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# **OPEN** Experimental and computational chemical studies on the corrosion inhibition of new pyrimidinone derivatives for copper in nitric acid

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Inhibition of copper corrosion by some pyrimidinone derivatives, namely; (E)-N-(3-((1,3dimethyl-2,4,6-trioxohexahydropyrimidin-5-yl)diazenyl)-2,5-diethoxyphenyl)benzamide (MA-975) and (E)-6-(4-((4-chlorophenyl)diazenyl)-3-methyl-5-oxo-4,5-dihydro-1H-pyrazol-1-yl)-1,3 dimethylpyrimidine-2,4(1H,3H)-dione (MA-978C) in 1.0 M nitric acid (HNO<sub>3</sub>) was studied using weight loss (WL), electrochemical impedance spectroscopy (EIS), and potentiodynamic polarization (PP) measurements. The efficiency of inhibition increases as the concentration of inhibitor increases, and it also increases as the temperature increases. With the addition of the examined inhibitors, significant corrosion protection was obtained, and (MA-975) showed a very promising % IE (89.59%) at 21 × 10<sup>-6</sup> M using the (WL) method. The polarization data revealed that these compounds act as mixed-type compounds and are adsorbed on the copper surface following Langmuir adsorption isotherm forming a protective thin film protecting the metal in the corrosive media. Scanning electron microscopy (SEM) and Energy Dispersive X-ray were used to examine the surface morphology of copper samples. Quantum calculations and Monte Carlo simulation techniques were applied with informative yields and the results matched the experimental findings.

Corrosion is an essential process to consider in terms of safety and economics, especially for metals. Copper is a moderately noble metal<sup>1-3</sup>, and it has great electrical and thermal conductivities, as well as good corrosion resistance and workability. It is used in a lot of heating and cooling systems also it is utilized broadly as a part of industry, because of its warm conductivity. Copper's major problem is its strong response to the acidic solutions. Several acid solutions (HCl, H2SO4, and HNO3) are it is utilized to remove harmful rust in various industrial operations. Among the commercially available acids, the most frequently used one is HNO<sub>3</sub>. The utilized corrosion protective of Cu in acid medium is mainly to less the corrosion of Cu at the time of acid descaling and cleaning. Copper corrosion depends on the way of nature as well as the state of utilization of materials. The most used method for copper corrosion protection is the utilization of organic inhibitors. Numerous organic inhibitors utilized are either created from low-cost raw materials or selected from compounds having hetero atoms in their long-chain carbon or aromatic system<sup>4</sup>. Most organic inhibitors are costly, toxic, and have a negative effect on the corrosion of metal. As a result, it is important and necessary to improve environmentally safe and lowcost corrosion protection<sup>5</sup>. The majority of the understood acid inhibitors are organic heterocyclic compounds containing O, S, P and/or N atoms<sup>6-9</sup>, these atoms enhance the activity of corrosion inhibitor. Adsorption of an inhibitor facilitates the protection of the metal surface<sup>10</sup>. As a result, covalent bonding (chemisorption) and/ or electrostatic interaction (physisorption) can be used to create an adsorption coating on metal, protecting it against corrosive species attack<sup>11</sup>. It has been thought that it would be more desired and significant to produce novel low- or non-toxic corrosion inhibitors because the majority of conventional organic inhibitors are dangerous to the environment and people<sup>12</sup>. The presence of these functional groups and hetero-atoms in organic compound molecules promotes their action as copper corrosion inhibitors because these functional groups and hetero-atoms induce chemisorption. Organic derivatives also have a unique aptitude for inhibiting metal corrosion in acidic media<sup>13</sup> and other solutions. The protection efficiency of organic inhibitors is primarily due to the presence of a polar group acting as an active center for adsorption on the metallic surface<sup>14</sup>. The presence of unoccupied d-orbitals in copper atoms that form coordinative bonds with atoms that can give electrons

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Pyrimidine derivatives	Sample	Medium	%IE	References
a 2,6-dimethylpyrimidine-2-amine, <i>N</i> -Benzylidene-4,6-dimethylpyrimidine-2-amine and 2-[(3,6-dimethylpyridimine-2-ylimino) methyl]-4-nitrophenol in 2 M HCl; thymine, uracil, thymidine, and uridine	Mild steel	0.5 M HCl	96–97 at 10 mM	17
a) 6-methyl-4-morpholin-4-yl-2-oxo-1,2,3,4-tetrahydro-pyrimidine-5-carboxylic acid ethyl ester	Carbon steel	0.5 M HCl	80–86 at 0,25 g/L	18
b) 6-methyl-4-morpholin-4-yl-2-thioxo-1,2,3,4-tetrahydro-pyrimidine-5-carboxylic acid ethyl ester c) 6-methyl-4-morpholin-4-yl-2-oxo-1,2,3,4-tetrahydro-pyrimidine-5-carboxylic acid hydrazide d) 6-methyl-4-morpholin-4-yl-2-thioxo-1,2,3,4-tetrahydro-pyrimidine-5- carboxylic acid hydrazide	Mild steel	0.5 M HCl	80–86 at 0.25 g/L	18
5-Benzoyl-4-(4-carboxphenyl)-6-phenyl-1,2,3,4-tetrahydro-2-iminopyrimidine, 5-ben- zoyl-4-tolyl-6-phenyl-1,2,3,4-tetrahydro-2-thioxopyrimidine in 1 M HCl	Stainless steel	1 M HCl	90 at5×10 <sup>-3</sup> M	19
5-benzoyl-4-(substituted phenyl)-6-phenyl-3,4-dihydropyrimidine-2(1 $H$ )- (thio)ones in 0.5 M $\rm H_2SO_4$	Stainless steel	0.5 M H <sub>2</sub> SO <sub>4</sub>	92 at 2×10 <sup>-3</sup> M	20
a)5-(4-methoxyphenyl)-1,3,5,6,8-pentahydro-7-thioxo-pyrimido[4,5- <i>d</i> ] pyrimidine- 2,4-dione, b) 5-phenyl-1,3,5,6,8-pentahydro-7-thioxo-pyrimido[4,5-d] pyrimidine-2,4-dione, c) 5-(4-methoxyphenyl)-1,3,5,6,8-pentahydro-pyrimido[4,5-d] pyrimidine-2,4,7-trione d) 5-phenyl-1,3,5,6,8-pentahydro-pyrimido[4,5-d] pyrimidine-2,4,7-trione in HCl:	Mild steel	1 M HCl	97.1–88.0 at 400 ppm	21
1-(7-methyl-5-morpholin-4-yl-thiazolo[4,5-d] pyrimidin-2-yl)-hydrazine	Carbon steel	0.5 M H <sub>2</sub> SO <sub>4</sub>		22
a) 4,6-diphenyl-3,4-dihydropyrimidine-2(1 <i>H</i> )-thione b) 4-(4-methylphenyl)-6-phenyl-3,4-dihydropyrimidine-2(1 <i>H</i> )-thione c) 4-(4-methoxy-phenyl)-6-phenyl-3,4-dihydropyrimidine-2(1 <i>H</i> )-thione	Carbon steel	1 M H <sub>2</sub> SO <sub>4</sub>	99–98 at 10 mM	23
a) 4-(4'-methylphenyl)-6-(phenyl)-3,4-dihydropyrimidine-2(1 <i>H</i> )-thione b) 4-(4'-methoxylphenyl)-6-(phenyl)-3,4-dihydro-pyrimidine-2(1 <i>H</i> )-thione in 2.0 M $H_2SO_4$ <sup>39</sup> for stainless steel 304	Stainless steel 304	2 M H2SO4	97.8, 96.2 at 5 mM	24
(3a, MA-1230), (3b, MA-1231) and (3c, MA-1232)	Copper	1 M HNO <sub>3</sub>	90.3-92.1 at 21 μM	25
(i) Ethyl(2-amino-5-methyl[1,4]-triazolo[1,5-a] pyrimidin-7-yl) acetate (ii) Ethyl (5-methyl[1,2,4] triazolo[1,5-a] pyrimidin-7-yl)-acetate	Mild steel	1 M HCl	84, 85, respectively at $10^{-3}$ M	26
D-Glucose derivatives of dihydropyrido-[2,3-d:6,5-d0]-dipyrimidine- ,4,6,8(1H,3H,5H,7H)- tetraone: GPH-3, GPH-2, GPH-1	Mild steel	1 M HCl	93.9–97.8 at 10.15×10 <sup>-5</sup> M	27
3-(2-(4-(Hydroxymethyl)-1H-1,2,3-triazol-1-yl) ethyl)-2-methyl-6,7,8,9-tetra-hydropyrido [1,2-a] pyrimidin-4-one	Mild steel	1 M HCl	91 at 5 mM	28
Losartan potassium (LP) drug	Q235 steel	1 M HCl	92.0 at 5 mM at 318 K	29
5-(Benzylthio)-1H-tetrazole (BTTA), 5-Benzyl-1H-Tetrazole (BTA)	Q235 steel	0.5 M H <sub>2</sub> SO <sub>4</sub>	98.3% BTTA , 21.6% BTA for 2 mM	30

