

Highly efficient removal of ammonia nitrogen from wastewater by dielectrophoresis-enhanced adsorption

Dongyang Liu¹, Chenyang Cui¹, Yanhong Wu¹, Huiying Chen¹, Junfeng Geng² and Jianxin Xia¹

¹ College of Life and Environmental Science, Minzu University of China, Beijing, China

² Institute for Materials Research and Innovation, Institute for Renewable Energy and Environmental Technologies, University of Bolton, Bolton, UK

ABSTRACT

A new approach, based on dielectrophoresis (DEP), was developed in this work to enhance traditional adsorption for the removal of ammonia nitrogen (NH₃-N) from wastewater. The factors that affected the removal efficiency were systematically investigated, which allowed us to determine optimal operation parameters. With this new method we found that the removal efficiency was significantly improved from 66.7% by adsorption only to 95% by adsorption-DEP using titanium metal mesh as electrodes of the DEP and zeolite as the absorbent material. In addition, the dosage of the absorbent/zeolite and the processing time needed for the removal were greatly reduced after the introduction of DEP into the process. In addition, a very low discharge concentration (C, 1.5 mg/L) of NH₃-N was achieved by the new method, which well met the discharge criterion of C < 8 mg/L (the emission standard of pollutants for rare earth industry in China).

Subjects Environmental Contamination and Remediation

Keywords Dielectrophoresis, Ammonia nitrogen, Adsorption, Wastewater, Zeolite

INTRODUCTION

Nitrogen is a basic structural element of biological proteins in life. In water, one of the major forms of nitrogen is ammonia nitrogen (NH₃-N). NH₃-N is essential to living organisms, but exceeding threshold level could cause environmental pollution (Rožić *et al.*, 2000). A large amount of NH₃-N could cause serious disorder of natural materials circulation, which threatens human health. According to WHO guidelines for drinking-water quality, the concentration of NH₃-N should not exceed 1.5 mg/L in drinking water (Gorchev & Ozolins, 1984). High level NH₃-N present in water may cause eutrophication to occur (Blomqvist, Pettersson & Hyenstrand, 2008; Huang *et al.*, 2014; Lin *et al.*, 2009). Under this circumstance, NH₃-N could be toxic to most cultured animals (Chang *et al.*, 2015; Ebeling, Timmons & Bisogni, 2006; He *et al.*, 2011). NH₃-N may also be oxidized into nitrite, when this is taken into human body, could cause cancer (Kim *et al.*, 2005; Li *et al.*, 2009; Wang, Kmiya & Okuhara, 2007).

How to efficiently remove NH₃-N from wastewater has, as a research topic, attracted great interests in recent years. The existing methods include ammonia stripping (Bonmati & Flotats, 2003; Liao, Chen & Lo, 1995), chemical precipitation (Diwani *et al.*, 2007;

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Corresponding authors

Yanhong Wu,

13801232755@139.com

Huiying Chen,

huiyingrchen@aliyun.com

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Li, Zhao & Hao, 1999; Ryu, Kim & Lee, 2008), electrochemical conversion (*Kim et al., 2006*) and membrane separation (*Ali et al., 2010; Domingos et al., 2011*). However, none of these can provide an ideal way for a large-scale operation for each of these methods has its own major shortcoming in terms of either the removal efficiency or the processing cost. Ammonia stripping is only suitable to high concentrations of $\text{NH}_3\text{-N}$ and the processing cost is high (*Zhang, Lee & Jahng, 2011*). Chemical precipitation would need high concentrations of $\text{NH}_3\text{-N}$ and additional reagents, which may cause secondary pollution (*Diwani et al., 2007*). Electrochemical method is typically of high cost for the method is energy consummative and needs precious metals as the electrode materials (*Kim et al., 2006*). Membrane separation could be efficient but it usually uses expensive materials to construct the membrane. Clearly, it is significant to develop a low-cost, high-efficiency method to remove $\text{NH}_3\text{-N}$ from wastewater.

On the other hand, adsorption technique has long been used to remove various types of impurities from wastewater due to its appreciable removal efficiency and relatively low cost (*Zheng, Xie & Wang, 2012*). Moreover it has been reported that zeolite shows a strong adsorption activity on $\text{NH}_3\text{-N}$ (*Watanabe et al., 2003; Wan et al., 2017*). It has thus been exploited to remove $\text{NH}_3\text{-N}$ from wastewater (*Delkash, Bakhshayesh & Kazemian, 2015; Halim et al., 2009; Wang & Peng, 2010*). However, the removal efficiency by adsorption itself with zeolite is not high enough, and the removal speed is quite slow (also see our experimental data in this paper), which makes us to consider how to significantly enhance the adsorption while still keep the operation at a relatively low cost. Here we report that with the support from dielectrophoresis (DEP), both the removal speed and removal efficiency can be largely improved. DEP is a powerful tool that can be used to manipulate polarized particles suspended in fluid media in a non-uniform applied electric field. In this work, DEP could have helped to effectively trap targeted zeolite particles (with $\text{NH}_3\text{-N}$ attached on top) onto the electrodes so that the post-process separating of the solid from wastewater and cleaning to the operation device become easy and handy.

