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Adsorption, thermodynamic, and quantum chemical investigations of an ionic liquid that inhibits corrosion of carbon steel in chloride solutions

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The purpose of this work lies in the use of ionic liquids as corrosion inhibitors due to the difficulty in some oil fields with the solubility of corrosion inhibitors and these materials can be miscible with water and thus provide a solution to such problems in the industry. The second purpose is concerned with the lower toxicity of these compounds compared with the most common corrosion inhibitors. The study covered the corrosion inhibition performance of the ionic liquid 1-butyl-3-methylimidazolium trifluoromethyl sulfonate ([BMIm]TfO) for carbon steel in 3.5% NaCl solutions. The study comprised electrochemical, adsorption, and quantum chemical investigations. The results manifested that [BMIm]TfO can be considered a promising corrosion inhibitor and the inhibition efficacy intensifies as the concentration rises. The observed inhibitive effect can be correlated to the adsorption of the ionic liquid species and the creation of protecting films on the surface. The mode of adsorption follows the Langmuir adsorption isotherm. The polarization results showed that the ionic liquid [BMIm]TfO functions as a mixed inhibitor. Reliance of the corrosion influence on the temperature in the existence and absence of [BMIm]TfO was demonstrated in the temperature range of 303–333 K using polarization data. Activation parameters were determined and discussed. The observed inhibition performance of [BMIm]TfO was correlated with the electronic properties of the ionic liquid using a quantum chemical study.

Corrosion is a serious and extremely costly problem especially in petrochemicals and petroleum production operations^{1,2}. Besides the high potential to employ more advanced corrosion-resistant components, carbon steel tillers are the main fabricated material used for the huge pipeline's construction in the different crude oil processing stages such as extraction, transmission, and storage. Carbon steel pipes have been widely employed in transporting gases and liquids^{3,4}. One of the most aggressive surroundings in petroleum production and oil refining processes is the saline water environment which contains different amounts of dissolved salts, especially sodium chloride^{5,6}. The protective oxide film created on the surface can deteriorate in the existence of chloride ions based on an aggressive environment^{7,8}.

Different corrosion mitigation regimes can be applied to reduce the harmful corrosion impacts. Among the conventional corrosion mitigation techniques, the utilization of eco-friendly inhibitors has advantages such as, e.g., high feasibility, high efficiency, and minimization of the environmental hazards⁹. In recent times, ionic liquids were proven to be effective, eco-friendly inhibitors for the corrosion of different types of metals and alloys in corrosive environments such as basic, acidic, or salty solutions^{10,11}. Due to their bulky structure and the presence of heteroatoms, ionic liquids are regarded as potential corrosion inhibitors¹².

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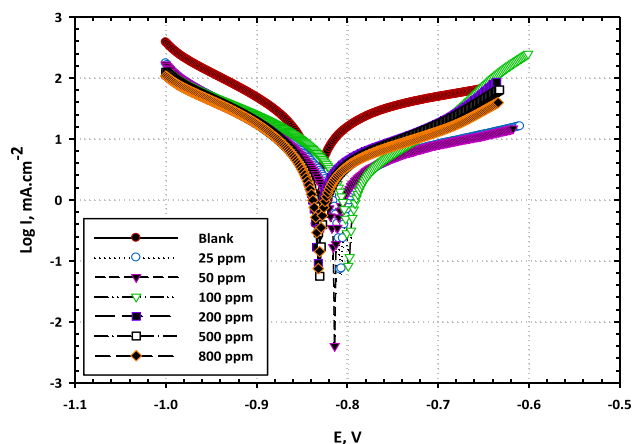


Figure 1. Potentiodynamic polarization curves for the carbon steel in a 3.5% NaCl medium with and without different concentrations of [BMIm]TfO.

Ionic liquids, in general, have a promising corrosion inhibition tendency due to their capacity for the adsorptive contact with the surface, which forms protective layers against corrosive media. In general, the majority of ionic liquids exhibit this tendency. The types of cations and anions present in ionic liquids have a direct bearing on the levels of adsorption and inhibition efficiency that may be achieved with those liquids. In a recent study, we demonstrated that the ionic liquid 1-butyl-1-methylpyrrolidinium trifluoromethyl sulfonate ([BMP] TfO) may serve as a bi-functional inhibitor for both the corrosion of carbon steel in chloride solutions and the growth of bacteria. [BMP]TfO inhibits both types of corrosion¹³. It was also shown that the ionic liquids 1-(2-hydroxyethyl)-3-methylimidazolium chloride and 1-ethyl-3-methylimidazolium chloride are effective corrosion inhibitors and biocides. These findings were published in the journal *Ionic Liquids*¹⁴. It was shown that the integration of the hydroxy group in the imidazolium cation enhances the corrosion inhibition impact¹⁵. In this paper, the corrosion inhibition performance of the ionic liquid [BMIm]TfO for carbon steel in 3.5% NaCl solutions was demonstrated. The study comprised electrochemical, adsorption, and quantum chemical investigations.

Materials and methods

Materials. High purity [BMIm]TfO, was obtained from Io.Li.Tec.Co., Germany, and it was used as received. Carbon steel specimens having dimensions of (5.6 cm L, 2.7 cm W, and 0.5 cm T) were used for the standard procedures of the corrosion measurements. Before use, the steel coupons were abraded with proper emery papers to give a homogeneous surface. An aggressive solution of 3.5% NaCl was prepared as a simulated corrosive environment. Different concentrations of the employed ionic liquid, 25, 50, 100, 200, and 500 ppm, were used, and various temperatures of 303, 313, 323, and 333 K, were applied.

