

ORIGINAL RESEARCH

High-frequency oscillatory ventilation versus conventional ventilation: hemodynamic effects on lung and heart

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Abstract

High-frequency oscillatory ventilation (HFOV) may improve gas exchange in patients who are inadequately ventilated by conventional mechanical ventilation (CV); however, the hemodynamic consequences of switching to HFOV remain unclear. We compared the effects of CV and HFOV on pulmonary vascular conductance and left ventricular (LV) preload and performance at different airway and filling pressures. In anesthetized dogs, we measured LV dimensions, aortic and pulmonary artery (PA) flow, and mean airway (\bar{P}_{AW}) and pericardial pressures. Catheter-tip pressure manometers measured aortic, LV, left atrial, and PA pressures. The pericardium and chest were closed. At LV end-diastolic pressure (P_{LVED}) = 5 mmHg and 12 mmHg, PEEP was varied (6 cm H₂O, 12 cm H₂O, and 18 cm H₂O) during CV. Then, at airway pressures equal to those during CV, HFOV was applied at 4 Hz, 10 Hz, and 15 Hz. Increased \bar{P}_{AW} decreased pulmonary vascular conductance. As cardiac output increased, conductance increased. At P_{LVED} = 12 mmHg, conductance was greatest during HFOV at 4 Hz. LV preload (i.e., A_{LV} , our index of end-diastolic volume) was similar during HFOV and CV for all conditions. At P_{LVED} = 12 mmHg, SW_{LV} was similar during CV and HFOV, but, at P_{LVED} = 5 mmHg and \bar{P}_{AW} 10 cm H₂O, SW_{LV} was lower during HFOV than CV. Compared to pulmonary vascular conductance at higher frequencies, at P_{LVED} = 12 mmHg, conductance was greater at HFOV of 4 Hz. Effects of CV and HFOV on LV preload and performance were similar except for decreased SW_{LV} at P_{LVED} = 5 mmHg. These observations suggest the need for further studies to assess their potential clinical relevance.

Introduction

Conventional mechanical ventilation (CV) may be insufficient to maintain adequate gas exchange in seriously ill patients and may also cause or aggravate lung injury. High-frequency oscillatory ventilation (HFOV) has been used to improve gas exchange in patients who cannot be adequately ventilated by conventional means, while putatively limiting lung injury (Heuer et al. 2012; Ip and Mehta 2012; Ferguson et al. 2013). Theoretically, HFOV achieves the goals of protective ventilation by optimizing

alveolar recruitment through sustained high mean airway pressures, while avoiding lung trauma associated with the swings in pressure associated with conventional methods (Fort et al. 1997; Mehta et al. 2001, 2004; Derdak et al. 2002). Recent clinical publications suggest that relatively early switching to HFOV may result in no outcome benefit (Young et al. 2013) or might cause harm (Ferguson et al. 2013) so that indications for the use of HFOV will require further refinement.

Although HFOV is used frequently in intensive care units, there are few systematic studies of its hemodynamic

effects. The results of studies using different experimental models have not been consistent so it remains still unclear as to what, if any, hemodynamic consequences should be anticipated when switching from CV to HFOV (Fort et al. 1997; Andersen et al. 2002; Derdak et al. 2002; David et al. 2004; Mehta et al. 2004; Nakagawa et al. 2007; Heuer et al. 2012).

A better understanding of the hemodynamic effects of HFOV would facilitate clinical decision making. We therefore performed a canine study at different airway and filling pressures to compare the effects of CV and HFOV. We focused on pulmonary vascular conductance (i.e., the amount of flow that the lungs will accept per unit driving (blood) pressure) and left ventricular (LV) preload and systolic performance.

Methods

The experimental protocol was approved by the University of Calgary animal care committee, whose criteria are consistent with those of the American Physiological Society.

Animal preparation

Ten mongrel dogs of both sexes, weighing 15–23 kg (mean 20.3 kg), were anesthetized initially with 25 mg/kg thiopental sodium i.v. (Abbott Laboratories, Montreal, PQ) and a 5 mg/mL i.v. bolus of midazolam (Sandoz, Boucherville, PQ) and were maintained with fentanyl citrate (0.04 mg/mL i.v., initially, followed by an infusion of 4 mg/h, prepared locally), which was adjusted as necessary to ensure deep sedation without spontaneous respiratory effort. The animals were intubated with a cuffed endotracheal tube (9 mm diameter) and ventilated initially with a constant-volume respirator (model 607, Harvard Apparatus, Mills, MA) with a 1:1 mixture of O₂ and nitrous oxide. Tidal volume and respiratory rate were initially set at 17 mL/kg and 18 breaths/min, respectively (in accordance with recommended ventilation parameters for large animals (Pascoe 1986)), and were adjusted to maintain physiological blood gas tensions and pH.

Instrumentation

A median sternotomy was performed with the animals in the supine position. For instrumentation, the heart was delivered from the pericardium via a base-to-apex incision. Sonomicrometry crystals (Sonometrics Corp., London, ON) were implanted in the LV endocardium and midwall of the septum to measure minor-axis septum-to-LV free wall (D_{SLVFW}) and LV anteroposterior (D_{LVAP}) dimensions (Mitchell et al. 2005a,b). Ultrasonic

flow probes (Transonic Systems, Ithaca, NY) were placed on the ascending aorta and main pulmonary artery. Airway pressure (P_{AW}) was measured at a port on the adapter attached to the proximal end of the endotracheal tube with an air-filled tube (2 mm diameter) connected to a pressure transducer (model, P23 ID; Statham Gould, Oxnard, CA). A single-lead electrocardiogram (ECG) was recorded. A flat, fluid-filled balloon transducer (Smiseth et al. 1986), connected to a pressure transducer (model P23 ID; Statham Gould, Oxnard, CA), was loosely attached to the lateral surface of the LV to measure pericardial pressure (P_{PERI}).

Catheter-tip pressure manometers with fluid-filled reference lumens (7-F, Millar Instruments Inc., Houston, TX) were used to measure aortic pressure (P_{AO}) (inserted through the right femoral artery) and LV pressure (P_{LV}) (inserted through a carotid artery). Catheter-tip pressure manometers (3.5-F, model SPR-524, Millar Instruments Inc., Houston, TX) were used to measure left atrial (P_{LA}) (inserted through the left atrial appendage), and pulmonary artery (P_{PA}) (inserted retrograde through a distal pulmonary artery branch) pressures. An intravenous line was placed in the left external jugular vein for volume loading (Pentaspan™ [10% pentastarch in 0.9% sodium chloride], Bristol-Myers-Squibb, St. Laurent, PQ). A left femoral arterial line was used to obtain samples for blood gas analysis (Nova Biomedical, Critical Care Express). The right atrium was paced slightly faster than the intrinsic rate (Grass S88 Stimulator, Grass Instruments, Quincy, MA) to maintain a constant heart rate and to be able to compare hemodynamics without confounding differences in heart rate. Body temperature was measured with a rectal or vaginal thermometer. After instrumentation, the heart was returned to the pericardium, which was closed with single interrupted sutures to approximate normal constraint (Scott-Douglas et al. 1991). The chest was closed under suction (~5 mmHg). An alternative ventilator (Servo, Siemens-Elema 900C) that enables precise application of PEEP was then connected; 100% O₂ was delivered throughout the experimental protocol.