MATERIALS AND METHODS

Ammonium chloride (Analytical reagent, China National Medicines Corporation Ltd, Beijing, China) was used as the source of $\text{NH}_3\text{-N}$. Ultrapure water was used for preparation of the solutions. Adsorbents were bentonite (China National Medicines Corporation Ltd, Beijing, China) and zeolite (Tianjin Fu Chen Chemical Reagents Factory, Tianjin, China). Stainless steel wire mesh and titanium mesh were used as the electrodes to determine the optimal operation parameters for achieving maximum removal efficiency of $\text{NH}_3\text{-N}$ from water.

The experimental apparatus is shown in [Fig. 1](#). A direct current power device (PS-305DM; Longwei Instruments (HK) Co., Ltd, Hong Kong, China) was used as the power source. $\text{NH}_3\text{-N}$ was measured by $\text{NH}_3\text{-N}$ Analyzer (DWS-296; Shanghai Electronics Science Instrument Co., Ltd, Shanghai, China). Zeolite particles and the electrodes were characterized by scanning electron microscopy (SEM) (S-4800; Shimadzu, Kyoto, Japan).

Adsorption experiments were performed at room temperature (25 °C) in a series of conical flasks containing $\text{NH}_3\text{-N}$ solutions with initial concentration of 30 mg/L, except

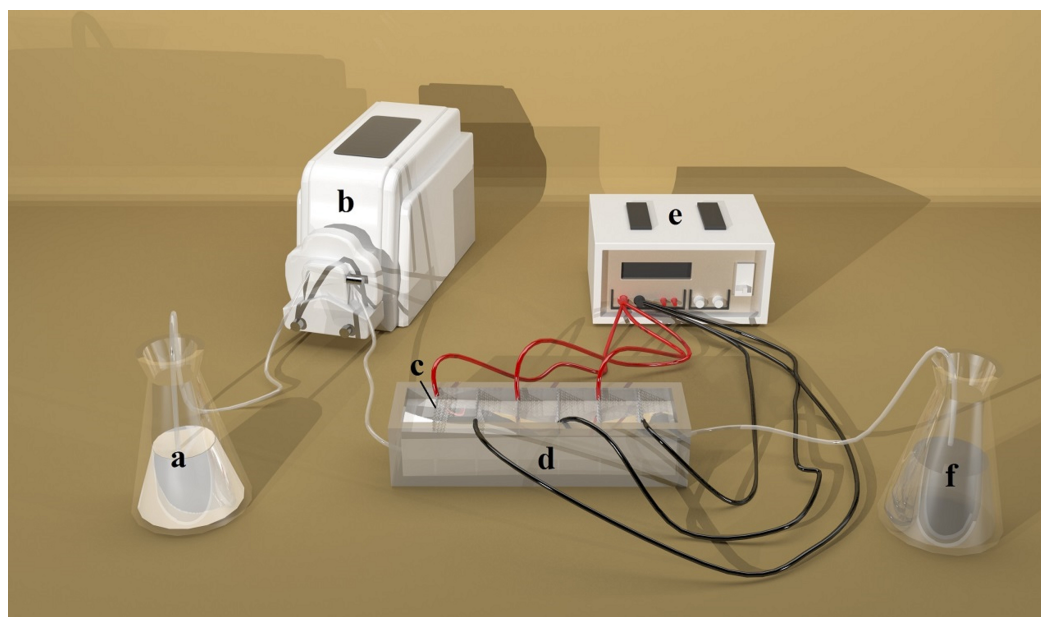


Figure 1 Schematic diagram of DEP apparatus. (A) Storage conical flasks; (B) Pump; (C) Titanium metal mesh; (D) Fluid vessel; (E) Direct current power source; (F). Reception conical flasks. Photo by Dongyang Liu. [Full-size](#) DOI: 10.7717/peerj.5001/fig-1

the experiment for effects of initial concentration. A total of 2 g/L adsorbent (except the experiment for effects of dosages) was first added to a solution and the suspension was then stirred for 20 min for adsorption to occur. This was followed up by a series of DEP processes carried out at room temperature (25 °C) with a home-made apparatus. Ten electrodes were installed to the slots on sidewalls of the vessel (Fig. 1). The distance within each pair of electrodes was set at 10 mm. A direct-current power device was used to supply voltage to the electrodes. Following a prior adsorption treatment, the suspension was forced by a pump to flow through the DEP device with the flow rate of 16 mL/min. The voltage was applied to mesh electrodes, which could create non-uniform electric field, and then, the zeolite particles with $\text{NH}_3\text{-N}$ attached on the top were trapped by the electrodes. The DEP processing time was 20 min, except the experiment for effects of processing time.