Methods. For the electrochemical measurements, a common cell, fitted with a reference electrode—saturated calomel reference electrode (SCE) a counter electrode (CE), platinum, and the working electrode (WE), carbon, steel, was utilized. All electrochemical tests were performed employing a Volta lab 40 Potentiostat PGZ 301. Polarization experiments were carried out by sweeping the electrode potential at a rate of 2 mV s⁻¹ and recordings the current. All polarization data were fitted using the fitting tools implemented in Volta Master 4 software by Tafel extrapolation method. The frequency range of 100 kHz–0.05 Hz with an amplitude peak of 10 mV using an AC signal was applied for the electrochemical impedance measurements. The impedance curves were fitted using the ZSimpWin3.60 software. For weight loss measurements, rectangular-shaped steel specimens with dimensions of 3 cm × 5 cm × 0.05 cm were used. The immersion time was 6 h in 3.5% NaCl at different temperatures in the absence and presence of different concentrations of [BMIm]TfO.

A scanning electron microscope, JEOL model JSM-53000, was employed for investigating the morphology of the electrodes. The quantum chemical investigations were executed using MP2 functional with a 3–21 G (d,p) basis set. The energies of high occupied molecular orbital (E_{HOMO}) and low unoccupied molecular orbital (E_{LUMO}) were estimated. Furthermore, the energy gap between LUMO and HOMO (ΔE) was determined¹⁶.

Results and discussions

Potentiodynamic polarization. The curves of Fig. 1 show potentiodynamic polarization responses of carbon steel in 3.5% NaCl solutions free and containing different amounts of [BMIm]TfO. The parameters obtained from the polarization curves, corrosion currents and potentials (i_{corr} , E_{corr} , respectively), corrosion rate (CR), inhibition efficiency based on corrosion current density ($EF_{i_{\text{corr}}}$ %), and efficiency based on the corrosion rate (EF_{CR} %), cathodic Tafel slope (b_c), and anodic Tafel slope (b_a) are presented in Table 1. As shown in Fig. 1, the polarization curve recorded in absence of [BMIm]TfO exhibits an active trend as the current steeply rises with sweeping the potential. In addition to the ionic liquid inhibitor, a slight impact was noticed on the cathodic branch of the curve. However, a pronounced effect was recorded on the anodic branch. Both the cathodic and

Concentration	Parameter							
	E_{corr} mV	i_{corr} mA/cm ²	b_a mV/dec	b_c mV/dec	CR $\mu\text{m}/\text{Y}$	θ	EF _{corr} %	EF _{CR} %
3.5% NaCl	- 834	0.016	259	- 131	185			
25 ppm	- 805	0.0069	262	- 147	81	0.568	56.8	56.3
50 ppm	- 813	0.0066	202	- 140	78	0.59	59	57.8
100 ppm	- 798	0.0063	185	- 148	74	0.606	60.6	60
200 ppm	- 833	0.0059	123	- 164	70	0.631	63.1	62.2
500 ppm	- 830	0.0044	384	- 128	52	0.726	72.6	71.8
800 ppm	- 832	0.0042	327	- 202	50	0.75	75	72.9

Table 1. Polarization parameters obtained for carbon steel in 3.5% NaCl-free and containing [BMIm]TfO.

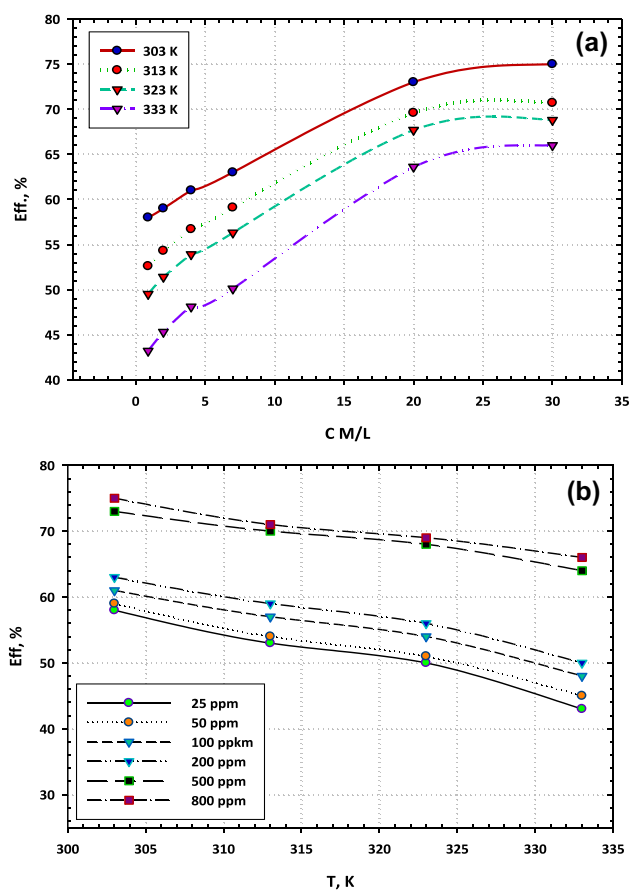


Figure 2. The dependence of the inhibition efficiency of [BMIm]TfO on the corrosion of carbon steel in 3.5% NaCl solutions as a function of (a) temperature and (b) concentration.

anodic curves shift to more negative and more positive potentials, respectively, on the addition of the [BMIm]TfO revealing the inhibiting influence.