Experimental protocol

After stabilization at a LV end-diastolic pressure (P_{LVED}) of 5 mmHg, positive end-expiratory pressures (PEEP) of 6 cm H₂O, 12 cm H₂O, and 18 cm H₂O were applied in random order during CV and the mean airway pressure (\bar{P}_{AW}) at each level of PEEP was noted. All interventions were initiated only after return to baseline with stable hemodynamics for 3–5 min. HFOV (Sensormedics 3100B, Viasys Healthcare, Burlington, ON) was then begun with frequencies of 4 Hz, 10 Hz, and 15 Hz applied to cover a wide, relevant range in randomized order. During ventila-

tion at each frequency, each of the three levels of \bar{P}_{AW} noted during CV was applied in randomized order. Once acceptable blood gases were achieved (by adjusting the tidal-volume amplitude), data were recorded for 1 min. The protocol was then repeated at a P_{LVED} of 12 mmHg (Pentaspán™ was infused until the desired P_{LVED} was achieved). At the end of the experiment, the animals were sacrificed by an intravenous bolus KCl injection and the positions of the crystals were verified.

Data analysis

The conditioned signals were amplified (Sonometrics Corp. Acquisition System, London, ON), passed through a low-pass filter (100 Hz), and digitized at 200 Hz. The digitized data were analyzed using software developed in our laboratory (CV Works, Advanced Measurements Inc., Calgary, AB). Five CV cycles (or the equivalent amount of time during HFOV), during which the cardiac rhythm was regular, were selected for analysis. Using a low-pass filter, P_{PERI} was variably filtered to achieve a smooth trace.

Calculations

Transmural LV end-diastolic pressure (P_{LVEDtm})

$$= P_{LVED} - P_{PERI}$$

Cardiac output = SV × heart rate

Pulmonary vascular conductance (i.e., the inverse of pulmonary vascular resistance) = $CO / [\bar{P}_{PA} - \bar{P}_{LA}]$

LV stroke work (SW_{LV}) = LV stroke volume (SV_{LV}) × $(\bar{P}_{LV} \text{ (systolic)} - \bar{P}_{LA})$

Where, $\bar{P}_{LV} \text{ (systolic)} = P_{Ao} \text{ (diastolic)} + 2/3 [P_{Ao} \text{ (systolic)} - P_{Ao} \text{ (diastolic)}]$

$$LV \text{ area } (A_{LV}) = D_{SLVFW} \times D_{LVAP}$$

A_{LV} was used as an index of LV end-diastolic volume, that is, LV preload (Suga and Sagawa 1974; Appleyard and Glantz 1990). To account for different ventricular dimensions and outputs among animals, selected measurements were normalized with the values at a P_{LVED} of 5 mmHg and PEEP of 6 cm H₂O set as 100%.

Statistical analysis

The Student's unpaired *t*-test was used to test for significant changes between CV and HFOV, for a given set of conditions. A *P* value <0.05 was considered statistically significant. Linear regression analysis was used to find the line of best fit for CV and HFOV at each filling pressure. The slopes and Y-intercepts of these lines were compared using multivariate regression analysis. Using individual values from each condition in each experiment, 95% confidence intervals of the regression line were calculated.

Results

All data are shown as mean values (\pm SE's). At a P_{LVED} of 5 mmHg, three of the 10 dogs did not tolerate a PEEP of 12 cm H₂O and five dogs did not tolerate a PEEP of 18 cm H₂O; they became hemodynamically unstable (systolic P_{Ao} < 50 mmHg). Mean tidal volume was 18.1 mL/kg (range 16–24 mL/kg) and mean respiratory rate was 17.7 breaths/min (range 17–18 breaths/min). Five of the 10 animals died before the completion of the protocol; thus, at the highest filling pressure, *n* = 5.

Table 1 lists mean airway pressures and the hemodynamic responses during CV (PEEP 6 cm H₂O) and HFOV ($\bar{P}_{AW} \sim 10$ cm H₂O) at P_{LVED} 5 mmHg and 12 mmHg. LV preload (A_{LV}) was affected similarly during both methods of ventilation. However, at a P_{LVED} of 5 mmHg, LV performance (SV_{LV} and SW_{LV}) was substantially lower during HFOV compared to during CV. At a P_{LVED} of 12 mmHg, the difference in LV performance was not statistically significant.

Figure 1 shows typical LV pressure traces during CV and HFOV at a P_{LVED} of 5 mmHg and $\bar{P}_{AW} \sim 10$ cm H₂O. The LV diastolic pressure trace during CV is characteristic of normal physiological changes during diastole. During HFOV, note the fluctuations in LV diastolic pressure due to the oscillations in airway pressure. No fluctuations are apparent during LV systolic pressure.

Pulmonary vascular conductance

The relations between pulmonary vascular conductance and \bar{P}_{AW} during CV and HFOV at P_{LVED} of 5 mmHg and 12 mmHg are illustrated in Figure 2. At both filling pressures, as \bar{P}_{AW} increased, conductance substantially decreased. At a P_{LVED} of 5 mmHg, conductance decreased by ~40% when \bar{P}_{AW} was increased from ~10 cm H₂O to ~20 cm H₂O. This decrease in conductance would seem to be a “cost” of increasing \bar{P}_{AW} , regardless of the mode of ventilation. As CO increased (here, due to an increase in P_{LVED}), conductance also increased (note that all the yellow and green symbols lie above their respective blue and purple symbols). This suggests that the lung adapts to increases in CO, increasing conductance by “recruitment” of pulmonary vasculature. When P_{LVED} was increased from 5 mmHg to 12 mmHg, note that conductance increased by ~50% at $\bar{P}_{AW} \sim 15$ cm H₂O. It is potentially important that at a P_{LVED} of 12 mmHg, HFOV at a frequency of 4 Hz seems to be particularly advantageous. At $\bar{P}_{AW} \sim 15$ cm H₂O, conductance was ~15% higher at HFOV 4 Hz than at the higher frequencies; this apparent 4-Hz “advantage” was not observed at P_{LVED} 5 mmHg.

Table 1. Baseline hemodynamics at low airway pressure (PEEP 6 cm H₂O) and both LV filling pressures during CV and HFOV.

