

# The influence of photochemistry on outdoor to indoor NO<sub>2</sub> in some European museums

Terje Grøntoft 

Norwegian Institute for Air Research,  
Kjeller, Norway

## Correspondence

Terje Grøntoft, Norwegian Institute for Air  
Research, P.O.Box 100, Kjeller NO-2027,  
Norway.  
Email: teg@nilu.no

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## Abstract

This paper reports 1 year of monthly average NO<sub>2</sub> indoor to outdoor (I/O) concentrations measured in 10 European museums, and a simple steady-state box model that explains the annual variation. The measurements were performed in the EU FP5 project Master (EVK-CT-2002-00093). The work provides extensive documentation of the annual variation of NO<sub>2</sub> I/O concentration ratios, with ratios above unity in the summer, in situations with no indoor emissions of NO<sub>2</sub>. The modelling included the most relevant production and removal processes of NO<sub>2</sub> and showed that the outdoor photolysis was the probable main explanation of the annual trends in the NO<sub>2</sub> I/O concentration ratios.

## KEYWORDS

indoor exposure, modelling, museums, nitrogen dioxide, outdoor to indoor concentrations, photochemical reaction

## 1 | INTRODUCTION

Nitrogen dioxide (NO<sub>2</sub>) can harm people's health and cultural heritage materials by its oxidizing and/or acidic effects. People spend much of their time indoors. The sometimes higher indoor as compared to outdoor exposure to NO<sub>2</sub> adds to the total person, and object, exposure. A major motivation for understanding the outdoor to indoor NO<sub>2</sub> concentrations in museums is the degradation due to the atmospheric exposure that has been reported of sensitive art materials. This work provides results from annual monthly measurements of NO<sub>2</sub> I/O ratios in 10 European museums. Then, tentatively, a simple model that can approximate the indoor to outdoor (I/O) ratios of NO<sub>2</sub>, and higher than unity ratios that are often observed in the summer, from the outdoor NO<sub>x</sub> and O<sub>3</sub> values that are more often available from regulatory measurement stations than indoor measured values. A recent paper reviewed the status of knowledge of indoor NO and NO<sub>2</sub> concentrations and chemistry, among other acids and bases that influence indoor air quality.<sup>1</sup> They stated that "in the absence of indoor sources, I/O concentration ratios of nitrogen

monoxide (NO) tend to be close to unity, while those for NO<sub>2</sub> tend to be in the range of 0.7 to 0.9 depending on the air exchange rate and relative humidity." The source of the indoor NO<sub>2</sub> is when excluding indoor emissions that are uncommon in museums, the outdoor NO<sub>x</sub> (NO + NO<sub>2</sub>) emissions and ventilation to the indoors, and the indoor reaction of NO with O<sub>3</sub> to NO<sub>2</sub>. Annual NO<sub>2</sub> I/O ratios of unity have been measured in for example the Victoria and Albert Museum in London.<sup>2</sup> Higher indoor than outdoor concentrations of NO<sub>2</sub> have, despite the indoor deposition, been measured in museums<sup>3</sup> in the summer. This was explained by splitting of NO<sub>2</sub> outdoors by ultraviolet (UV) light, to NO and O<sub>3</sub>, and reaction back to NO<sub>2</sub> in the relative indoor darkness.

Weschler et al.<sup>4</sup> showed that, in the absence of photolysis, due to the rapid reaction of NO with O<sub>3</sub>, only the surplus gas of the two will be present at any one time. The dynamic NO<sub>x</sub>-O<sub>3</sub> chemistry happens at similar rates as the typical exchanges of indoor air (~1 h<sup>-1</sup>), which is a reason why it affects the indoor air quality. With a surplus of O<sub>3</sub> indoors most of the incoming NO will react to NO<sub>2</sub>.<sup>1,3,5,6</sup> Indoor NO<sub>2</sub> is a source of nitric (HONO) and nitrous acid (HNO<sub>3</sub>) through

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heterogeneous and homogeneous reactions. The homogeneous reactions can involve ozone ( $O_3$ ) and volatile organic compounds. The HONO is mainly released back to the air after formation with water on the surfaces. The  $HNO_3$  can be formed together with HONO on the surfaces or deposit and react on the surfaces after oxidation of  $NO_2$  by  $O_3$  in air.<sup>1,4,7,8,9,10,11</sup> Whereas exposure to peak concentrations can be the most damaging to health, it is the long duration accumulated exposure that is usually considered to damage sensitive heritage materials. Outdoor values of  $NO_2$  are more commonly available than values from indoor measurements. Museums can thus benefit from a simple model to estimate long duration indoor exposure doses from the outdoor concentration values. IAQ (Indoor Air Quality) models that calculate I/O gas concentration ratios, including  $O_3$  and  $NO_2$ , have been proposed and tested in many studies. Dynamic models (e.g.,<sup>12-14</sup>) some including advanced chemistry schemes,<sup>5,15,16,17,18</sup> and steady-state models (e.g.,<sup>11,19,20</sup>) have been used. Wang<sup>17</sup> provided a literature review of indoor air modelling involving photolysis. Weschler et al.<sup>4</sup> described and explained the dynamic trends of, the  $O_3$ ,  $NO$ , and  $NO_2^*$  ( $NO_x$  minus  $NO$ ) species. Drakou et al.<sup>16</sup> observed higher than unity I/O  $NO_2^*$  ( $NO_2 + HONO + HNO_3 + PAN$  (peroxyacetyl nitrate) =  $NO_x$  minus  $NO$ ) ratios in a building in Thessaloniki, Greece. They found that this could not fully be explained by the reaction of  $NO$  with  $O_3$ , but that in “the particular building, which was like a smog chamber, it seemed as if  $NO$  was transformed to  $NO_2$  mainly by heterogeneous processes and less through the reaction of  $O_3$  with  $NO$ .” They hypothesized that  $NO$  might be oxidized to  $NO_2$  through heterogeneous reactions involving the formation of HONO, and subsequently homogeneous reactions with OH radicals and VOCs that would “alter all the indoor gas-phase chemistry.” They concluded that in this building “there seemed to be at times a contribution to indoor  $NO_2$  from  $HNO_2$  and at times from  $HNO_3$  and PAN, and that the homogeneous chemistry and the heterogeneous removal of air pollutants in the applied model (from Nazaroff and Cass<sup>6</sup>) could not fully explain the interplay among  $O_3$ ,  $NO$ , and  $NO_2$  in the building.” Zhou et al.<sup>21</sup> reported concentrations of HONO that were on the level of  $NO_2$  in indoor air. As HONO is expected to have been reported with the  $NO_2$  from the passive sampling performed in this work,<sup>1,22</sup> the here reported “ $NO_2$ ” should, probably, be interpreted as  $NO_2 + HONO$  (it is still described in the following simply as  $NO_2$ —as reported from the analysis). The HONO would be a product of the indoor  $NO_2$  which was partly formed by reaction of  $NO$  with  $O_3$  (Equation (1) below). The inclusion of HONO with the  $NO_2$  seems thus not to disqualify the performed modelling approximation of the monthly averaged indoor  $NO_2$  (interpreted as  $NO_2 + HONO$ ). It seems, however, that it may have led to some underestimation of the deposition of the  $NO_2$  (exclusive of the HONO, which would be a product from this additional deposition). The above references testify to the complexity of the indoor  $NO_x$  heterogeneous and homogeneous chemistry, which this work did, however, not try to simulate in detail.

The aim of this work was to add comparative annual monthly site data to the evidence of increased, and often higher than unity, summer  $NO_2$  I/O ratios. Then, to investigate if a simplified steady-state  $NO_2$  I/O model, adding the effect of outdoor  $NO_2$  photolysis to the

### Practical implications

Outdoor photolysis of  $NO_2$  and indoor back-reaction of  $NO$  with  $O_3$  can contribute to higher indoor than outdoor exposures to  $NO_2$  in the summer. This is a health concern, and an objects conservation concern in museums. As indoor  $NO_2$  concentrations are seldom measured, but values for outdoor concentrations are often available from regulatory measurement stations, it is of interest to approximate the expected indoor integrated exposures from the outdoor values, with a relatively simple method that shows reasonable fit to measurements. A model expression for the  $NO_2$  indoor to outdoor ratio including the photolysis effect and meeting these criteria was presented.

heterogeneous indoor removal, could reasonably explain the monthly averaged  $NO_2$  I/O ratios. The reported  $NO_2$  and  $O_3$  measurements were performed in 10 European museums some years ago, from 2004 to 2005, in the EU Master project.<sup>23</sup> Although  $NO_2$  concentrations have since then decreased somewhat in Europe,<sup>24</sup> the presence of nitrogen oxides ( $NO_x$ ) is still a major worldwide and European air quality challenge.<sup>25-28</sup> Few data on the annual variation and higher average  $NO_2$  indoor than outdoor concentrations in the summer seems to have been reported. It therefore seemed appropriate to report these results that documents many such cases. The presented steady-state box model simplify the dynamic complexity of the homogeneous  $NO_x$ - $O_3$  chemistry with the purpose of approximating the measured time-integrated gas concentrations, and doses, in a single room.

