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# Impact of solvents on doctor blade coatings and bathocuproine cathode interlayer for large-area organic solar cell modules

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#### ABSTRACT

Efforts to commercialize organic solar cells (OSCs) by developing roll-to-roll compatible modules have encountered challenges in optimizing printing processes to attain laboratory-level performance in fully printable OSC architectures. In this study, we present efficient OSC modules fabricated solely through printing methods. We systematically evaluated the impact of processing solvents on the morphology of crucial layers, such as the hole transport, photoactive, and electron transport layers, applied using the doctor blade coating method, with a particular focus on processability. Notably, deposition of charge transport layer using printing techniques is still a challenging task, mainly due to the hydrophobic characteristic of the organic photoactive layer. To overcome this issue, we investigated the solvent effect of a well-studied cathode interlayer, bathocuproine (BCP). We were able to form a uniform thin BCP film ( $\sim 10$  nm) on a non-fullerene based organic photoactive layer using the doctor bladed coating method. Our results showed that the use of volatile alcohols in the BCP processing required a delicate balance between wettability and vaporization, which contrasted with the results for spin-coated films. These findings provide important insights into improving the efficiency of printing techniques for depositing charge transport layers. The fully printed OSC modules, featuring uniform and continuous BCP layer formation, achieved an impressive power conversion efficiency of 10.8% with a total area of 10.0 cm<sup>2</sup> and a geometrical fill factor of 86.5%.

# 1. Introduction

Organic solar cells (OSCs) made from small molecules and polymers have gained attention as a promising source of renewable energy due to their low cost, lightweight, flexibility, and transparency, making them suitable for portable, wearable, and building-integrated photovoltaic applications [1–5]. Over the past few decades, researchers have made significant advancements in the development of OSCs, focusing on increasing their power conversion efficiency (PCE). These advancements include improved device structures, interfacial layers, organic photoactive materials, and other techniques, leading to a certified PCE of 18.2% in 2021 [6–10].

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Recently, researchers have shifted their focus to developing printed OSCs using techniques such as doctor blade coating, slot-die coating, and screen printing [11–14]. These methods are considered a step closer to large-scale production [15–21], and pioneers like Krebs and his team have explored scalable printing technologies for large-area OSCs and flexible devices using full roll-to-roll processing [22–25]. Furthermore, advancements in module structures and laser scribing pattern techniques have increased the photoactive area to total area ratio and resulted in higher module PCEs [26–28].

Despite the significant progress made in printed organic solar cells (OSCs), their reported efficiencies and performance are still lower than those of spin-coated small-area counterparts. Previous studies have mainly focused on synthesizing new photoactive materials and using time-consuming and labor-intensive testing procedures to achieve optimal device performance through spin coating. In comparison to the conventional spin coating method, where the solution is dropped onto the substrate's center and rapidly rotated to form a uniform solid film through centrifugal force, the printing method has been considered challenging for fabricating uniform films and efficient devices due to its complex coating mechanism. The printing process relies on the fluid dynamics of the meniscus, which involves the wettability and adsorption of the solution on the substrate. Therefore, controlling shear stress and substrate temperature can promote the formation of uniform and crystalline films during the relatively slow evaporation of the solution [29–32]. Although methods such as hot substrate coating, hot slot-die coating, and bilayer blade coating have shown promise, there is still limited research on the use of widely applicable high-throughput methods for fabricating large-area OSC modules [33–35]. Furthermore, despite advancements in the development of organic electron transport layers (ETLs) between the photoactive layer and top electrode, such as conjugated polyelectrolytes and small molecules, the successful printing of these interfacial layers onto hydrophobic non-fullerene-based photoactive layers has not been demonstrated [36–43]. Therefore, it is crucial to urgently demonstrate a printable OSC module prototype compatible with continuous roll-to-roll processing to facilitate the transition from laboratory to industrial scales.

In this study, we successfully prepared printed OSC modules with high power conversion efficiencies (PCEs) of 14.0% and 10.8% for active areas of 1  $\text{cm}^2$  and total areas of 10  $\text{cm}^2$ , respectively, with a geometrical fill factor of 86.5%. By investigating the relationship between printing process conditions and organic thin film morphology, we developed protocols for fabricating well-structured OSC modules using the doctor blade printing process, and analyzed the distinct effects of spin coating and meniscus processing on film morphology. Achieving a balance between wettability and solution evaporation was identified as a crucial factor in obtaining uniform surface morphology through meniscus-guided thin-film deposition. These findings indicate that efficient and scalable OSC modules can be fabricated by employing an appropriate solvent system and optimizing printing conditions.