Table 1. List of pyrimidine derivatives utilized as corrosion inhibitors for various metals and alloys.

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confirms this. There is also interaction with rings having conjugated bonds  $\pi$ -electrons. Heterocycle-containing pyrimidines have been reported to be safe inhibitors with excellent corrosion inhibition actions on copper metal in acidic media<sup>15</sup>. The corrosion inhibition properties of two pyrimidinone compounds were investigated in this study, coded MA-975 and MA-978C which clearly indicates that these derivatives work well as corrosion inhibitors, and that further research is recommended. Furthermore, considering recent environmental issues, these compounds are of significant concern due to their non-toxic appearances and high solubility in the test solution, which promotes protection efficiency. Some pyrimidine derivatives were utilized as corrosion inhibitors for steel and other metals in HCl and H<sub>2</sub>SO<sub>4</sub> solutions with their percent *IE* predicted in Table 1. The most popular method of examining inhibitors today is still dazzle filtration. Researchers have coupled molecular dynamics simulation with thickness utility hypothesis calculation to urge deep insights into the barrier component of natural substances in an effort to understand this problem<sup>16</sup>.

Our objective is to study more about the inhibitory action of these pyrimidinone compounds because these derivatives have high molecular size, low toxicity (safe) and contain O, N, CH<sub>3</sub> groups and benzene rings. Some advanced techniques are used, SEM and EDX were employed to examine the surface, in addition to the application of quantum chemical calculations and Monte Carlo simulation was applied also.

# Materials and techniques

**Composition of copper samples.** The chemical composition of the copper alloy used in this paper is as follows: (weight %) 0.0050 Zn, 0.0023 Pb, 0.0023 P, 0.0018 Co, 0.019 Fe, 0.0015 Si, 0.004 Ni, 0.0011 S.

**Solutions.** The aggressive solution 0.5 M HNO<sub>3</sub> was made by diluting analytical grade HNO<sub>3</sub> (69%) with bidistilled water, and all WL tests were performed in 100 ml unstirred solutions. Every studied compound's 100 ml stock solutions ( $10^{-3}$  M) were prepared by dissolving an accurately weighed quantity of each compound in an appropriate volume of dimethyl formamide (DMF) and absolute ethanol, then diluting with bi-distilled water to the needed concentrations ( $5 \times 10^{-6} - 21 \times 10^{-6}$  M). The solutions of these compounds are completely soluble in HNO<sub>3</sub> due to it can be protonated in acid medium.



**Figure 1.** The identified pyrimidinone derivatives' synthetic pathway MA-975 and MA-978C, reagents and conditions: (i) AcONa, H<sub>2</sub>O, DMSO, 5–10 °C; (ii) EtOH/AcOH, reflux.





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**Inhibitors.** The synthesis of two pyrimidinone inhibitors was depicted in Fig. 1 as reported previously<sup>31</sup> and their chemical structures and molecular formulas were listed in Table 2. The investigations of the two pyrimidinone compounds were done at different concentrations  $(5 \times 10^{-6}, 9 \times 10^{-6}, 13 \times 10^{-6}, 17 \times 10^{-6} \text{ and } 21 \times 10^{-6} \text{ M})$  in the attendance and non-existence of the investigated compounds. In thermostatic conditions, all experiments were conducted.

**Corrosion methods.** *WL method.* In corrosion investigations, WL measurements were utilized to select the best corrosion inhibitor<sup>32</sup>. The ASTM standard G  $31-72^{31}$  was used to take this measurement. Mechanical polishing was done on the Cu alloy samples using various grades of emery sheets (1/0, 2/0, 3/0, 4/0, 5/0, and 6/0). The specimens are carefully cleaned with bi-distilled water and then degreased with acetone, dried at room temperature and then weighed. The test pieces were suspended by appropriate glass hooks at the beaker's edge and about 1 cm below the surface of the test fluid. The pieces were removed after a set amount of time, washed with bi-distilled water, dried, and weighed again. For three hours, different concentrations of inhibitors were tested for corrosion. 100 ml of blank without inhibitor and 1 M HNO<sub>3</sub> with inhibitor were used to create these concentrations. The average value was calculated after the experiment was repeated three times. The percent *E<sub>w</sub>* of the different solutions is calculated using the WL values acquired after a specified period in the mathematical Eq. (1):

$$\% E_w = \theta \times 100 = [1 - (\Delta W / \Delta W^\circ)] \times 100 \tag{1}$$

where  $\Delta W$  and  $\Delta W^{\circ}$  are weight losses per unit area (mg.cm<sup>-2</sup>) in the presence and the absence of the tested inhibitors, respectively.