Degradation due to the atmospheric exposure to  $NO_2$  and/or  $O_3$  has been reported of sensitive art materials such as pigments, dyes, and inks,<sup>29-36</sup> textiles (Whitmore and Cass, 1989,<sup>37</sup> paper,<sup>38-40</sup> varnish,<sup>41</sup> and metals<sup>42-44</sup>). The damage might be due to both oxidation by the nitrate radical ( $NO_3^*$ ) and acidic effects of nitric acid ( $HNO_3$ ). The  $NO_3^*$  radical will react with both saturated and unsaturated organic compounds and form gaseous and surface adsorbed/dissolved  $HNO_3$ . The high water solubility and acidity of  $HNO_3$  means that its potential for reducing the surface pH is high, even at its common low indoor concentrations below one ppb.<sup>1</sup> However, as the  $O_3 + NO$  reaction decreases  $O_3$  concentrations as much as it increases the  $NO_2$  concentrations, it seems that the effect of this reaction depends on the relative sensitivity of materials to  $O_3$  versus  $NO_2$  and its reaction products. It has been recommended that the concentrations of the pollution gases in museums should be below measurable levels ( $1 \mu g m^{-3} \sim 0.5$  ppb), based on the precautionary thinking that there is no lower threshold of their effects and that a “no observed adverse effect level” (NOAEL) has not generally been observed.<sup>45</sup> Different materials are, however, clearly at different risk from exposure to the gases.<sup>45-47</sup> To perform realistic evaluations of the damage risk of materials or objects more specific information is needed about the oxidizing and acidic reactions of the deposited gases. As an example, the longer duration degradation of oil paintings, happens by similar

mechanisms as those involved in the initial curing. The oil-containing paint film changes both by oxidation of unsaturated bonds and by hydrolysis of ester bonds in the oils, with both mechanisms leading to the formation of carboxylic groups and the possibility for subsequent metal complexation and substitution with fatty acids to create the often-whitish disfiguring crystallizations of metal soaps.<sup>48</sup> The oxidation of double bonds can be induced by UV irradiation, and/or, probably, by reaction with oxygen radicals and is accelerated by air pollutants such as NO<sub>2</sub> and SO<sub>2</sub>,<sup>49,50</sup> and probably also by O<sub>3</sub> and other oxidants, and progress by autoxidation.<sup>51</sup> The hydrolysis reaction is RH-dependent (Modugno et al., 2019). The influence of the deposition of oxidizing and acidic air pollutants on the detailed mechanisms and practical rates of such reactions in the objects at risk seems, however, in most cases not well known.

## 2 | EXPERIMENTAL AND SITES

In the EU Master project an extensive field test was carried out to measure, and evaluate, the effect of the air environment and particularly of contaminant gases present indoors, on vulnerable art objects in museums. The measurements were performed indoors and just outdoors of galleries over one year with monthly changing of duplicate passive badge samplers of NO<sub>2</sub> and O<sub>3</sub> of the IVL type (Ferm and Bloom, 2010)<sup>52</sup> in one urban and one rurally located museum in five different European regions represented by six different countries, 10 museums in all (Table 1). The supporting Table S1 provides the museums' materials and site description. In the following, the museums will, for simplicity and as the geographical location is of importance for the NO + O<sub>3</sub> reaction, often be described by their geographical location, given in Table 1, rather than by the full museum name.

The monthly pollution gas uptake was found to be well within the chemical absorption capacity of the passive samplers. Røyset<sup>22</sup> found that the NILU (Norwegian Institute for Air Research) produced

passive NO<sub>2</sub> samplers that were used in this work, were within 10%–20% of results from NO/NO<sub>x</sub> monitors calibrated against standards, that the detection limit was one µg m<sup>-3</sup> (0.5 ppb) NO<sub>2</sub> (7 days), that the precision was 5% and the accuracy 20%. No indoor NO<sub>2</sub> sources were reported in the museums or observed on inspection. The visible (lux) and UV (W m<sup>-2</sup>) light levels were measured with light meters continuously (lux) in some sites, or with spot measurements mid-day (12 a.m.) each month when the sum of the (possible) natural + artificial light intensity was at its maximum and was reported as mid-day annual averages.<sup>53</sup> The UV wavelength band of the individual light meters could unfortunately not be verified. Light meters used in museums typically measure the UV wavelength band 300–400 nm.<sup>54</sup> The temperature and relative humidity (RH) were measured with the continuous loggers of the different types in regular use by the museums and reported as monthly averages.<sup>53</sup> The area to volume ratios of the measurement rooms and description of ventilation from the museums are given in Table 3 of the modelling results, for easier comparison with those results. The values of the light measurements are, for simplicity, given in the same Table 3.

It is important to note that the conditions in Trondheim (no. 2), Zakopane (no. 8), and partly the Malta (no. 10) museum were found to be deviating in some respects. In the Trondheim site, a chimney was observed to emit smoke from the burning of fuel oil very close to the air intake of the ventilation system on the roof. Zakopane is a much-frequented winter sports location at an elevation of ~850 m in the Tatra Mountains. In Wignacourt, the (natural) ventilation was much higher in the hot summer months, due to more opening of doors and windows, as is often the case in Malta (Cassar, J., 2005, personal communication).

## 3 | RESULTS

Figure 1 shows the outdoor and indoor mean monthly concentrations of NO<sub>2</sub> and O<sub>3</sub> measured in the 10 museums.<sup>53</sup>

The outdoor O<sub>3</sub> measurement in no. 4, Blickling Hall in September (9) failed. The NO<sub>2</sub> outdoor concentration reported from the measurement in no. 6, Haslach in September (9) (0.6 ppb) was about one magnitude lower than in August and October. This out-layer was considered highly dubious, and without it being possible to locate the reason for the deviance, the value was removed. The NO<sub>2</sub> values in no. 7. The Jan Matejko House in October (8) were found to be suspicious but are reported. Figure 2 shows the NO<sub>2</sub> I/O ratios measured in the 10 museums. The figure also shows the result from the model fitting (See Section 4).

The figure clearly shows the higher indoor summer than winter concentrations of NO<sub>2</sub> measured in nine of the 10 museums and the higher than unity NO<sub>2</sub> I/O ratios measured in the summer in some of them. The highest summer indoor NO<sub>2</sub> concentrations and NO<sub>2</sub> I/O ratios among the 10 museums were observed in Stuttgart, excepting the special case of Trondheim (see Experimental). The indoor concentrations of NO<sub>2</sub> were measured to be higher than outdoors in Stuttgart from April to August. In the rural comparison, case in the

TABLE 1 Museums and site descriptions

Name of museum/historic building, (U) = Urban. (R) = rural	Location, Country
1. The Museum of Decorative Arts & Design (U)	Oslo, Norway
2. Trøndelag Folk Museum (U/R)	Trondheim, Norway
3. Tower of London, Bloody Tower (U)	London, UK
4. Blickling Hall (R)	Norfolk, UK
5. Haus der Geschichte Baden- Württemberg (U)	Stuttgart, Germany
6. Schwarzwälder Trachtenmuseum (R)	Haslach, Germany
7. The Jan Matejko House (U)	Krakow, Poland
8. The Karol Szymanowski Museum "Atma" (R)	Zakopane, Poland
9. The Historical Museum of Crete (U)	Heraklion, Greece
10. Wignacourt Collegiate Museum (U/R)	Rabat, Malta

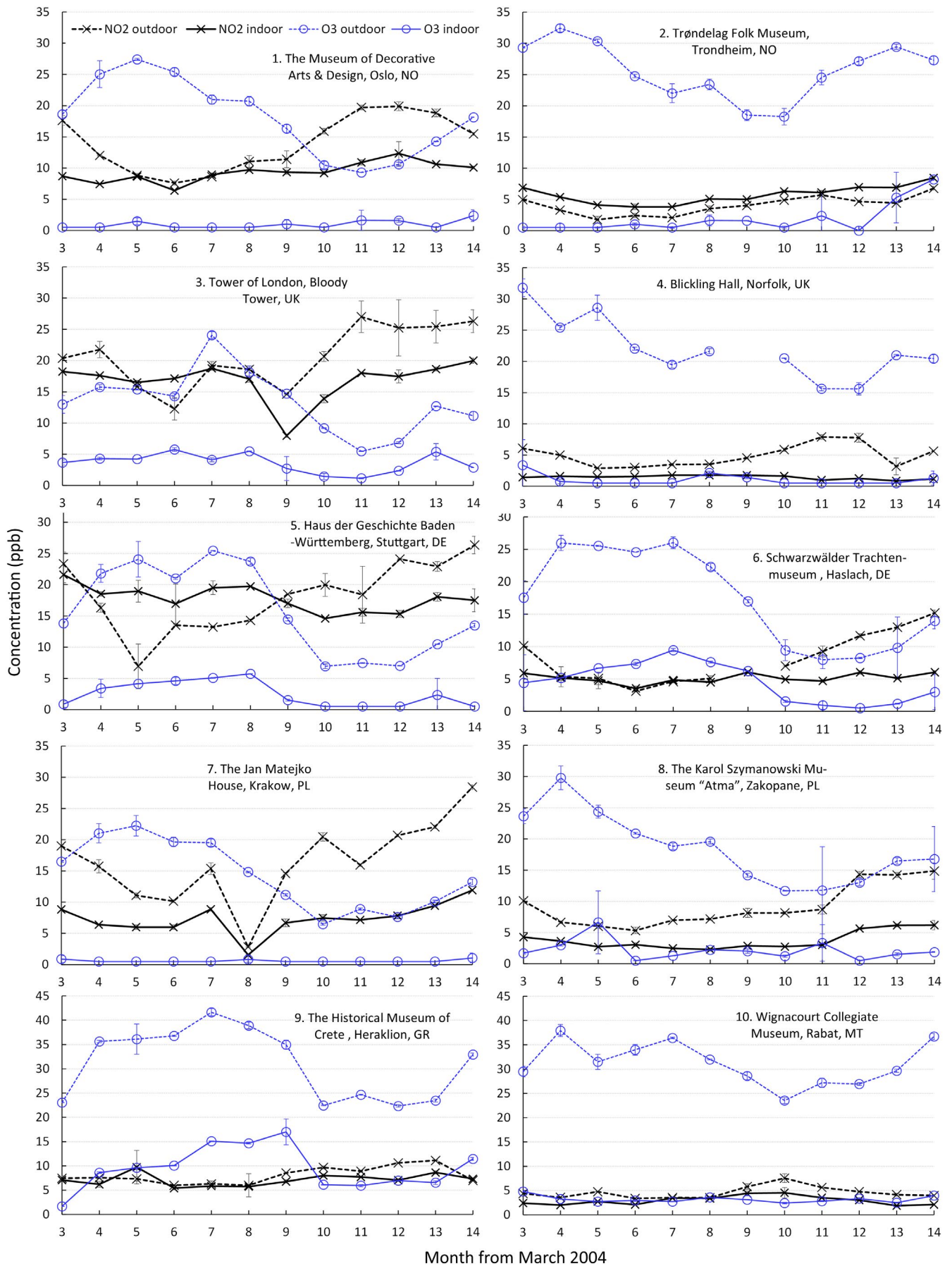


FIGURE 1 Mean monthly outdoor and indoor NO<sub>2</sub> and O<sub>3</sub> concentrations measured from March 2004 to March 2005 in 10 European museums. The error bars represent the standard deviation of duplicate measurements