# 2. Experimental procedures

# 2.1. Materials

Poly (3,4-ethylenedioxythiophene) polystyrene sulfonate (PEDOT:PSS), specifically Clevios P VP AI4083 from Heraeus, was diluted with isopropyl alcohol (IPA) obtained from Sigma Aldrich. The dilution was performed at volume ratios of 1:0, 1:1, and 1:2. PM6 and Y6 were purchased from 1-Material (Nano Clean Tech) and dissolved in chloroform (Sigma Aldrich) at a concentration of 12 mg/ml, using a 1:1 ratio. To this solution,  $PC_{70}BM$  additives purchased from Nano-C were added, resulting in a concentration of 14 mg/ml. Subsequently, the photoactive solution stored at room temperature was divided into two variants, one with 0.5 vol% of 1-chloronaphthalene (CN) and one without. Bathocuproine (BCP) obtained from Sigma Aldrich was diluted to concentrations of 0.7 and 1.5 mg/ml in methanol, 1-butanol, and isopropyl alcohol (IPA) for thin and thick BCP layers. To prepare the ZnO solution, zinc acetate dihydrate and ethanolamine were dissolved in IPA and stirred for 12 h. The PTB7-Th:PC<sub>70</sub>BM solution was created by mixing PTB7-Th with  $PC_{70}BM$  at a ratio of 1:1.8 in chlorobenzene (Sigma Aldrich). Additionally, 3 vol% of 1,8-diiodooctane (Sigma Aldrich) was included to achieve a desirable concentration (13 mg/ml). Finally, the precursor solution to form MoO<sub>3</sub> was made by dissolving 5 mg of molybdenum dioxide bis(acetylacetonate) in 1 ml of a mixture of 1-butanol and cosolvent (methanol:1-butanol = 0.2:0.8).

# 2.2. Device fabrication

The Indium tin oxide (ITO)-coated glass substrates underwent a cleaning process using detergent and were subsequently ultrasonicated in deionized water, acetone, and isopropanol for 15 min each. For the fabrication of small-area normal structured OSCs, a PEPOT:PSS solution was spin-coated onto the substrates at 5000 rpm for 40 s and annealed at 150 °C for 20 min. The photoactive layer (PM6:Y6:PC<sub>70</sub>BM) was then deposited by spin coating the solution at 1200 rpm for 40 s. The BCP solutions were applied by spin coating at 5000 rpm for 20 s. In the case of large-area normal structured OSCs and OSC modules, a PEDOT:PSS solution (AI 4083 diluted in IPA) was applied using a coating blade and annealed at 150 °C for 20 min. Subsequently, the photoactive layer (PM6:Y6:PC<sub>70</sub>BM) was deposited using the doctor blade at a coating speed of 10 mm/s. The BCP solutions were also applied using the doctor blade, with the coating speed ranging from 10 mm/s to 50 mm/s. For the fabrication of large-area inverted structured OSCs, the ZnO solution was applied using a coating blade and conducted thermal treatments. The PTB7-Th:PC<sub>70</sub>BM and MoO<sub>3</sub> solutions were sequentially deposited using a coating blade. Finally, silver (Ag) was deposited onto each device through a vacuum evaporation technique conducted under vacuum condition of  $1 \times 10^{-6}$  torr.

#### 2.3. Characterization

The current density-voltage (*J-V*) characteristics of devices were measured using an Iviumsoft under AM1.5 illumination (100 mW/ cm<sup>2</sup>) with an Abet Technologies Sun 3000 under normal atmospheric conditions. The light intensity from the xenon (Xe) lamp in the solar simulator was calibrated using a National Renewable Energy Laboratory (NREL)-calibrated KG5 filtered silicon reference cell. The incident photon to current (IPCE) spectra were measured using an IPCE measurement system from PV measurements, Inc. Topographic atomic force microscopy (AFM) images were obtained using a Park System with an XE-100 microscope. For the cross-sectional images of the OSC module, transmission electron microscopy (TEM) was employed. To prepare the samples for imaging, they were first coated with sputtered carbon and platinum and then subjected to an in situ focused ion beam (FIB) process. The imaging of the samples was conducted using an FE-TEM (Tecnai F-30 S-Twin) operating at 300 kV in bright-field (BF) TEM mode.