P_{LVED} 5 mmHg	CV	4 Hz	10 Hz	15 Hz
\bar{P}_{AW} (cm H ₂ O)	9.7 ± 0.3 (10)	9.1 ± 0.4 (9)	9.0 ± 0.4(10)	*8.7 ± 0.3 (10)
HR (beats/min)	98 ± 4.2 (10)	107 ± 3.5 (8)	106 ± 3.1(9)	107 ± 3.1 (9)
A_{LV} (mm ²)	1200 ± 130 (10)	1133 ± 139 (8)	1167 ± 127 (9)	1193 ± 129 (9)
P_{LVEDtm} (mmHg)	1.4 ± 0.6 (5)	0.9 ± 0.4 (6)	1.1 ± 0.4 (6)	1.7 ± 0.4 (6)
P_{LVED} (mmHg)	6.7 ± 0.5 (8)	6.1 ± 0.6 (8)	6.5 ± 0.6 (9)	6.8 ± 0.7 (9)
m P_{LV} (sys) (mmHg)	89 ± 4.4 (8)	87 ± 4.5(8)	81 ± 4.5 (9)	82 ± 3.7 (9)
P_{Ao} (ps) (mmHg)	98 ± 4.5 (9)	96 ± 5.0 (8)	91 ± 5.0 (9)	92 ± 4.2 (9)
SV_{LV} (mL)	16.8 ± 2.1(10)	11.9 ± 1.1(9)	*12.0 ± 0.9 (10)	12.5 ± 1.0 (10)
SW_{LV} (mL)	1568 ± 170 (8)	*1015 ± 114 (8)	*945 ± 84 (9)	*974 ± 83 (9)
CO (L/min)	1.6 ± 0.2 (10)	1.3 ± 0.1 (9)	1.3 ± 0.1 (10)	1.3 ± 0.1 (10)
P_{LVED} 12 mmHg	CV	4 Hz	10 Hz	15 Hz
\bar{P}_{AW} (cm H ₂ O)	9.4 ± 0.2 (6)	8.4 ± 0.7 (5)	9.0 ± 0.6 (6)	8.4 ± 0.5 (6)
HR (beats/min)	108 ± 6.8 (5)	103 ± 8.5 (4)	104 ± 9.3 (6)	107 ± 11.2(5)
A_{LV} (mm ²)	1314 ± 220 (5)	1147 ± 166 (4)	1286 ± 177 (6)	1311 ± 209 (5)
P_{LVEDtm} (mmHg)	3.1 ± 1.5 (4)	3.8 ± 0.7 (4)	4.0 ± 1.3 (4)	4.0 ± 0.9 (4)
P_{LVED} (mmHg)	13.9 ± 0.9 (5)	11.6 ± 0.7 (4)	14.1 ± 1.1 (5)	13.0 ± 0.6 (5)
m P_{LV} (sys) (mmHg)	93 ± 3.4 (5)	89 ± 3.1 (4)	85 ± 3.1 (5)	*90 ± 1.5 (5)
P_{Ao} (ps) (mmHg)	103 ± 4.0 (5)	99 ± 3.9 (4)	96 ± 3.5 (5)	95 ± 2.3 (5)
SV_{LV} (mL)	17.2 ± 3.0 (6)	18.2 ± 3.2 (5)	17.1 ± 2.8 (6)	17.5 ± 3.0 (6)
SW_{LV} (mL)	1518 ± 273 (5)	1583 ± 226 (<i>n</i> = 4)	1367 ± 198 (<i>n</i> = 5)	1371 ± 202 (5)
CO (L/min)	1.8 ± 0.2 (6)	1.8 ± 0.3 (<i>n</i> = 5)	1.7 ± 0.2 (<i>n</i> = 6)	1.8 ± 0.2 (6)

\bar{P}_{AW} , mean airway pressure; HR, heart rate; A_{LV} , LV area; P_{LVEDtm} , transmural LV end-diastolic pressure; P_{LVED} , LV end-diastolic pressure; P_{LV} (sys), mean LV systolic pressure; P_{Ao} (ps), aortic systolic pressure; SV_{LV} , LV stroke volume; SW_{LV} , LV stroke work; CO, cardiac output.

* $P < .05$: *n* is shown in brackets.

Figure 3 shows how HFOV appears to augment pulmonary vascular conductance at a P_{LVED} of 5 mmHg. The HFOV data lie to the left of the CV data such that a normalized conductance of 100% is achieved at a CO of ~70% with HFOV, rather than a CO of 100% with CV. As indicated in Figure 2, conductance generally increases as CO increases, as the lung accommodates by recruitment. However, note the apparent advantage of HFOV where, as CO increases, the lung can accept increased CO as compared to CV. There was no such difference between CV and HFOV at a P_{LVED} of 12 mmHg.

Cardiac function during CV and HFOV

The effects of manipulating \bar{P}_{AW} and P_{LVED} on cardiac performance are shown in Figures 4 and 5. Figure 4 shows how increasing \bar{P}_{AW} reduced LV preload (i.e., A_{LV}) and how volume loading increased preload. LV preload at each value of \bar{P}_{AW} and P_{LVED} was similar during both modes of ventilation. Figure 5 shows the dependence of SW_{LV} on A_{LV} . As expected, SW_{LV} increased as A_{LV} increased.

The relations between \bar{P}_{AW} and LV performance [normalized SV_{LV} (A) and normalized SW_{LV} (B)] during CV and HFOV are illustrated in Figures 6A and B, respectively. SV_{LV} and SW_{LV} were greater at the higher filling pressure and decreased at higher airway pressures.

At a P_{LVED} of 12 mmHg and at each \bar{P}_{AW} , SV_{LV} and SW_{LV} were statistically similar during CV and HFOV. However, at the lower filling pressure ($P_{LVED} = 5$ mmHg) and $\bar{P}_{AW} \sim 10$ cm H₂O, SV_{LV} and SW_{LV} were significantly lower during HFOV (all frequencies) than during CV ($P < 0.001$, $P = 0.001$, respectively). The differences were not significant at higher airway pressures.

The regression relationships that relate LV performance (normalized SV_{LV} and normalized SW_{LV}) to \bar{P}_{AW} during CV and HFOV are shown in Figures 7A and B, respectively. Note that these regressions are only for data obtained at a P_{LVED} of 5 mmHg. In both Figures 7A and B, the regression lines for HFOV have a significantly different slope than those for CV ($P < 0.01$ for both) and a significantly different Y-intercept ($P < 0.01$ and $P < 0.001$, respectively), which suggests that LV performance is reduced more during HFOV than during CV at low filling pressures.

The relations between P_{LVED} , P_{LVEDtm} , and A_{LV} are shown in Figure 8. Increased PEEP increased LV intracavitary pressure which might suggest increased LV preload. However, after accounting for external constraint, it was shown that preload (A_{LV}) increased as a quasi-sigmoidal function of P_{LVEDtm} . The scatter in that relationship was minimal and the sigmoidal shape was expected, the LV being a structure with an unstressed volume that becomes stiffer as volume increases.