As the content of [BMIm]TfO increases, the current density decreases, and subsequently the corrosion rate reduces Table 1. The highest inhibition efficiency was 75% for the inhibitor concentration of 800 ppm. The observed inhibition influence is due to the creation of a protecting layer because of the adsorption of the ionic liquid species on the electrode surface. This layer isolates the surface from the corrosive environment which, in turn, leads to the observed inhibition. The extent of covering the surface (θ) [BMIm]TfO was estimated. The degree of surface coverage rises as the content of [BMIm]TfO in the electrolyte increases. Full coverage of the electrode surface by the ionic liquid species was not reached in the studied concentration range of [BMIm]TfO.

The dependence of the corrosion inhibiting efficacy of [BMIm]TfO on the concentration and temperature was explored. Figure 2a manifests the change in the inhibiting efficiency with the concentration of [BMIm]TfO at various temperatures. As seen, the inhibiting efficacy rises as the [BMIm]TfO concentration increases for all temperatures. Figure 2b displays the dependence of the inhibition efficiency on the temperature of the electrolyte at different concentrations of [BMIm]TfO. It is seen that at one, and the same concentration of [BMIm]TfO, the

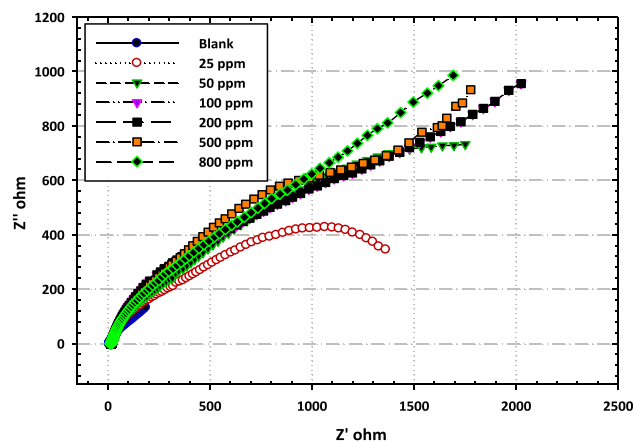


Figure 3. Typical Nyquist plots for the carbon steel in 3.5% NaCl without and with different concentrations of [BMIm]TfO.

Conc	Parameters											
	R_s (ohm cm ²)	Q (S s ⁿ /cm ²) × 10 ⁻⁶	n	R_{p1} (ohm.cm ²)	C_{coat} (mF/cm ²)	Q (S s ⁿ /cm ²) 10 ⁻⁶	n	R_{ct} (ohm cm ²)	C_{dl} (mF/cm ²)	θ	EF%	
3.5% NaCl	14.6	4307	0.65	246	4.44	2000	0.68	1165	2.97			
25 ppm	7.96	1785	0.74	357	1.52	718	0.66	1920	0.84	0.393	39.3	
50 ppm	7.31	1270	0.79	490	1.12	701	0.76	2025	0.78	0.425	42.5	
100 ppm	3.97	1100	0.82	593	1.001	576	0.8	3093	0.66	0.623	62.3	
200 ppm	6.8	923	0.8	747	0.84	435	0.83	3692	0.47	0.685	68.5	
500 ppm	1.6	756	0.82	792	0.67	266	0.8	3963	0.26	0.706	70.6	
800 ppm	5.8	530	0.76	873	0.42	155	0.57	4628	0.12	0.749	74.9	

Table 2. EIS parameters for carbon steel in 3.5% NaCl free and containing [BMIm]TfO.

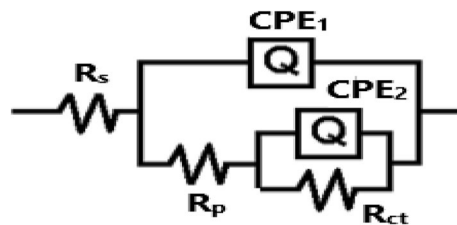


Figure 4. Equivalent circuit model fitted the electrochemical impedance spectroscopy (EIS) data.

corrosion inhibition efficacy decreases as the temperature increases. At higher concentrations of [BMIm]TfO, the extent of the negative influence of the temperature on the inhibition efficiency shrinks¹⁷.

Electrochemical impedance spectroscopy. The corrosion inhibition performance of [BMIm]TfO was investigated using the electrochemical impedance spectroscopy (EIS) technique. Figure 3 exhibits the Nyquist plots of the carbon steel electrode in the test electrolyte-free and containing different concentrations of [BMIm]TfO. As manifested in Fig. 3, the plots show imperfect capacitive loops. The higher the loop diameter always reveals stop corrosion resistance¹⁸. With the addition of [BMIm]TfO, the diameter increases signifying its inhibiting effect on the corrosion of carbon steel in the test electrolyte. This is attributable to the adsorption and formation of a protecting film of the ionic liquid on the electrode surface. This film masks the surface, leading to the lessening of the corrosion attack as evidenced by the reduction of the estimated double layer capacitance C_{dl} , Table 2. Also, the values of (R_s), (R_{p1}), and (R_{p2}) increase as the content of [BMIm]TfO increases¹⁹.

The equivalent circuit used to fit the Nyquist plots is shown in Fig. 4. The values of the estimated EIS parameters are compiled in Table 2. The parameters include the solution resistance (R_s), the constant phase element (Q), the polarization resistance between the surface and the formed film during the immersion in the test electrolyte (R_{p1}), the capacitance of double layer (C_{dl}), and the corrosion resistance at the surface film/electrolyte interface (R_{p2}).

