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# Strain effects on catalytic activity and stability of PdM nanoalloys with grain boundaries†

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Formate has emerged as a promising liquid hydrogen carrier for fuel cell applications, yet the kinetic limitations and stability issues of catalysts for formate dehydrogenation (FDH) and oxidation (FOR) remain challenging. Through systematic density functional theory (DFT) calculations, we computationally investigated how strain engineering modulates the electronic structure and catalytic behavior of PdM<sub>38</sub> and PdM<sub>79</sub> nanoalloys (M = Ir/Ag). Our theoretical models revealed that Ir atoms exhibit surface segregation driven by hydrogen/oxygen adsorption, effectively alleviating core lattice strain. Compressive strain was computationally observed to induce a negative shift in the d-band center of surface Pd sites. First-principles calculations identified core-shell PdIr and Janus-type PdAg configurations as optimal candidates, demonstrating enhanced theoretical activity for both FDH and FOR. This improvement was attributed to the elevated hydrogen adsorption free energy at Ir-enriched surfaces. By establishing a correlation between atomic strain, electronic structure, and catalytic descriptors, this computational study provides a theoretical framework for designing strain-engineered Pd-based catalysts, highlighting the critical role of element-specific segregation patterns in optimizing formate-based hydrogen storage systems as a hydrogen carrier and fuel.

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## 1. Introduction

Hydrogen is a promising clean energy carrier, capable of storing excess energy from renewable sources through water electrolysis.<sup>1,2</sup> However, its widespread adoption is hindered by inefficient storage technologies.<sup>3</sup> Storing hydrogen in chemical bonds (*e.g.*, formate salts, MHCO<sub>2</sub>, M = Na<sup>+</sup>, K<sup>+</sup>, and NH<sub>4</sub><sup>+</sup>)<sup>2</sup> offers a hydrogen storage capacity of 1.2–1.6 wt% (20–28 g H<sub>2</sub> per L) and ambient reversibility.<sup>4–6</sup> Formate further enables a closed carbon cycle through CO<sub>2</sub> electroreduction,<sup>7</sup> making it a sustainable energy carrier. Since Sasson *et al.* (1986) pioneered the sodium formate hydrogen storage system, research on FDH catalysts has been continuously advancing.<sup>8</sup> Although the homogeneous Ru/Ir systems have reversible hydrogen storage capabilities, they face the bottleneck of homogeneous separation.<sup>9,10</sup> Heterogeneous Pd-based catalysts (such as Pd/C and PdAg core-shell structures) achieve high activity (with a TOF of up to 311 h<sup>−1</sup>) through morphology/carrier regulation.<sup>7,9,11,12</sup> Current research mostly focuses on physical dimensions

(morphology, composition, carrier), but there is still a lack of systematic first-principles analysis of the in-depth mechanisms for performance improvement, such as atomic scale theories including electron transfer pathways, the regulation of the d-band center by strain effects, and the interfacial dynamic adsorption mechanism. This has restricted the targeted design of catalysts and breakthroughs in their performance.

Formate shows potential as an energy-conversion device. In direct formate fuel cells (DFFC), it oxidizes easily to generate electricity, with a theoretical voltage of 1.45 V.<sup>12,13</sup> Formate for DFFC can be produced *via* CO<sub>2</sub> electroreduction, promoting carbon-cycle sustainability.<sup>13</sup> However, DFFC's commercialization is hindered by the lack of efficient, stable catalysts for the anodic formate oxidation reaction (FOR).<sup>14</sup> Pd-based catalysts avoid CO poisoning but suffer from slow FOR kinetics due to strong hydrogen intermediate (H\*) binding, which blocks reactant adsorption. PdAg and PdCeO<sub>2</sub> catalysts show excellent FOR activity.<sup>11,15–20</sup> Adding Ir to PdAgIr nanoflower catalysts lowers the FOR onset potential. Doping AgPd core-shell nanoalloys with Ni creates AgPd Janus nanoalloys, but atomic-scale mechanisms remain unclear.<sup>21</sup> Computational analysis suggests alloying Pd with Ag/Ir weakens H\* adsorption, crucial for FOR kinetics.

Simulations of small clusters (38/79 atoms) reveal how truncated octahedral geometry links structural symmetry to catalytic activity, similar to high-index crystal plane behavior. Yudanov *et al.* simulated large particles (1000 atoms) using

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smaller clusters ( $\sim 300$  atoms), optimizing the outer shell while keeping the core as bulk structure.<sup>22</sup> Standard DFT calculations scale as  $O(N^3)$  with valence electrons, limiting nanoparticle modeling to diameters of about 2–3 nm, smaller than the typical 4–10 nm range studied experimentally.<sup>23</sup> Cao *et al.* found optimal specific activity for Pt–Ni octahedral catalysts at edge lengths  $>5.5$  nm and  $\text{Pt}_{0.85}\text{Ni}_{0.15}$  composition, while mass activity peaks at 3.3–3.8 nm and  $\text{Pt}_{0.8}\text{Ni}_{0.2}$  composition. For nanoparticles of 10 nm (ref. 24) and 50 nm,<sup>21</sup> compressive or tensile strain can be regulated to alter the d-band center and intermediate adsorption, enhancing FOR electrocatalytic activity or FDH catalytic performance.

In polymetallic nanomaterials, grain boundaries, as critical structural features, have a significant impact on catalytic performance.<sup>25</sup> Firstly, the presence of grain boundaries increases the number of active sites, providing more adsorption positions for reactants.<sup>26</sup> Secondly, the local strain at grain boundaries optimizes the electronic structure of the catalyst, adjusts the position of the d-band center, thereby enhancing the adsorption capacity for reaction intermediates.<sup>25</sup> Moreover, the existence of grain boundaries stabilizes the catalyst structure, reduces the migration of defects such as dislocations and dissolution, thereby improving the durability of the catalyst.<sup>24</sup> Taking the core–shell and sandwich structures of PdIr and AgPd as examples, the grain boundaries in these structures play a crucial role in enhancing catalytic activity and stability. Research shows that the presence of grain boundaries not only increases the number of active sites but also enhances the strength of the material by hindering dislocation movement, thereby improving the stability of the catalyst.

Structural distortions at grain boundaries can induce localized strain fields, which in turn cooperatively regulate the position of the d-band center. Strain effects can enhance catalytic performance.<sup>27</sup> Atomic strain is controlled by adjusting metal composition and structure.<sup>28</sup> Size effects are significant in catalysis, as size changes alter atomic strain and electronic properties.<sup>29</sup> A 1% atomic strain shifts the Pt catalyst's d-band center by 0.1 eV, altering intermediate adsorption energy.<sup>30</sup> Strain engineering optimizes intermediate adsorption energy through d-band center tuning, combined with elemental segregation dynamics, providing a theoretical framework for catalyst design. Jin *et al.* reported that compressive strain in AgPd bulk alloys shifts the d-band center downward, weakening intermediate adsorption and enhancing FOR catalytic efficiency.<sup>19</sup>

The precise synthesis of  $\text{PdM}_{38}$  and  $\text{PdM}_{79}$  ( $M = \text{Ir}, \text{Ag}$ ) nanoalloys remains a significant challenge. However, recent advancements in the spatially controlled growth of bimetallic nanoparticles, such as PdAu Janus and PtNi core-frame structures, provide promising pathways.<sup>21,31</sup> In PdAg systems, the high miscibility of Pd and Ag may facilitate interfacial alloying, yet the thermodynamic preference for Janus configurations can be strategically controlled through kinetic regulation during reduction.<sup>32,33</sup> Notably, Zhang *et al.* successfully synthesized  $\text{Au@PdAg}$  and  $\text{Au@PtRh}$  sandwich structures using a seed-assisted reduction method, demonstrating the experimental feasibility of multi-layer metal deposition.<sup>34</sup> This achievement

offers experimental validation for the PdIr and PdAg sandwich structures predicted by DFT in this study. Although the synthesis of PdIr and PdAg sandwich structures still faces challenges, including metal compatibility, interface control, and precise control over size and morphology, existing experimental methods suggest their feasibility. Future research should prioritize optimizing synthesis techniques, such as ligand-assisted approaches, and validating their catalytic performance to substantiate the theoretically predicted structures and properties. No systematic theoretical study has explored PdIr and PdAg nanoalloys' catalytic activities for FDH and FOR. FDH and FOR occur in liquid phase, where catalysts are embedded in solvents, and adsorbates accumulate on the surface.