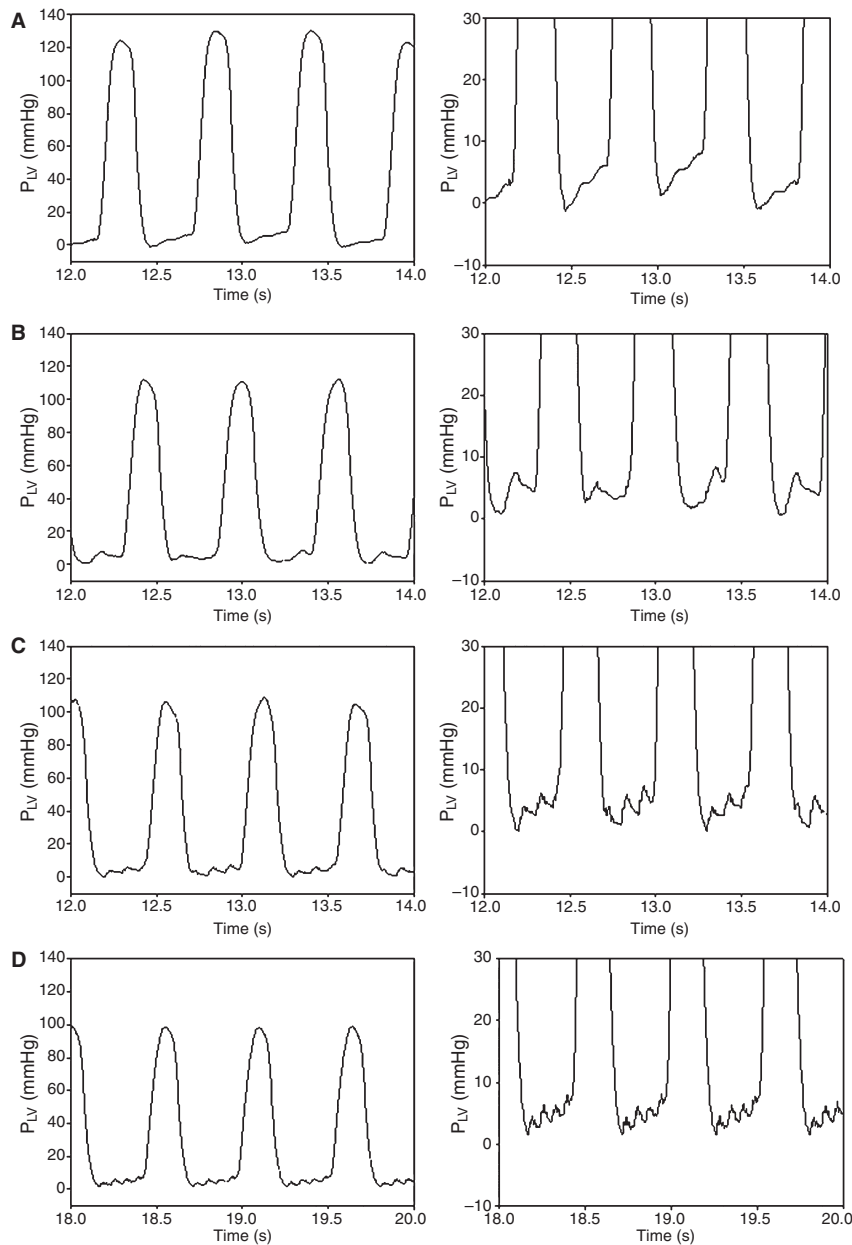


Figure 1. Representative examples of LV pressure traces (mmHg) at P_{LVED} 5 mmHg and PEEP 6 cm H_2O during CV and HFOV ($\bar{P}_{AW} \sim 10$ cm H_2O). Panel A is an example of LV pressure during CV. Panels B, C, and D are examples of LV pressure during HFOV 4 Hz, 10 Hz, and 15 Hz, respectively. The vertical scales on the left range are -10 mmHg to 140 mmHg and those on the right are from -10 mmHg to 30 mmHg.

Table 2 lists normalized RV stroke work (SW_{RV}) and SW_{LV} during CV (all PEEP levels) and HFOV (all frequencies and matched airway pressures) (100% set at prevolume load, CV PEEP 6 cm H_2O). At $P_{LVED} = 5$ mmHg, both SW_{RV} and SW_{LV} decreased during CV with increasing airway pressure; however, during HFOV, while SW_{LV} decreased, SW_{RV} generally increased with increased \bar{P}_{AW} . This reciprocal relationship may explain the apparent differences in LV performance during the two modes of ventila-

tion – see Discussion. At the higher filling pressure, both SW_{RV} and SW_{LV} decreased with increasing airway pressure during both CV and HFOV (except at 10 Hz, 20 cm H_2O \bar{P}_{AW}).

Discussion

In this study, we made two important observations. First, we observed that pulmonary vascular conductance,

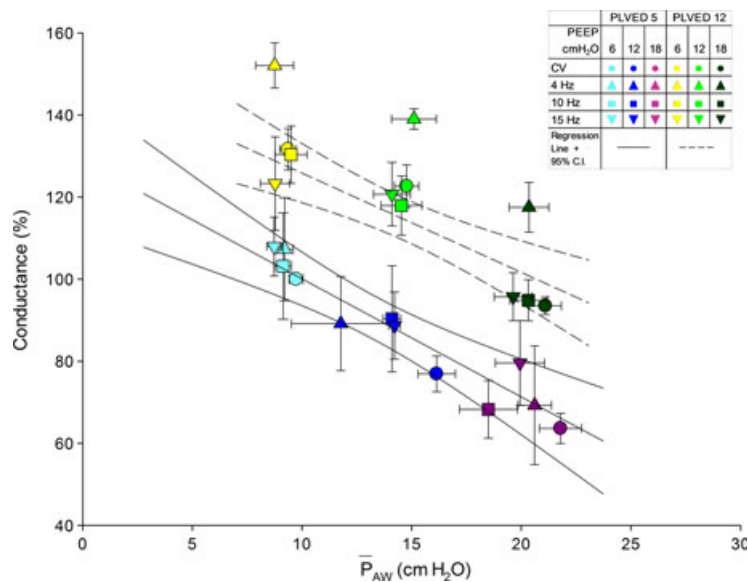


Figure 2. Relations between normalized pulmonary vascular conductance and \bar{P}_{AW} during CV and HFOV. The solid lines illustrate the best-fit linear regression and 95% confidence intervals for all the data at P_{LVED} 5 mmHg. The dashed lines indicate the best-fit linear regression and 95% confidence intervals for all the data at P_{LVED} 12 mmHg, except for HFOV at 4 Hz.