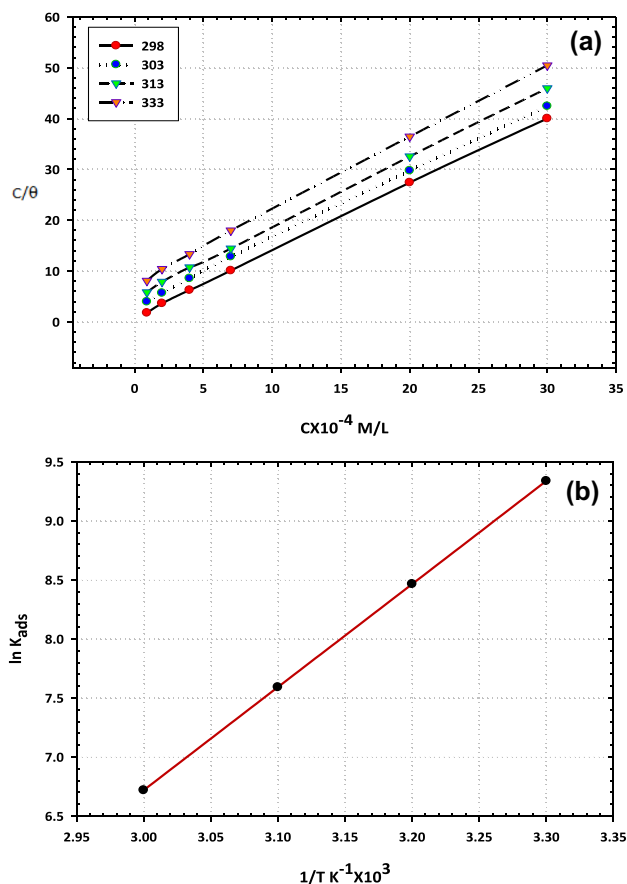


Figure 5. Langmuir (a) and Temkin (b) isotherms for adsorption of the ionic liquid on the carbon steel in 3.5% NaCl solutions.

T, K	R ²	Slope	K _{ads} (M ⁻¹)	ΔG ^o _{ads} (KJ mol ⁻¹)	ΔH ^o _{ads} (KJ mol ⁻¹)	ΔS ^o _{ads} (J mol ⁻¹ K ⁻¹)
303	0.9998	1.3	11,061	- 34	- 73	- 162
313	0.9996	1.3	3145	- 31		
323	0.9998	1.4	2014	- 31		
333	0.9995	1.4	1348	- 31		

Table 3. Adsorption isotherms parameters.

Adsorption isotherms. Adsorption isotherm studies were performed to explore the nature of the interaction of the ionic liquid species with the carbon steel surface. Several adsorption isotherms can describe the relationship between the extent of surface coverage and the content of adsorbed species such as Langmuir, Freundlich, and Temkin isotherms. The adsorptive interaction of [BMIm]TfO was found to obey Langmuir isotherm. The Langmuir adsorption isotherm can be defined in the following Eq. (1)²⁰.

$$\frac{C_{inb}}{\theta} = \frac{1}{k_{ads}} + C_{inb} \quad (1)$$

where (θ) is the surface coverage degree (obtained previously from EIS and PDP measurements), (C_{inb}) is the concentration of [BMIm]TfO, and (K_{ads}) is the adsorption equilibrium constant.

Plotting the Langmuir relation between C_{inb}/θ and C_{inb} gives significant straight lines with a correlation coefficient of unity and an average slope value of 1.35, Fig. 5a. Thus, it is evidence that the ionic liquid species are adsorbed in absence of any side interactions¹⁸. The equilibrium constant for [BMIm]TfO adsorption (K_{ads}) was calculated using the intercept of the C_{inb}/θ versus C_{inb} line, Table 3. Consequently, K_{ads} value was employed to estimate the adsorption standard free energy (ΔG^o_{ads}) based on the Eq. (2):

$$K_{ads} = \frac{1}{55.5} \exp\left(-\frac{\Delta G_{ads}^0}{RT}\right) \quad (2)$$

where R , T , and 55.5 are gas constant, the temperature of the system, and water molecules concentration in molar. The values of ΔG_{ads}^0 were determined for the ionic liquid inhibitor at different temperatures as shown in Table 3. It is seen that the high negative values of ΔG_{ads}^0 are correlated to the impulsive adsorption performance of [BMIm]TfO on the surface and refer to the steadiness state of the adsorbed layer. This behaviour indicates the intensive interaction between the ionic liquid constituents and the electrode surface²¹. As a common concept, the values of ΔG_{ads}^0 up to -20 kJ mol^{-1} are associated with the electrostatic interaction of the charged compounds with the charged surface in which the adsorption process, in this case, is only physical. With increasing the values of ΔG_{ads}^0 above -40 kJ mol^{-1} the chemical adsorption will be found²².

From the obtained measurements, the values of ΔG_{ads}^0 were stabilized at -31 kJ mol^{-1} in the temperature range from 303 to 333 K. This indicates that the adsorption of ionic liquid species is typical physical sorption. The results reveal that the adsorption of the species of the ionic liquid, typically the imidazolium cation, occurs physically, electrostatically, via the interaction between the imidazolium cation and the charged centers on the electrode surface. The spontaneous nature of the adsorption of the ionic liquid species on the surface is indicated by the negative values of ΔG_{ads}^0 ²³. The heat of adsorption ΔH_{ads}^0 was also estimated from the Van't Hoff Eq. (3):

$$\ln K_{ads} = -\frac{H_{ads}^0}{RT} + A \quad (3)$$

By plotting the relation between $\ln K_{ads}$ against $1/T$ a straight line is obtained as manifested in Fig. 5b. The slope of the obtained line is equivalent to $(-\Delta H_{ads}^0/R)$ in which the adsorption heat value (ΔH_{ads}^0) is nearly the standard adsorption heat value under the testing procedures²⁰. From the thermodynamics, the standard entropy of adsorption (ΔS_{ads}^0) can be obtained using the Eq. (4):