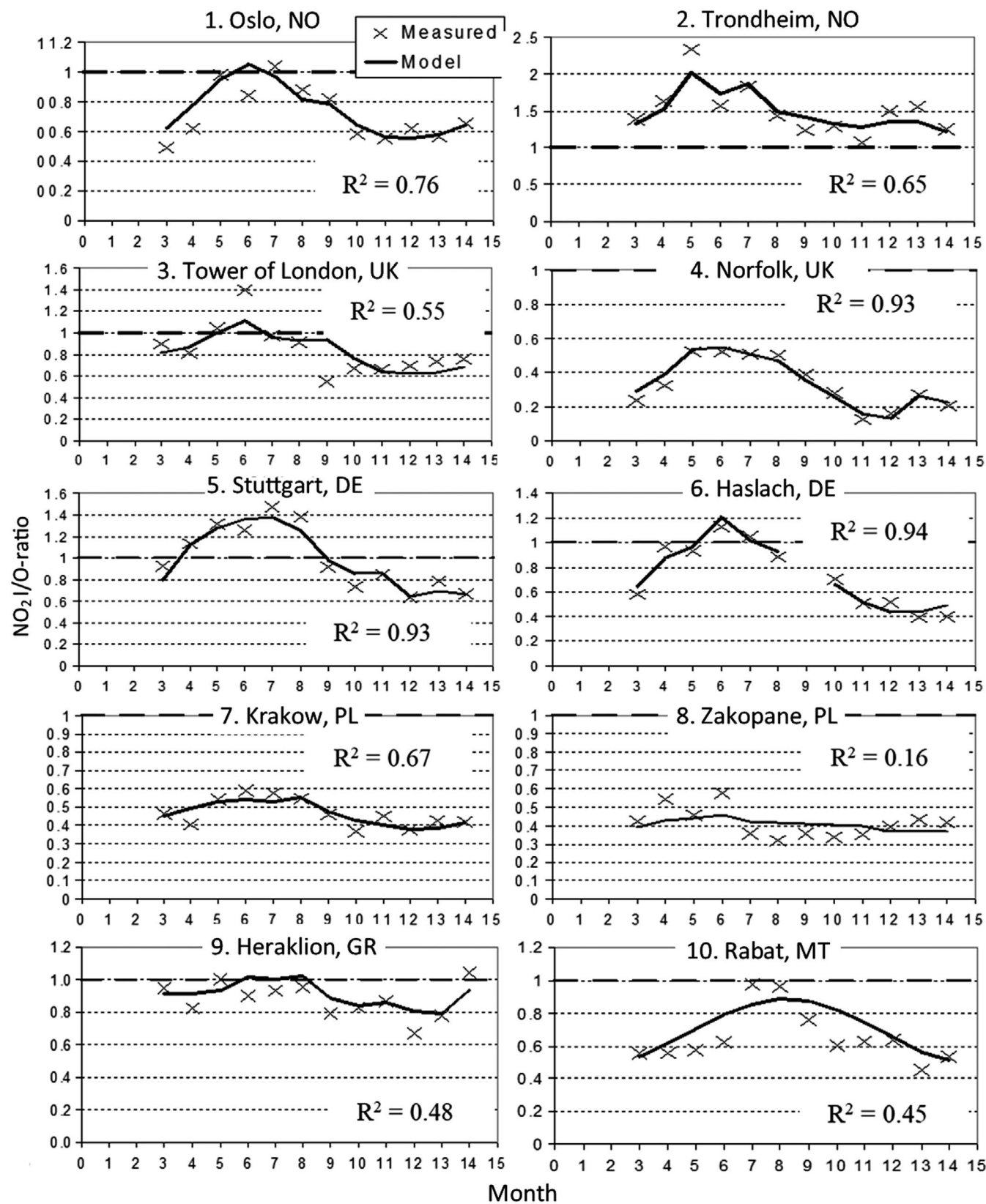


FIGURE 2 Measured and modelled monthly indoor to outdoor NO<sub>2</sub> I/O ratios from March 2004 to March 2005 in 10 European museums

same region (Germany), Haslach, near equal indoor and outdoor concentrations of NO<sub>2</sub> were observed during the summer. The observations in these two museums (nos. 5 and 6) will be discussed in some

more detail together with the other sites to understand the modelling parameter fit and in the final Discussion. The annual monthly average O<sub>3</sub> indoor and outdoor measured values are given in Table 2.

TABLE 2 Annual average monthly O concentrations (ppb)

Site no:	1	2	3	4	5	6	7	8	9	10
O <sub>3</sub> (i)	18.1	25.6	13.4	22.0	15.8	17.4	14.3	18.6	31.1	31.2
O <sub>3</sub> (o)	1.0	5.7	3.6	1.0	2.5	4.5	0.6	2.2	9.5	3.2
O <sub>3</sub> I/O	0.05	0.22	0.27	0.05	0.16	0.26	0.04	0.12	0.31	0.10

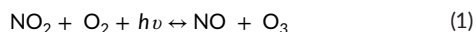
The average annual O<sub>3</sub> I/O ratio over all the sites was found to be 0.16 (from Table 2).

A weak positive single parameter correlation ( $ax + b$ ,  $R^2$ ) was observed over all the sites and months for the outdoor ( $a = 5$ ,  $R^2 = 0.07$ ) and for the indoor ( $a = 2$ ,  $R^2 = 0.03$ ) monthly temperatures, and the NO<sub>2</sub> I/O ratio, which could be expected from the dependence of the annual variation in the NO<sub>2</sub> I/O ratios on the season seen in Figure 2. No significant single parameter correlations were, however, observed between the monthly outdoor or indoor temperatures or RHs and the NO<sub>2</sub> I/O ratios. Thus, the temperature and humidity variations seemed not to be major factors in explaining the annual variations in the NO<sub>2</sub> I/O ratios.

## 4 | MODELLING

### 4.1 | Model derivation and model fitting

A steady-state NO<sub>2</sub> I/O model that included the effect of outdoor photolysis was developed and simplified to be applied with the available mean monthly experimental measurement values. By describing (consecutive) steady states such a model will not replicate the dynamic reactivity that will be important for the concentration changes and values on short-time scales (hours). It will typically not well replicate concentration peaks or accumulated changes in long duration monotonous trends. The main influences on the NO<sub>2</sub> I/O ratios in a situation without indoor NO emissions can be described as follows: The higher the NO<sub>2</sub> ventilation from the outdoor is, and the (possible) indoor NO<sub>2</sub> emissions are, the higher NO<sub>2</sub> I/O ratios will be. The higher the deposition velocity of NO<sub>2</sub> to indoor surfaces (e.g.<sup>55-58</sup>), and the room surface area to volume (A/V) ratios, are, the lower NO<sub>2</sub> I/O ratios will be. In addition, one needs to consider the effects of homogeneous reactions.<sup>10</sup> The reversible reaction involving photolysis of NO<sub>2</sub>, to NO and O<sub>3</sub> is that which mainly influences indoor NO<sub>2</sub> concentrations<sup>1</sup>:



where  $h$  is Planck's constant, and  $\nu$  is the frequency of light at wavelengths from 202 to 422 nm. This reaction moves toward the right outdoors, where NO<sub>2</sub> is split to NO and O<sub>3</sub> by sunlight, and to the left indoors, where there is much less light.<sup>10,59,60</sup>

Ozone can also react with NO<sub>2</sub> to generate the nitrate radical (NO<sub>3</sub>·) which can react further to nitric acid. The second order rate constant of this reaction is, however, much slower than that of the reaction of O<sub>3</sub> with NO (0.0028 ppb<sup>-1</sup> h<sup>-1</sup> as compared to 1.6 ppb<sup>-1</sup> h<sup>-1</sup>

at 25°C) and it is "not expected to greatly influence the indoor concentrations of either NO<sub>2</sub> or O<sub>3</sub>."<sup>1</sup> Nazaroff and Weschler<sup>1</sup> further reported that due to the high rate of formation of NO<sub>2</sub> by reaction (1), NO and O<sub>3</sub> will usually not only be simultaneously present indoors at levels above 5 ppb, but also that the I/O ratios of NO tend to be close to unity. This is likely to be the case if near all the outdoor NO or O<sub>3</sub> is consumed in their rapid reaction before ventilation to the indoors. As can be the case centrally in cities with the near-total consumption of O<sub>3</sub> by surplus NO from traffic emissions or oppositely the near-total consumption of the remaining NO by surplus O<sub>3</sub> some distance away from the traffic emissions. In such situations, a typical "urban tropospheric ozone hole" is formed in the center of cities, such as for example in London.<sup>61</sup> The ventilation to the indoors of either O<sub>3</sub> or NO will then be low, and the Equation (1) equilibrium will have little influence on the indoor concentrations.

The indoor reaction of O<sub>3</sub> with NO is usually faster than other removal processes and thus has the potential to affect indoor concentrations, as is shown by the following examples: If an NO concentration of 5 ppb is ventilated to the indoors in the presence of O<sub>3</sub>, the indoor removal rate of O<sub>3</sub> will be 7.9 h<sup>-1</sup>. This is near a magnitude higher than a typical natural ventilation rate of ~1 h<sup>-1</sup> and higher than that expected of the deposition of O<sub>3</sub> to the surfaces in a medium size room. For a typical deposition velocity of O<sub>3</sub> of 1.8 m h<sup>-1</sup> ( $5 \times 10^{-4} \text{ m s}^{-1}$ )<sup>12,57,62,63</sup> and room surface area to volume (A/V) of unity (for example a room of dimensions ≈ 10\*10\*3.5 m) the deposition rate would be 1.8 h<sup>-1</sup>.