RESULTS

Effects of processing factors on the removal efficiency

The factors of removal of $\text{NH}_3\text{-N}$ by DEP-enhanced adsorption are given in Figs. 2–6.

Effects of adsorbents and electrode materials

In order to select suitable materials acting as adsorbent for the adsorption and electrodes for DEP, initial tests were carried out. Figure 2 shows the variation of the removal efficiency by using 2 g/L zeolite and bentonite as the adsorbent separately and stainless steel mesh and titanium mesh as the electrodes, with initial $\text{NH}_3\text{-N}$ concentration of 30 mg/L and voltage of 11 V. The removal efficiency of $\text{NH}_3\text{-N}$ was only 23.3% using bentonite adsorption only, while this figure was much higher (66.7%) using zeolite

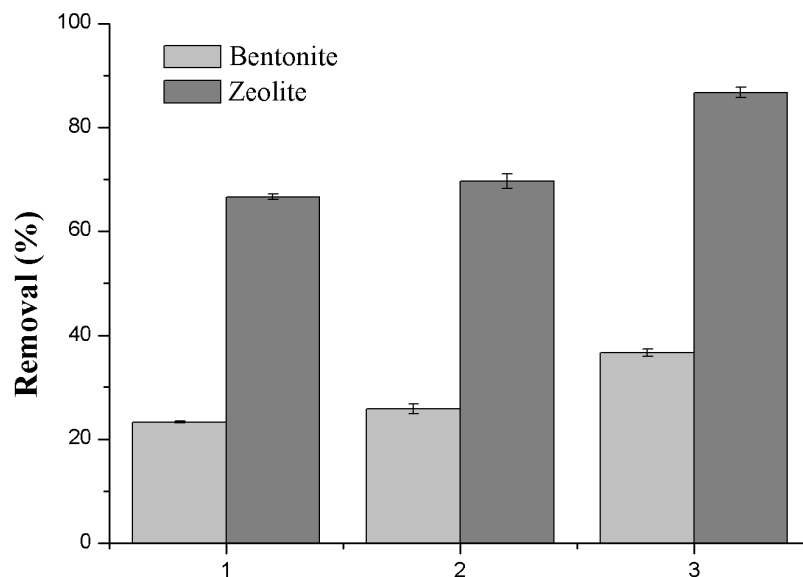


Figure 2 Effect of absorbents and electrode materials on the removal efficiency of $\text{NH}_3\text{-N}$. (1) Using ADS only; (2) using ADS-DEP with stainless steel mesh as the electrodes; (3) using ADS-DEP with titanium mesh as the electrodes. [Full-size !\[\]\(5f471a71b78d7676bc356df190b88ab4_img.jpg\) DOI: 10.7717/peerj.5001/fig-2](https://doi.org/10.7717/peerj.5001/fig-2)

(case 1 in Fig. 2). Moreover, both figures were slightly increased after the introduction of DEP using stainless steel mesh as the electrodes (case 2 in Fig. 2). However, it was observed that the removal efficiency was largely enhanced when titanium mesh electrodes were employed in the DEP, resulting in much better figures, i.e., 37% with bentonite and 87% with zeolite (case 3 in Fig. 2). Therefore, the titanium mesh electrodes and zeolite were used in the following experiments.

Effects of dosages for different processes

The zeolite dosage exerts a strong effect on the removal efficiency in both adsorption only and adsorption-DEP processes. The effect of zeolite dose, varying from 1 to 4 g/L, on removal of $\text{NH}_3\text{-N}$ is presented in Fig. 4. The initial $\text{NH}_3\text{-N}$ concentration was 30 mg/L with applied voltage of 11 V.

It can be seen from Fig. 3 that in an adsorption process only, the removal efficiency of $\text{NH}_3\text{-N}$ increased continuously with the increase of the zeolite dosage. In the adsorption-DEP process, it is interesting to see the experimental data that clearly showed the optimal dosage of zeolite (in this case, it was about 2.0 g/L), which corresponded to a peak removal efficiency of 86.7% (Fig. 3).