$$\Delta S_{ads}^0 = -\frac{\Delta H_{ads}^0 - \Delta G_{ads}^0}{T} \quad (4)$$

The calculated thermodynamic parameters (ΔG_{ads}^0 , ΔH_{ads}^0 and ΔS_{ads}^0) are compiled in Table 3. It is seen that the ΔH_{ads}^0 value is negative (-73 kJ mol^{-1}) indicating the impact of [BMIm]TfO adsorption on the surface. By inspection of the values of (ΔS_{ads}^0) as listed in Table 3, it is obvious that the ΔS_{ads}^0 value is the negative sign ($-162 \text{ J mol}^{-1} \text{ K}^{-1}$). The negative signal of ΔS_{ads}^0 can be correlated to dissolute medium which is generally proved as a growth in the disorder, as the reactants are turning into efficient complexes. Moreover, the observed manner can be explained by the substitution mechanism of more water molecules throughout the adsorption process of ionic liquid on the surface²⁴.

Kinetic activation. Additional to the thermodynamic investigations, the kinetic activation model is also an important technique to study the inhibition mechanism and explain the features of the protective action of [BMIm]TfO at different temperatures. Arrhenius equation was employed to estimate the activation parameters of the corrosion see Eq. (5)²⁵:

$$\ln CR = -\frac{E_a}{RT} \times \ln A \quad (5)$$

where, (CR) represents the corrosion rate, (E_a) is the energy of activation, (R) is the gas constant, and (A) is the pre-exponential factor.

The Arrhenius plots of the relation between the $\ln (CR)$ and $1/T$ are depicted in Fig. 6a. As seen, a linear behavior is obtained and the slopes of the straight lines is $(-E_a/R)$ hence, the values of the activation energy (E_a) in the presence and absence of various concentrations of [BMIm]TfO were determined. Moreover, there is another formulation for the transition state as described in the following Eq. (6)²⁶.

$$\ln CR = -\frac{RT}{Nh} \exp\left\{\frac{\Delta S^*}{R}\right\} \exp\left\{\frac{-\Delta H^*}{RT}\right\} \quad (6)$$

The terms of the equation are, Plank's constant (h), Avogadro's number (N), the activation entropy (ΔS^*), and the activation enthalpy (ΔH^*). The plots of $\ln CR/T$ versus $1/T$ for the ionic liquid inhibitor are presented in Fig. 6b. The slope of the obtained lines equals $(-\Delta H^*/R)$ and the intercept is $(\ln R/Nh + \Delta S^*/R)$, hence the values of ΔH^* and ΔS^* can be estimated. At definite concentration ranges of the ionic liquid inhibitor, the activation parameters for carbon steel in sodium chloride medium are gathered and illustrated in Table 4. The results reveal that with the existence of [BMIm]TfO the activation energy rises, and the activation enthalpy slightly reduces meanwhile the values of the entropy for the corrosion process significantly rise. The energy of activation (E_a), which is the minimal amount of energy required to launch a chemical reaction, reaches a value of 24 kJ mol^{-1} at a high ionic liquid content and for the blank solution is only 16 kJ mol^{-1} . The increase of the E_a value under the effect of ionic liquid inhibitor might be attributed to the physical sorption regime²⁷. Additional explanation reported that the raising of the activation energy value might also be attributable to the gradual reduction in the adsorption process of [BMIm]TfO on the surface under the effect of heat. Based on these phenomena, as the adsorption process reduces more desorption action of ionic liquid species occurs as the protection and dissolution systems are in balance. It is also revealed that the sequential values of E_a and ΔH^0 as presented in Table 4

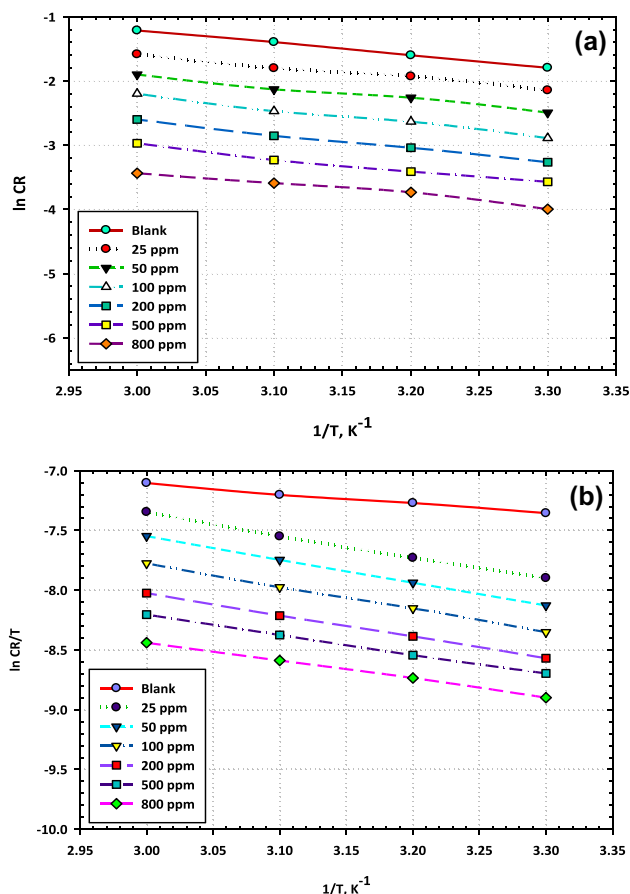


Figure 6. (a) Arrhenius and (b) Transition-state plots for carbon steel corrosion in 3.5% NaCl without and with different concentrations of [BMIm]TfO.