The reaction between NO and O<sub>3</sub> will, because of its high rate, typically take place in a smaller volume than the whole room and at higher concentrations of the gases than the average (measured) room concentrations (see also Section 4.3). This "problem" was avoided by deriving a model with only the outdoor concentrations as input. If mainly O<sub>3</sub> and NO<sub>2</sub> is ventilated to the indoors, then, obviously, the situation would be different with expected smaller gradients.

The model expressions for the NO<sub>2</sub> I/O ratio were derived based on the fundamental Equation (1), then with input from the below Equations (2), (4) and (6) that describe the rate of formation of indoor NO<sub>2</sub>, NO, and O<sub>3</sub>, and Equation (5) that describe the rate of formation of outdoor NO. From Equation (1) and the indoor air exchange rate with the outdoors, the change in the indoor concentration of NO<sub>2</sub> is given by:

$$\frac{d\text{NO}_2(i)}{dt} = \lambda \cdot \text{NO}_2(o) - \lambda \cdot \text{NO}_2(i) - \frac{A}{V} \cdot v_{d,\text{NO}_2} \cdot \text{NO}_2(i) + k \cdot \text{O}_3(i) \cdot \text{NO}(i) \quad (2)$$

where NO<sub>2</sub>(i), NO(i), and O<sub>3</sub>(i) are the indoor concentrations of NO<sub>2</sub>, NO, and O<sub>3</sub> (ppb), NO<sub>2</sub>(o) is the outdoor concentration of NO<sub>2</sub> (ppb),

$v_{d,NO_2}$  is the indoor mean deposition velocity of  $NO_2$  ( $m\ s^{-1}$ ),  $k$  is the rate constant for the reaction of  $O_3$  with  $NO$  ( $=4.43 \cdot 10^{-4}\ ppb^{-1}\ s^{-1}$  at  $25^\circ C$ ),  $\lambda$  is the air exchange rate ( $s^{-1}$ ),  $A$  is the room surface area ( $m^2$ ), and  $V$  is the room volume ( $m^3$ ). Equation (2) assumes that there is no indoor photolysis of  $NO_2$  to  $NO$ . Nearly all the  $NO_2$  photolysis happens due to UV radiation (over 90% by radiation between 300 and 370 nm and not by radiation over 420 nm<sup>60</sup>). In line with Fiazdomor<sup>64</sup> and based on previous studies, Carslaw<sup>5</sup> reports that the attenuation of UV light from outdoor to indoor is typically about 0.03. She further refers to the modelling work of Nazaroff and Cass<sup>6</sup> that showed an increase in indoor from outdoor  $NO_2$  (of 3%) when the indoor visible and UV light fluxes were 0.7% and 0.15% of outdoors. It is a general aim of museums to keep low light and especially UV levels to prevent damage to objects. The day maximum annual average visible, and UV light intensities measured in the museums of 200 lux in Blicling Hall and 15  $mW\ m^{-2}$  in the Tower of London (Table 3) were about 0.3% in the winter to 1% in the summer (visible light), and 0.015% (UV light) of the outdoor radiation (of ~17 000 lux in the winter to 67 500 lux in the summer,<sup>65</sup> and 100  $W\ m^{-2}$ <sup>66</sup>). This shows a similar outdoor to indoor visible light attenuation (or alternatively outdoor natural to indoor artificial light intensity) as in the modelling example from Nazaroff and Cass<sup>6</sup> and considerably higher outdoor to indoor UV attenuation in the museums than in that example and reported as typical in the general indoors by Carslaw.<sup>5</sup> At the low UV levels in the museums, there should be little indoor  $NO_2$  photolysis, and as in the example of Nazaroff and Cass<sup>6</sup> an increase in the indoor to outdoor  $NO_2$  concentration could be expected in the summer.

The following derivation assumes that there were no indoor emissions in the museums, of  $NO$  or  $NO_2$  (that can happen from for example gas-fired stoves for heating and cooking, cellulose nitrate films or wool textiles), of  $O_3$  (from for example photocopiers) or of terpenes or other VOC (volatile organic compounds, from for example plants, or chemical solvents) that react with  $O_3$  at a high rate. If needed a term for indoor emissions or homogeneous production of  $NO_2$  by another route than Equation (1) could be added to the right side of Equation (2). An expression for the  $NO_2$  I/O ratio in the steady state was derived from Equation (2) to give:

$$\frac{NO_2(i)}{NO_2(o)} = \frac{\lambda + [kO_3 \cdot (i) \cdot NO(i)] / NO_2(o)}{\lambda + \frac{A}{V} \cdot v_{d,NO_2}} \quad (3)$$

The interest was now to obtain an expression for the  $NO_2$  I/O ratio with the outdoor pollution (the outdoor concentrations of  $NO_2$  and  $O_3$ , and the outdoor emission rate of  $NO$ ) and indoor building parameters (the room volume and surface area, and the deposition velocities of  $NO_2$  and  $O_3$  to the room surfaces) as input. This was achieved by the following derivation of expressions for  $O_3(i)$  and  $NO(i)$  from these parameters, to be input in Equation (3).

The change in the concentration of  $NO$  in the indoor air was calculated as:

$$\frac{dNO(i)}{dt} = \lambda \cdot NO(o) - \lambda \cdot NO(i) - k \cdot O_3(i) \cdot NO(i) \quad (4)$$

where  $NO(o)$  is the outdoor concentration of  $NO$  (ppb). The indoor deposition velocity of  $NO$  was set to 0.<sup>1,4</sup> In the absence of  $NO$  data, as input for  $NO(o)$  in the steady-state solution of Equation (4) (see Equation (7) below), the change in the concentration of  $NO$  in outdoor air was calculated as:

$$\frac{dNO(o)}{dt} = -k \cdot O_3(o) \cdot NO(o) + j \cdot NO_2(o) + e \quad (5)$$

where  $O_3(o)$  is the outdoor concentration of  $O_3$  (ppb),  $j$  is the photolysis rate constant for  $NO_2$  ( $s^{-1}$ ), and  $e$  is the outdoor emission rate of  $NO$  (ppb  $s^{-1}$ ). Finally, the change in the concentration of  $O_3$  in indoor air was calculated as:

$$\frac{dO_3(i)}{dt} = \lambda \cdot O_3(o) - \lambda \cdot O_3(i) - k \cdot O_3(i) \cdot NO(i) - \frac{A}{V} \cdot v_{d,O_3} \cdot O_3(i) \quad (6)$$

where  $v_d(O_3)$  is the indoor mean deposition velocity of  $O_3$  ( $m\ s^{-1}$ ). For a steady-state situation,  $NO(i)$ ,  $NO(o)$ , and  $O_3(i)$  were then calculated from Equations (4), (5), and (6) to give, respectively, Equations (7), (8), and (9):

$$NO(i) = \frac{\lambda}{\lambda + k \cdot O_3(i)} NO(o) \quad (7)$$

$$NO(o) = \frac{j \cdot NO_2(o) + e}{k \cdot O_3(o)} \quad (8)$$

$$O_3(i) = \frac{\lambda \cdot O_3(o)}{\lambda + k \cdot NO(i) + \frac{A}{V} \cdot v_{d,O_3}} \quad (9)$$

A new expression for  $NO(i)$  was then obtained by substituting  $NO(o)$  and  $O_3(i)$  in Equation (7) with the expressions for these parameters given by Equations (8) and (9), and then solve as a second order polynomial to obtain:

$$NO(i) = \frac{-B + (B^2 - 4AC)^{-0.5}}{2A} \quad (10)$$

with

$$A = k \cdot \lambda \quad (11)$$

$$B = \lambda^2 + k \cdot \lambda \cdot O_3(o) + \lambda \cdot v_{d,O_3} \cdot \frac{A}{V} - \lambda \left( \frac{j \cdot NO_2(o) + e}{O_3(o)} \right) \quad (12)$$

$$C = \left( \lambda^2 + \lambda \cdot v_{d,O_3} \cdot \frac{A}{V} \right) \left( \frac{j \cdot NO_2(o) + e}{k \cdot O_3(o)} \right) \quad (13)$$

The expression for  $O_3(i)$  given by Equation (9) and that for  $NO(i)$  given by Equations (10) to (13), were then inserted for these parameters in Equation (3) to obtain the needed expression for the  $NO_2$  I/O ratio. The outdoor emission rate of  $NO$ ,  $e$ , given as concentration per time unit, was interpreted here as the contribution

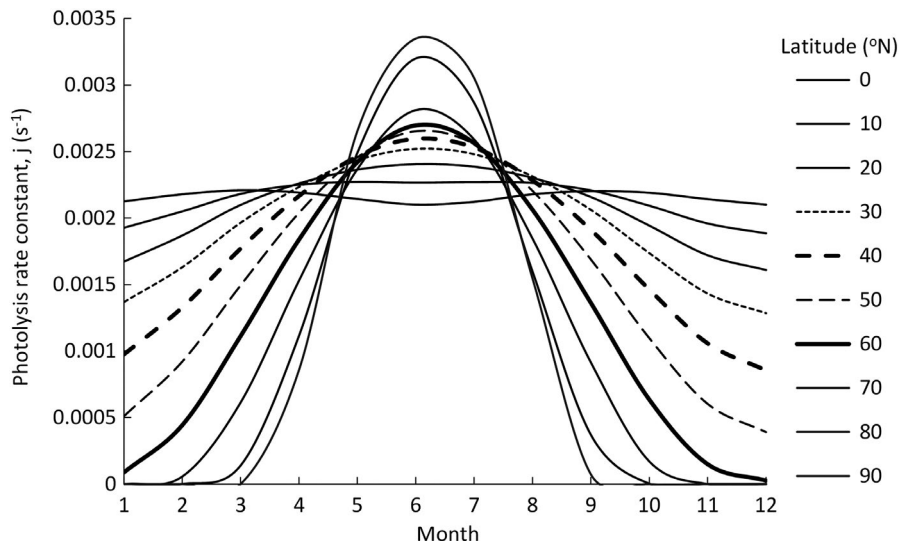
TABLE 3 The model, Equation (14) best fitting parameter values in the 10 European museums