# 3. Results and discussion

In our experiment, we utilized the doctor blade coating method, which is the most commonly used printing equipment, to prepare printed layers of organic solar cells (OSCs). The doctor blade coating method is a noncontact printing technique that involves injecting a solution between the blade and the substrate to form a meniscus. In contrast, the spin coating method applies centrifugal force. In the doctor blade process, the film forms naturally and relies on the adhesion between the bottom layer of the solution and the substrate (Fig. S1). The resulting film thickness can be theoretically derived by the concentration of the solution, the size of the gap between the blade and substrate, and the coating speed. Precise control of these parameters is essential to achieve the optimal thickness and desired surface quality with minimal morphological defects, which are crucial factors for obtaining high-performance printed OSCs. Our previous studies have shown that film morphology can be influenced by solution properties such as viscosity, boiling point, and surface energy. Hence, in this study, we focused on investigating the effect of the solvent on the doctor blade-coated photoactive layer, particularly the electron transport layer (ETL), to develop highly efficient large-area OSC modules.

OSCs typically exhibit two representative device structures: a normal type with the structure of ITO/HTL/photoactive layer/ETL/ electrode, and an inverted type with the structure of ITO/ETL/photoactive layer/HTL/electrode. While both normal and inverted structures have demonstrated high efficiencies in spin-coated OSCs, most printed OSCs have been demonstrated with inverted structures due to the desirable processability of HTLs, such as molybdenum oxides, onto the hydrophobic photoactive layer through thermal evaporation. To enable the preparation of OSCs solely through printing methods, it is crucial to develop multiple layers that can be coated using printing techniques. In our case, we selected OSCs with a normal structure and without any vacuum-evaporated charge transport layers. Fig. 1a-e illustrates the doctor blade coating process for three layers (excluding the electrodes) in OSCs with a normal structure, an energy level diagram of the corresponding materials in the devices, and the molecular structures of the photoactive materials.

In the first layer, we employed the commonly used hole transport material PEDOT:PSS, which was coated to achieve the best thickness and uniformity in large-area devices. Pristine PEDOT:PSS (AI 4083) exhibited poor wetting on ITO/glass substrates and resulted in a thick film (~100 nm) when applied at the optimal doctor blade coating speed of 10 mm/s. To improve wettability and achieve the desired thickness (~35 nm), pristine PEDOT:PSS was diluted with an ambipolar solvent, IPA. Optical microscope (OM) images demonstrated that the diluted PEDOT:PSS solution was uniformly coated on the ITO/glass substrate using the doctor blade



Fig. 1. (a) Schematic illustration of the doctor blade coating process for normal-structured OSCs. (b) Energy level diagram of the corresponding materials in devices. The molecular structures of (c) PM6, (d) Y6, and (e) PC<sub>70</sub>BM.

#### coating method (Fig. S2).

In the preparation of spin-coated small-area organic solar cells (OSCs), a tiny volume of a high boiling point solvent, known as a solvent additive, has been used in photoactive solutions to improve the power conversion efficiency (PCE) by 0.5%–1% [9–11]. The commonly employed solvent additives are 1,8-diiodooctane (DIO) and 1-chloronaphthalene (1-CN), which have high boiling points of 332.5 °C and 263 °C at 760 mm Hg, respectively [9–11,44,45]. While DIO has a higher boiling point and lower vapor pressure (0.0375 Pa at 25 °C) compared to 1-CN, it can oxidize in the presence of air and act as a photoacid under UV irradiation, leading to degradation of device performance. To mitigate this issue, the photoactive layers were formed using a blade coating process with the addition of 1-CN in PM6:Y6-based photoactive materials.

In terms of the spin coating method, the inclusion of 1-CN improved the morphology of the photoactive layer and resulted in slightly better phase separation, as depicted in Fig. 2a, e and (b, f), as well as Fig. S3. However, the doctor-blade-coated photoactive layer with 1-CN additive exhibited poor morphology, which had a negative impact on device performance, as shown in Fig. 2c, g and (d, h), and Fig. S4. The bulk heterojunction morphology consisted of separated donor and acceptor materials that collapsed because of the high boiling point of 1-CN, causing the doctor blade-coated photoactive layer to form under wet film conditions. This allowed sufficient time for the formation of segregated morphology. Additionally, we attempted to observe clear domains of donor and acceptor phase separation using high-resolution transmission electron microscopy (TEM). Although the TEM images did not clearly show the donor and acceptor-rich domains, they exhibited similar tendencies to the atomic force microscopy (AFM) images (Fig. S5). The natural evaporation of the solvent during the doctor blade coating process eventually acted as an additive during the spin coating, as it slowed down the rapid solvent evaporation and provided ample time for the formation of an ideal solid film. Consequently, the development of printed OSCs was carried out using a solvent additive-free photoactive layer coating.