Surface segregation in alloy nanoparticles, induced by CO, H, and adsorbed oxygen, raises the question of whether H (an FDH/FOR intermediate) and O in oxidative settings can induce segregation.<sup>35,36</sup> In this computational study, we employ density functional theory (DFT) and molecular dynamics simulations to systematically investigate PdIr and PdAg nanoalloys (Janus, core–shell, sandwich) for FDH/FOR, along with investigating the electronic structure and atomic strain of  $\text{PdM}_{38}$  and  $\text{PdM}_{79}$  ( $M = \text{Ir}, \text{Ag}$ ) nanoalloys. We also explore segregation, anti-segregation phenomena and the structural stability of Janus and core–shell nanoalloys. Results show  $\text{Pd}_{32}\text{Ir}_6$ ,  $\text{Pd}_{60}\text{Ir}_{19}$  core–shell and  $\text{Pd}_{19}\text{Ag}_{19}$ ,  $\text{Pd}_{34}\text{Ag}_{45}$  Janus nanoalloys have the highest FDH and FOR catalytic activities in relevant groups. In vacuum, Ag segregates from core to shell; with H and O adsorption, Pd in PdAg and Ir in PdIr do so, relieving internal stress. The component redistribution induced by segregation behavior alters the strain field distribution near grain boundaries, thereby enabling dynamic regulation of active sites.

Additionally, the analysis of atomic strain shows tensile strain in the Ag region and compressive strain in the Pd region of PdAg Janus and sandwich nanoalloys. In PdAg core–shell ones, cores have tensile strain and shells have compressive strain. Compressive strain exists at the interface of PdIr sandwich nanoalloys. This research deepens understanding of PdIr and PdAg nanoalloys' effects on formate reactions, guiding catalyst development and providing new views on formate-related power sources for portable devices. Importantly, the proposed core–shell and Janus configurations build upon experimentally realized analogs: PdAg core–shell structures<sup>10</sup> and PdAu Janus nanoparticles<sup>32</sup> synthesized *via* kinetically controlled reduction, demonstrating the feasibility of our design principles.

## 2. Methods

### 2.1 Nanoalloy structure generation

The Birmingham Nanoalloy Genetic Algorithm (BCGA) software,<sup>37</sup> in combination with a many-body Gupta potential,<sup>38</sup> was utilized to create  $\text{PdM}_{38}$  and  $\text{PdM}_{79}$  ( $M = \text{Ir}, \text{Ag}$ ) nanoalloys. These nanoalloys include pure monometallic nanoalloys of Ir, Ag, and Pd, as well as bimetallic nanoalloys with Janus, sandwich, and core–shell structures. The choice of nanoalloys with 38 and 79 atoms was based on their magical numbers, resulting

in complete truncated octahedral (TO) structures.<sup>39</sup> Both (100) and (111) surfaces enclose these nanoalloys. Henceforth, the PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys were donated as Ir<sub>38</sub>, Ag<sub>38</sub>, Pd<sub>38</sub>, Pd<sub>19</sub>M<sub>19</sub> Janus, Pd<sub>20</sub>M<sub>18</sub> sandwich, Pd<sub>32</sub>M<sub>6</sub> core-shell, Pd<sub>34</sub>M<sub>45</sub> Janus, Pd<sub>19</sub>M<sub>60</sub> sandwich, and Pd<sub>60</sub>M<sub>19</sub> core-shell (M = Ir, Ag) nanoalloys, respectively. The Gupta potential<sup>35</sup> accurately describes the surface energy of a metal compared to other empirical potential, such as the embedded atom method (EAM) potential.<sup>40</sup> It can be applied at the appropriate time corresponding to each structure, ensuring the structure converges directly to its stable conformation regardless of the initial configuration.

## 2.2 Molecular dynamics (MD) simulations

The MD simulations were used to determine the atomic strain fields and stress distributions of the PdIr and PdAg nanoalloys. The simulations employed the neural network (NN) interatomic potential<sup>41</sup> with the LAMMPS software<sup>42</sup> due to the absence of an empirical potential for PdIr. To achieve the equilibrium configuration, conjugate gradient (CG) minimization was initially applied to the entire nanoalloy, following by MD simulations using the canonical ensemble (NVT) at 50 K with a Nose–Hoover thermostat<sup>43</sup> for 100 picoseconds. The atomic strain was calculated by comparing the final configuration with the initial configuration and then mapped atom-wise onto the final configuration using the OVITO software.<sup>44</sup> The ESI† contains detailed instructions for calculating and visualizing the atomic strain using the OVITO software. This methodology is consistent with previously reported studies.<sup>45–47</sup>

## 2.3 Density functional theory (DFT) calculations

The DFT calculations were performed using the Vienna *Ab initio* Simulation Package (VASP) employing the periodic plane-wave method.<sup>48–50</sup> The electron exchange and correlation interaction were described using the projected augmented wave (PAW) scheme<sup>51</sup> and the Perdew–Burke–Ernzerhof (PBE)<sup>52</sup> functional, employing the generalized gradient approximation (GGA). To ensure complete structural relaxation, all model atomic configurations were relaxed. The plane wave cutoff was set to 450 eV, and the self-consistent field and atomic force convergence criteria were set to  $1 \times 10^{-7}$  eV and  $0.02 \text{ eV } \text{\AA}^{-1}$ , respectively, for both structural relaxation and other calculations. The nanoalloys were positioned in the centre of a suitably large supercell (30 Å) to ensure a sufficient separation between periodic images. The Brillouin zone was sampled using the  $\Gamma$  point. Additionally, *ab initio* molecular dynamics simulations (AIMD) were performed in the canonical ensemble (NVT)<sup>53</sup> with Nose–Hoover thermostat<sup>54</sup> at 300, 400, 500 and 600 K for a time period of 20 ps.

## 2.4 Thermodynamic treatment

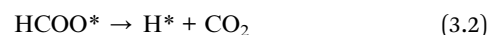
The thermodynamics of the formate oxidation and formate dehydrogenation reaction mechanisms were evaluated by computing the Gibbs free energy of the various reaction steps as follows:  $\Delta G = \Delta H - T\Delta S$  where  $\Delta H$  is the enthalpy change (including total energy of electrons, vibrational contribution,

zero-point energy (ZPE) and neglecting  $p\Delta V$ ),  $T$  is set to the room temperature of 298.15 K, and  $\Delta S$  is the vibrational entropy change (obtained from the partition function as the reactant molecules are adsorbed on the catalyst surface and the translational and rotational entropy is restricted). The total energy of the adsorbent was calculated by VASP, and the thermodynamic corrections including the ZPE, the vibrational internal energy, and the vibrational entropy obtained from the partition function are obtained from the VASPKIT script.<sup>55</sup> The other details of the calculations are provided in the ESI.†

## 3. Results and discussion

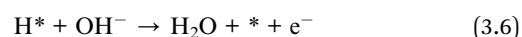
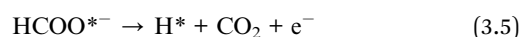
Initially, the PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys obtained through genetic algorithm were subjected to DFT structural relaxation. Fig. S1† illustrates the atomic structures of PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys with truncated octahedral (TO) structures following DFT relaxation. Fig. S1(a) and (c)† demonstrate that the PdIr<sub>38</sub> and PdAg<sub>38</sub> nanoalloys maintained complete TO structures after DFT relaxation, while Fig. S1(b) and (d)† reveal that the Pd<sub>34</sub>Ir<sub>45</sub> Janus and Pd<sub>34</sub>Ag<sub>45</sub> Janus nanoalloys displayed minor deformations. These nanoalloys have a core-shell structure, with Pd atoms forming the shell and Ir or Ag atoms occupying the core.

The DFT calculations were conducted on PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys to investigate their catalytic activity for FDH and electrocatalytic activity for FOR. At room temperature, formate can release hydrogen through the dehydrogenation reaction, and the elementary steps of FDH<sup>56</sup> are as follows:



where \*, HCOO\* and H\* represent the active site on the catalyst surface, the adsorbed formate molecules, and the adsorbed H intermediates, respectively. The changes in free energy for reactions (3.1), (3.2), and (3.3) are indicated as  $\Delta G_1$ ,  $\Delta G_2$ , and  $\Delta G_3$ , correspondingly. FDH is a thermocatalytic reaction. In a liquid environment, it promotes the spontaneous decomposition of formic acid to produce hydrogen through catalysts (such as the PdAg Janus structure), relying on the regulation of the Gibbs free energy of H intermediate desorption.