Site no.	Measurements		Parameter boundaries						Combined evaluation parameter $(e \times x^2)/(A/V \times v_d \text{NO}_2)$
	Visible light (Lux)	UV ( $\text{W m}^{-2}$ )	Room A/V ( $\text{m}^{-1}$ )	Model parameters		Min = 0, max = 1			
				$\lambda$ ( $\text{h}^{-1}$ ), modelled ventilation	$\lambda$ ( $\text{h}^{-1}$ ), description from museums	$v_d \text{NO}_2$ ( $\text{m s}^{-1}$ )	e (ppb $\text{s}^{-1}$ )	x	
1	2.0	0	1.0	1.5	Natural	0.0011	0.25	0.18	7.4
2	0.4	0	0.5	10	$\sim 4 \text{ h}^{-1}$ during opening hours	0.00036	0.25	0.15	<b>31</b>
3	120	15	0.6	2.2	Natural, very considerable	0.0016	0.040	0.45	<b>3.9</b>
4	200	5	0.8	0.28	Natural, barely noticeable to noticeable	0.0092	0.0053	0.96	0.67
5	21	0	0.5	0.10	Barely noticeable	0.010	0.25	0.58	<b>17</b>
6	6.5	0	3.6	0.82	Barely to easily noticeable	0.00023	0.010	0.42	2.1
7	16	0.1	1.1	6.8	Natural	0.0032	0.0026	0.61	0.27
8	12	0	1.5	6.8	Natural	0.0028	0.25	0.13	1.0
9	140	0.7	1.3	9.4	Mechanical	0.0021	0.25	0.25	<b>5.7</b>
10	23	3	1.1	0.12	Natural, very still air	0.000091	0	0.16	0

Note: The hatched horizontal lines distinguish between the two museums in each of the five European regions. The bold figures represent the highest combined evaluation parameter value of the two museums in each region. A ranking seemed not meaningful between Krakow (no. 7) and Zakopane (no. 8) due to the low  $R^2$  in Zakopane (Figure 2).



**FIGURE 3** Mean monthly photolysis rate constant for the outdoors splitting of the NO<sub>2</sub> molecule dependent on month and latitude, at 50% cloud cover



of outdoor emissions of NO to the concentration of NO at the air intake to the building. In the modelling, the NO emission rate was set to be constant through the year and contribute to the varying outdoor NO concentrations by Equation (8). It was beyond this work to collect traffic counts representative for the emissions at the study sites. However, some reports show little monthly variations in Europe. Statistical evaluations from Poland<sup>67</sup> showed that month of the year was of little importance in explaining seasonal road traffic variations. Measurements of real-time traffic flows in Athens, Greece from 1997 to 1999 showed no monthly variation in 10 months, but somewhat lower counts in July and August<sup>68</sup> (see also Discussion). In other modelling cases, it may be more practical to use NO concentrations, from for example measurements, as input directly, and thus simply substitute Equation (8) and the similar last terms in Equation (12) and (13) with “NO(o).”

A model simplification was then derived to be used with the available monthly mean values for the outdoor concentrations of NO<sub>2</sub>. Instead of the, supposedly more physically correct, derivation of NO(*i*) and O<sub>3</sub>(*i*) described above as input in Equation (3), the I/O concentrations of NO and O<sub>3</sub> (NO(*i*)/NO(*o*) and O<sub>3</sub>(*i*)/O<sub>3</sub>(*o*)) were in the simplification assumed to be a fraction, *x*, being present in a steady state through the year. The value of this fraction should be interpreted as the root product ( $x_1 \times x_2$ )<sup>0.5</sup> of the average annual I/O ratio *x*<sub>1</sub> of O<sub>3</sub> and *x*<sub>2</sub> of NO. From the literature, it seems that the I/O ratio of O<sub>3</sub> is commonly about 0.5<sup>19</sup> and of NO closer to 1,<sup>1</sup> which would give a single parameter value of *x* = 0.7. The overall annual average O<sub>3</sub> I/O ratio measured at the sites in this work was 0.16 (Table 2), which would with an NO I/O ratio of 1 give a value of *x* = 0.4. With reaction of NO indoors to an NO I/O ratio < 1, *x* would be lower. By multiplying Equation (8) with *k* × O<sub>3</sub>(*o*) and then dividing the numerator and denominator of the fraction in the numerator of Equation (3) ([kO<sub>3</sub>(*i*) × NO(*i*)]/NO<sub>2</sub>(*o*)), with respectively, the left and right side of this developed Equation (8), and then substituting for the NO I/O- and O<sub>3</sub> I/O-concentration fractions their assumed equal ratios, *x*, the model simplification was obtained as:

$$\frac{\text{NO}_2(i)}{\text{NO}_2(o)} = \frac{\lambda + x^2 \cdot \left( j + \frac{e}{\text{NO}_2(o)} \right)}{\lambda + \frac{A}{V} \cdot v_{d,\text{NO}_2}} \quad (14)$$

The temperature-dependent NO + O<sub>3</sub> rate constant, *k* (Equation (2)), does not appear in Equation (14). The temperature dependence of the NO<sub>2</sub> photolysis rate is slight in the ambient temperature ranges of the 10 museums.<sup>60</sup> If the emission rate, *e*, in the Equation (14) is expressed by calculation from Equation (8), then Equation (14) is equal to Equation (3), only with *x*O<sub>3</sub>(*o*) and *x*NO(*o*) substituted for O<sub>3</sub>(*i*) and NO(*i*) in Equation (3). This simple formula, Equation (14), had the advantage that there was no need for measured values for, or complicated modelling of, the indoor concentrations of O<sub>3</sub>. The procedure for the calculation of the photolysis rate, *j*, of NO<sub>2</sub>, was adopted from the EMEP Unified model<sup>69,70</sup>:(22). The calculation was made from the general expressions, and coefficients for the NO<sub>2</sub> photolysis, in<sup>70</sup>:(22) for every day and hour of the year for each 10th degree of latitude from the Equator (0°) to the North Pole (90°). A cloud cover of 50% through the year was used for all the sites except Malta and Crete where a cloud cover of 30% was used, based on rough annual averages<sup>71-73</sup>. Figure 3 shows the latitude-dependent mean monthly averaged values for the photolysis rate constant for the O<sub>3</sub> + NO reaction, with 50% cloud cover, that can be used as input in Equations (14), and (15), to avoid lengthy calculations of this.

From Equation (14), it can be observed that for a case when the outdoor photolysis of NO<sub>2</sub> is the only source of indoor NO, and there is thus no ventilation from outdoor of directly emitted NO (*e* = 0), or indoor direct emissions of NO, then the concentration of NO<sub>2</sub> indoors can still be larger than outdoors. This will be the case when the indoor formation rate of NO<sub>2</sub> from NO and O<sub>3</sub> (by Equation (1) and given in Equation (14) as the multiple of the indoor to outdoor fractions of NO and O<sub>3</sub> and the photolysis rate, *x*<sup>2</sup>*j*), is larger than its deposition rate to the indoor surfaces ( $A/V \times v_{d,\text{NO}_2}$ ). Thus, the chance for an NO<sub>2</sub> I/O ratio > 1 increases in the summer, except close to the equator, and more so at higher latitudes (Figure 3).

The model fitting to the annual  $\text{NO}_2$  I/O values at the 10 museums was performed with Equation (14) and was shown in Figure 2 with the experimental measurements. Mean monthly outdoor  $\text{NO}_2$  concentrations and the calculated mean monthly photolysis rates in a situation with 50% cloud cover (from Figure 3), or 30% cloud cover for the sites in Crete (No. 9) and Malta (No. 10), were used. The other parameters in Equation (14) were assumed constant throughout the year and their values found from the modelling. Maximum and minimum allowed model parameter boundary values (Table 3) were set to avoid modelling to unreasonable continuously increasing values with infinitesimal improvement in the fitting. The low boundary was set to zero, or to a "low" value where this was needed to obtain a result from Equation 14 (of the ventilation rate, Table 3). The high boundary was set to a value in the high range of what was thought realistic for any site, compared to reported values. Thus, it was assumed that a ventilation rate above  $10 \text{ h}^{-1}$ , a deposition velocity of  $\text{NO}_2$  above  $0.01 \text{ m s}^{-1}$ ,<sup>57</sup> and an NO emission rate ( $e$ ) over 0.25 to be unrealistic (Table 3).  $e = 0.25$  represents a mean monthly NO concentration of 34 ppb by Equation (8) when assuming a photolysis rate of 0.0026 (Figure 4), or of 47 ppb mid-summer (July 1st) in Madrid, Spain (see below), and equal  $\text{NO}_2$  and  $\text{O}_3$  concentrations of 20 ppb. The model fitting was performed with a least-squares multiple parameter nonlinear regression method in SPSS<sup>1</sup>. The parameter values were from the start of the manual modelling procedure set to the mid-point within their boundary ranges (see Table 3). The parameter values were then changed, consecutively between the parameters, and iteratively one small step at a time, until the apparent best possible fit and  $R^2$  was achieved. The procedure was repeated several times with some changing of the start values and orders of change in values of the parameters, to be confident about the solutions. In practice, the optimal (largest possible)  $R^2$  was typically obtained by doing a few (3–4) initial rounds of iterations with initial larger changes in the parameter values to investigate the sensitivity, then with fine tuning with minor changes to obtain the maximum  $R^2$ .