Potentiodynamic polarization (PP) tests. A three electrode cell assembly with copper as the working electrode, a saturated calomel electrode (SCE) as the reference electrode, and platinum foil as the counter electrode was employed for these electrochemical research. The test sample was given 30 min to attain the steady state value of OCP before beginning the electrochemical studies. The potential range was (-200 to + 200 mV vs. SCE) at OCP with a scan rate of 0.1  $mVs^{-1}$ . The i<sub>corr</sub> calculation was used to calculate the E<sub>p</sub> and the  $\theta$  from the following Eq. (2):

$$\% E_p = \theta \times 100 = \left[1 - \left(i_{corr}/i_{corr}^\circ\right)\right] \times 100 \tag{2}$$

where  $i_{corr}$  and  $i^{o}_{corr}$  are the corrosion current densities with and without inhibitors, respectively.

*Electrochemical impedance spectroscopy (EIS) tests.* EIS measurements were carried out by using *AC* signal of 10 mV amplitude for the frequency spectrum from 100 kHz to 0.01 Hz. A Gamry Potentiostat / Galvanostat / ZRA" was utilized in electrochemical (PP & EIS) investigations (PCI4-G750). The *DC*105 *DC* Corrosion Program, the *EIS300* EIS Program, and a data collection computer are all part of Gamry. Echem Analyst version 5.5 was used to plot and calculate data.

**Surface morphology investigation by (SEM and EDX) analysis.** The applied technique to study metal surface morphology are SEM and EDX it is used to give data about the surface morphology of Cu coins with and without highest degree of concentration of the three pyrimidine inhibitors utilizing (SEM model JOEL, JSM-T20, Japan). An energy dispersive X-ray (EDX) spectroscopy device was also used to evaluate the copper samples (Zeiss Evo 10 instrument model). The beam accelerating voltage was 25 kV.

**Quantum chemical calculations.** All the quantum chemical tests occurred with finishing geometry similarity utilized Accelrys Material Studio.

**Quantum Monte Carlo simulation.** MC is a molecular dynamics method based on classical mechanics and is one of the most broadly used theoretical techniques to describe the interaction between metal and inhibitor because it provides some essential parameters such as total energy, adsorption energy, and rigid adsorption energy. In our present study, the Monte Carlo simulation calculation was used to find the lowest energy for the tested system. The outputs and descriptors achieved by the Monte Carlo simulations, such as the whole adsorption energy, firm adsorption, and deformation energies represent the most stable low energy configuration for the adsorption of the studied pyrimidine inhibitors on Cu (111) surface obtained through the Monte Carlo simulations <sup>33</sup>.

### **Results and discussion**

**WL measurements.** Effect of concentrations and temperature. The corrosion rate of copper alloy in nonexistence and existence of various concentrations of pyrimidine derivatives  $(5 \times 10^{-6} \text{ M to } 21 \times 10^{-6} \text{ M})$  in 1.0 M HNO<sub>3</sub> at 25–45 °C was studied. WL-time curves are graphically represented in Fig. 2 of pyrimidine derivatives. Corrosion parameters derived from WL method at different temperatures are given in Table 3, illustrate the calculated values of corrosion rate  $k_{corr}$  (mg.cm<sup>-2</sup>.min<sup>-1</sup>), (% $E_w$ ) and the ( $\theta$ ) for copper alloy dissolution from which a reduction in  $k_{corr}$  is noticed when copper alloy the concentration of pyrimidine derivatives increases. This behavior can be explained based on the strong interaction among pyrimidine derivatives and copper alloy surface<sup>34</sup>. In general, when the concentration of these pyrimidine derivatives rises, the value of (percent  $E_w$ ) rises as well. These findings offer evidence that pyrimidines are effective inhibitors for Cu alloy against dissolution<sup>35</sup>.



**Figure 2.** WL- time curves for dissolution of Cu alloy in 1 M HNO<sub>3</sub> at different pyrimidine derivative concentrations (MA-978C and MA-975) at 25 °C.

		MA-978C		MA-975		
Temp., °C	Conc, × 10 <sup>6</sup> M	$k_{corr}$ (mg cm <sup>-2</sup> min <sup>-1</sup> )	%η	$k_{corr}$ (mg cm <sup>-2</sup> min <sup>-1</sup> )	%η	
	Blank	$0.052 \pm 0.0021$	-	$0.052 \pm 0.0021$	-	
	5	$0.0179 \pm 0.0015$	65.6	$0.0157 \pm 0.0012$	69.8	
0.5	9	$0.0172 \pm 0.0023$	66.9	$0.0125 \pm 0.0014$	76.0	
25	14	$0.0156 \pm 0.0026$	70.0	$0.0122 \pm 0.0021$	76.5	
	17	$0.0138 \pm 0.0009$	73.5	$0.0116 \pm 0.0020$	77.7	
	21	$0.0088 \pm 0.0019$	83.1	$0.0087 \pm 0.0019$	83.3	
	Blank	$0.089 \pm 0.0022$	-	$0.089 \pm 0.0022$	-	
	5	$0.0305 \pm 0.0009$	65.7	$0.0211 \pm 0.0017$	76.3	
20	9	$0.0242 \pm 0.0023$	72.8	$0.0192 \pm 0.0023$	78.4	
50	14	$0.0208 \pm 0.0017$	76.6	$0.0179 \pm 0.0020$	79.9	
	17	0.0178±0.0026	80.0	$0.0153 \pm 0.0018$	82.8	
	21	$0.0145 \pm 0.0021$	83.7	$0.0136 \pm 0.0021$	84.7	
	Blank	0.101±0.0015	-	$0.101 \pm 0.0015$	-	
	5	$0.0318 \pm 0.0017$	68.5	$0.0216 \pm 0.0002$	78.6	
25	9	$0.0209 \pm 0.0020$	79.3	$0.0202 \pm 0.0023$	80.0	
55	14	$0.0181 \pm 0.0021$	82.1	$0.0169 \pm 0.0017$	83.3	
	17	0.0173±0.0012	82.9	$0.0108 \pm 0.0018$	89.3	
	21	0.0161±0.0017	84.1	$0.0123 \pm 0.0015$	87.8	
	Blank	$0.137 \pm 0.0020$	-	$0.137 \pm 0.0020$	-	
	5	$0.0420 \pm 0.0020$	69.3	$0.0274 \pm 0.0017$	80.0	
40	9	$0.0276 \pm 0.0023$	79.9	$0.0252 \pm 0.0020$	81.6	
40	14	$0.0223 \pm 0.0018$	83.7	$0.0205 \pm 0.0018$	85.0	
	17	$0.0209 \pm 0.0026$	84.7	$0.0182 \pm 0.0023$	86.7	
	21	$0.0154 \pm 0.0023$	88.8	$0.0151 \pm 0.0020$	89.0	
	Blank	$0.151 \pm 0.0015$	-	$0.151 \pm 0.0015$	-	
	5	$0.0379 \pm 0.0023$	74.9	$0.0302 \pm 0.0010$	80.0	
45	9	$0.0259 \pm 0.0021$	82.9	$0.0257 \pm 0.0015$	83.0	
45	14	$0.0227 \pm 0.0013$	85.0	$0.0214 \pm 0.0017$	85.8	
	17	$0.0197 \pm 0.0017$	87.0	$0.0194 \pm 0.0020$	87.2	
	21	$0.0164 \pm 0.0018$	89.1	$0.0157 \pm 0.0012$	89.6	

**Table 3.**  $k_{corr}$  and  $\% E_w$  of pyrimidine derivatives at various temperatures.



**Figure 3.** Arrhenius diagrams for Cu dissolution in the 1 M HNO<sub>3</sub> solution of pyrimidine derivatives (MA-978C, MA-975).