Effects of voltages

Apart from the dosage effect, the voltage applied to the electrodes also showed an appreciable effect on the removal of $\text{NH}_3\text{-N}$. The effect of voltage on $\text{NH}_3\text{-N}$ removal rates was investigated at zeolite dose of 2 g/L, initial $\text{NH}_3\text{-N}$ concentration of 30 mg/L and the applied voltage of 9–25 V.

Figure 4 clearly indicates that there was an optimal voltage for the operation, in this work this optimal voltage was 15 V, which corresponded to the maximum removal

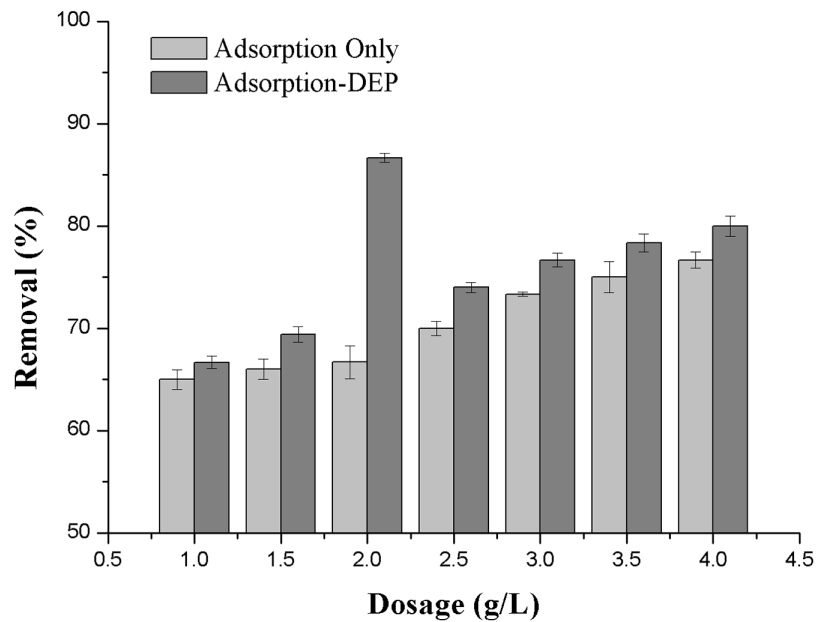


Figure 3 Effect of adsorbent dosage on the removal efficiency of NH₃-N.

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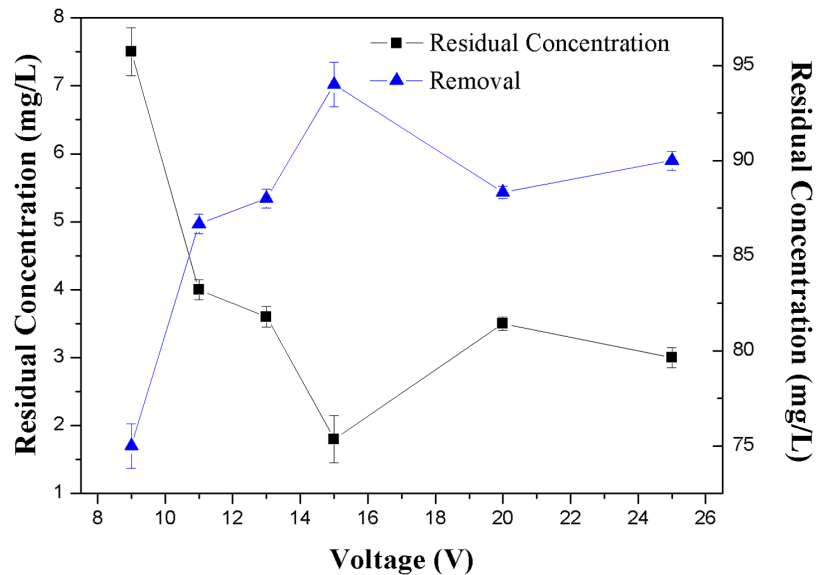


Figure 4 Effect of the voltage on the removal efficiency of NH₃-N.

Full-size DOI: 10.7717/peerj.5001/fig-4

efficiency of 94% and minimum residue concentration of 1.5 mg/L of NH₃-N in the solution.