Conc., ppm	E_{a^*} (KJ mol ⁻¹)	ΔH^{\ddagger} (KJ mol ⁻¹)	ΔS^{\ddagger} (J mol ⁻¹ K ⁻¹)
3.5% NaCl	16	7	-236
25	15	15	-213
50	16	16	-212
100	19	16	-215
200	20	15	-219
500	21	14	-225
800	24	13	-230

Table 4. Activation energy parameters at different concentrations of [BMIm]TfO.

are varied in the same trend confirming the common thermodynamic phenomena. On particular monitoring, it has been observed that the value of the activation entropies is negative signifying that the activated complex is in the rate-determining stage and demonstrating combination rather than separation²⁸.

Surface analysis. The utilization of surface analytical techniques is quite significant for realizing the characteristics of materials, especially the metallic surfaces after exposure to the various aggressive environments. SEM-EDX examination of the electrode surface following dipping in the test electrolytes was performed. The SEM images of Fig. 7a and b show the surface after the exposure to 3.5% NaCl without and with the addition of [BMIm]TfO, respectively. Figure 7a representative the SEM image of the uninhibited steel surface shows a deteriorated, rough surface as a result of the corrosion²⁹.

In the absence of [BMIm]TfO the whole surface of the carbon steel is usually concealed with the corrosion products. The porous corrosion product layer is unable to protect the surface from extreme corrosion. The addition of the ionic liquid inhibitor to the test electrolyte reduced the aggressive attack on the steel surface as revealed in Fig. 7b. The surface is relatively free from the corrosion products and compared with the uninhibited sample the surface is smoother signifying the inhibiting action of [BMIm]TfO³⁰.

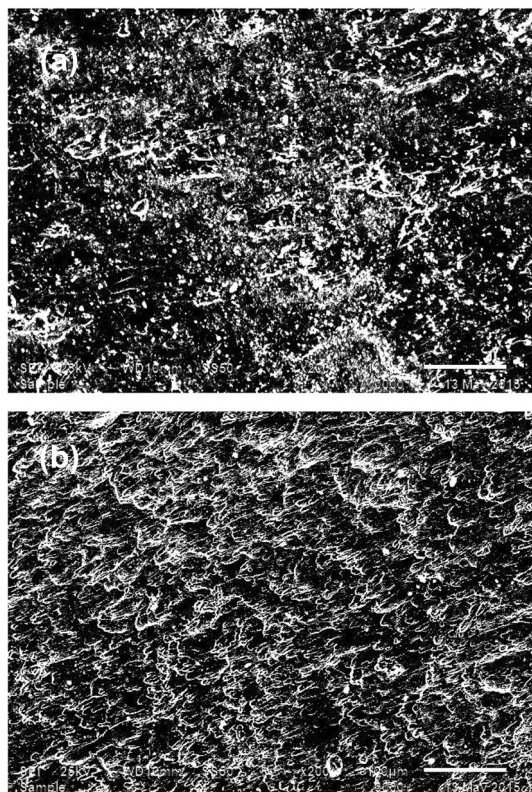


Figure 7. SEM images of (a) polished carbon steel, and (b) after 24 h of immersion in 3.5% NaCl and [BMIm] TfO.

Figure 8 represents the EDX spectrum of the uninhibited sample Fig. 8a and inhibited sample Fig. 8b since it shows confirms the SEM results as, in addition to the Fe, O, and C peaks, a peak of N is recorded owing to the adsorption of the imidazolium cation leading to the observed corrosion inhibition. Furthermore, under the continuation of the IL coverage, the spectrum intensities decrease because of the formation of the IL adsorptive layer on the surface³¹.

Quantum chemical studies. As known, the application of quantum chemical calculations is necessary to demonstrate the relation between the molecular/electronic structure of the inhibitor and its corrosion inhibiting efficiency³². Furthermore, the theoretical studies allow the optimum pre-selection of the inhibitor with the desired characteristics³³.

The molecular geometry of the employed ionic liquid was optimized using the PM6 semiempirical method. The optimized structures were then re-optimized by ab initio Hartree–Fock method (HF) using 6–31 + G(d,p) basis set at Hartree–Fock level (HF)³⁴, and by density functional theory (DFT) method using 6–31 + G(d,p) basis set. The values of the calculated bond length, bond angle, and dihedral angle using the DFT 6–31 + G(d,p) method are compiled in Table 5. All calculations were made by gaussian 09 W software using the B3LYP functional³⁵. B3LYP utilizes Bache’s three-parameter functional (B3) and comprises a combination of HF with DFT exchange terms and the Lee, Yang, and Parr (LYP) correlation functional³⁶.

The optimized molecular structure, the electrostatic potential feature, and the identical HOMO and LUMO electron density surfaces of the ionic liquid inhibitor, as demonstrated patterns by IL employing PM3 model chemistry, are symbolized in Fig. 9a–d. From the optimized structure, Fig. 9a it is seen the planar pentagon structure of the imidazolium ring. The electrostatic potential Fig. 9b it shows the electron cloud around the chemical structure. The sequential distribution of electrons of HOMO Fig. 9c shows information about the positions or locations that are significant in the system to accord the electrons to the contrasting orbital of the recipient molecule. On the other hand, the prevalence of electrons of LUMO Fig. 9d shows information about the molecule sites that are restricted to recognize the electron from a-convenient granter one³⁷.