The format oxidation reaction (FOR) plays a critical role as the anode reaction in the DFFC, ultimately determining its performance. According to prior research,<sup>15,17</sup> the electrochemical oxidation of HCOO<sup>−</sup> to CO<sub>2</sub> and H<sub>2</sub>O in an alkaline environment follows a direct associative pathway, typically involving of the following elementary steps:



where  $\text{HCOO}^-$ ,  $*$ ,  $\text{HCOO}^{*-}$  and  $\text{H}^*$  represent formate molecules, active sites on the catalyst surface, formate and H intermediates adsorbed on the catalyst surface, respectively. The equilibrium potential ( $U_0$ ) for FOR is  $-1.05$  V. The overpotential ( $\eta$ )<sup>17</sup> can be calculated using the equation  $e\eta = \max\{\Delta G_2, \Delta G_3\} - U_0 \times e$ , where  $\Delta G_2$  and  $\Delta G_3$  refer to the change in free energy for reactions (3.5) and (3.6), respectively. FOR is an electrocatalytic reaction. As the anode of a direct formic acid fuel cell (DFFC), it oxidizes formic acid to  $\text{CO}_2$  through an electrochemical pathway (electron transfer), and its activity is restricted by the H adsorption energy and over-potential.

The adsorption of reactants onto the catalyst surface is a fundamental process in catalytic reactions, and accordingly, the adsorption energy serves as a crucial determinant of reaction catalytic activity. Excessive or insufficient adsorption energy can hinder the catalytic reaction. Therefore, it is imperative to optimize the adsorption energy of the catalyst towards the reactants and their intermediate products to achieve optimal catalytic activity. The adsorption energies of H, OH, and HCOO on  $\text{PdM}_{38}$  and  $\text{PdM}_{79}$  ( $M = \text{Ir}, \text{Ag}$ ) nanoalloys are presented in Fig. 1.

Fig. 1(a) and (b) shows that the core-shell PdIr nanoalloy displays moderate adsorption energy for H, OH, and HCOO,

whereas the sandwich and Janus PdIr nanoalloys exhibit strong adsorption energy for these species. This difference is attributed to the Ir element's robust adsorption energy on its surface for H, OH, and HCOO. As Fig. 1(c) and (d) demonstrates, the Janus structure of PdAg nanoalloy exhibits moderate adsorption energy for H, OH, and HCOO, whereas the sandwich and core-shell structures exhibit stronger adsorption energy.

Fig. 2 summarizes the FDH catalytic properties of  $\text{PdM}_{38}$  and  $\text{PdM}_{79}$  ( $M = \text{Ir}, \text{Ag}$ ) nanoalloys. The results reveal that the primary limitation to FDH activity stems from the hindered desorption of hydrogen intermediates (denoted as  $\Delta G_3$ ), which results from excessively strong hydrogen adsorption free energy, as illustrated in Fig. 2(a–d). Consequently,  $\Delta G_3$  emerges as the crucial evaluation parameter for assessing FDH reaction performance.

Fig. 2(e) illustrates the  $\Delta G_3$  for the FDH of  $\text{PdM}_{38}$  and  $\text{PdM}_{79}$  ( $M = \text{Ir}, \text{Ag}$ ) nanoalloys. The  $\text{Ir}_{38}$ ,  $\text{Ag}_{38}$ ,  $\text{Ir}_{79}$  and  $\text{Ag}_{79}$  nanoalloys exhibit inferior FDH catalytic activity, with  $\Delta G_3$  values of 0.536, 0.568, 0.563 and 0.613 eV, respectively. In contrast, the  $\text{Pd}_{38}$  and  $\text{Pd}_{79}$  nanoalloys demonstrate  $\Delta G_3$  values of 0.362 and 0.369 eV, respectively, indicating Pd as the active element for FDH. Moreover, the  $\Delta G_3$  values for FDH of  $\text{Pd}_{32}\text{Ir}_6$  core-shell,  $\text{Pd}_{60}\text{Ir}_{19}$  core-shell,  $\text{Pd}_{19}\text{Ag}_{19}$  Janus and  $\text{Pd}_{34}\text{Ag}_{45}$  Janus nanoalloys are

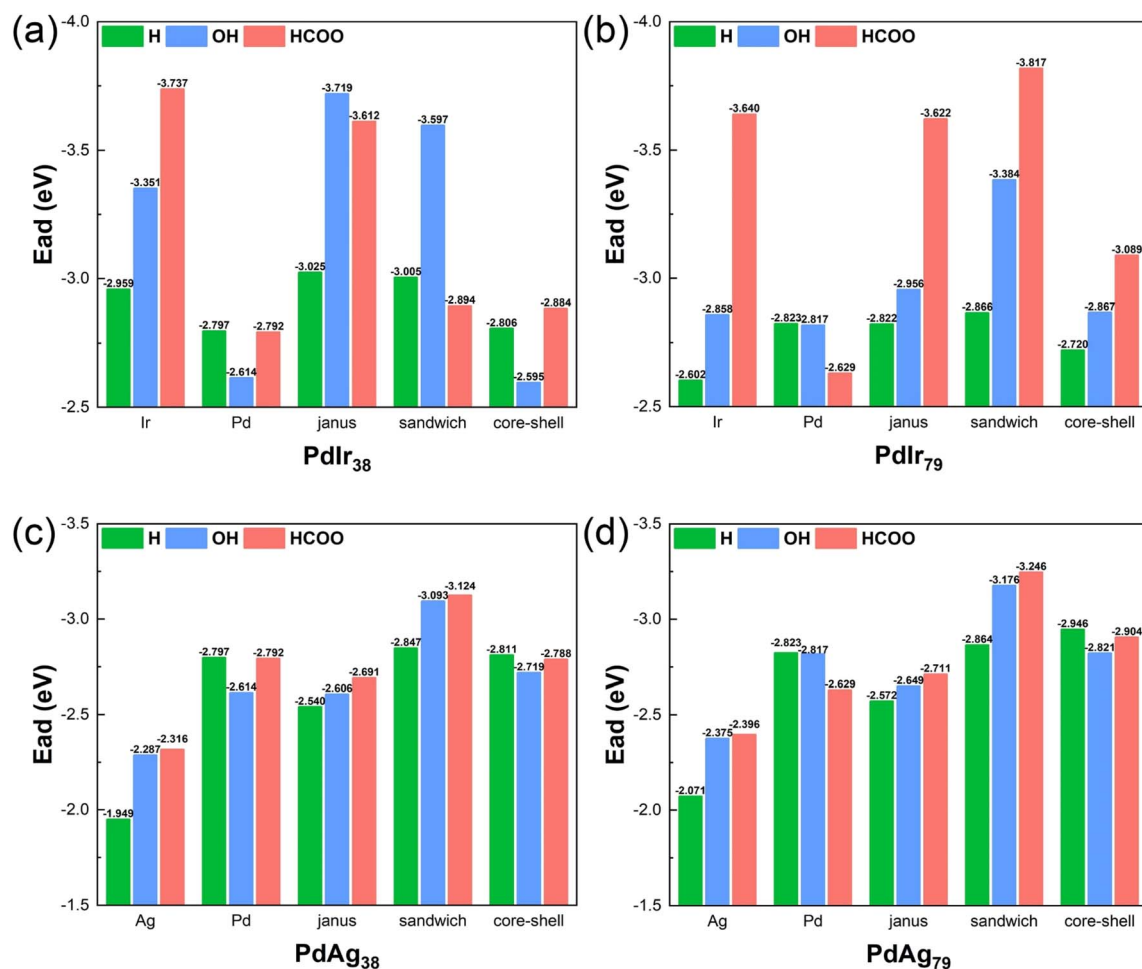


Fig. 1 The absorption energy of H, OH, and HCOO on (a)  $\text{PdIr}_{38}$ , (b)  $\text{PdIr}_{79}$ , (c)  $\text{PdAg}_{38}$  and (d)  $\text{PdAg}_{79}$  nanoalloys.