In conventional structured OSCs, the deposition of the charge transport layer using printing techniques remains a challenge due to the hydrophobic nature of the organic photoactive layer. To address this issue, we conducted an investigation on the influence of solvents in the doctor blade coating process for a bathocuproine (BCP) organic electron transport layer (ETL), aiming to achieve a uniform thin film ( $\sim$ 10 nm) on a nonfullerene-based organic photoactive layer. The ETL materials were dissolved in various alcohol solvents such as methanol, ethanol, 1-butanol, and IPA. These alcohol solvents possess different properties such as viscosity, surface tension, and boiling point, which directly impact the film formation on the photoactive layer.

In this study, we specifically selected three solvents: methanol (boiling point  $\approx$  65 °C), 1-butanol (boiling point  $\approx$  117 °C), and IPA (boiling point  $\approx$  82.6 °C), each possessing distinct boiling points and wettability characteristics. Methanol is commonly used for dissolving organic ETL materials due to its favorable volatility, solubility, and compatibility with the photoactive layer [40–43]. However, as depicted in Fig. 3 (a, d), the rapid evaporation of methanol is unsuitable for coating an approximately 10 nm thin film onto the organic photoactive layer based on a blade coating process. Similar to 1-butanol and IPA, the surface energy of methanol (22.7 mN/m) closely matches that of the organic photoactive layer, thereby preventing droplet formation on the substrate. At the nanometer scale, methanol evaporates before the BCP layer can fully form, resulting in circular marks on the surface of the photoactive layer. Optical microscopy (OM) images illustrate the non-uniformity of BCP film formation when employing methanol-based doctor blade coating (Fig. S6).

Fig. 3 (b, e) and (c, f) demonstrate that there is no significant difference between 1-butanol and IPA; however, a wave pattern is consistently observed when using 1-butanol in our experiments. This pattern was faintly visible under OM when BCP was coated with the high-throughput (50 mm/s) doctor blade coating process, as shown in Fig. S7. Despite 1-butanol having a slightly higher surface energy (25.0 mN/m) compared to IPA (23.3 mN/m), its excessively high boiling point causes the wet BCP film to remain on the surface



**Fig. 2.** AFM height (a–d) and phase (e–h) images of spin coated PM6:Y6:PC<sub>70</sub>BM films (a, e) without and (b, f) with CN additive, and doctor blade coated PM6:Y6:PC<sub>70</sub>BM films (c, g) without and (d, f) with CN additive.



Fig. 3. (a) SEM images of the spin-coated BCP film with (a) methanol, (b) 1-butanol, and (c) IPA. SEM images of the doctor blade-coated BCP film with (d) ethanol, (e) 1-butanol, and (f) IPA.

of the photoactive layer for an extended period, resulting in an uneven film formation.

The *J*-V characteristics of the spin-coated small-area and blade-coated large-area OSCs exhibited similar trends as observed in the SEM and OM images (Fig. 4a-d, and Tables 1 and 2). Due to the centrifugal forces during spin coating, the BCP ETL was uniformly coated, regardless of the solvent used. Consequently, all devices with an active area of 4.64 mm<sup>2</sup> showed a similar PCE of approximately 15%. However, for doctor blade-coated devices with a larger active area of 1 cm<sup>2</sup>, methanol was not suitable for BCP ETL coatings on organic photoactive layers. The use of methanol leaded to reduced open circuit voltage ( $V_{oc}$ ) of 0.79 V and a fill factor (FF) value of 0.51, resulting in a relatively low PCE of 10.1%. Although butanol exhibited good wettability on the organic film, the PCE was still limited to 13% due to reductions in  $V_{oc}$  and FF. The highest PCE was achieved when BCP dissolved in IPA was applied using a doctor blade. The large-area OSC demonstrated a short circuit current density ( $J_{sc}$ ) of 24.9 mA/cm<sup>2</sup>, a  $V_{oc}$  of 0.86, an FF of 0.66, and a resulting PCE of 14.0%. The current values were similar across the different BCP solvent types, but variations were observed in  $V_{oc}$  and FF (Fig. S8). Additionally, OM images revealed that the morphology of the thick BCP layer (~20 nm) was similar for each solvent compared to the thin BCP layer (Fig. S9). Despite the uniform thick BCP film achieved through the doctor blade coating method using IPA solvent, the insulating property of the BCP layer led to charge accumulation and ultimately resulted in lower PCEs compared to devices based on thin BCP layers (Fig. S10).