		Activation parameters				
		E_a*	$\Delta H^{\star}$	$-\Delta S^*$		
Inhibitor	Conc., × 10 <sup>-6</sup> M	kJ mol <sup>-1</sup>	kJ mol <sup>-1</sup>	J mol <sup>-1</sup> K <sup>-1</sup>		
Free Acid (1 M HNO <sub>3</sub> )		$68.71 \pm 0.2028$	$88.29 \pm 0.2403$	$175 \pm 0.2504$		
	5	29.06±0.2309	$43.05 \pm 0.1453$	$139 \pm 0.2309$		
	9	$27.81 \pm 0.1732$	$40.46 \pm 0.2309$	$150 \pm 0.2027$		
MA-978C	13	26.96±0.2333	$37.37 \pm 0.2729$	161±0.2603		
	17	$26.05 \pm 0.2404$	$37.36 \pm 0.1453$	$162 \pm 0.1732$		
	21	$25.19 \pm 0.1453$	$36.24 \pm 0.1453$	167±0.2333		
	5	67.51±0.2028	$74.31 \pm 0.1856$	200±0.2333		
	9	$65.60 \pm 0.1528$	$79.62 \pm 0.1764$	205±0.2333		
MA-975	13	$64.92 \pm 0.2603$	$76.69 \pm 0.1528$	211±0.1856		
	17	63.57±0.2048	$76.31 \pm 0.1453$	$223 \pm 0.1764$		
	21	$62.68 \pm 0.2028$	$61.89 \pm 0.2646$	224±0.1453		

**Table 4.** Activation parameter for Cu dissolution in  $1.0 \text{ M HNO}_3$  in the absence and presence of (MA-978C and MA-975).

By increasing temperature, this lead to increase adsorption of inhibitor molecules on the alloy surface and some chemical changes in the inhibitor molecules may occur, resulting in an increase in electron densities at the adsorption centers of the molecules. There is a slight decrease in the corrosion rate  $k_{corr}$  of pyrimidine derivatives<sup>13</sup> and hence the % $E_w$  reaches (89.59%) at the optimum concentration (21 × 10<sup>-6</sup> M). The trend of % $E_w$  follows the order MA-975 > MA-978C.

*Thermodynamic activation parameters.* Corrosion reactions obey Arrhenius processes and the apparent activation energy,  $E_a^*$ , for corrosion of copper alloy in 1 M HNO<sub>3</sub> solution in the existence, and absence at different concentrations of pyrimidine derivatives at 25–45 °C was calculated from Arrhenius Eq.3:

$$\log k_{corr} = \left(\frac{-E_a^*}{2.303\text{R}T}\right) + \log A \tag{3}$$

where  $E_a^*$  is the apparent activation energy of copper alloy dissolution and A is the pre-exponential factor, R is the molar gas constant, T is the absolute temperature. Plots of log  $k_{corr}$  vs. 1/T are displayed as straight lines for the tested inhibitors and the  $E_a^*$  was calculated from the slope of these lines Fig. 3. It can be seen from Table 4 the data that  $E_a^*$  values for the inhibitors attains lower values for inhibitor-containing solutions. Similar results have been obtained in the corrosion inhibition of copper alloy and the decrease in  $E_a^*$  signifies chemisorption<sup>36</sup>. The transition state equation (4) was used to calculate other important thermodynamic activation parameters<sup>36</sup>:



**Figure 4.** Transition state diagrams for Cu dissolution in the 1 M HNO<sub>3</sub> solution of pyrimidine derivatives (MA-978C, MA-975).

$$\log k_{corr} = \log \left(\frac{R}{Nh}\right) + \frac{\Delta S^*}{2.303R} + \frac{\Delta H^*}{2.303RT}$$
(4)

where,  $k_{corr}$  denotes to the corrosion rate, R is the molar gas constant,  $\Delta H^*$  and  $\Delta S^*$  is the enthalpy and entropy of activation, respectively. Plots of log  $k_{corr}/T$  vs 1000/T in Fig. 4 for the two derivatives, from which the values of  $\Delta H^*$  and  $\Delta S^*$  were calculated and are recorded in Table 4 for the investigated inhibitors Fig. 4 shows  $E_a^*$  for blank solution is 68 0.71 kJ mol<sup>-1</sup> and it decreased with increasing the concentrations of pyrimidine inhibitors. The decreased value of  $E_a^*$  when inhibitors are present is owing to their adsorption on the Cu surface. The chemisorption process<sup>37</sup> has this tendency. When  $\Delta H^*$  reaches a positive value, the corrosion process is endothermic, and it is classified as chemical adsorption. The activation entropy  $\Delta S^*$  is large and negative, showing that the creation of an activated complex in the transition state involves association rather than dissociation, and that there is a decrease in disorder as reactants transform into the activated complex <sup>38</sup>.

**Adsorption study.** Isotherms provide significant information for understanding the nature of the corrosion inhibition process. The best fit was found using the Langmuir isotherm, which created a linear relationship between  $\theta$  values and inhibitor concentration C. The Langmuir model asserts that the metal surface has a definite proportion of adsorption sites with one adsorbate, and the Gibbs free energy of adsorption for the sites is the same, regardless of the value of  $\theta$ . This adsorption isotherm is described by the following equation Eq. (5) <sup>39</sup>

$$\frac{C}{O} = \left(\frac{1}{\mathbf{K}_{\mathrm{ads}}}\right) + C \tag{5}$$

where  $K_{ads}$  is the equilibrium constant of adsorption process and C is the concentration of inhibitor and  $\theta$  is the fraction of surface coverage. The  $\Delta G^o ads$  of adsorption process was calculated from the following Eq. (6):

$$\mathbf{K}_{\mathrm{ads}} = \frac{1}{55}.5 \exp\left(\frac{-\Delta \mathrm{G}_{\mathrm{ads}}^{\circ}}{\mathrm{RT}}\right) \tag{6}$$

Table 4 displays that the  $\Delta G^o_{ads}$  attained slightly more negative values than -40 kJ mol<sup>-1</sup> and increases slightly by raising the temperature. This indicates that pyrimidine inhibitors may adsorbed physically or chemically on Cu surface, but the chemical adsorption is acceptable than the physical one <sup>40</sup>. Also, other important adsorption parameters were calculated such as the enthalpy ( $\Delta H^o_{ads}$ ) and the entropy ( $\Delta S^o_{ads}$ ) of adsorption by applying Van't Hoff (7) and thermodynamic general Eq. (8) <sup>34</sup>:

$$\ln \mathbf{K}_{\text{ads}} = \frac{-\Delta H^{\circ}}{RT} + \text{constant}$$
(7)

$$\Delta G^{\circ}_{ads} = \Delta H^{\circ}_{ads} - T \Delta S^{\circ}_{ads} \tag{8}$$