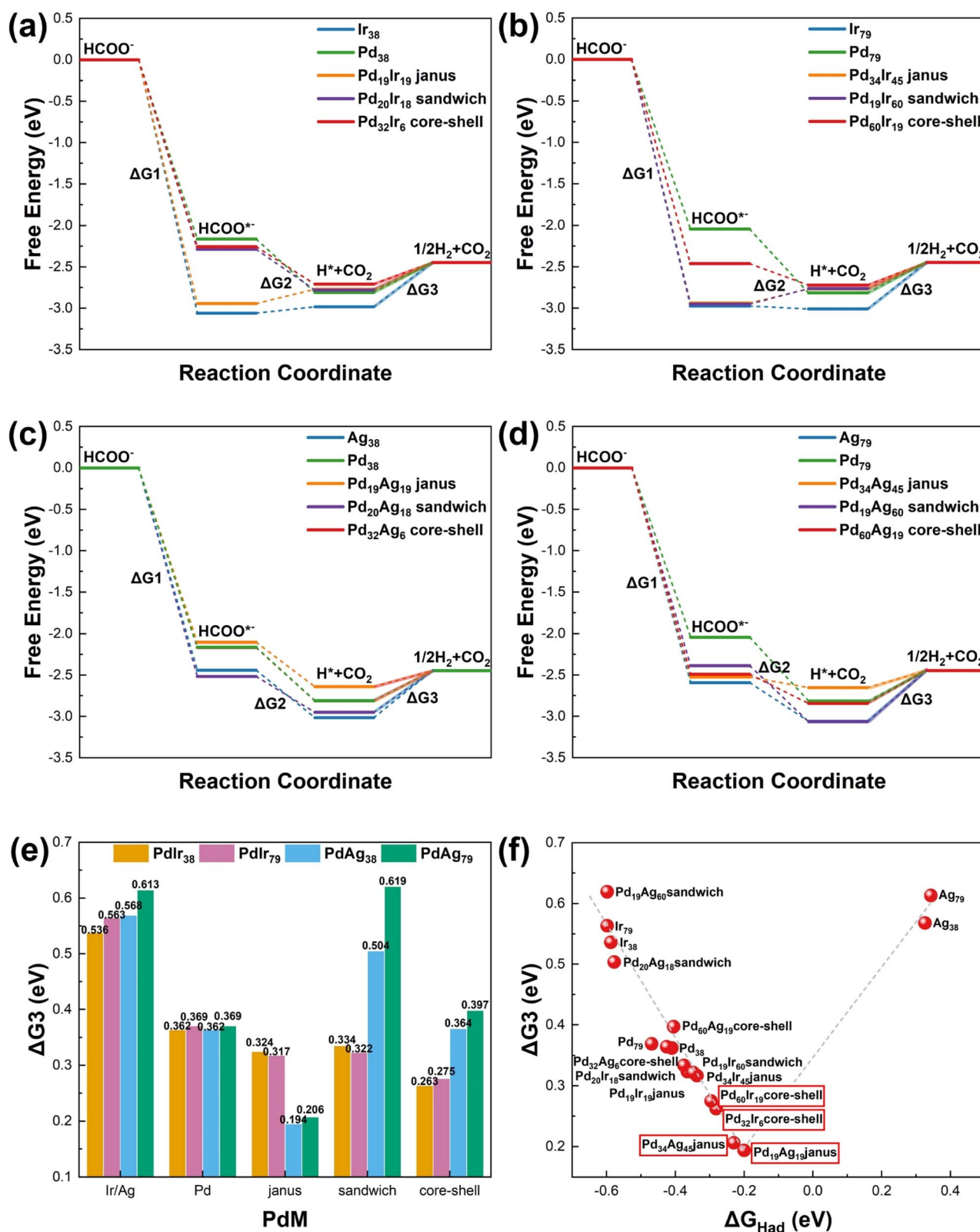


Fig. 2 Catalytic activity of the formate dehydrogenation reaction (FDH) on PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys. The free energy diagram of FDH on (a) PdIr<sub>38</sub>, (b) PdIr<sub>79</sub>, (c) PdAg<sub>38</sub> and (d) PdAg<sub>79</sub> nanoalloys. (e) The ΔG3 of FDH of the PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys. (f) A plot of the ΔG3 of FDH versus the hydrogen adsorption free energy.

0.263, 0.275, 0.194 and 0.206 eV, respectively. These findings suggest that synthesizing catalysts with specific shapes can enhance the catalytic activity of FDH. Additionally, we computed the catalytic activity of FDH in bulk Ir, Ag, and Pd, comparing it to that of nanoalloys. As illustrated in Fig. S2,<sup>†</sup> the FDH catalytic activity of the nanoalloys surpasses that of the bulk Ir, Ag, and Pd.

Fig. 2(f) provides a summary of the relationship between hydrogen adsorption free energy and  $\Delta G_3$  in FDH. The free energy of hydrogen adsorption exhibits a volcano-type relationship with FDH activity, with an optimum free energy value yielding the highest activity. This is due to the stronger hydrogen adsorption free energy hindering the desorption of H intermediates, while the weaker hydrogen adsorption free energy is not conducive to the reaction. Among the PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys, the Pd<sub>19</sub>Ag<sub>19</sub> Janus nanoalloy exhibits the highest FDH catalytic activity, primarily attributed to its moderate H adsorption free energy.

Furthermore, a previous study<sup>57</sup> has indicated that the selectivity of PdAu nanoalloys in HCOOH dehydrogenation relies on the surface Pd atoms. In particular, the Pd atom positioned at the Pd–Au interface demonstrates a higher inclination for HCOOH dehydrogenation, while the Pd atoms located at the Pd(111) surface, lacking coordination with Au atom, preferentially facilitate the dehydration of HCOOH. Consequently, the Janus-structured PdAu nanoalloy proves favourable for HCOOH dehydrogenation, consistent with the current calculations demonstrating that the Pd<sub>19</sub>Ag<sub>19</sub> Janus nanoalloy exhibits the best FDH catalytic activity. The Janus structure also serves as a miniature model of grain boundaries. Grain boundaries have a significant impact on the adsorption energy. The local strain at grain boundaries can optimize the electronic structure of the catalyst, thereby modulating the adsorption energy of reactants. For example, the Pd<sub>19</sub>Ag<sub>19</sub> Janus nanoalloy exhibits moderate H adsorption energy at the grain boundaries, contributing to its superior FDH catalytic activity. This electronic structure optimization induced by grain boundaries offers new insights for catalyst design.

The catalytic activities of PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys for the FOR were evaluated by calculating their overpotentials, as depicted in Fig. 3. Fig. 3(a–d) presents the free energy diagram of PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys at equilibrium potential, revealing that the obstacle step for Ir<sub>38</sub>, Ag<sub>38</sub>, Pd<sub>38</sub>, Ir<sub>79</sub>, Ag<sub>79</sub>, Pd<sub>79</sub>, Pd<sub>19</sub>Ir<sub>60</sub> sandwich, Pd<sub>34</sub>Ag<sub>45</sub> Janus and Pd<sub>60</sub>Ag<sub>19</sub> core-shell nanoalloys is the breaking of the C–H bond in the formate molecule. Conversely, for Pd<sub>19</sub>Ir<sub>19</sub> Janus, Pd<sub>20</sub>Ir<sub>18</sub> sandwich, Pd<sub>32</sub>Ir<sub>6</sub> core-shell, Pd<sub>34</sub>Ir<sub>45</sub> Janus, Pd<sub>60</sub>Ir<sub>19</sub> core-shell, Pd<sub>20</sub>Ag<sub>18</sub> sandwich, Pd<sub>32</sub>Ag<sub>6</sub> core-shell and Pd<sub>19</sub>Ag<sub>60</sub> sandwich nanoalloys, the obstacle step is the oxidation of the H intermediate to H<sub>2</sub>O. The Pd<sub>32</sub>Ir<sub>6</sub> core-shell, Pd<sub>60</sub>Ir<sub>19</sub> core-shell, Pd<sub>19</sub>Ag<sub>19</sub> Janus and Pd<sub>34</sub>Ag<sub>45</sub> Janus nanoalloys exhibit the highest FOR catalytic activity among the PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys. The core-shell structure of the PdIr<sub>38</sub> and PdIr<sub>79</sub> nanoalloys demonstrates the best FOR catalytic activity due to the excessive hydrogen adsorption free energy of Ir elements on the surface of Janus and sandwich structures.