We conducted further investigations into the relationship between photovoltaic parameters and light intensity, aiming to compare the recombination characteristics among different devices [46–49]. Each photovoltaic parameter was determined based on the J-V characteristics measured under varying light intensities ranging from 1 to 100 mW/cm<sup>2</sup>. In the case of organic solar cells (OSCs), the J<sub>sc</sub> values typically exhibit a power-law dependence on light intensity, which can be described as J<sub>sc</sub>  $\propto$  I<sup> $\alpha$ </sup>, where I represents the light intensity and  $\alpha$  represents the exponential factor. When the devices exhibit weak second-order recombination, a linear relationship with  $\alpha$  approaching unity is observed, whereas a sub-linear dependence indicates strong recombination. By analyzing the linearly fitted data for OSCs, as shown in Fig. 5a, we obtained  $\alpha$  values of 0.89, 0.92, and 0.92 for methanol, 1-butanol, and IPA, respectively. The nonlinear behavior observed in devices with methanol-processed BCP ETL suggests significant nongeminate recombination losses under short-circuit conditions, indicating relatively inefficient charge collection. Additionally, the light intensity dependence of V<sub>OC</sub>



Fig. 4. Photographs of (a) spin-coated small-area OSCs (size:  $15 \times 15 \text{ mm}^2$ ) and (b) doctor blade-coated large-area OSCs (size:  $40 \times 46 \text{ mm}^2$ ). J-V characteristics of (c) spin-coated small-area OSCs and (d) doctor blade-coated large-area OSCs for each solvent.

#### Table 1

Photovoltaic performance parameters of the spin-coated small-area OSCs.

Area 4.64 mm <sup>2</sup>	V <sub>oc</sub> (V)	J <sub>sc</sub> (mA/cm <sup>2</sup> )	FF	PCE (%)
Methanol	0.84	26.2	0.68	14.9
1-Butanol	0.84	25.9	0.68	14.8
IPA	0.84	25.8	0.68	14.7

Photovoltaic performance parameters of the doctor blade-coated large-area OSCs.

Area 1 cm <sup>2</sup>	V <sub>oc</sub> (V)	J <sub>sc</sub> (mA/cm <sup>2</sup> )	FF	PCE (%)
Methanol	0.79	25.1	0.51	10.1
1-Butanol	0.84	25.2	0.62	13.1
IPA	0.86	24.9	0.66	14.0



Fig. 5. Variation in (a) J<sub>sc</sub> and (b) V<sub>oc</sub> of OSCs as functions of light intensity.

offers insights into trap-assisted recombination during open-circuit conditions, where photogenerated charges recombine. Fig. 5b illustrates the slope of  $V_{OC}$  versus logarithmic light intensity, where a slope greater than kT/q suggests the presence of additional trap-assisted recombination losses. For IPA, the value of 1.29 kT/q was close to unity, indicating less significant trap-assisted recombination. Conversely, when methanol was used for BCP ETL doctor blade coating, the stronger dependence of  $V_{oc}$  on light intensity was reflected in the value of 2.41 kT/q. We speculate that the ideality factor higher than 2 might be attributed to non-uniform recombination currents within the device or tail states within the bandgap of the photoactive materials. As a result, the uniformly coated BCP ETL increased the built-in voltage across the devices due to its low work function and the suppression of recombination at interfacial trap sites, leading to the highest PCE among the printed OSCs. In the high-speed doctor blade coating (50 mm/s) of BCP ETLs, the J-V characteristics exhibited a similar trend to that observed with the low-speed doctor blade coating (10 mm/s). However, the PCE of 1-butanol-based OSCs decreased from 13.1% to 11.5%, while the IPA-based OSCs maintained a PCE of 14.0%, as shown in Fig. S11 and Table S1. This outcome can also be attributed to interfacial recombination resulting from non-uniform BCP ETL doctor blade coating (Fig. S12).