Table 5 reveals that positive values of  $\Delta H^o_{ads}$  indicate that pyrimidine derivative adsorption is an endothermic process<sup>41</sup>, implying that the inhibition efficiency increases as the temperature rises. This behavior can be explained by the fact that as the temperature rose, inhibitor molecules adhered to the metal surface<sup>42</sup>. In the presence of pyrimidine derivatives, the value of  $\Delta S^o_{ads}$  is positive because the endothermic adsorption process is always accompanied by a rise in entropy. The adsorption of inhibitor onto the Cu surface was propelled by an

Inhibitor	Temp °C	$-\Delta G^{\circ}_{ads}$ kJ mol <sup>-1</sup>	$\Delta H^{\circ}_{ads} \mathrm{kJ} \mathrm{mol}^{-1}$	$\Delta S^{\circ}_{ads}$ J mol <sup>-1</sup> K <sup>-1</sup>
MA-978C	25	$40.79 \pm 0.2028$		35.89±0.2333
	30	$42.25 \pm 0.1453$		37.92±0.2028
	35	$42.91 \pm 0.1741$	70.77±0.1413	36.31±0.1453
	40	$44.14 \pm 0.1732$		37.92±0.1732
	45	$45.10 \pm 0.2025$		38.00±0.2128
	25	$40.11 \pm 0.1000$		30.37±0.1453
	30	$41.19 \pm 0.1453$		$30.22 \pm 0.1764$
MA-975	35	$42.57 \pm 0.1732$	$50.4 \pm 0.1673$	$301.8 \pm 0.1453$
	40	$42.23 \pm 0.1453$		$30.23 \pm 0.1732$
	45	$43.03 \pm 0.1732$		$30.32 \pm 0.2028$





**Figure 5.** Langmuir diagrams for Cu dissolution in the 1 M HNO<sub>3</sub> solution of pyrimidine derivatives (MA-978C, MA-975).

increase in entropy.<sup>44</sup>. Figure 5 shows Langmuir isotherm plots for the corrosion of Cu in the 1 M  $HNO_3$  with optimum concentrations of the investigated inhibitors.

Electrochemical impedance spectroscopy (EIS) measurements. The corrosion manners of copper alloy in 1 M HNO<sub>3</sub> solution absence and presence of various doses of investigated pyrimidine was studied at  $25 \pm 1$  °C. The impedance plots including the Nyquist (a) and Bode (b) are presented in Figs. 6 and 7. In the presence of inhibitor, the Nyquist diagram shows two-time constants: the capacitive loop at high frequencies and a straight line perceived as Warburg impedance at low frequencies. The charge transfer process can be related to higher frequency capacitive loops. Surface layer resistance, surface layer capacity, and the Warburg element, which signals a diffusion process across the surface layer, make up the second time constant in the low frequency range. With the addition of MA-978C and MA-975 to the Bode plots recorded in the presence of inhibitor, the Bode amplitude values over the entire frequency range increase. As further inspection in Fig. 7 in most cases of copper alloy corrosion in acid solution, the obtained Nyquist impedance diagrams in most cases does not show perfect semicircle, and this is arising from the frequency dispersion due to the roughness and heterogeneity of the electrode surface<sup>42,43</sup>. From EIS measurements, the impedance diagram is presented as a large capacitive loop with low frequencies dispersion<sup>44</sup>. The EIS spectra were analyzed by assuming CPE circuit and modeling the impedance data with the simplest equivalent electrical circuit (Fig. 8). In this equivalent circuit, the solution resistance  $R_s$  and the double layer capacitance  $C_{dl}$  are considered in parallel to the charge transfer resistance  $Rct^{45}$ . The standard criteria for evaluation of pyrimidine derivatives best-fit were followed: The chi-square error was low (< 10<sup>-3</sup>) and the acceptable errors of elements in fitting (5%). In inhibited solution of 1.0 M HNO<sub>3</sub> with various concentrations of inhibitors, the impedance diagrams follow the same pattern (one capacitive loop), however, the diameter of this capacitive loop increases with increasing concentration<sup>46</sup>. "n" is the CPE parameter which characterizes the deviation of the system from ideal capacitive behavior. The values *n* is between -1 and 1. For a perfect resistor, n = 0 and for an inductor n = -1 for solutions contain pyrimidine are higher than those obtained for pyrimidine free solution which reflects their inhibitive action for copper alloy dissolution process. The (n)value is a measure of a surface's roughness, and its rise in this study could indicate a drop in the heterogeneity of the working electrode surface due to inhibitor molecule adsorption and increases with inhibitor concentra-



**Figure 6.** Nyquist bends for dissolution of copper metal in 1.0 M HNO<sub>3</sub> attendance and nonattendance different concentrations of (**a**) MA-1978C, (**b**) MA-975 at 25 °C.



**Figure 7.** Bode bends for dissolution of copper metal in 1.0 M HNO<sub>3</sub> attendance and nonattendance different concentrations of (**a**) MA-978C (**b**) MA-975 at 25 °C.



Figure 8. Equivalent circuit model for measuring EIS data.

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Inh	Conc., µM	Rs, $(\Omega \text{ cm}^2)$	$Y^{o}$ ( $\mu\Omega^{-1}$ s <sup>n</sup> cm <sup>-2</sup> )	n	$C_{\rm dl,}$ ( $\mu {\rm F} {\rm ~cm}^{-2}$ )	$R_{\rm ct,} (\Omega \ {\rm cm}^2)$	$\%\eta_{EIS}$	X <sup>2</sup>
blank	-	1.839	576.2	0.963	$316.2 \pm 0.2333$	$68.2 \pm 0.1453$	-	0.000087
	5	1.914	451.7	0.972	$205.7 \pm 0.1453$	$113.7 \pm 0.1764$	40.1	0.000341
	9	2.175	397.3	0.975	$182.3 \pm 0.1732$	$149.4 \pm 0.2028$	54.4	0.000653
MA-978C	13	2.372	351.4	0.977	$139.1 \pm 0.1453$	$208.2 \pm 0.2309$	67.3	0.000453
	17	2.486	312.5	0.978	$107.4 \pm 0.2333$	$327.9 \pm 0.1732$	79.2	0.000654
	21	2.591	268.1	0.980	$72.6 \pm 0.1453$	$614.2 \pm 0.1732$	88.9	0.000745
	5	1.758	439.1	0.914	$197.2 \pm 0.1202$	$120.6 \pm 0.2028$	43.5	0.000065
	9	1.831	392.4	0.969	$174.6 \pm 0.2309$	$156.1 \pm 0.1732$	56.3	0.000451
MA-975	13	1.905	345.2	0.982	$132.5 \pm 0.2028$	$213.9 \pm 0.1453$	68.1	0.000123
	17	1.938	306.3	0.985	$98.1 \pm 0.1732$	$374.2 \pm 0.2028$	81.8	0.000231
	21	2.106	262.5	0.987	$67.3 \pm 0.1553$	685.8±0.2309	90.1	0.000129

**Table 6.** Impedance parameters for copper alloy in 1 M HNO<sub>3</sub> in presence and absence different concentrations of pyrimidine derivatives at 25 °C.