Fig. 3(e) presents the FOR overpotentials of PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys. The FOR overpotentials for Ir<sub>38</sub>, Ag<sub>38</sub>, Pd<sub>38</sub>, Ir<sub>79</sub>, Ag<sub>79</sub>, and Pd<sub>79</sub> nanoalloys are 1.129, 1.377, 0.967, 1.325, 1.421 and 1.196 V, respectively. However, the inclusion of the alloying effect of Pd with Ir or Ag significantly reduced the overpotentials of Pd<sub>32</sub>Ir<sub>6</sub> core-shell, Pd<sub>60</sub>Ir<sub>19</sub> core-shell, Pd<sub>19</sub>Ag<sub>19</sub> Janus and Pd<sub>34</sub>Ag<sub>45</sub> Janus nanoalloys to 0.584, 0.591, 0.515 and 0.536 V, respectively. Fig. 3(f) illustrates the relationship between the H adsorption free energy and FOR overpotential, indicating the presence of an optimum free energy value that results in the highest activity. This relationship is consistent with the relationship between H adsorption free energy and FDH catalytic activity. Fig. S3–S6<sup>†</sup> illustrates the FOR free energy of PdM<sub>38</sub>, PdM<sub>79</sub> (M = Ir, Ag) nanoalloys at 0 V, equilibrium potential and overpotential, as well as the overpotential of FOR. Additionally, we calculated the free energy and overpotential of the FOR for bulk Ir, Ag, and Pd. This data is illustrated in Fig. S7 and S8.<sup>†</sup> The FOR catalytic activity of the PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys surpasses that of the bulk Ir, Ag, and Pd. Table 1 summarizes the catalytic and electrocatalytic activities of nanoalloy PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) for the FDH and FOR, as well as the adsorption free energy of hydrogen and formate, in comparison to their bulk counterparts, Ir, Ag, and Pd.

For a catalyst, a lower relative d-band center to the Fermi level results in lower adsorption energy for the adsorbed intermediates. As the d-band center shifts upward, a distinctive antibonding state emerges above the Fermi level.<sup>58</sup> The empty antibonding states above the Fermi level correspond to stronger bonds, which becomes increasingly stronger as their numbers increase.<sup>59</sup> Consequently, strong bonding occurs when the antibonding states are shifted upward through the Fermi level, resulting in their emptiness, whereas weak bonding occurs when the antibonding states are shifted downward through the Fermi level, leading to their filling.<sup>60</sup>

We calculated the projected density of states (PDOS) and d-band center for PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys. As shown in Fig. S9 and S10,<sup>†</sup> the Pd<sub>32</sub>Ir<sub>6</sub> core-shell, Pd<sub>60</sub>Ir<sub>19</sub> core-shell, Pd<sub>19</sub>Ag<sub>19</sub> Janus and Pd<sub>34</sub>Ag<sub>45</sub> Janus nanoalloys have a d-band center of –2.320, –2.819, –2.855 and –2.598 eV, located between the Ir<sub>38</sub>, Ag<sub>38</sub>, Pd<sub>38</sub>, Ir<sub>79</sub>, Ag<sub>79</sub>, and Pd<sub>79</sub> nanoalloys. These findings suggest that the Pd<sub>32</sub>Ir<sub>6</sub> core-shell, Pd<sub>60</sub>Ir<sub>19</sub> core-shell, Pd<sub>19</sub>Ag<sub>19</sub> Janus and Pd<sub>34</sub>Ag<sub>45</sub> Janus nanoalloys have moderate d-band center, indicating moderate adsorption free energy of H intermediates. The d-band center of PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys is shown in Fig. S10.<sup>†</sup> This d-band modulation mechanism provides a unified framework for understanding both FDH and FOR enhancements. While FDH activity is directly governed by H desorption energetics ( $\Delta G_3$ ), the improved FOR performance in core-shell/Janus structures originates from dual effects: (1) strain-induced d-band downshifting weakens HCOO adsorption to facilitate C–H cleavage in simple structures, and (2) optimized H adsorption energy enables efficient H oxidation kinetics in complex architectures. The structural design flexibility allows decoupling of adsorption energetics for different intermediates, circumventing the traditional scaling relationship limitations.

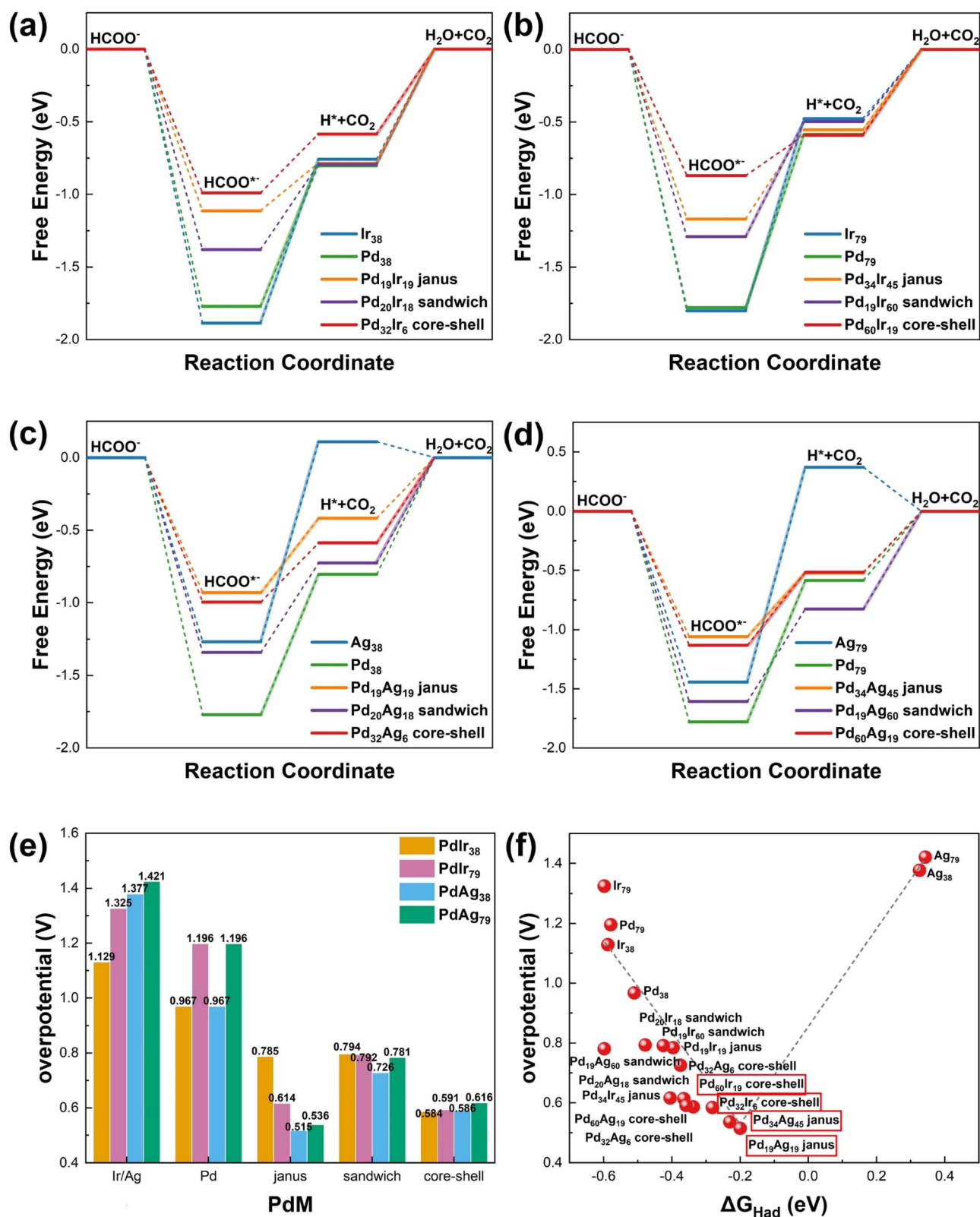


Fig. 3 Catalytic activity of the formate oxidation reaction (FOR) on PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys. The free energy diagram of FOR on (a) PdIr<sub>38</sub>, (b) PdIr<sub>79</sub>, (c) PdAg<sub>38</sub> and (d) PdAg<sub>79</sub> nanoalloys. (e) The overpotential of FOR of the PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys. (f) A plot of the overpotential of FOR versus the hydrogen adsorption free energy.