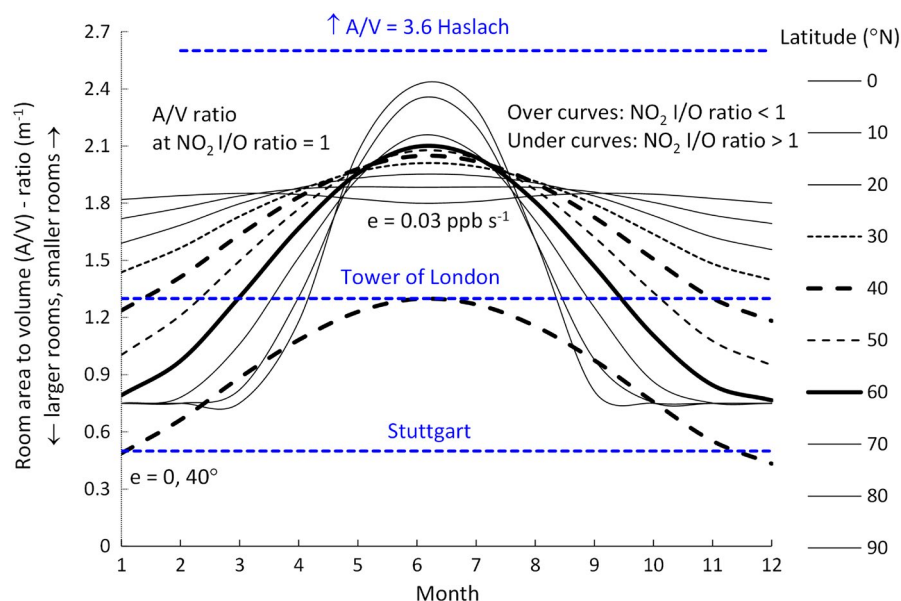
Figure 2 shows that Equation (14) could reasonably simulate the annual variation in the  $\text{NO}_2$  I/O ratio, except in Zakopane where the  $R^2$  was low. The model fit was quite close for Blickling Hall in Norfolk, UK (no. 4) and the two German museums in Stuttgart and Haslach (nos. 5 and 6). Table 3 gives the parameter values from the modelling.

Although the results from the manual iterations seemed convincing in finding the best possible fits, it was realized that this method might not guarantee the testing of all possible parameter value combinations and full randomization of the input. With the four independent variables ( $\lambda$ ,  $v_{\text{dNO}_2}$ ,  $e$ , and  $x$ ) combined in Equation (14) and, additionally the ill-defined A/V ratios it was suspected that the modelling might not result in parameter values that could be simply explained by the observed site characteristics (Table S1 and Table 3). It was expected that interpretation by the combined equation parameters:  $x^2 \times e$ , describing the contribution of the outdoor emission of NO and the I/O ratios of NO and  $\text{O}_3$  to the indoor  $\text{NO}_2$ , and  $A/V \times v_{\text{dNO}_2}$  describing the heterogeneous indoor removal of  $\text{NO}_2$ , might be more realistic, although it would give less specific information. This is not so surprising as the (non-measured) individual independent parameters are in direct combination in Equation (14), and thus not clearly distinguishable in the modelling, and also, as this combined parameter start to resemble the full model expression in Equation (14). It can be observed in Table 3 that the combined parameter distinguishes roughly between the urban and more polluted sites, and rural and less polluted sites.

## 4.2 | Model evaluation and sensitivity

The expression for the A/V ratio giving an  $\text{NO}_2$  I/O ratio equal to 1 can be derived from Equation (14) to be:

$$\frac{A}{V} = \frac{x^2 \left( j + \frac{e}{\text{NO}_2(o)} \right)}{v_{\text{dNO}_2}} \quad (15)$$



**FIGURE 4** Room size, given by the room surface area to volume (A/V) where an  $\text{NO}_2$  I/O ratio = 1 is expected, without ( $e = 0$ , as a reference at latitude  $40^\circ\text{N}$ ) and with ( $e = 0.03 \text{ ppb s}^{-1}$ ) close to the building outdoor NO emissions, depending on month of the year and latitude. ( $\text{NO}_2(o) = 20 \text{ ppb}$ ,  $v_{\text{dNO}_2} = 5 \times 10^{-4} \text{ m s}^{-1}$ ,  $x = 0.5$ ). The room A/V ratios in some of the museums are given

Figure 4 shows the room sizes, given by the room surface area to volume ( $A/V$ ) from Equation (15), where an  $\text{NO}_2$  I/O ratio of unity is expected, depending on the month of the year and latitude, as given by the mean monthly photolysis rates of  $\text{NO}_2$ ,  $j$ , with a 50% cloud cover from Figure 3 and with outdoor  $\text{NO}$  emissions,  $e$ , of  $0.03 \text{ ppb s}^{-1}$  close to the building air intake. With an  $\text{NO}$  emission rate of  $0.03 \text{ ppb s}^{-1}$  the outdoor mean monthly  $\text{NO}$  concentration would, by Equation (8) and assuming equal  $\text{NO}_2$  and  $\text{O}_3$  concentrations of  $20 \text{ ppb}$ , be about  $10 \text{ ppb}$  in the summer, but varying with the photolysis rate through the year and depending on latitude, from  $3.4$  to  $11 \text{ ppb}$ . A mean annual average  $\text{NO}_2$  of  $20 \text{ ppb}$  was measured at the 10 museums.  $\text{O}_3$  concentrations can typically be below  $20 \text{ ppb}$  in city centers and above  $20 \text{ ppb}$  away from traffic emissions<sup>(61)</sup>.  $\text{NO}$  concentrations from  $3.4$  to  $11 \text{ ppb}$  represent typical annual measurements at stations in Europe.<sup>24</sup> The  $\text{NO}_2$  deposition velocity to the indoor surfaces was set to  $5 \times 10^{-4} \text{ m s}^{-1}$ ,<sup>57</sup> and the multiple of the I/O ratios of  $\text{NO}$  and  $\text{O}_3$  ( $x^2$ ) to  $0.25$  ( $x = 0.5$ ) like the mean of the modelling results in Table 3 when excluding the deviating sites, no 2, 8, and 10 (see Experimental and sites), which is in the range of reported values and complemented with the  $\text{O}_3$  measurements in this work (see Modelling).

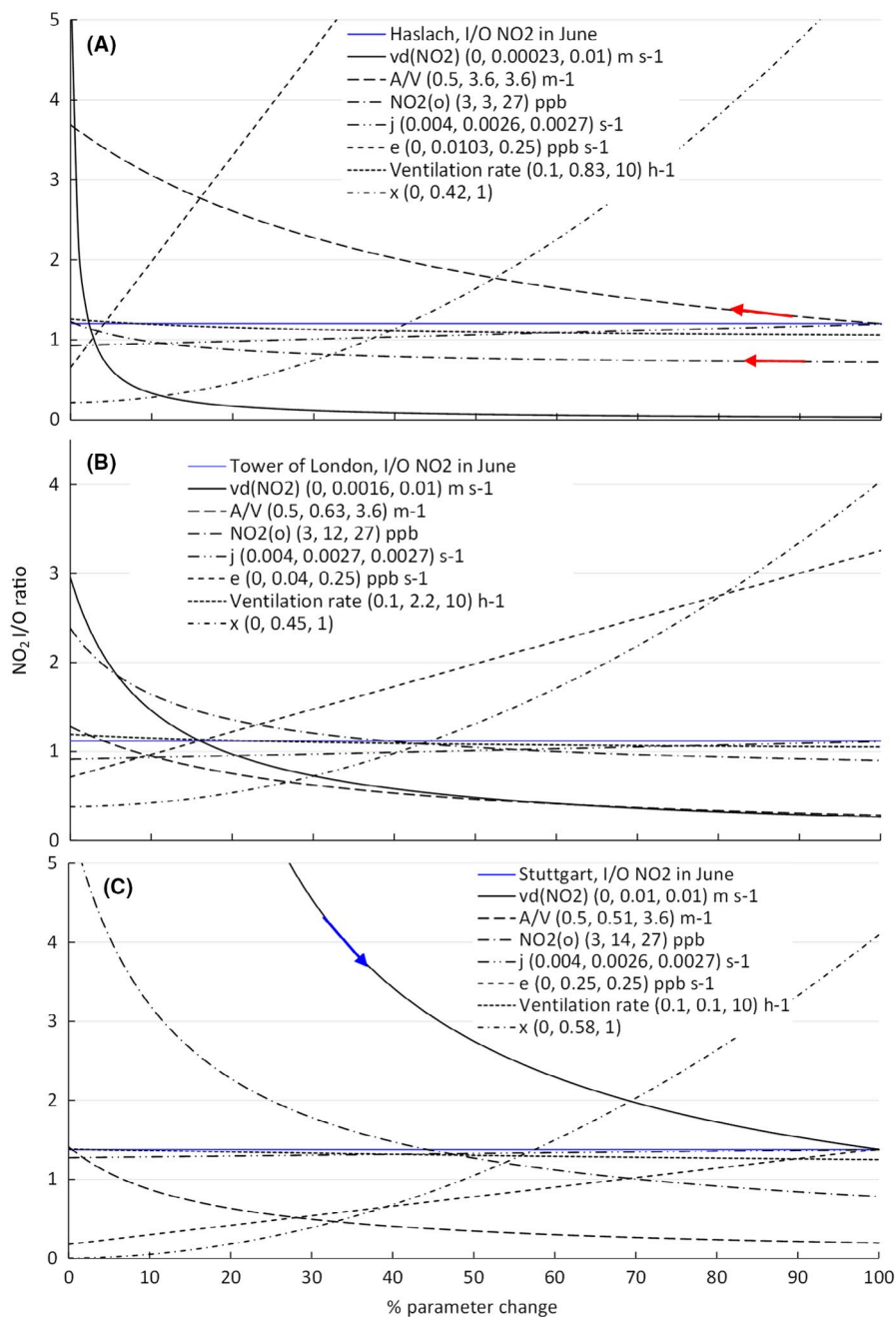
Rooms positioned under the curves in Figure 4, that is, with a smaller  $A/V$  ratio and thus being larger, are expected to have  $\text{NO}_2$  I/O ratios larger than unity. As  $A/V$  ratios are usually, due to the roughness of room surfaces, furniture, installations, and other features, larger than those calculated from the nominal room dimensions, rooms usually need to be larger than indicated by the nominal  $A/V$  ratios for  $\text{NO}_2$  I/O ratios above unity to be observed. Indoor deposition velocities are expected to vary more than one magnitude depending on the surface material, humidity, and temperature.<sup>57</sup> An  $\text{NO}_2$  deposition velocity of  $5 \times 10^{-4} \text{ m s}^{-1}$  is in the upper range of values measured for common room surface materials in the laboratory,<sup>57</sup> and could include some measure of the effect of the typical more complex room features. As an example, for a case as described by Figure 4 at  $40^\circ\text{N}$  (that could be in Madrid, Spain), and with an outdoor  $\text{NO}$  emission of  $0.03 \text{ ppb s}^{-1}$ , it could be expected that mid-summer, as an average for June and July, then for rooms with  $A/V$  ratios less than  $\sim 2 \text{ m}^{-1}$  (i.e., of, unfurnished, dimensions larger than about  $4 \times 4 \times 2 \text{ m}$ ) the indoor concentration of  $\text{NO}_2$  will be larger than the outdoor concentration. Around July 1st the photolysis rate would be at its largest in Madrid:  $j = 8.14 \times 10^{-3} \text{ s}^{-1}$ .<sup>60</sup> A larger indoor than outdoor concentration is then expected in volumes larger than  $1.2 \text{ m}^3$ , and thus in practice nearly always. In other seasons the rooms would need to be larger for the  $\text{NO}_2$  I/O ratio to be above unity at the otherwise same conditions. With a higher photolysis rate than in Madrid, which could be expected further north in the summer or further south in the other seasons, and otherwise similar conditions as laid out above, higher  $\text{NO}_2$  I/O ratios could be expected in smaller rooms than in the Madrid example. With increasing infiltration of  $\text{NO}$  and  $\text{O}_3$  (to  $x > 0.5$ ) the sizes of rooms where an  $\text{NO}_2$  I/O ratio above unity is expected is decreasing even more quickly, to an extent that the infiltration becomes relatively more important for the  $\text{NO}_2$  I/O ratio than the latitude or time of year (see Figure S1).