From Fig. 9c, it is obvious that the electron density of the HOMO is generally combined with the imidazolium cation in the ionic liquid structure indicating the contribution of the imidazolium ring in the adsorption of ionic liquid on the steel surface. This is consistent with the recently published results which indicated, based on quantum chemical studies, that the imidazolium ring is likely the crucial active site in imidazolium-based ionic liquids³⁸. The calculated values of the quantum chemical parameters, E_{HOMO} , E_{LUMO} , and ΔE , which are mainly affected by the electron interactions between the steel surface and the ionic liquid inhibitor were illustrated in Table 6. The E_{HOMO} value describes the ability of the inhibitor to donate electrons to the electrode surface, while the E_{LUMO} measures the capability to receive electrons into the LUMO molecule from a suited donor molecule^{39–41}.

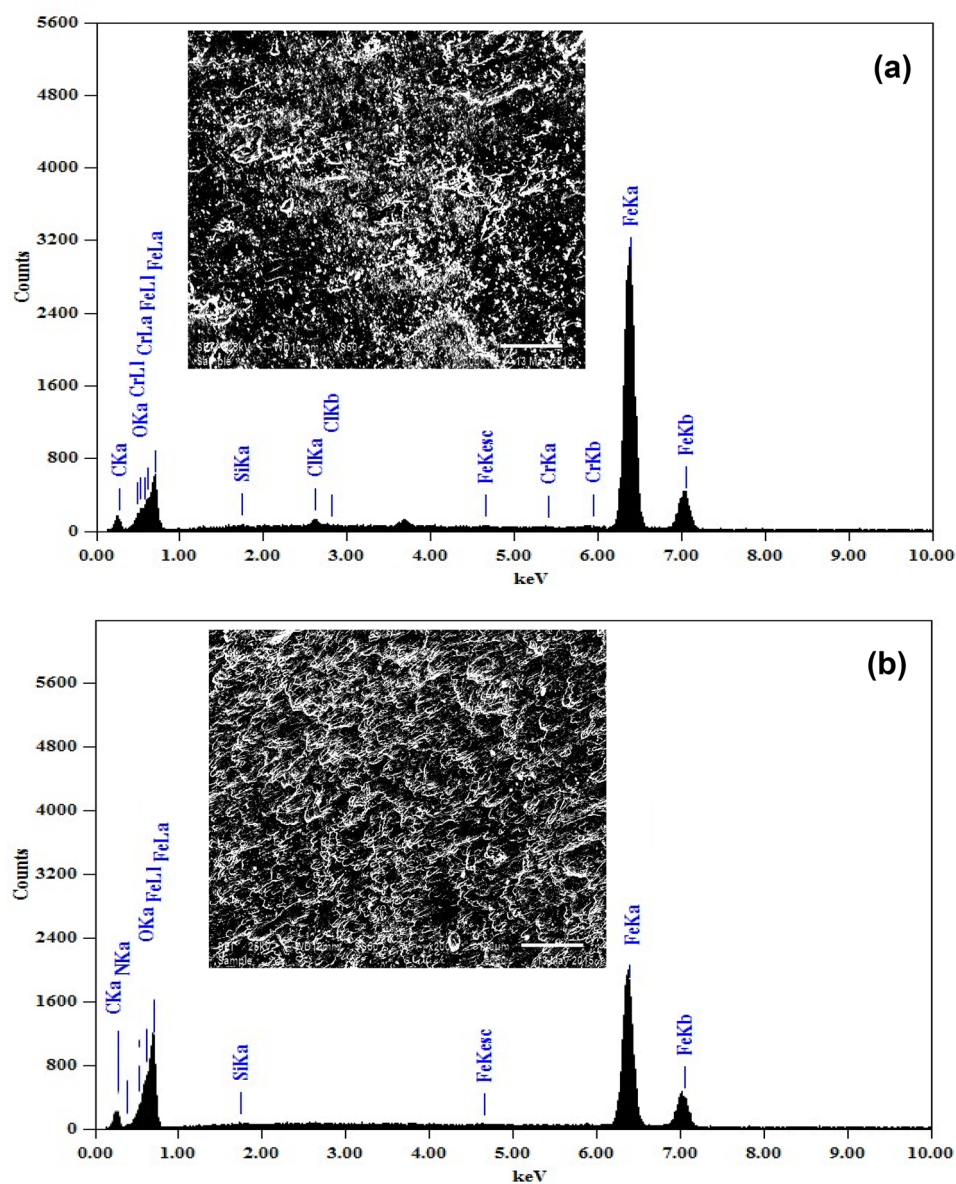


Figure 8. EDX spectra of (a) polished carbon steel, (b) after 24 h of immersion in 3.5% NaCl and [BMIm]TfO.

The energy gap (ΔE), which is obtained from the difference between E_{LUMO} and E_{HOMO} , is also a substantial factor that can be employed to detect the molecule's activity. Mainly, the minimal ΔE value is related to large inhibition efficiency and chemical reactivity^{42–44}. This means the inhibitor on the surface more easily gives/receives electrons and subsequently the adsorption of the inhibitor on the surface becomes easier. The negative sign of E_{HOMO} refers to the physical adsorption nature of the ionic liquid inhibitor^{45–47}.