**Table 1** Catalytic activity of various PdM<sub>38</sub> and PdM<sub>79</sub> (M = Ir, Ag) nanoalloys for formate dehydrogenation and oxidation reactions. The PdAg<sub>55</sub> nanoalloys with Oh and Ih shapes and bulk M(100) and M(111) surfaces (M = Ir, Ag and Pd) were used as controls

|                                             | $\Delta G_{\text{Had}}/\text{eV}$ | $\Delta G_{\text{HCOOad}}/\text{eV}$ | $\Delta G_3/\text{eV}$ | $\eta/\text{V}$ |                                              | $\Delta G_{\text{Had}}/\text{eV}$ | $\Delta G_{\text{HCOOad}}/\text{eV}$ | $\Delta G_3/\text{eV}$ | $\eta/\text{V}$ |
|---------------------------------------------|-----------------------------------|--------------------------------------|------------------------|-----------------|----------------------------------------------|-----------------------------------|--------------------------------------|------------------------|-----------------|
| Ir(100)                                     | −0.505                            | −2.471                               | 0.657                  | 1.281           | Ir(111)                                      | −0.539                            | −2.082                               | 0.628                  | 1.079           |
| Ag(100)                                     | 0.425                             | −1.909                               | 0.987                  | 1.338           | Ag(111)                                      | 0.461                             | −1.682                               | 1.052                  | 1.203           |
| Pd(100)                                     | −0.491                            | −1.863                               | 0.437                  | 0.659           | Pd(111)                                      | −0.513                            | −1.756                               | 0.385                  | 0.607           |
| Ir <sub>38</sub>                            | −0.587                            | −3.060                               | 0.536                  | 1.129           | Ir <sub>79</sub>                             | −0.598                            | −2.974                               | 0.563                  | 1.325           |
| Ag <sub>38</sub>                            | 0.326                             | −2.440                               | 0.568                  | 1.377           | Ag <sub>79</sub>                             | 0.343                             | −2.593                               | 0.613                  | 1.421           |
| Pd <sub>38</sub>                            | −0.510                            | −2.164                               | 0.362                  | 0.967           | Pd <sub>79</sub>                             | −0.579                            | −2.043                               | 0.369                  | 1.196           |
| Pd <sub>19</sub> Ir <sub>19</sub> Janus     | −0.396                            | −2.944                               | 0.324                  | 0.785           | Pd <sub>34</sub> Ir <sub>45</sub> Janus      | −0.365                            | −2.938                               | 0.317                  | 0.614           |
| Pd <sub>20</sub> Ir <sub>18</sub> sandwich  | −0.478                            | −2.286                               | 0.334                  | 0.794           | Pd <sub>19</sub> Ir <sub>60</sub> sandwich   | −0.425                            | −2.952                               | 0.322                  | 0.792           |
| Pd <sub>32</sub> Ir <sub>6</sub> core-shell | −0.281                            | −2.254                               | 0.263                  | 0.584           | Pd <sub>60</sub> Ir <sub>19</sub> core-shell | −0.358                            | −2.462                               | 0.275                  | 0.591           |
| Pd <sub>19</sub> Ag <sub>19</sub> Janus     | −0.200                            | −2.104                               | 0.194                  | 0.515           | Pd <sub>34</sub> Ag <sub>45</sub> Janus      | −0.230                            | −2.523                               | 0.206                  | 0.536           |
| Pd <sub>20</sub> Ag <sub>18</sub> sandwich  | −0.375                            | −2.515                               | 0.504                  | 0.726           | Pd <sub>19</sub> Ag <sub>60</sub> sandwich   | −0.598                            | −2.386                               | 0.619                  | 0.781           |
| Pd <sub>32</sub> Ag <sub>6</sub> core-shell | −0.337                            | −2.168                               | 0.364                  | 0.586           | Pd <sub>60</sub> Ag <sub>19</sub> core-shell | −0.405                            | −2.491                               | 0.397                  | 0.616           |

Given that a large library of atomically precise metal nano-catalysts have been structurally resolved, it is important to probe the segregation or anti-segregation during the reactions from *ab initio* calculations to advance the fundamental understanding of the catalytic stability.<sup>61</sup> Fig. S11<sup>†</sup> illustrates the vacuum  $E_{\text{seg}}$  of core-shell PdIr and PdAg nanoalloys, Ag@Pd and Ir@Pd nanoalloys as −0.100 and 0.488 eV, respectively, indicating an Ag surface segregation trend for Ag@Pd, while Ir shows no tendency to segregate. This behavior is due to the higher surface energy of Ir (3.048 J m<sup>−2</sup>) compared to that of Pd (2.003 J m<sup>−2</sup>) and Ag (1.246 J m<sup>−2</sup>).<sup>62</sup> Conversely, under H and O adsorption, the segregation energy is above zero for Ag@Pd and below zero for Ir@Pd, signifying a propensity for Pd atom surface segregation in Ag@Pd and Ir atom surface segregation in Ir@Pd during the reaction. This occurrence arises from the stronger binding energy of H and O on Ir in comparison to Pd and Ag.<sup>63</sup>

The stability of Janus and core-shell nanoalloys exhibiting higher FDH and FOR catalytic activities was investigated using AIMD simulations. The illustration in Fig. S12<sup>†</sup> demonstrates that Ir atoms consistently occupy the core, aligning with the segregation energy calculations. Conversely, Ag atoms segregate from the core to the shell at a temperature of 600 K under vacuum conditions. This observation is consistent with prior research,<sup>64</sup> indicating that the segregation processes can be stopped at any time by lowering temperature below 573 K. Consequently, subsequent AIMD simulations were conducted at a temperature of 600 K. Fig. S13<sup>†</sup> displays the atomic structures of Ir<sub>6</sub>@Pd<sub>32</sub>, Ag<sub>6</sub>@Pd<sub>32</sub>, Pd<sub>6</sub>@Ag<sub>32</sub> core-shell nanoalloys, and Pd<sub>19</sub>M<sub>19</sub> Janus (M = Ir, Ag) nanoalloys after DFT optimization and AIMD simulation. After AIMD simulation, Ag atoms initially situated in the core of the Ag<sub>6</sub>@Pd<sub>32</sub> nanoalloy undergo segregated into the shell. Conversely, the remaining core-shell nanoalloys did not experience segregation, and the Janus nanoalloys preserved their structural stability after the AIMD simulation.

The atomic structure of PdM<sub>38</sub> Janus (M = Ir, Ag) nanoalloys under various H and O coverages is depicted in Fig. 4, following DFT optimization and AIMD simulation. After DFT optimization and AIMD simulations, the Pd<sub>19</sub>M<sub>19</sub> Janus (M = Ir, Ag) nanoalloys demonstrate sustained structural stability. This

stability is further reinforced by grain boundaries, which play a pivotal role in enhancing durability by inhibiting dislocation motion, as evidenced in PdIr/PdAg core-shell and sandwich configurations. Additionally, grain boundaries significantly contribute to the structural stability of catalysts, mitigating deactivation during reactions. For example, in the core-shell and sandwich structures of PdIr and PdAg, grain boundaries stabilize the catalyst structure and enhance its durability. This stability is essential for the long-term performance of catalysts in practical applications.