From the room  $A/V$  ratios (Figure 4) a much larger difference in the  $\text{NO}_2$  I/O ratios between the Stuttgart and Haslach sites than observed in Figure 2 might be expected, with ratios always above unity in Stuttgart and never above unity in Haslach. In comparison for three of the locations with an  $A/V$  ratio of between 1 and 1.5 (no. 3, Tower of London in Figure 4, and nos. 1 and 9 (Table 3), the prediction from Equation (14) of  $\text{NO}_2$  I/O ratios above unity in the summer (Figure 2) seems reasonably correct. Possible reasons for the smaller measured than modelled difference in the  $\text{NO}_2$  I/O ratio between the Stuttgart and Haslach sites can be evaluated through the model (Equation (14)) sensitivity to the input parameters. Figure 5 shows the change in the  $\text{NO}_2$  I/O ratios at the three sites (Stuttgart, Tower of London, and Haslach) estimated to happen by changing the value of each model parameter (Equation (14)) from those measured in June 2004 (the crossing points of each parameter curve with the horizontal line for the  $\text{NO}_2$  I/O ratios).

Figure 5 shows the negative influence on the  $\text{NO}_2$  I/O ratio of the indoor deposition velocity  $v_d(\text{NO}_2)$ , of smaller rooms (higher  $A/V$ ) and of the outdoor  $\text{NO}_2$  concentration, and a positive influence of the other parameters. The  $\text{NO}_2$  I/O ratio is at all the three sites most sensitive to changes in the indoor deposition velocity with a somewhat different ranking of the sensitivities to the parameters between the sites. The figure shows that the measured or most likely separate site deviances from the average modelling conditions, used in Figure 4, would reduce the difference in the I/O ratio between the sites observed in that figure: It may be that the deposition of  $\text{NO}_2$  in the mechanical ventilation system and through the modern building shell in Stuttgart was higher than the average value used in the modelling, which was also indicated by the high modelling results of the deposition velocity in Stuttgart (Table 3); the outdoor  $\text{NO}_2$  concentrations in Haslach were considerably lower ( $\sim 5 \text{ ppb}$ , Figure 1) than the used museums average of  $20 \text{ ppb}$ ; and the larger complex of interconnected rooms in the Haslach museum may have had a lower effective  $A/V$  ratio than  $3.6$ . A change in these directions along the parameter curves in Figure 5 (as visualized with the arrows) would reduce the  $\text{NO}_2$  I/O ratio in Stuttgart and increase it in Haslach, and thus work in the direction of the measurements (as compared to the modelling in Figure 4).

### 4.3 | Limitation of the model and available data

It should be stressed that the steady-state model presented in this paper does not include homogeneous reactions of  $\text{NO}_x$  with other species (than  $\text{O}_3$ ), that were not measured but may have been present and had an influence on the  $\text{NO}_x$  values. The reported monthly averaged data do not describe variations in the indoor concentrations of  $\text{NO}_x$  and  $\text{O}_3$  due to the dynamic reaction between them. For that purpose, time-dependent analytical solutions or, more reasonably, numerical modelling to much more time resolved concentration data (<hourly) would be needed. How well the presented steady-state box modelling would describe data with a different, for example, from hourly to monthly, time resolution is a question of



**FIGURE 5** Sensitivity of the modelled June 2004 NO<sub>2</sub> I/O ratios (by Equation (14)) to the input parameters in (A) Haslach, (B) Tower of London, and (C) Stuttgart. The three values in the brackets are the minimum (0%), the measured values at the sites that were kept constant when varying the other parameters, and maximum values (100%) in the modelling ranges over all the sites (nos. 1 to 10, Table 3), but in the monthly mean variation of  $j$  at the latitude (50° north) of the three sites, and in the NO<sub>2</sub>(o) concentration measured over the three sites (Figure 1). The arrows indicate the measured or likely direction of changes in the given parameter values and resulting NO<sub>2</sub> I/O ratios from the average model values used in the calculations of the curves in Figure 4, for the Stuttgart and Haslach museums (according to Figure 1, NO<sub>2</sub>(o), and Table 3, A/V and  $v_d$ NO<sub>2</sub>)

interest. The parameter values that could be obtained from fitting of time-dependent dynamic models to data with higher time resolution could be different from those obtained in this work and could be expected to be more physically correct.

There is, typically, large fluctuations in the diurnal concentrations of NO<sub>x</sub> and ground level O<sub>3</sub>, especially due to traffic emission cycles.<sup>74</sup> The variations in the outdoor concentrations and rapid reaction between NO and O<sub>3</sub> implies that homogeneous mixing of O<sub>3</sub> and NO will seldom happen in rooms after ventilation to the indoors. Gradients in the indoor concentrations of the gases are expected from inlets to outlets and depending on the air flows and mixing situations. In low ventilation situations, the reaction of O<sub>3</sub> with NO could go to completion close to the inflow of air into a room but depending on the UV light presence and NO<sub>2</sub> photolysis. The reaction

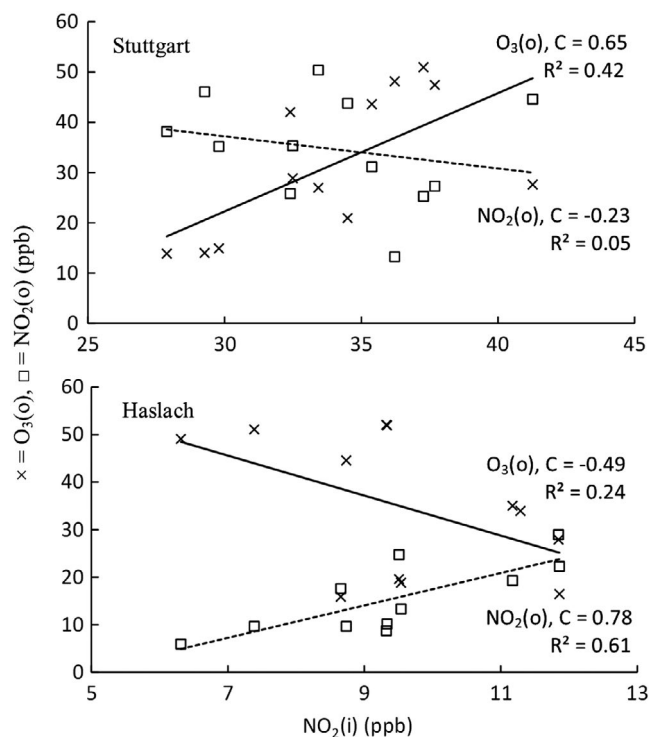
may thus happen in smaller volumes, than the total rooms, and at higher than measured mean indoor room concentrations. This might affect reaction rates and the NO<sub>2</sub> I/O ratios in ways that were not captured by the performed modelling.