Tag	Symbol	NA	NB	NC	Bond	Angle	Dihedral
1	C						
2	C	1			1.3649388		
3	N	1	2		1.3826703	107.2577112	
4	C	3	1	2	1.3385765	108.2901377	0.1342003
5	H	1	2	3	1.0786527	130.5797538	- 179.7446671
6	H	2	1	4	1.0788841	130.7968854	179.5585425
7	H	3	1	2	1.0793932	162.0315182	- 179.4096889
8	C	4	3	1	1.4833922	125.7694245	- 178.2340041
9	H	8	4	3	1.0930267	106.6857276	- 17.4207763
10	H	8	4	3	1.0936370	106.8490727	- 132.2691668
11	C	8	4	3	1.5319684	112.6994544	104.9556159
12	H	11	8	4	1.0974252	109.5501526	58.6957637
13	H	11	8	4	1.0975405	109.2694754	- 58.0633895
14	C	11	8	4	1.5368842	111.5173836	- 179.7949393
15	H	14	11	8	1.0979581	109.3489727	- 57.6517339
16	H	14	11	8	1.0979929	109.3446071	58.5127304
17	C	14	11	8	1.5327518	112.4516784	- 179.5556948
18	H	17	14	11	1.0954488	111.3223019	60.4191595
19	H	17	14	11	1.0935363	110.7318492	- 179.8474457
20	H	17	14	11	1.0955026	111.3679463	- 60.0826591
21	N	3	1	2	1.3402623	72.5094756	0.0235677
22	C	21	3	1	1.4709147	125.9328112	- 179.6726306
23	H	22	21	3	1.0913211	109.4349618	- 119.9287493
24	H	22	21	3	1.0897125	108.9581759	- 0.2996535
25	H	22	21	3	1.0913515	109.4608757	119.3369532

Table 5. Calculated bond length, bond angle, and dihedral angle using DFT 6-31 + G (d,p) method.

In the light of the above results, it can be concluded that the employed ionic liquid is electrostatically adsorbed on the steel surface and the imidazolium cation is responsible for the observed inhibiting influence as the imidazolium ring is parallelly absorbed on the steel surface.

Conclusions

[BMIm]TfO was examined as a possible corrosion inhibitor for carbon steel in chloride solutions. The results revealed the inhibiting action of [BMIm]TfO which increases as the concentration increases. The potentiodynamic polarization results showed that the ionic liquid is a mixed inhibitor as both cathodic and anodic processes were influenced. The inhibiting act of [BMIm]TfO is attributable to the adsorption of the imidazolium cations on the carbon steel surface establishing a barrier layer that protects the surface from the aggressive medium. The adsorption of the [BMIm]TfO was found to obey Langmuir isotherm. The free energy of adsorption revealed that the adsorption of the ionic liquid species occurs physically via the electrostatic interaction of the imidazolium cation with the charged centers on the electrode surface. The results proved that ionic liquids can be used as corrosion inhibitors for carbon steel in brine solutions with a high efficiency that enables them to compete with the commercial inhibitors currently used, despite their high price, they are considered competitive for more than one reason, including their effectiveness and the most important reason is that they are less toxic and therefore in line with the global trend to replace toxic materials. So, it could be currently used with potential effects and less toxic materials, which makes these materials ready to compete in the field of oil and gas industry.

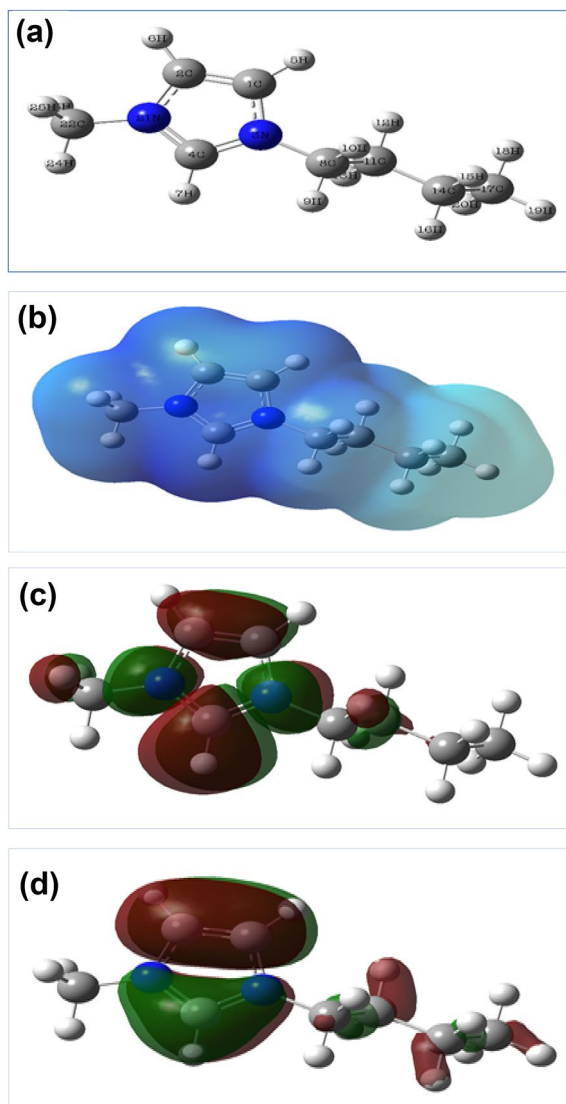


Figure 9. The frontier molecular orbital (a) optimized structure, (b) electrostatic potential (ESP), (c) HOMO, and (d) LUMO of the ionic liquid [BMIm]TfO.

E_{HOMO} (eV)	E_{LUMO} (eV)	ΔE (eV)
DFT/B3LYP/6-31G+(d,p)		
- 11.740	- 5.067	6.673
HF/6-31G+(d,p)		
- 14.185	- 1.611	12.573
Semi-empirical /PM6		
- 14.506	- 4.509	9.996

Table 6. The calculated quantum chemical parameters in eV for the investigated inhibitor.

Data availability

The datasets generated and/or analyzed during the current study are available in this published article.

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Author contributions

M.A.A., A.S.I., and K.Z. analyzed the data and wrote the experimental work in this manuscript; S.Z.E.A. act as a consultant for the scientific information, and S.Z.E.A. and A.M.E.-S. helped perform the analysis with constructive discussions.

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Competing interests

The authors declare no competing interests.

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