The atomic structure of PdM<sub>38</sub> core-shell (M = Ir, Ag) nanoalloys is illustrated in Fig. S14,<sup>†</sup> following DFT optimization and AIMD simulation at different H and O atomic coverage. Upon the adsorption of a single H and O atom on the surface of the Pd<sub>32</sub>Ir<sub>6</sub> core-shell nanoalloy, Ir atoms remain confined within the core and do not segregate to the shell. Conversely, when eight or more H and O atoms are adsorbed on the surface, AIMD simulations reveal the segregation of Ir atoms from the core to the shell, as depicted in Fig. S14(a).<sup>†</sup> In the case of the Pd<sub>32</sub>Ag<sub>6</sub> core-shell nanoalloy, the adsorption of H and O atoms onto the surface does not prompt the segregation of Ag atoms from the core to the shell. This outcome is attributed to the stronger binding energy of Pd with H and O, as visually depicted in Fig. S14(b).<sup>†</sup> To establish a comparison, we conducted additional investigations into the segregation behavior of the Pd<sub>6</sub>@Ag<sub>32</sub> core-shell nanoalloy under different H and O coverage. As shown in Fig. S15,<sup>†</sup> the adsorption of 8 or more H and O atoms onto the surface led to the segregation of Pd atoms from the core to the shell. This phenomenon can be attributed to the higher binding energy between Pd and H or O. The total energy *versus* the time for AIMD simulations is depicted in Fig. S16 and S17.<sup>†</sup>

Several critical factors contribute to segregation. Firstly, differences in cohesive energy play a significant role. Secondly, disparities in surface energy drive the tendency for elements with lower surface energy to segregate to the surface. Thirdly, variations in atomic size, with larger atomic radii, promote surface segregation, aiding the release of internally accumulated stress. Lastly, variations in binding energy are also influential.<sup>65</sup>

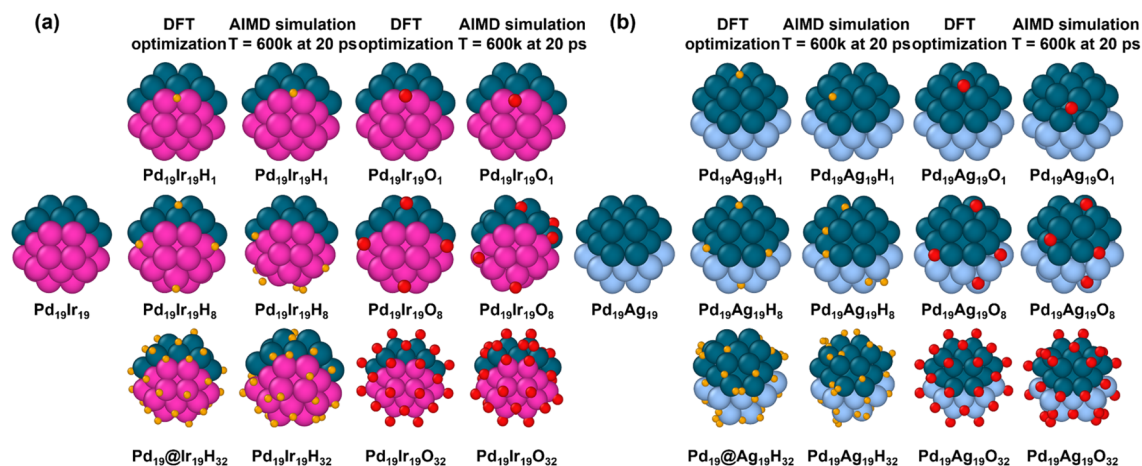


Fig. 4 Atomic structure evolution of PdIr Janus (a), PdAg Janus (b) nanoalloys after adsorption of hydrogen and oxygen atoms with varying coverage, investigated using DFT optimization and AIMD simulations at 600 K. The PdM Janus ( $M = \text{Ir, Ag}$ ) nanoalloys maintain structural stability after AIMD simulations.

The relationship between atomic strain and the activity of formate dehydrogenation and oxidation was investigated through theoretical calculations. To assess the impact of size on atomic strain, we focused on comparing two isomers of PdM ( $M = \text{Ir, Ag}$ ) nanoalloys containing 38 and 79 atoms. Fig. S1† demonstrates that both PdM<sub>38</sub> and PdM<sub>79</sub> ( $M = \text{Ir, Ag}$ ) nanoalloys have a substantial density of edge and corner sites on their surfaces. During the minimization stage of the MD simulation, surface atoms have a tendency to minimize their energy by deviating from their original positions, which is termed as atomic strain.<sup>42</sup>

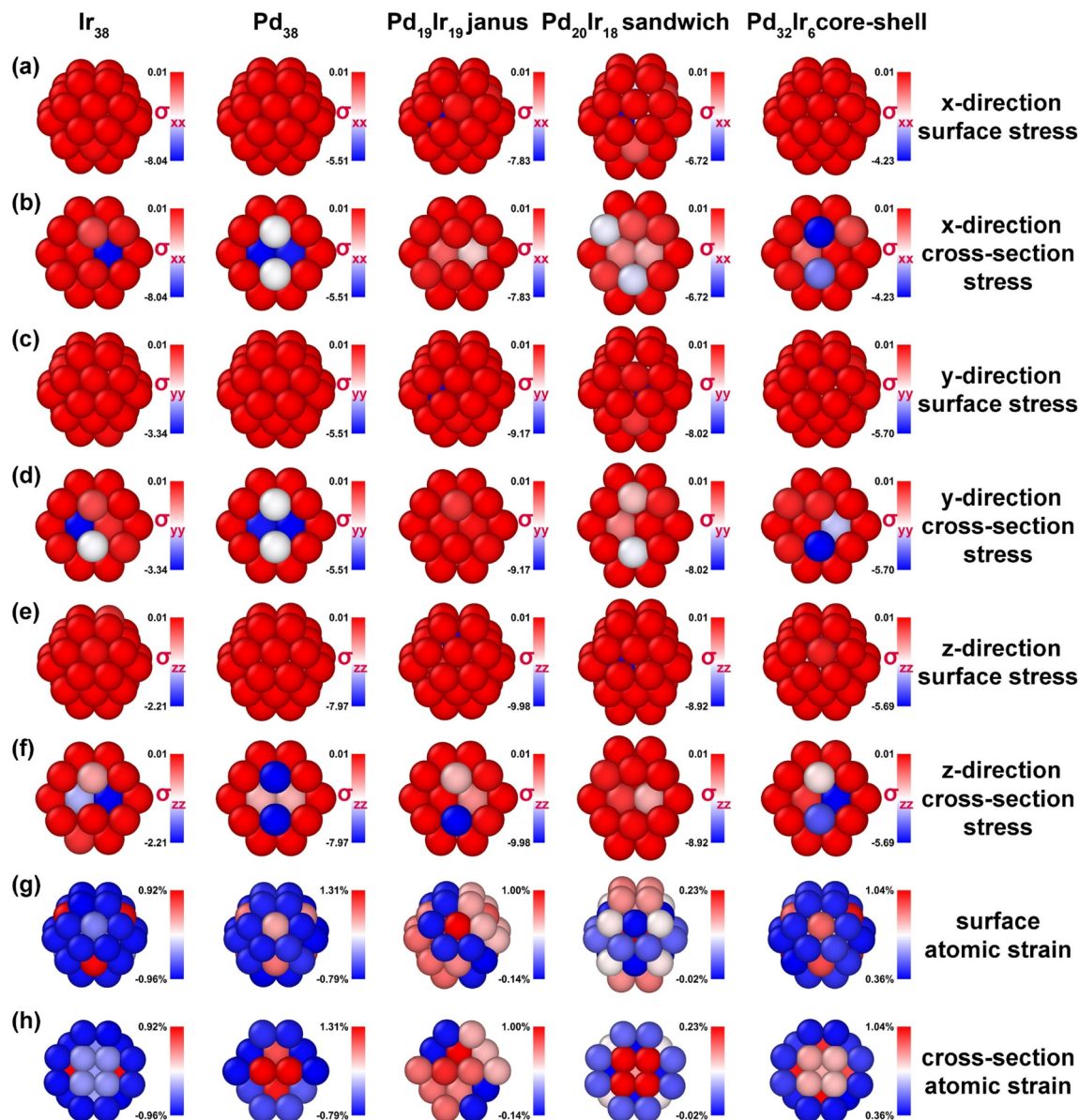
Fig. 5 depict the stress distribution in the surface and cross-section of PdIr<sub>38</sub> nanoalloy along the  $x$ -,  $y$ -, and  $z$ -directions. The results show that the subsurface of the nanoalloy experienced compressive stress, which is consistent with previous research.<sup>66</sup> In addition, the outer surface atoms, which lack coordinating atoms, were found to be under tensile stress. The Ir<sub>38</sub> and Pd<sub>38</sub> nanoalloy exhibits tensile strain at the face center and compressive strain at the corners and edges. For the Pd<sub>19</sub>Ir<sub>19</sub> Janush and Pd<sub>20</sub>Ir<sub>18</sub> sandwich nanoalloys, compressive strain was observed at the Pd–Ir interface. The Pd<sub>32</sub>Ir<sub>6</sub> core-shell nanoalloy has a slight tensile strain. This similarity in atomic radii, with Ir and Pd measuring 1.27 and 1.28 Å,<sup>64</sup> respectively, could account for this observation.