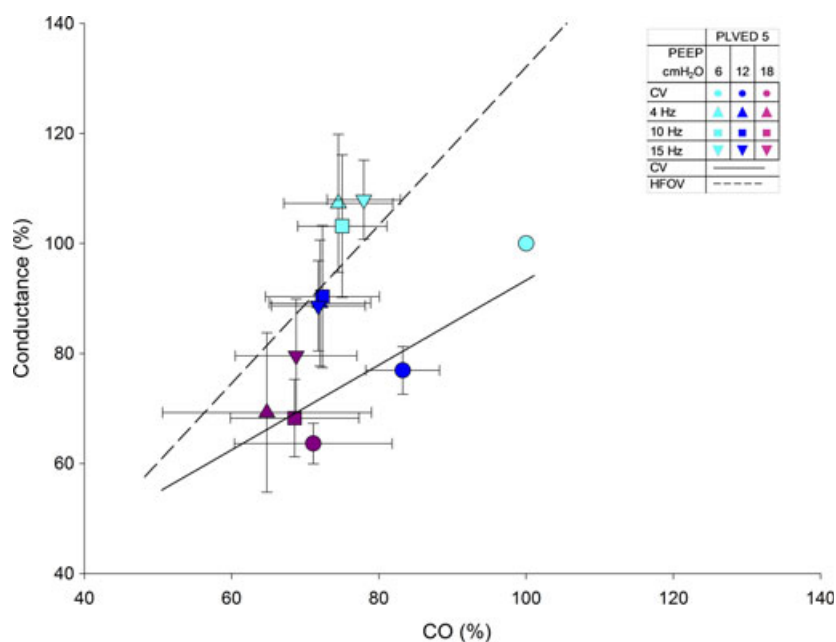


Figure 3. Relations between normalized pulmonary vascular conductance and normalized CO for P_{LVED} 5 mmHg. The solid line is the best-fit linear regression of the CV data and the dashed line, of the HFOV data. The slopes of the HFOV and CV data are statistically different ($P < 0.001$).

the amount of flow that the lungs will accept per unit driving (blood) pressure, varied under the different experimental conditions to a degree that may be clinically important. Second, we found that LV perfor-

mance was similar during CV and HFOV at similar airway pressures, consistent with the fact that LV preload was not changed by switching to from CV to HFOV.

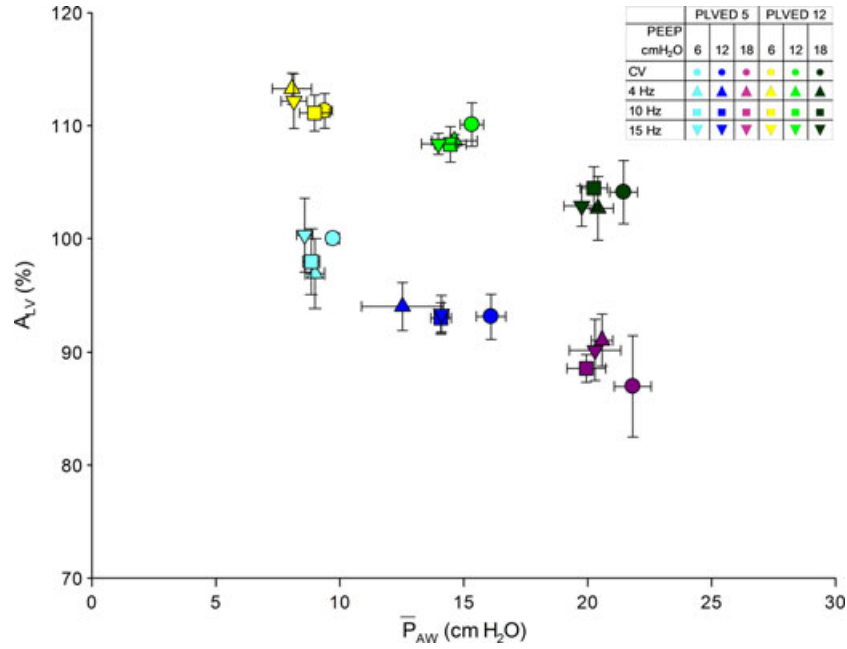


Figure 4. Relations between normalized LV preload (A_{LV}) and \bar{P}_{AW} during CV and HFOV. At each airway and filling pressure, A_{LV} was similar during both modes of ventilation. Volume loading increased A_{LV} at a given \bar{P}_{AW} , and increasing \bar{P}_{AW} decreased A_{LV} at both filling pressures.

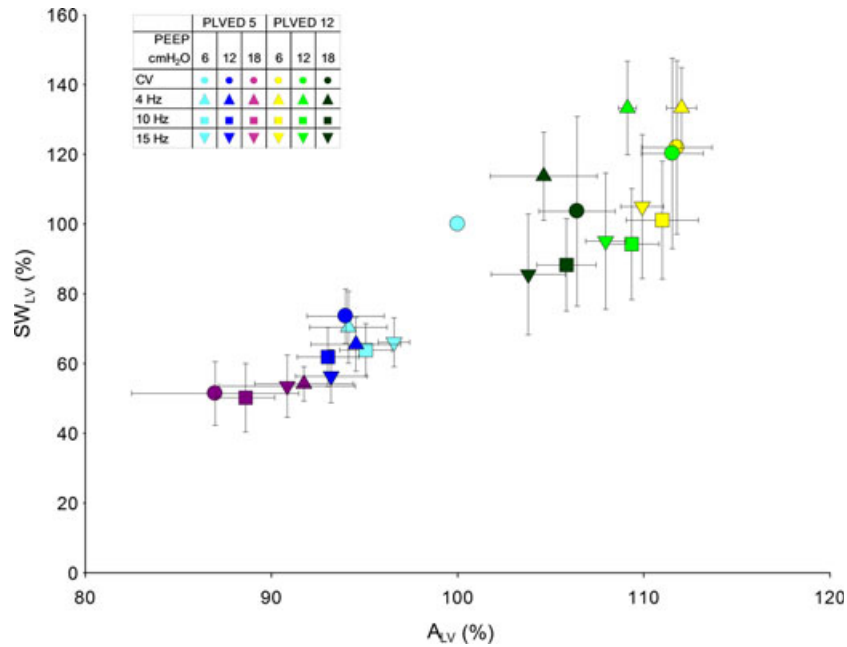
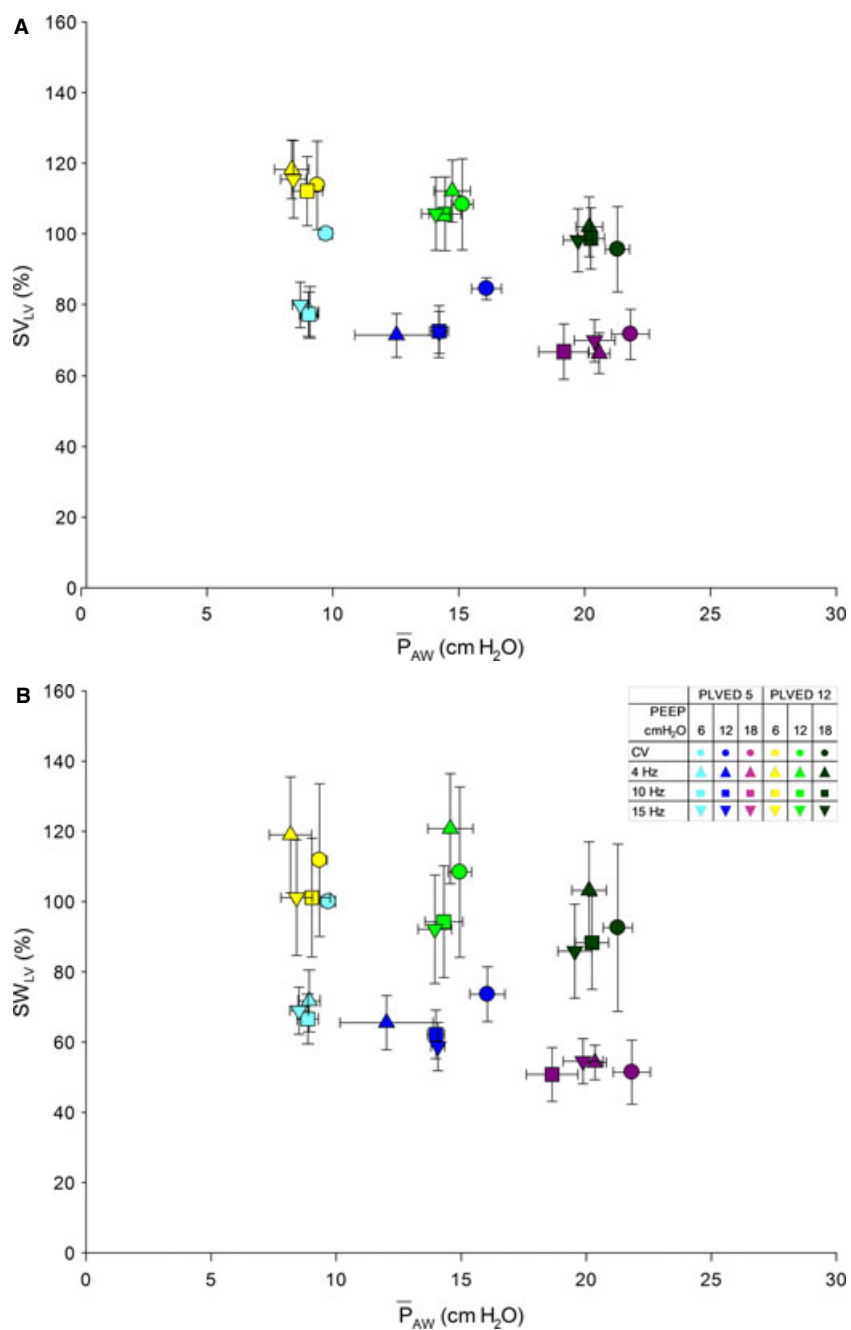