Effects of processing time

The effect of zeolite processing time on the removal of NH₃-N was subsequently investigated by setting the voltage to 15 V with initial NH₃-N concentration of 30 mg/L and zeolite dosage of 2.0 g/L. The DEP processing time was 30 min. The treated water was

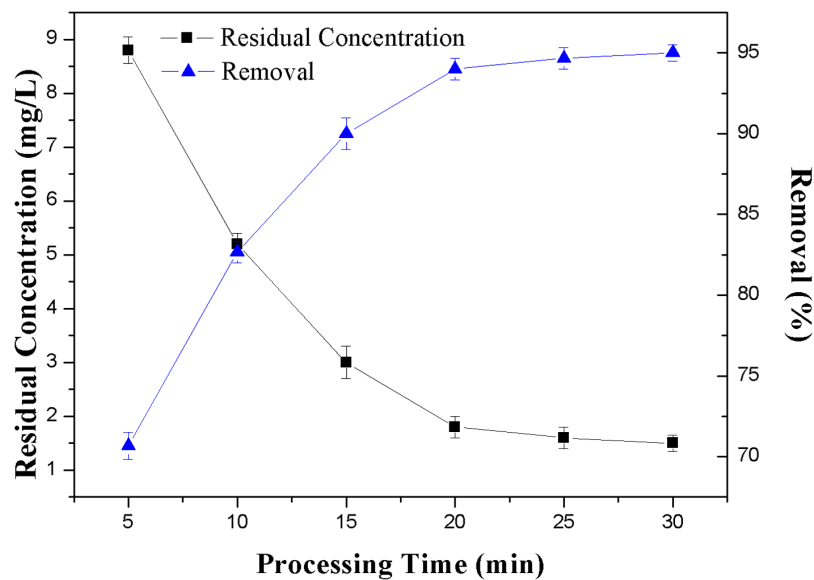


Figure 5 Effect of processing time on the removal rate of $\text{NH}_3\text{-N}$.

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sampled and measured every 5 min. As can be seen from Fig. 5, the removal efficiency in the adsorption-DEP process increased considerably with the increase of the processing time. When the processing time went up from 5 to 30 min, the removal efficiency was improved from 70% to 95%, and correspondingly, the residual concentration of $\text{NH}_3\text{-N}$ decreased from 9.0 to 1.5 mg/L. The removal efficiency was almost constant after 20 min.

Effects of initial concentration

Furthermore, we tested the effect of the initial ammonia concentration vary from 20 to 50 mg/L on the removal efficiency at a fixed zeolite dosage of 2 g/L, voltage of 15 V. It can be seen from Fig. 6 that removal efficiency decreased with the increasing of initial concentration.

Characterization of the zeolite particles

To find out how adsorption and adsorption-DEP processes affected the zeolite particles, we performed SEM examination on the samples taken after each process (Fig. 7).

Scanning electron microscopy image taken from the sample after an adsorption-only process did not show any morphological change in the particles (Fig. 7A). However, the particles were broken down by the adsorption-DEP process, which indicates the important effect of DEP on the particles (Fig. 7B). We have also examined the electrodes after the adsorption-DEP by SEM, and the result is shown in Figs. 7C and 7D. It can be seen that both positive and negative electrodes were deposited by zeolite particles.

DISCUSSION

Theory of DEP

We would like to propose the following mechanism to explain the DEP process: a non-uniform electric field generated in the DEP device polarizes adsorbents and induces

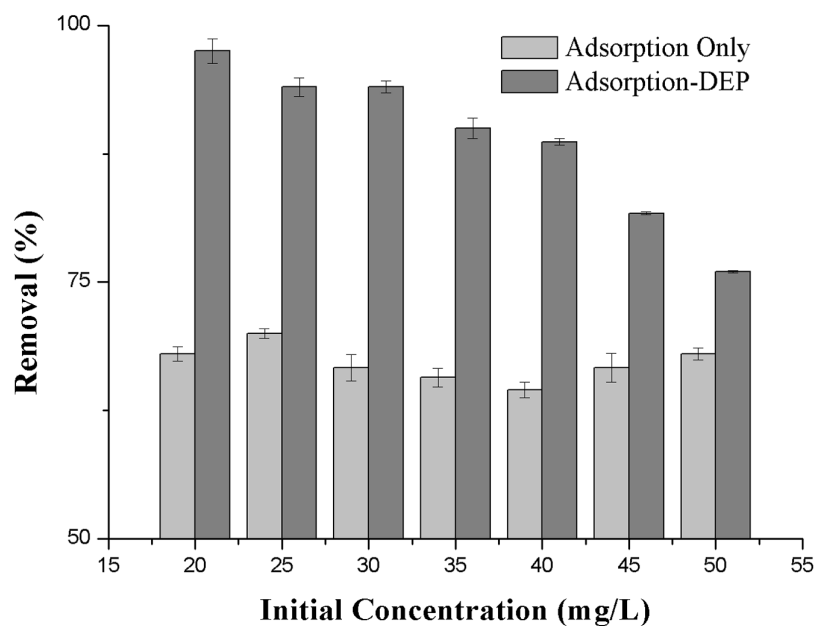
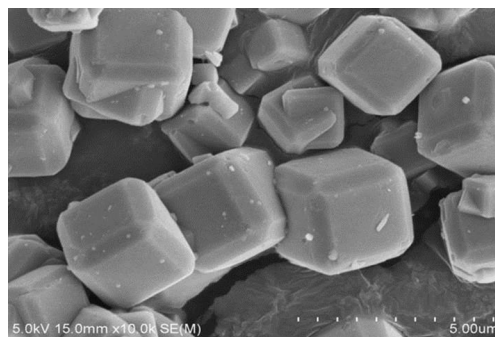
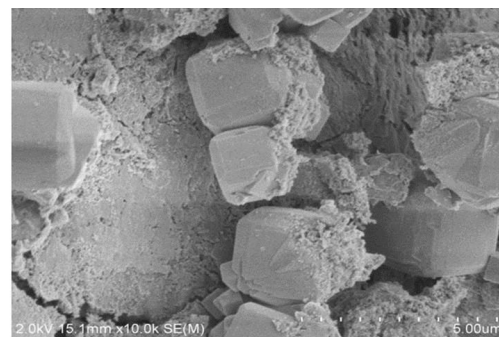