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tion, while the reverse is the case with  $Y_o$ . The EIS parameters such as  $R_{cp} R_{sp} C_{db}$  and  $\theta$  and  $\% E_{EIS}$  were listed in Table 6, from which we can conclude that<sup>47</sup>,  $R_{ct}$  increases and  $Y^o$  decreases when the concentration of pyrimidine inhibitors increased and hence, the  $\% E_{EIS}$  increases. This is due to the increased thickness of the double layer or a reduced dielectric constant. The decreased  $Y^o$  values recommended the decreased thickness of the oxide layer in the presence of inhibitors. The lowering in  $C_{db}$  might be caused by a decrease in local dielectric constant and/ or an increase in the thickness of the electrical double layer, indicates that the inhibitor molecules have adsorb at the metal/solution interface<sup>48</sup>. The increase of  $R_s$  with inhibitor concentration proofs the increase of the thickness of double layer. Also, single charge transfer process occurred during dissolution of copper alloy in 1.0 M HNO<sub>3</sub> which does not change in the presence of investigated pyrimidine. This is indicated from the presence of single semicircle loop <sup>49</sup>. The impedance of the CPE represented by the next Eq. (9):

$$Z_{CPE} = 1/Y^0 (j\omega)^n \tag{9}$$

 $Y^{o}$  is referred to CPE constant, j is referring to the imaginary root,  $\omega$  is refer to the angular frequency, n (-1 < n < 1) stands for the deviation index.

The  $C_{dl}$  value was obtained from this eq. (10)<sup>50</sup>.

$$C_{dl} = \frac{1}{2\pi f_{\max} R_{ct}} \tag{10}$$

The corrosion  $\%\eta$  was calculated by using the Eq. (11):

$$\%\eta_{EIS} = \left(\frac{R_{ct} - R_{ct}^*}{R_{ct}}\right) \times 100 \tag{11}$$

where  $R_{ct}^{o}$  and  $R_{ct}$  are the resistance of the charge transfer in the absence and presence of the tested compounds respectively.

*Open circuit potential* ( $E_{OC}$ ). Figure 9 shows the  $E_{OC}$  fluctuation with time for copper in an acid corrosive media with no dose of organic component ( $21 \times 10^{-6}$ ) present. Figure 9 shows that after 100 s, the blank solution stabilizes at a value of -7 mV/SCE. Cu oxidizes, resulting in the formation of corrosive products on its surface. As a result, when an organic compound is present at a dose of  $21 \times 10^{-6}$  M, the potential changes quickly and remains stable over time. The resistance of Cu dissolving in the acid corrosive media is indicated by the initial shifts in  $E_{OC}$  while adding concentrations of organic substance. The disintegration of the oxide coating and the formation of a protective film on the Cu surface can explain this phenomenon.

Potentiodynamic polarization (PP) measurements. Tafel polarization curves of copper alloy in uninhibited and inhibited 1 M HNO<sub>3</sub> solution with different concentrations of pyrimidine derivatives at 25°Care illustrated in Fig. 10. Cu exposed to an uncontrolled system corroded severely; this is due to the aggressive NO<sup>-3</sup> ions, which drive strong Cu dissolution. Fortunately, the addition of pyrimidine analogues to a solution minimized Cu oxidation due to considerable reductions in  $i_{corr}$ . The variation of PP parameters with the concentration of pyrimidine compounds are given in Table 7. The PP indicates that, the behavior of pyrimidine derivatives is of Tafel-type because the addition of pyrimidine compounds increases the cathodic and anodic potential with a displacement to more negative and positive values, respectively. The corrosion current density ( $i_{corr}$ ) drops as the concentration of pyrimidine increases, indicating that the presence of these compounds slows Cu dissolution and that the degree of inhibition is proportional to the concentration. The order of additives is MA – 975 > MA – 978C. The maximum difference in  $E_{corr}$  values between the inhibited and uninhibited systems was less than 39 mV, indicating that the investigated pyrimidine derivatives are mixed type inhibitors that affect both the cathodic and



**Figure 9.**  $E_{OC}$  versus time at 25 °C for Cu in the acid corrosive medium in the absence and attendance dose of organic compound ( $21 \times 10^{-6}$  M).



**Figure 10.** PP bends for copper alloy in the 1 M HNO<sub>3</sub> solution at altered dose of pyrimidine derivatives (**a**) MA-978C, (**b**) MA-975 at 25 °C.

anodic polarization curves<sup>51</sup>. Moreover, the cathodic and anodic polarization Tafel lines keep a similar pattern and slightly changed by adding the pyrimidine derivatives. In other words, the nature of the polarization curves remains approximately the same irrespective of different concentration of these derivatives addition to acid solution which suggests that the mechanism of Cu in nitric acid does not change by adding these derivatives to the acid solution. The inhibitive action of pyrimidine compounds is initiated by adsorption on the reactive sites on the electrode surface and blocking corrosion cells and reducing the exposed surface area available for attack from corrosion environment<sup>52</sup>. The  $E_p$ % was calculated next Eq. (12):

$$Ep\% = \left(\frac{i_{corr} - i'_{corr}}{i_{corr}}\right) \times 100$$
(12)

where  $i_{corr}$  and  $i_{corr}$  refer to the corrosion current of the copper metal presence and absence pyrimidine derivatives, respectively. The results showed that  $i_{corr}$  reduces with increasing concentration up to  $21 \times 10^{-6}$  M and then significantly decreases when the concentration of pyrimidine derivatives reaches  $25 \times 10^{-6}$  M. As a result, when the concentration of pyrimidine compounds was raised to  $21 \times 10^{-6}$  M, the inhibitory performance improved.

Conc, M×10 <sup>6</sup>	$-E_{\rm corr.}$ mV (vs.SCE)	$i_{\rm corr}$ , $\mu A  \rm cm^{-2}$	$\beta_a$ , mV dec <sup>-1</sup>	$-\beta_c$ , mV dec <sup>-1</sup>	θ	<i>E<sub>p</sub>%</i>	
Blank		$-7 \pm 0.1453$	$352.7 \pm .1732$	86.4±0.2309	$145.2 \pm 0.2028$	-	-
	5	$19.1 \pm 0.2028$	$209.3 \pm 0.2028$	$77.7 \pm 0.2028$	191.4±0.1453	0.407	40.7
	9	$-29.2 \pm 0.2431$	$168.1 \pm 0.1155$	$85.4 \pm 0.1732$	157.50.2028	0.523	52.3
MA-978C	13	$-43.4 \pm 0.2055$	$135.2 \pm 0.2603$	$72.8 \pm 0.2309$	179.1±0.2906	0.617	61.7
	17	$-2.5\pm0.1452$	$87.4 \pm 0.1764$	91.3±0.2333	190.1±0.1732	0.752	75.2
	21	$-13.2 \pm 0.1742$	42.1±0.2028	80.2±0.1202	204.6±0.2028	0.881	88.1
MA-975	5	$-18.8 \pm 0.2102$	$201.4 \pm 0.1732$	89.9±0.1732	$144.2 \pm 0.17638$	0.429	42.9
	9	$-1.1 \pm 0.2209$	$158.1 \pm 0.1453$	$137.6 \pm 0.1453$	148.6±0.2082	0.552	55.2
	13	$10.2 \pm 0.2010$	$121.7 \pm 0.1732$	$186.6 \pm 0.2027$	$155.4 \pm 0.1732$	0.655	65.5
	17	$-22.5 \pm 0.1753$	84.3±0.2028	72.1±0.2333	94.2±0.2082	0.761	76.1
	21	$19.1 \pm 0.1208$	35.7±0.2010	$124.1 \pm 0.1764$	$139.9 \pm 0.1764$	0.899	89.9

Table 7. PP measurements for copper alloy in 1 M  $HNO_3$  with and without altered concentrations of the tested pyrimidine derivatives at 25 °C.



