, M.-T. & Dressman, J. B. Analysis of the enhanced oral bioavailability of fenofibrate lipid formulations in fasted humans using an *in vitro-in silico-in vivo* approach. *Eur. J. Pharm. Biopharm.* **85**, 1274–1284 (2013).
26. Kostewicz, E. S. *et al.* PBPK models for the prediction of *in vivo* performance of oral dosage forms. *Eur. J. Pharm. Sci.* **57**, 300–321 (2014).
27. Mikulecky, D. C. Modeling Intestinal absorption and other nutrition-related processes using PSPICE and STELLA. *J. Pediatr. Gastroenterol. Nutr.* **11**, 7–20 (1990).
28. Otsuka, K., Shono, Y. & Dressman, J. Coupling biorelevant dissolution methods with physiologically based pharmacokinetic modelling to forecast *in-vivo* performance of solid oral dosage forms. *J. Pharm. Pharmacol.* **65**, 937–952 (2013).
29. Shono, Y. *et al.* Prediction of food effects on the absorption of celecoxib based on biorelevant dissolution testing coupled with physiologically based pharmacokinetic modeling. *Eur. J. Pharm. Biopharm.* **73**, 107–114 (2009).
30. Kambayashi, A. & Dressman, J. B. Forecasting gastrointestinal precipitation and oral pharmacokinetics of dantrolene in dogs using an *in vitro* precipitation testing coupled with *in silico* modeling and simulation. *Eur. J. Pharm. Biopharm.* **119**, 107–113 (2017).
31. Kambayashi, A. & Dressman, J. B. Predicting the changes in oral absorption of weak base drugs under elevated gastric pH using an *in vitro-in silico-in vivo* approach: case examples-dipyridamole, prasugrel, and nelfinavir. *J. Pharm. Sci.* **108**, 584–591 (2019).
32. Kambayashi, A., Yasuji, T. & Dressman, J. B. Prediction of the precipitation profiles of weak base drugs in the small intestine using a simplified transfer (“dumping”) model coupled with *in silico* modeling and simulation approach. *Eur. J. Pharm. Biopharm.* **103**, 95–103 (2016).
33. Kaur, N., Narang, A. & Bansal, A. K. Use of biorelevant dissolution and PBPK modeling to predict oral drug absorption. *Eur. J. Pharm. Biopharm.* **129**, 222–246 (2018).
34. Ruff, A., Fiolka, T. & Kostewicz, E. S. Prediction of Ketoconazole absorption using an updated *in vitro* transfer model coupled to physiologically based pharmacokinetic modelling. *Eur. J. Pharm. Sci.* **100**, 42–55 (2017).
35. Grass, G. M. & Lee, V. H. A model to predict aqueous humor and plasma pharmacokinetics of ocularly applied drugs. *Invest. Ophthalmol. Vis. Sci.* **34**, 2251–2259 (1993).
36. Otsuka, K., Wagner, C., Selen, A. & Dressman, J. Prediction of *in-vivo* pharmacokinetic profile for immediate and modified release oral dosage forms of furosemide using an *in-vitro-in-silico-in-vivo* approach. *J. Pharm. Pharmacol.* **67**, 651–665 (2015).
37. Kambayashi, A., Blume, H. & Dressman, J. Understanding the *in vivo* performance of enteric coated tablets using an *in vitro-in silico-in vivo* approach: case example diclofenac. *Eur. J. Pharm. Biopharm.* **85**, 1337–1347 (2013).
38. Grass, G. M. & Morehead, W. T. Evidence for site-specific absorption of a novel ACE inhibitor. *Pharm. Res.* **6**, 759–765 (1989).
39. Hargrove, J., Hulsey, M. & Summers, A. From genotype to phenotype: computer-based modeling of gene expression with STELLA II. *Biotechniques* **15**, 1096–1101 (1993).
40. Eedara, B. B. *et al.* Crystalline adduct of moxifloxacin with trans-cinnamic acid to reduce the aqueous solubility and dissolution rate for improved residence time in the lungs. *Eur. J. Pharm. Sci.* **136**, 104961 (2019).
41. Rohrschneider, M. *et al.* Evaluation of the transwell system for characterization of dissolution behavior of inhalation drugs: effects of membrane and surfactant. *Mol. Pharm.* **12**, 2618–2624 (2015).
42. Bhatta, R. S. *et al.* Mucoadhesive nanoparticles for prolonged ocular delivery of natamycin: *In vitro* and pharmacokinetics studies. *Int. J. Pharm.* **432**, 105–112 (2012).
43. Kumar, R. & Sinha, V. R. Preparation and optimization of voriconazole microemulsion for ocular delivery. *Colloids Surf. B Biointerfaces.* **117**, 82–88 (2014).
44. Yalcin, T. E., Ilbasimis-Tamer, S. & Takka, S. Development and characterization of gemcitabine hydrochloride loaded lipid polymer hybrid nanoparticles (LPHNs) using central composite design. *Int. J. Pharm.* **548**, 255–262 (2018).
45. Shah, S., Fung, K., Brim, S. & Rubin, B. K. An *in vitro* evaluation of the effectiveness of endotracheal suction catheters. *Chest.* **128**, 3699–3704 (2005).
46. Noyes, A. A. & Whitney, W. R. The rate of solution of solid substances in their own solutions. *J. Am. Chem. Soc.* **19**, 930–934 (1897).
47. Edwards, D. A., Ben-Jebria, A. & Langer, R. Recent advances in pulmonary drug delivery using large, porous inhaled particles. *J. Appl. Physiol.* **85**, 379–385 (1998).
48. Youdim, K. A., Avdeef, A. & Abbott, N. J. *In vitro* trans-monolayer permeability calculations: often forgotten assumptions. *Drug Discov. Today* **8**, 997–1003 (2003).
49. Karlsson, J. & Artursson, P. A method for the determination of cellular permeability coefficients and aqueous boundary layer thickness in monolayers of intestinal epithelial (Caco-2) cells grown in permeable filter chambers. *Int. J. Pharm.* **71**, 55–64 (1991).

Acknowledgements

This research was funded by the Health Research Council (HRC) of New Zealand (Grant No. 15/477). Basanth Babu Eedara is grateful for support from the University of Otago Doctoral Scholarship.

Author contributions

B.B.E. designed and performed the modelling and simulation work, analysed the data and wrote the paper. I.G.T. and S.C.D. designed the modelling and simulation work, reviewed and revised the manuscript. All authors approved the final version of the manuscript for publication.

Competing interests

The authors declare no competing interests.

Additional information

Supplementary information is available for this paper at <https://doi.org/10.1038/s41598-019-55164-0>.

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