Figure 6 Effect of the initial concentration on the removal efficiency of $\text{NH}_3\text{-N}$.

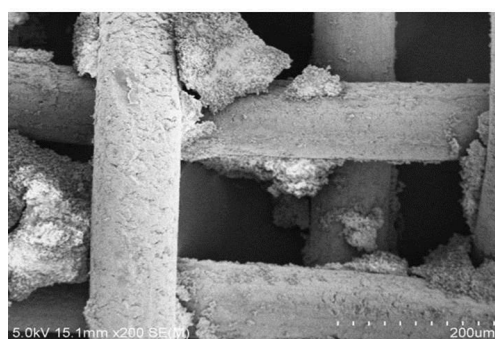
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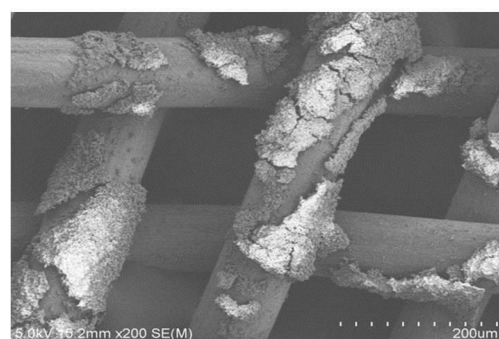
(a)



(b)



(c)



(d)

Figure 7 SEM images of the zeolite and electrodes after ADS-DEP process. (A) zeolite after adsorption only; (B) zeolite after ADS-DEP process; (C) positive electrode after ADS-DEP process; (D) negative electrode after ADS-DEP process.

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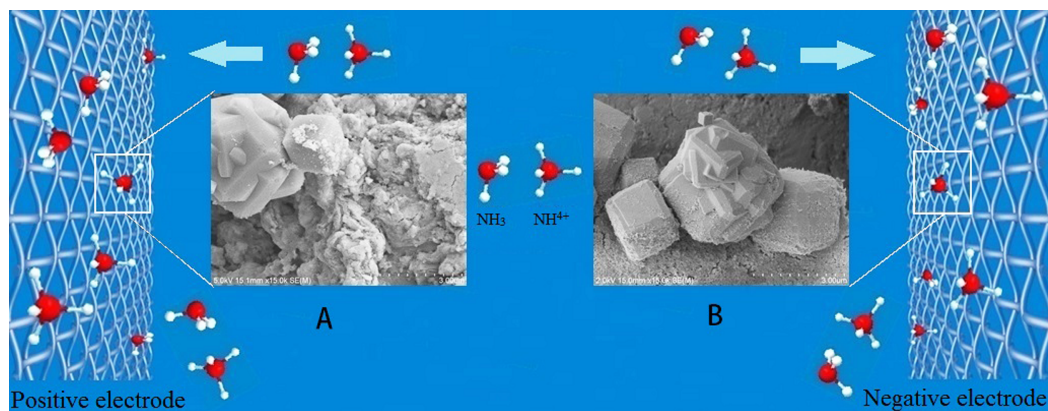


Figure 8 Schematic show of the movement of zeolite particles in $\text{NH}_3\text{-N}$ solution towards the electrodes. The voltage used in the DEP was 15 V. (A) SEM image of the zeolite particles trapped on positive electrode; (B) SEM image of the zeolite particles trapped on negative electrode.