Figure 11. SEM images of copper alloy without (blank) and with 21 µM of MA-978C, and MA-975 at 25 °C.

The addition of more pyrimidine derivatives than  $21 \times 10^{-6}$  M may lead to a slower kinetic at the adsorption sites, allowing the desorption of the adsorbed layer and hence lower inhibition efficiency.

**Surface analysis.** Scanning electron microscope (SEM) and energy dispersive X-ray (EDX) analysis.. The morphology of the copper metal surface was investigated using a scanning electron microscope, when copper samples were immersed in 1 M HNO<sub>3</sub> solution for 24 h with and without the tested pyrimidine derivatives<sup>53</sup>. The effect of these derivatives on the corroding copper metal surface is also analyzed by EDX with SEM images to investigate the pyrimidine derivatives adsorption by comparing the elements identified and detected on the copper metal surface with the elements in the pyrimidine derivatives molecular structure. Figures 11 and 12 show SEM and EDX images, respectively. According to EDX analysis, the copper surface is heavily damaged without the inhibited solution, where the images of inhibited copper surface indicated less corrosion in the presence of



Figure 12. EDX images of Cu alloy without (blank) and with 21  $\mu M$  of MA-978C, and MA-975 at 25 °C.

examined pyrimidine derivatives. Also, the percentage of iron in the copper surface immersed in inhibited solution is decreasing, while the percentage of the carbon and heteroatoms (S, O and N) is increasing<sup>54</sup>. From the SEM–EDX tests, we can conclude that the examined derivatives adsorbed on the copper metal surface show an excellent image for preventing severe corrosion of the metal surface<sup>55</sup>.

*Quantum calculations*. To determine whether there is a correlation between the molecular structures of investigated inhibitors and their inhibitory actions, quantum chemical simulations were conducted<sup>46</sup>. The synthesized MA-978C and MA-975 inhibitors' computed quantum chemical characteristics ( $E_{HOMO}$ ,  $E_{LUMO}$ , and  $\Delta E$ ) were determined and are displayed in Table 8. The  $E_{HOMO}$ ,  $E_{LUMO}$  represented a molecule's capacity for electron donation and acceptance. These values may be seen in Fig. 13 as well. The ability of the inhibitor to give electrons was stronger the higher the  $E_{HOMO}$  value, whereas the ability of the inhibitor to receive electrons was stronger the lower the  $E_{LUMO}$  value<sup>56</sup>. A molecule's ability to deliver electrons to a suitable acceptor with unoccupied molecular orbitals is indicated by high values of  $E_{HOMO}$ . The  $E_{LUMO}$ , on the other hand, demonstrates a molecule's capacity to accept electrons; lower values correspond to a higher electron-accepting capacity.

The energy to eliminate an electron from the last orbital occupied is called the gap in the energy band  $(\Delta E = E_{LUMO} - E_{HOMO})^{57}$ . Low  $\Delta E$  facilitates adsorption of the molecule and thus will cause higher inhibition efficiency, as  $\Delta E$  decreases, the reactivity of the molecule increases leading to increase the inhibition efficiency of the molecule. The dipolar moment ( $\mu$ ) is a measurement of the polarity of the covalent bond between the compounds under examination Eq. (13). The high  $\mu$  values are thought to improve the adsorption tendency of the compounds examined on metal surfaces. According to theoretical calculations, the band gap energy values  $\Delta E$  for MA-975 is less than MA-978C, so the inhibition efficiency is supposed to be in the order MA-975 > MA-978C. This reflects a greater correlation between corrosion IE and this result<sup>58</sup>. The inhibitor (MA-975) has the lowest total energy, which suggests that its adsorption is higher with the highest softness, as shown in all the data

Compound	MA-978C	MA-975
$E_{HOMO}$ , eV	-9.43	- 8.92
$E_{LUMO}$ , eV	-1.24	- 1.01
$\Delta E$ , eV	8.190	7.910
$I_{P}$ , eV	9.43	8.92
$E_A$ , eV	1.24	1.01
η , eV	4.095	3.955
$\sigma$ , eV	0.244	0.253
$\mu$ , eV	5.335	4.965
Dipole moment (Debye)	2.930	3.220

Table 8. The calculated quantum chemical parameters for the investigated pyrimidine compounds.



**Figure 13.** Molecular structure of the pyrimidine compound, and its frontier molecular orbital density distribution (HOMO and LUMO).

in Fig. 13 and Table 8. In addition, the dipole moment is the parameter most used to describe the polarity of a molecule. It is clearly proved in the literature that molecules with high dipole moments are more reactive and hence, MA-975 > MA-978C<sup>59</sup>. Chemical properties that are important for determining molecular stability and reactivity include chemical hardness ( $\eta$ ) (Eq. 15), which evaluates an atom's resistance to charge transfer, and softness ( $\sigma$ ) (Eq. 16), which defines an atom or group of atoms' ability to accept electrons. From the results, as the chemical reactivity increases, the percent IE of adsorption increases, and the molecule with the lowest hardness value should have the highest inhibitory efficiency<sup>60</sup>. Because of the increase in softness ( $\sigma$ =0.253, 0.224 eV-1 for MA-975, MA-978C, respectively) and reduction in hardness (( $\eta$ ) = 4.095, 3.955 eV, for MA-975C, MA-978, respectively), the CBIPM inhibitor has high chemical reactivity with the metallic surface. The following equations were used to calculate the global hardness ( $\eta$ ), softness ( $\sigma$ ), and chemical potential ( $\mu$ ) in terms of IP and EA <sup>61</sup>:

$$\mu = -\chi = -\frac{I_p + E_A}{2} \tag{13}$$

$$\chi = \frac{I_p + E_A}{2} \tag{14}$$

$$\eta = \frac{I_{P-}E_A}{2} \tag{15}$$



**Figure 14.** Equilibrium adsorption configurations of the inhibitors molecules on the Cu (111) surface: inhibitors side view and top view.