Figure 5. Relations between normalized SW_{LV} and normalized A_{LV} during CV and HFOV. SW_{LV} was closely related to A_{LV} , as predicted by the Frank–Starling mechanism.

Since the lung is a very complicated hydraulic-pneumatic system, ventilation may have profound phase-specific effects on cardiac and lung function through a

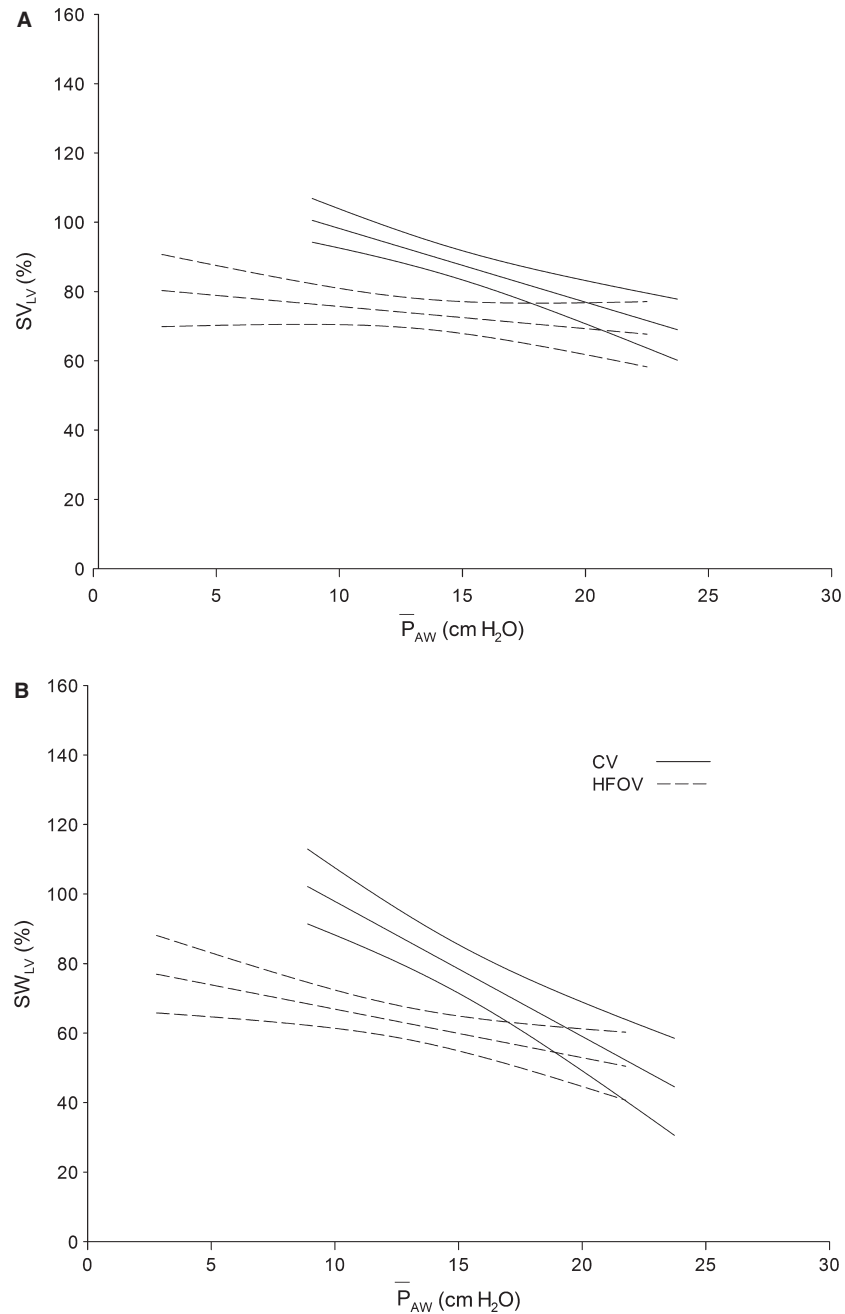
number of complex and interactive mechanisms (Morgan et al. 1966). These effects are primarily through changes in lung volume and intrathoracic pressure (Pinsky 1997).



Figures 6. Relations between \bar{P}_{AW} and normalized SV_{LV} (A) and normalized SW_{LV} (B) during CV and HFOV. At P_{LVED} 12 mmHg, SV_{LV} and SW_{LV} were statistically similar during CV and HFOV for a given \bar{P}_{AW} . At P_{LVED} 5 mmHg and \bar{P}_{AW} ~10 cm H₂O, SV_{LV} and SW_{LV} were significantly lower during HFOV (all frequencies) than during CV ($P < 0.001$, $P = 0.001$, respectively).