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a dipole moment on each of them. As a consequence, the electric field exerts an unbalanced force on the adsorbent particles, which drives them to move along the electric field gradient in the solution. Those particles near the electrodes were first captured and trapped by the electrodes. Due to the strong electric field in the cross-wire areas of the mesh electrodes, coupled with a possible polarization induction effect between adjacent adsorbent particles, other particles close to the wire junctions were polarized and subsequently trapped by the electrodes. In this way, continuous capture of the adsorbent particles would occur, so more and more adsorbent particles would be trapped and deposited on the electrodes (see Fig. 8). This mechanism is supported by the working principle of DEP—a technique that has been used to manipulate polarized particles suspended in fluid media in non-uniform electric field (Khashei et al., 2015). In the case of a spherical particle, the DEP force F_{DEP} is given by the equation below:

$$F_{\text{DEP}} = 2\pi R^3 \epsilon_m \text{Re}[K(\omega)] \nabla E^2 \quad (1)$$

Where the real part of Clausius–Mossotti factor, $\text{Re}[K(\omega)]$, is defined as:

$$K(\omega) = \frac{\epsilon_p^* - \epsilon_m^*}{\epsilon_p^* + 2\epsilon_m^*} \quad (2)$$

Where R denotes the radius of the particle, ∇E the magnitude of the electric field gradient, ϵ_p^* the complex permittivity of the particle, and ϵ_m^* that of the media. A non-uniform electric field is necessary to induce a DEP force as stated in Eq. (1) (otherwise $\nabla E = 0$). Positive values of $\text{Re}[K(\omega)]$ denote the induction of a positive DEP force that causes particles to be trapped in the regions of high electric field gradient. Negative values of $\text{Re}[K(\omega)]$ denote negative DEP, which means the particles would move towards the regions of low or no electric field.

Effects of processing factors on the removal efficiency

As can be seen from Fig. 2 (case 1), the adsorption by zeolite was better than bentonite. The $\text{NH}_3\text{-N}$ adsorption mechanism by zeolite is mainly chemical adsorption and

ion exchange. With the increase of $\text{NH}_3\text{-N}$ concentration, more $\text{NH}_3\text{-N}$ is available for exchange, which enhance the capacity of exchange reactions (*Zhang et al., 2003*).

During the DEP process, it was observed that the removal efficiency was largely enhanced when titanium mesh electrodes were employed in the DEP, resulting in much better efficiency (cases 2 and 3 in *Fig. 2*). Besides, the stainless steel mesh could be electrolyzed slightly during the DEP process. This clearly indicates that DEP can significantly help improve the removal of $\text{NH}_3\text{-N}$ as long as a suitable and durable material is used for the electrodes. Based on this initial test result we subsequently chose zeolite as the adsorbent, and titanium mesh as the electrodes, with which we could determine the best possible working conditions for the system.

A phenomenon that the removal efficiency of $\text{NH}_3\text{-N}$ increased continuously in an adsorption process only with the increase of the zeolite dosage (*Fig. 3*) may be straightly understood from the increased adsorption sites of zeolite particles in the system (*Wan et al., 2017*). We also supposed that two factors caused the optimal zeolite dosage during DEP process in *Fig. 3*. When in the absence of DEP, the removal rate improved with the increase of zeolite dose, which increase adsorption sites. During the DEP-enhanced adsorption, the adsorbed ion number per unit mass of zeolite could reach highest at the dose of 2 g/L which makes the highest efficiency of DEP. And after the dose of 2 g/L, more adsorbents may weaken polarization ability by DEP process. So any further increase of the amount of adsorbent would lead to a reduced removal efficiency.

It can be seen from *Fig. 4* that in the lower voltage region (≤ 15 V), the removal efficiency was increased with the increase of the voltage. As described in *Eq. (1)*, with the increase of applied voltage, the enhance of electric field gradient increased the DEP force. However, after the voltage reached a certain point, the removal efficiency decreased. This can be explained by DEP principle. Different kinds of particles have their own characteristic voltages, in which the positive DEP could happened strongly. Over the characteristic voltage, the particle would leave the original trapped region (*Chen et al., 2009; Lapizco-Encinas et al., 2005*). In this work the positive DEP would happen when the voltage was 15 V. This speculation is also consistent with the phenomenon observed by *Kim et al. (2004)* in a diamond suspension.