Structures		Adsorption energy	Rigid adsorption energy	Deformation energy	Compound dE <sub>ad</sub> /dNi	H <sub>3</sub> O <sup>+</sup> dE <sub>ad</sub> /dNi	H <sub>2</sub> O dE <sub>ad</sub> /dNi
Noutral	Cu (111)/C <sub>23</sub> H <sub>25</sub> N <sub>5</sub> O <sub>6</sub> )	- 4095.203	-4027.378	-67.825	-272.939	- 259.03	-11.271
incuttai	Cu (111)/C <sub>16</sub> H <sub>15</sub> ClN <sub>6</sub> O <sub>3</sub> )	- 4090.983	-4022.109	-68.874	-283.114	- 261.79	-7.387
Protonated	Cu (111)/C <sub>23</sub> H <sub>25</sub> N <sub>5</sub> O <sub>6</sub> H <sup>+</sup>	- 4163.765	-4083.24	-80.525	-281.869	-262.64	- 12.361
	Cu (111)/C <sub>16</sub> H <sub>15</sub> ClN <sub>6</sub> O <sub>3</sub> H <sup>+</sup> )	-4156.544	-4074.97	-81.574	-293.044	- 265.28	- 9.478

Table 9. Equilibrium adsorption configurations of the inhibitors molecules on the Cu (111) surface.



**Figure 15.** Mechanism of corrosion protection of Cu dipped in 1 M HNO<sub>3</sub> media using MA-975, and MA-978C.

 $\sigma = \frac{1}{\eta} \tag{16}$ 

The results show that the hetero atoms (N, S, and O) in the structure of compounds have a significant impact on quantum chemical parameters. This theoretically illustrates that the hetero atom (S) influences the adsorption of inhibitor chemicals on metal. We performed a molecular dynamics simulation on the inhibitors' adsorption on the copper surface.

Monte Carlo (MC) simulation. MC is an excellent technique for determining the most stable adsorption conformations of substituted pyrimidine derivatives in 1 M HNO<sub>3</sub>. Figure 14 shows the equilibrium adsorption configurations of the inhibitors molecules on the Cu (111) surface: inhibitors side view and top view. Different parameters derived from the Monte Carlo simulation shown in Table 9. The parameters contain total energy of the substrate-adsorbate outline. The sum of the rigid energy and the deformation energy is called to be the adsorption energy. In this study, the substrate energy is considered as zero. In addition, the energy of the adsorption in reports energy liberated when the relaxed adsorbate component is adsorbed on the substrate. The energy of the rigid adsorption reports the energy, liberated when the unrelaxed adsorbate components are adsorbed on the substrate, meaning that before the geometry optimization step. The deformation energy reports the energy, liberated when the adsorbed adsorbate constituents are relaxed on the substrate surface<sup>6</sup> Table 9 shows also  $(dE_{ads}/dNi)$ , which reports the energy, of substrate-adsorbate configurations where one of the adsorbate components has been eliminated. As shown in Table 9, MA-975 and MA-978C Inhibitors gave high adsorption energy in negative value found during the simulation process. Furthermore, the protonated form of  $C_{23}H_{25}N_5O_6H^+$  and  $C_{16}H_{15}ClN_6O_3H^+$  molecules in corrosive solution have a higher negative adsorption energy than the neutral form, indicating that the protonated form of  $C_{23}H_{25}N_5O_6H^+$  and  $C_{16}H_{15}ClN_6O_3H^+$  molecules in corrosive solution has a positive impact on the corrosion protection process. Superior inhibition efficiency is typically correlated with high binding energy (E<sub>binding</sub>) between the inhibitor and alloy<sup>63</sup>. Inhibitor molecule equilibrium adsorption configurations on the Cu (111) surface for neutral and protonated side views and top views are shown in Fig. 14. (MA-975>MA-978C) is the order of the manufactured inhibitors based on IE percent. It is obvious that both inhibitor molecules, in their various forms, adhere to the surface of Cu (111) in a nearly parallel pattern, covering the Cu alloy's maximum surface area. This behavior is primarily attributed to two inhibitor compounds' strong propensity to donate electrons to the vacant Cu orbitals and to accept electrons from copper's d-orbitals via a back-bonding<sup>64</sup>.

*Mechanism of corrosion inhibition.* Physicochemical characteristics and the Cu charge may be utilized to illustrate adsorption based on the experimental study and theoretical calculations. Figure 15 depicts the inhibitory action of these pyrimidine derivatives on the surface of copper. Several studies have been revealed that the Cu surface in HNO<sub>3</sub> solution is positively charged<sup>65</sup>. The presence of function groups capable of securely attaching

the inhibitor molecules on the metal surface explains the inhibitor's propensity for being adsorbed on the metal surface. When the inhibitor concentration is raised, the formation of a protective coating of inhibitor molecules at the metal/solution interface improves inhibition effectiveness. The charge that is positive Cu surfaces encourage NO<sup>3-</sup> adsorption, resulting in a negative charge surface that makes it simpler to adsorb cations in solution. These organic pyrimidine derivatives can be protonated in solution due to the unshared electron pairs of the N, O, and S electrons. Because of electrostatic interaction the protonated molecules were physisorbed on the metal surface. Meanwhile, as shown in Fig. 15, further adsorption of these inhibitors can be accomplished by forming covalent interactions (chemisorption). Based on quantum chemical measurements of both WL and electrochemical values, the percent IE of the two investigated pyrimidine derivatives is as follows: MA-975 > MA-978C. This is due to the following factors: MA-975 has a larger molecular size than MA-978C, allowing it to cover a larger area from the surface; MA-975 has 5 N and 6O atoms, but MA-978C contains 6 N, 3O, and one Cl, which is a withdrawing group, reducing the electron density on the molecule.

# Conclusion

- (1) The study revealed that the investigated pyrimidine derivatives were utilized as highly, safe efficient inhibitors for copper in 1 M HNO<sub>3</sub>.
- (2) The adsorption of the investigated inhibitors on copper surface follows the Langmuir adsorption isotherm. The development of a protective layer on the copper surface was confirmed using SEM and EDX analyses.
- (3) Tafel curves indicated that pyrimidine derivatives acted as a mixed-type corrosion inhibitor and provided superior inhibition performance for Cu corrosion in  $HNO_3$  medium at different temperatures, which was further confirmed by EIS method. The obtained IE values from EIS increased with increasing pyrimidine derivatives concentration which agreed well with those obtained from Tafel method.
- (4) The charge transfer resistance increases while the capacitance double layer drops by raising the inhibitor dosage which may be attributed to the adsorption of inhibitor molecules on the copper surface.
- (5) The high and low E<sub>binding</sub> values indicated substantial pyrimidine derivative adsorption on copper surface. The pyrimidine derivatives' excellent capacity to donate and absorb electrons to/from copper was validated by the flat adsorption orientation of the compounds, creating an anchoring barrier to stop copper from corroding.
- (6) The obtained results of chemical, electrochemical and theoretical studies are in good agreement.

#### Data availability

Authors can confirm that all relevant data are included in the article.

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# Author contributions

A.El-A.S.F., M.A.I., M.A.K., A.A.El-H., wrote the main manuscript text. M.A.K. prepared figures, A.A.El-H. calculate the quantum part, A.El-A.S.F., M.A.I. reviewed the manuscript.

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# **Competing interests**

The authors declare no competing interests.

# Additional information

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