Given the very different patterns of changes in airway and intrathoracic pressure with the two modes of ventilation, it is not surprising that hemodynamic differences may exist between CV and HFOV. The cyclic changes in airway pressure during CV have considerably different

effects on changes in LV and RV preload (and therefore performance) (Mitchell et al. 2005a) than those that would be expected during HFOV, which should resemble the effects observed with variations in PEEP, yet lack the cyclic effects associated with CV.



Figures 7. Regression relations of normalized SV_{LV} (A) and normalized SW_{LV} (B) with \bar{P}_{AW} measured only at P_{LVED} 5 mmHg during CV and HFOV. In both of these relations, it can be seen that at the lower filling pressure, the regression lines for HFOV have a significantly different slope than for CV (both $P < 0.01$) and a significantly different Y-intercept ($P < 0.01$ and $P < 0.001$, respectively).

Effects of mechanical ventilation on pulmonary vascular conductance

A major objective of this study was to determine the effects of HFOV on the pulmonary vasculature of the lung. It can be argued that pulmonary vascular conductance is a better and more appropriate measure of the vascular properties of

the lung than the common measure, pulmonary vascular resistance (PVR). Conductance is normalized flow – the rate of blood flow that an organ will accept at a given driving pressure (i.e., conventionally, the difference between mean arterial and venous pressures).

The observed changes in pulmonary vascular conductance are consistent with previously reported work (Mitch-

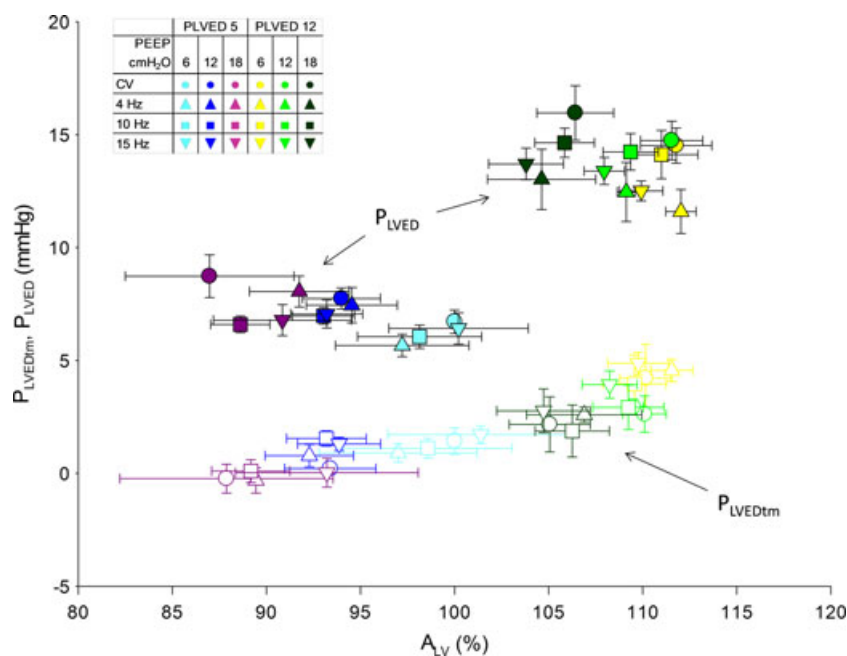


Figure 8. The predictable relations between P_{LVED} , P_{LVEDtm} , and A_{LV} over the range of filling pressures and positive end-expiratory pressures are apparent.

Table 2. Normalized RV and LV stroke work

	P_{LVED} 5 mmHg		P_{LVED} 12 mmHg	
	SW_{RV}	SW_{LV}	SW_{RV}	SW_{LV}
PEEP 6 cm H ₂ O	100 ± 0 (7)	100 ± 0 (8)	74 ± 14.3 (4)	112 ± 21.8 (5)
PEEP 12 cm H ₂ O	83 ± 9.1 (5)	74 ± 8.6 (6)	72 ± 17.2 (4)	108 ± 24.3 (5)
PEEP 18 cm H ₂ O	65 ± 4.8 (4)	51 ± 9.1 (5)	70 ± 17.2 (4)	93 ± 23.8 (5)
4 Hz; 10 cm H ₂ O	62 ± 7.2 (7)	72 ± 8.8 (7)	85 ± 16.6 (3)	119 ± 16.5 (4)
4 Hz; 15 cm H ₂ O	62 ± 8.7 (5)	66 ± 7.7 (6)	83 ± 16.4 (3)	121 ± 15.7 (4)
4 Hz; 20 cm H ₂ O	72 ± 9.7 (3)	54 ± 4.9 (5)	82 ± 17.1 (3)	103 ± 13.8 (4)
10 Hz; 10 cm H ₂ O	67 ± 8.4 (8)	67 ± 7.0 (8)	71 ± 11.9 (4)	101 ± 16.9 (5)
10 Hz; 15 cm H ₂ O	68 ± 10 (5)	62 ± 6.9 (6)	71 ± 11.8 (4)	94 ± 15.9 (5)
10 Hz; 20 cm H ₂ O	66 ± 14.2 (4)	51 ± 7.6 (5)	75 ± 11.7 (4)	88 ± 13.3 (5)
15 Hz; 10 cm H ₂ O	68 ± 7 (8)	69 ± 6.7 (8)	81 ± 9.9 (4)	101 ± 16.5 (5)
15 Hz; 15 cm H ₂ O	63 ± 10 (6)	59 ± 6.9 (7)	75 ± 7.8 (4)	92 ± 15.4 (5)
15 Hz; 20 cm H ₂ O	70 ± 14 (3)	55 ± 6.4 (4)	75 ± 7.0 (4)	86 ± 13.4 (5)

SW_{RV} , RV stroke work; SW_{LV} , LV stroke work.

ell et al. 2005a). Increased airway pressure, presumably through compression of the pulmonary vessels, increased resistance and decreased conductance. Volume loading increased conductance, presumably through recruitment of pulmonary vessels and distension of the already recruited vessels, thereby reducing the effects of external compression due to increased lung volume (Fig. 2) (Mitchell et al. 2005b; West 2006). At the higher filling pressure, it is interesting and perhaps important that HFOV at 4 Hz appears

to confer a special advantage in terms of increased pulmonary vascular conductance suggesting frequency-dependent effects on lung conductance. We cannot explain the increased conductance at 4 Hz. However, the magnitude of the increased conductance may represent a clinically relevant hemodynamic advantage. Additional studies would be required to determine what the optimal range of HFOV frequencies are, particularly in patients with unstable hemodynamics.

Cardiac output and conductance are linearly related (Fig. 3), which indicates that the pulmonary vasculature accepts an increase in flow without a proportional increase in the pressure gradient (Bouwmeester et al. 1985).