Because DEP force was short-distance force, the largely enhanced removal efficiency was due to the fact that with the increase of the processing time, more and more zeolite particles could have chances to be carried to the electrodes by flowing water and trapped on the electrodes, and removed from the solution. By calculating the flowing rate and the device size, the wastewater would flow through all the electrodes and be treated in 20 min. So the removal efficiency of $\text{NH}_3\text{-N}$ almost reached the highest in 20 min (*Fig. 5*). It is also worthy to note that in comparison with a similar adsorption-only result (*Wang, Wang & Zhou, 2012*), where it took about 1,440 min to reach the adsorption equilibrium of $\text{NH}_3\text{-N}$ by zeolite, our adsorption-DEP approach took only 30 min to reach the equilibrium, thus a much faster removal speed. In addition, our approach achieved a significantly higher removal efficiency compared with the adsorption-only method.

It is seen from *Fig. 6* that the removal process by adsorption-DEP was particularly powerful at lower initial concentrations: the lower the concentration, the higher the removal

efficiency. Figure 6 also shows the difference of the removal efficiency between adsorption-only process and adsorption-DEP process under identical experimental conditions.

Analysis of zeolite particles by SEM

As seen from Figs. 7A and 7B, the broken-down of the zeolite particles resulted in a significant increase of the particle surface area, thus the number of active adsorption sites to $\text{NH}_3\text{-N}$. This may explain why the DEP-assisted process had significantly enhanced the removal of $\text{NH}_3\text{-N}$ in comparison with the adsorption-only method.

Figures 7C and 7D could be understood from the mechanism of DEP rather than electrophoresis. Most of the adsorbent particles were trapped on the cross-wire areas of electrodes where the electric field gradient was the strongest, indicating that positive DEP took place in this work. Zeolite particles first trapped onto the electrode were polarized again by the electrical field. They produced secondary non-uniform electric field. More particles nearby can be attracted to them because of particle-particle interactions (Ai & Qian, 2010; Cui et al., 2015; Doh & Cho, 2005; Hossain et al., 2013; Jones, 2003), which is illustrated schematically by Fig. 8. Therefore, the $\text{NH}_3\text{-N}$ removal efficiency could be improved.

CONCLUSION

A new approach for the removal of $\text{NH}_3\text{-N}$ in wastewater has been developed in this work using DEP to greatly enhance traditional adsorption method. The factors that affect the removal efficiency have been investigated, and the optimal working parameters determined. The experimental results show that our DEP-enhanced method can significantly improve the removal efficiency of $\text{NH}_3\text{-N}$, in comparison with adsorption-only method, when titanium metal mesh is used as the electrode material and zeolite as the adsorbent. Under identical experimental conditions, this removal efficiency has been found to increase from 66.7% to 95.0%. In addition, the dosage of the adsorbent/zeolite and the processing time have been greatly reduced with the assistance from DEP. Furthermore, we find that a low discharge concentration of $\text{NH}_3\text{-N}$ in wastewater, which is as low as 1.5 mg/L after adsorption-DEP treatment, can be achieved, and this is well below the discharge criterion of $[\text{NH}_4^+] < 8$ mg/L (the emission standard of pollutants for rare earth industry in China). All these suggest that our adsorption-DEP method provides a high-efficiency approach for the removal of $\text{NH}_3\text{-N}$ from wastewater and the technology holds a high potential for future industrial applications.

ADDITIONAL INFORMATION AND DECLARATIONS

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Competing Interests

The authors declare that they have no competing interests.

Author Contributions

- Dongyang Liu analyzed the data, prepared figures and/or tables, authored or reviewed drafts of the paper, approved the final draft.
- Chenyang Cui conceived and designed the experiments, performed the experiments, analyzed the data, prepared figures and/or tables, authored or reviewed drafts of the paper, approved the final draft.
- Yanhong Wu analyzed the data, contributed reagents/materials/analysis tools, prepared figures and/or tables, authored or reviewed drafts of the paper, approved the final draft.
- Huiying Chen conceived and designed the experiments, analyzed the data, contributed reagents/materials/analysis tools, prepared figures and/or tables, authored or reviewed drafts of the paper, approved the final draft.
- Junfeng Geng prepared figures and/or tables, authored or reviewed drafts of the paper, approved the final draft.
- Jianxin Xia contributed reagents/materials/analysis tools, prepared figures and/or tables, authored or reviewed drafts of the paper, approved the final draft.

Data Availability

The following information was supplied regarding data availability:

The raw data are provided in the [Supplemental File](#).

Supplemental Information

Supplemental information for this article can be found online at <http://dx.doi.org/10.7717/peerj.5001#supplemental-information>.

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