The BCP layer, serving as an organic insulator, was extremely thin. TEM images (Fig. 6a and b) confirmed that the spin coating and doctor blade coating processes uniformly coated only the photoactive and PEDOT:PSS layers. To create efficient printed large-area OSC modules, we adopted a monolithic module structure comprising four serially connected sub-cells, as depicted in Fig. 7a and b. The HTL and photoactive layer were formed without the use of an additive solvent, while the BCP ETL coating utilized the doctor blade coating method with different solvents. Among the various solvents tested in the large-area single-cell experiments, the IPA solvent-based OSC module demonstrated the highest PCE of 10.8%. This module achieved a short circuit current (I<sub>sc</sub>) of 56.0 mA, a V<sub>oc</sub> of 3.24, and an FF of 0.59 over a total area of 10 cm<sup>2</sup>, with a geometrical fill factor of 86.5% (Fig. 7c and Fig. S13) (see Table 3). However, similar to the results obtained from the large-area single cells, the module exhibited the lowest PCE of 6.57% primarily due to a reduction in V<sub>oc</sub> and FF. To assess the general solvent effect on the coating of charge transport layers on hydrophobic photoactive layers, we fabricated inverted OSCs using a doctor blade coating method with ZnO, PTB7-Th:PC<sub>70</sub>BM, and MoO<sub>3</sub> layers. Since MoO<sub>3</sub> powder is not highly soluble in IPA, methanol was added to achieve a suitable boiling point for the solution. This co-solvent system yielded improved PCEs (Fig. S14 and Table S2), highlighting the significance of solvent choice in the printing process of charge transport layers.



Fig. 6. TEM images of (a) spin-coated and (b) doctor blade-coated OSCs.



Fig. 7. (a) Schematic and (b) photographic images of the blade-coated large-area monolithic OSC modules (size  $42 \times 60 \text{ mm}^2$ ). (c) J-V characteristics of blade-coated large-area OSC modules for each solvent.

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hotovoltaic performance parameters of the doctor blade-coated large-area OSC modules.

Area 10 cm <sup>2</sup>	V <sub>oc</sub> (V)	I <sub>sc</sub> (mA)	FF	APCE (%)	MPCE (%)
Methanol	3.00	54.9	0.40	7.60	6.37
1-Butanol	3.24	57.2	0.50	10.8	9.31
IPA	3.24	56.0	0.59	12.5	10.8

Geometrical fill factor 86.5%.

# 4. Conclusions

In summary, our study successfully showcased the production of printed large-area OSC (Organic Solar Cell) modules through the optimization of processing conditions in the doctor blade coating method. Our efficient fabrication process for normally structured organic solar cells involved several steps. Firstly, we diluted the PEDOT:PSS HTL (Hole Transport Layer) solution with ambipolar IPA (Isopropyl Alcohol) solvent. Next, we prepared the non-fullerene photoactive solution without the use of any high boiling point solvent additives. We then dissolved the BCP (Bathocuproine) ETL (Electron Transport Layer) material in IPA solvent. Finally, we applied these solutions using the doctor blade coating method to create uniform films, eliminating the need for additional treatment.

Through a comprehensive analysis of the effect of the process solvent on each component layer, we discovered the significance of proper boiling point and solvent orthogonality during the coating process for the charge transport layer on the organic photoactive layer. By achieving uniform coating of the BCP ETL, we mitigated weak recombination in the interfacial region between the ETL and photoactive layer. This resulted in higher power conversion efficiencies (PCEs) in large-area printed OSCs and modules. The OSCs we produced using the doctor blade coating method achieved remarkable results, with a high PCE of 14.0% in 1 cm<sup>2</sup> active area samples, at both low coating speeds of 10 mm/s and high coating speeds of 50 mm/s. Notably, this achievement of 14% efficiency in OSCs with a 1 cm<sup>2</sup> area, particularly at high throughput (50 mm/s), is significant as it demonstrates a successful alternative to the commonly used spin coating method.

Furthermore, we expanded our demonstration to include uniform large-area OSC modules, with a total area of 10 cm<sup>2</sup>, exhibiting the best PCE of 10.8% and a geometrical fill factor of 86.5%. These results highlight the scalability and applicability of our approach.

We believe that our findings and methodology can significantly contribute to the seamless transition of OSC technology from laboratory research to commercialization, opening up new opportunities in the field.

# Author contribution statement

Soonil Hong; Byoungwook Park: Conceived and designed the experiments; Performed the experiments. Chandran Balamurugan: Analyzed and interpreted the data. Jinho Lee; Sooncheol Kwon: Contributed reagents, materials, analysis tools or data; Wrote the paper.

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# Data availability statement

Data included in article/supplementary material/referenced in article.

# Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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# Appendix A. Supplementary data

Supplementary data to this article can be found online at https://doi.org/10.1016/j.heliyon.2023.e18209.

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