Four independent model parameters were not measured and are interdependent (more or less) in the model expression. This situation was expected to result in considerable uncertainty, and there may have been a risk for “overfitting” and obtaining too high explanatory power ( $R^2$ ). Parameter value boundaries were set in the modelling to avoid this. The main reason for the model fit ( $R^2$ ) to the annual trends in Figure 2, seemed to be the similar shape through the year of the curve of the NO<sub>2</sub> photolysis rate as the NO<sub>2</sub> I/O ratios. Fitting to the variations over the year (from the smooth change in the annual trend of the photolysis rate) was then obtained, to a larger or lesser

degree, by varying the other model parameters. Resulting in clearly differing model fit between the museums. Without measured values for these properties in the museums (Table 3) that could be used as input and/or verification, caution was needed in the interpretation of their model values. Much of the experimental variation that could not be explained by the modelling (excluding effects of experimental uncertainty) might be explained by variations through the year in the assumed constant model parameters. Despite such imprecisions, the results seem to substantiate the, often, dominating effect of the outdoor  $\text{NO}_2$  photolysis in giving systematic annual variations in the  $\text{NO}_2$  I/O ratios with higher values in the summer. This seemed to be the case in nine of the 10 investigated museums.

## 5 | DISCUSSION

In all the museums except in Zakopane, higher  $\text{NO}_2$  I/O ratios were measured in the summer than winter, corresponding with the higher outdoor photolysis rates in the summer and thus supporting the hypothesis that the difference in the outdoor to indoor photolysis rate of  $\text{NO}_2$  was a main reason for the observed monthly variations in the I/O  $\text{NO}_2$  ratios over the year. The lower than unity  $\text{NO}_2$  I/O ratios measured through the year in four of the 10 locations (nos. 4, 7, 8, and 10) indicate relatively larger indoor  $\text{NO}_2$  sinks and/or lower ventilation to the indoors of  $\text{NO}_2$ , by the precursors  $\text{NO}$  and  $\text{O}_3$  in these than the other locations. In Trondheim (no. 2), it seemed that more  $\text{NO}_2$  from the close to the air intake chimney emissions were measured indoors than at the outdoors location, which was positioned at some distance from the chimney and lower down on a wall, and that this could explain the high  $\text{NO}_2$  I/O ratios  $> 1$  in the winter. The comparison of the indoor and outdoor  $\text{NO}_2$  and  $\text{O}_3$  concentrations measured in Stuttgart (no. 5) and Haslach (no. 6; Figures 1 and 2) illustrate differences between a modern museum centrally located in a city, close to roads with expected significant  $\text{NO}$  traffic emissions, and a more traditional building in a rural location. A reason for the lower indoor  $\text{O}_3$  and higher  $\text{NO}_2$  I/O values in Stuttgart than Haslach in the summer seemed to be the higher  $\text{NO}$  outdoor emissions in Stuttgart and homogeneous  $\text{NO}_x$ - $\text{O}_3$  chemistry. The  $\text{NO}_2$  concentrations were measured to be considerably higher in Stuttgart than Haslach, and the modelling results (Table 3) supported the expectation of higher outdoor  $\text{NO}$  emissions in Stuttgart. In the winter, the  $\text{NO}_2$  concentration was considerably higher outdoors than indoors at both sites. In the summer, the opposite situation, with considerably higher indoor than outdoor concentrations, was measured in Stuttgart whereas in Haslach the outdoor and indoor  $\text{NO}_2$  concentrations were found to be near similar. In Stuttgart more than Haslach, and especially in the summer, the indoor  $\text{NO}_2$  concentration followed the (pattern of the) variation in the outdoor  $\text{O}_3$  rather than outdoor  $\text{NO}_2$  concentrations, which indicates formation of  $\text{NO}_2$  indoor from  $\text{O}_3$  and  $\text{NO}$  by Equation (1). In Haslach the indoor  $\text{NO}_2$  followed the values and variations of the outdoor  $\text{NO}_2$ , but with lower indoor than outdoor values in the winter months with expected less ventilation. In Stuttgart the indoor  $\text{NO}_2$  did not follow the values and variations



**FIGURE 6** Correlation coefficient (C) and linear trend explanatory power ( $R^2$ ) of the monthly averages of  $\text{NO}_2$  measured indoors (i) with those of  $\text{NO}_2$  and  $\text{O}_3$  measured outdoors (o) through the year in Stuttgart and Haslach

of the outdoor  $\text{NO}_2$ . This is clearly seen in the correlation diagrams for all the months of the year in Figure 6.

The higher outdoor and, more so, indoor  $\text{O}_3$  concentration in Haslach than Stuttgart from February to September support the hypothesis of more indoor  $\text{O}_3$  loss in Stuttgart than Haslach due to reaction with  $\text{NO}$ . It was speculated that some infiltration through a near window, which the museum however informed was always kept closed, might have contributed to the relatively higher  $\text{O}_3$  indoor values in Haslach.

The emission rates of  $\text{NO}$  were found in the modelling (Table 3) to be larger in three of the five regional urban than more rural sites. The two exceptions being the urban sites of Oslo (no. 1) and Krakow (no. 7), as compared to the smaller towns of Trondheim (no. 2) and Zakopane (no. 8; Table 3) both with, seemingly, special emission conditions, as was explained above. The literature<sup>68</sup> indicated that road traffic counts, and then probably  $\text{NO}$  emissions, might in some cases be lower in the summer vacation months (July and August) than other months of the year. If this was the case at the museum sites it would imply less outdoor (Equation (5)) and then indoor (Equation (4))  $\text{NO}$ , a lower  $\text{NO}_2$  I/O ratio (Equation (14) and Figure 6) in the summer, and an expected worse model fit. At the winter sports location of Zakopane, especially, it could be hypothesized that this was a factor. Lower  $\text{NO}_2$  I/O values were observed in Zakopane from July to November, contrary to the model expectations, giving the worst model fit among the museums. A meaningful comparison of the modelling results for the two Polish sites was thus



difficult. One could speculate that during the colder winter than in Krakow, and with the winter sports activities in Zakopane, there was also relatively more NO emissions from solid fuel burning, of coal and wood, and/or from traffic emissions in the winter than summer in Zakopane than Krakow, that reacted indoors with O<sub>3</sub> to NO<sub>2</sub>.

Unfortunately, measurements of the building and/or room *ventilation rates* were not generally available from the sites. The qualitative descriptions of the ventilation, and in one case (Trondheim) a quantification (Table 3), seemed to be in rough accordance with the values obtained from the modelling. A much higher natural ventilation in the Wignacourt Collegiate Museum in Malta in the summer than winter (see Experimental) probably explained the high values of the NO<sub>2</sub> I/O ratio in July and August that the model could not be fit very well. The modelling gave a similar spread in the *deposition velocity of NO<sub>2</sub>* between the museums, as has been measured in the laboratory (~two orders of magnitude), but with an average value about six times higher, 0.003 m s<sup>-1</sup> as compared to 5 × 10<sup>-4</sup> m s<sup>-1</sup>.<sup>57</sup> The measurement data were not sufficient to explain the high values and differences between museums. They might be due to the modelling to a situation with the nominal (smaller than real) room areas, and possibly due to additional deposition happening along the infiltration path of the inflowing air in the museums, through the building shell and in ducts, and in adjoining rooms. It could be suggested that the low deposition velocity in the Wignacourt Collegiate Museum in Malta (no. 10) was related to low ventilation and air flows at that site. The model values of the NO and O<sub>3</sub> I/O ratios, “x” in Equation (14), showed a wide variation between 0 and 1 (Table 3). The mean of x = 0.5 (when excluding the deviating sites, no 2, 8, and 10, see above) seems reasonable, but the data seemed insufficient to explain the variation between the sites.

## 6 | CONCLUSION

The photolysis of NO<sub>2</sub> outdoors and back-reaction of NO and O<sub>3</sub> to NO<sub>2</sub> indoors can result in higher than unity NO<sub>2</sub> I/O ratios in rooms that are sufficiently large for this production to be higher than the heterogeneous loss by surface deposition. This can happen especially on sunny summer days, in urban areas with high NO emissions. The measurements in 10 European museums clearly showed higher NO<sub>2</sub> I/O ratios in the summer than winter and in the urban than more rural sites. A steady-state model of the NO<sub>2</sub> I/O ratio, including the photolysis effect and main indoor sources and sinks of NO<sub>2</sub> were derived. With a fractional (x) reduction in O<sub>3</sub> and NO from the outdoors to the indoors, a reasonable fit to the yearly trend of monthly mean NO<sub>2</sub> I/O ratios was obtained in nine of the 10 museums. The model can be used to approximate (with considerable uncertainty) indoor from outdoor NO<sub>2</sub> mean monthly concentrations and exposure doses that could be compared with recommended levels in museums. It is suggested that the model (Equation (14)) could, generally when other specific information is not available, be used with the average values of x = 0.5, v<sub>d</sub>(NO<sub>2</sub>) ≈ 0.003 m s<sup>-1</sup> found from the modelling of the sites

in this work and with nominal room surface areas. The location-dependent mean monthly photolysis rate, j, at 50% cloud cover could be read from Figure 3. The emission rate of NO which is needed for the estimation can be found from the close to the building outdoor concentrations of NO<sub>2</sub>, O<sub>3</sub>, and NO (by Equation (8)). For outdoor concentrations of NO<sub>2</sub> and O<sub>3</sub> of 20 ppb, and a summer value of NO in Europe of about 10 ppb, a value of the emission of NO of 0.03 ppb s<sup>-1</sup> can be used. The model could in practice provide sufficiently good indications of high indoors, and in the summer sometimes higher than outdoors, NO<sub>2</sub> values that would be a preventive conservation concern. The model and its sensitivity analysis might be equally useful as a tutorial. Measurements are still recommended to obtain certain site values. The photolysis part of the modelling could possibly be added to available I/O gaseous pollution estimation tools for cultural heritage, such as IMPACT.<sup>75,76</sup> Such integration may be needed for the model to be practically applicable in most situations.

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## CONFLICT OF INTEREST

No conflict of interest was declared.

## ORCID

Terje Grøntoft  <https://orcid.org/0000-0002-6200-9460>

## ENDNOTE

<sup>1</sup> At the time of the regression analysis (2006) called «Statistical package for the Social Sciences». Acquired by IBM in 2009 and now called "Statistical Product and Service Solutions".

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#### SUPPORTING INFORMATION

Additional supporting information may be found in the online version of the article at the publisher's website.

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