High-frequency oscillatory ventilation had a noticeable advantage on pulmonary vascular conductance at the lower filling pressure (P_{LVED} 5 mmHg); as cardiac output increased, the lung was able to accept increased output (Fig. 3). Interestingly, there was no such effect at the higher filling pressure, P_{LVED} 12 mmHg. This suggests that most or all pulmonary vessels were already recruited at the higher filling pressure.

The “chicken versus egg” debate between conductance and cardiac output still remains. Is decreased conductance the primary response to increased airway pressure (due to compression of the pulmonary vessels) and cardiac output decreases as a result? Or, is decreased cardiac output the primary response to increased airway pressure (due to external cardiac constraint) and conductance decreases as a result? Our study does not resolve this issue but demonstrates that regardless of the mechanism, the linear relationship differs between the two modes of ventilation at the lower filling pressure (Fig. 3).

Effects of mechanical ventilation on LV preload

The other major objective of this study was to determine if switching from conventional to high-frequency oscillatory ventilation at similar airway pressures would have similar effects on LV preload. Increased intrathoracic pressure may limit diastolic filling by several mechanisms. These include increased external constraint to the heart (Haynes et al. 1980; Marini et al. 1981; Cassidy and Ramanathan 1984; Kingma et al. 1987), redistribution of blood from the thorax to the periphery, and direct ventricular interaction (Cassidy and Mitchell 1981; Cassidy and Ramanathan 1984; Gibbons Kroeker CA 2003; Mitchell et al. 2005a,b). Importantly, our data suggest that the effects of mechanical ventilation on LV preload (i.e., end-diastolic A_{LV}) are closely related to mean airway and filling pressures and not to the mode of ventilation (Fig. 4). Thus, during both CV and HFOV, LV preload decreased similarly with increased airway pressure, and increased with volume loading, which also limited the decrease in LV preload associated with increased airway pressure. As one might predict in these acute studies, LV performance (SV_{LV} and SW_{LV}) was similar and closely related to LV preload during both modes of ventilation, except, as discussed below, at the lower filling pressure (Haynes et al. 1980; Marini et al. 1981; Linderer et al. 1983; Belenkie et al. 1989).

Effects of mechanical ventilation on LV performance

The relationship between LV preload (defined as LV end-diastolic area or transmural pressure) and systolic performance (LV stroke work) has been remarkably predictive during acute experiments in which the hemodynamic effects of mechanical ventilation have been studied (Mitchell et al. 2005a, 2011). Although this was generally true in this study as well, LV performance appeared to be adversely affected during HFOV compared to CV at low LV filling pressure (P_{LVED} 5 mmHg) and PEEP 6 cm H₂O (Fig. 6), while these differences were not apparent with increased filling and airway pressures. We recognize that clinically, there are strong arguments to avoid low filling pressures in ventilated patients. Nevertheless, it remains interesting that there is a difference in LV performance between the two modes of ventilation under those conditions. Heuer et al. (2012) similarly found no hemodynamic differences between CV and HFOV with increased airway pressure and demonstrated that, at a LV filling pressure of 12 mmHg, HFOV was associated with less adverse hemodynamic effects.

Decreased LV performance at low filling pressure

Positive end-expiratory pressures may increase the RV end-diastolic volume with both a decreased D_{LVAP} and a leftward septal shift (and flattening) through direct ventricular interaction. We and others have shown that this is more likely at low filling pressures (Jardin et al. 1981; Mitchell et al. 2005a,b). This may explain the apparent differences in LV performance between CV and HFOV at the lower filling pressure. Direct ventricular interaction during HFOV should resemble that observed at end-expiration with PEEP since HFOV delivers a sustained high airway pressure and minimizes swings in airway pressure. There is no apparent difference in LV performance between CV and HFOV at the higher filling pressure when little or no leftward septal shift would be expected (Fig. 5). We speculate that at the low filling pressure, there was septal flattening and less systolic leftward (normal) septal motion and possibly even paradoxical (systolic rightward septal motion). This, in effect, would transfer LV work to the RV. That the decrease in SW_{LV} was generally associated with an increase in SW_{RV} (Table 2) is consistent with the suggested mechanism. Paradoxical septal motion presumably decreased LV performance by decreasing the septal contribution to LV output while increasing the septal contribution to RV performance through transfer of pressure via the septum. This is similar to what occurs with left bundle branch block where LV dysfunction can be improved

when paradoxical septal motion is corrected through cardiac resynchronization pacing.

Clinical significance

Many hemodynamic variables appear to be affected similarly during CV and HFOV, which provide a degree of confidence to the clinician that switching to HFOV might not be associated with a hemodynamic disadvantage. In any mode of ventilation, high airway pressures and low filling pressures are associated with worse outcomes. Our data are in keeping with the well-known concepts that LV performance may be decreased at lower LV filling pressures, which can be prevented by insuring adequate filling pressures. In addition, our finding of improved pulmonary vascular conductance at the lower frequency during HFOV deserves further study to determine its potential clinical relevance.

Limitations

A normal, anesthetized animal model was used in this study. Clinically, HFOV is used in patients with abnormal lungs. Therefore, while our data provide insight into the hemodynamic effects of HFOV in healthy animals, our observations cannot be extrapolated to clinical situations without first performing similar work in appropriate models.

Although 10 dogs were studied, five died before completion of the protocol. The cause(s) of death could not be determined, but the long, complicated protocol, which included high levels of PEEP at a low filling pressure, may have had detrimental effects on the animals. Acidosis was observed in several dogs, especially in earlier experiments, when amplitude adjustments were not adequate to maintain normal CO₂ and pH levels. However, our data do not show a consistent effect of pH (within our observed ranges: 7.10–7.45) on cardiac function (data not shown).

Left ventricular preload is sometimes difficult to assess. Although LV transmural pressure is an appropriate measure to assess LV preload (Marini et al. 1981; Belenkie et al. 2002), there were challenges with its measurement during HFOV. Large high-frequency oscillations in airway pressure complicated the measurement of low pressures such as pericardial and diastolic intracavitary pressures. LV area was minimally affected by the rapid pressure oscillations and therefore was relied upon as the measure of LV preload in this study (Suga and Sagawa 1974; Appleyard and Glantz 1990).

Conclusions

Although increased airway pressure decreases pulmonary vascular conductance (i.e., the blood flow the lung will

accept for the same pressure difference) regardless of the mode of ventilation, HFOV at a frequency of 4 Hz appears to increase conductance substantially more than at the higher frequencies we studied. Also, HFOV appears to increase conductance relative to conventional ventilation at any level of cardiac output. These observations suggest that there is a need for further study in appropriate models to assess the potential clinical importance of such differences.

We also conclude that switching from CV to HFOV at similar airway pressures appears to have no significant effect on LV preload and that LV performance should also be unaffected except at low filling pressures, which are generally avoided clinically.

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Conflict of Interest

The authors declare no conflict of interest.

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