Fig. 6 illustrates the stress distribution and atomic strain field of the PdAg<sub>38</sub> nanoalloy. The subsurface of the nanoalloy experienced compressive stress, which is consistent with previous research.<sup>63</sup> In addition, the outer surface atoms, which lack coordinating atoms, were found to be under tensile stress. The Ag<sub>38</sub> cluster exhibits compressive strain at the face center and tensile strain at the corners and edges. In contrast, the Pd<sub>38</sub> cluster has the opposite distribution of atomic strain, with tensile strain at the face center and compressive strain at the corners and edges. For the Pd<sub>19</sub>Ag<sub>19</sub> Janus and Pd<sub>20</sub>Ag<sub>18</sub> sandwich clusters, tensile strain was observed in the Ag atoms region, and compressive strain in Pd atoms region. The Pd<sub>32</sub>Ag<sub>6</sub> core-shell cluster has the same distribution of atomic strain as

the Pd<sub>38</sub> cluster, with tensile strain at the face center and compressive strain at the corners and edges. The atomic strain distribution in the cross-section of the PdAg<sub>38</sub> nanoalloy is consistent with the atomic strain at the surface, as shown in Fig. 6(h). The compressive strain on the surfaces of Ag<sub>38</sub>, Pd<sub>38</sub>, Pd<sub>19</sub>Ag<sub>19</sub> Janus, Pd<sub>20</sub>Ag<sub>18</sub> sandwich and Pd<sub>32</sub>Ag<sub>6</sub> core-shell clusters is  $-0.77\%$ ,  $-0.79\%$ ,  $-0.75\%$ ,  $-0.87\%$  and  $-0.70\%$ , respectively. This is due to the larger atomic radius of Ag than that of Pd, which are 1.34 and 1.28 Å,<sup>67</sup> respectively.

To investigate the impact of size on atomic strain in PdM ( $M = \text{Ir, Ag}$ ) nanoalloys, we calculated the atomic strain field of PdIr<sub>79</sub> and PdAg<sub>79</sub> nanoalloys, as shown in Fig. S18 and S19.† The PdIr<sub>79</sub> and PdAg<sub>79</sub> nanoalloy indicates compressive stress in the subsurface, consistent with the results of the PdIr<sub>38</sub> and PdAg<sub>38</sub> nanoalloy. Additionally, the surface of the PdIr<sub>79</sub> and PdAg<sub>79</sub> nanoalloy experiences slightly tensile stressed due to the lack of coordination atoms. The compressive strain of Ag<sub>79</sub>, Pd<sub>79</sub>, Pd<sub>34</sub>Ag<sub>45</sub> Janus, Pd<sub>19</sub>Ag<sub>60</sub> sandwich and Pd<sub>60</sub>Ag<sub>19</sub> core-shell nanoalloys is  $-1.01\%$ ,  $-1.12\%$ ,  $-1.27\%$ ,  $-0.88\%$  and  $-0.89\%$ , respectively. These results indicate that increasing the size of the nanoalloys leads to higher compressive strain, while the tensile strain remains constant. The displacements of PdM<sub>38</sub> and PdM<sub>79</sub> ( $M = \text{Ir, Ag}$ ) nanoalloys along the  $x$ ,  $y$ , and  $z$  direction after MD simulations are shown in Fig. S20–S23.†

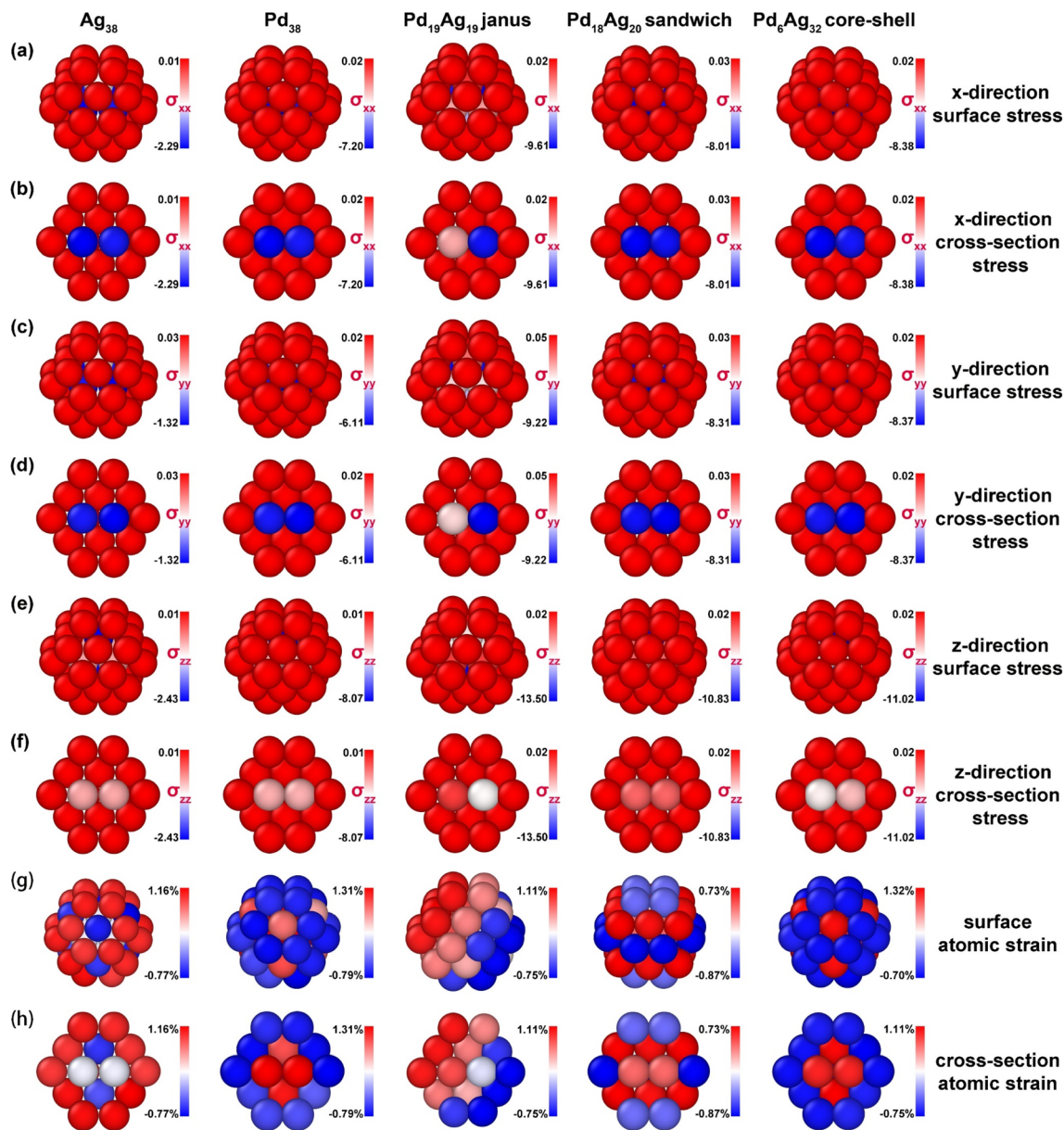
In this study, the PdIr core-shell structure (e.g., Pd<sub>32</sub>Ir<sub>6</sub>) shifts the d-band center of surface Pd downward ( $-2.32$  eV) through interfacial compressive strain ( $\sim -0.79\%$ ), reducing hydrogen adsorption strength ( $\Delta G_{\text{H}} = 0.263$  eV) and enhancing FDH/FOR activity. Under H/O adsorption, Ir migrates to the surface to relieve internal stress, while high surface energy inhibits segregation. In the PdAg Janus structure (e.g., Pd<sub>19</sub>Ag<sub>19</sub>), tensile strain in the Ag region and compressive strain in the Pd region synergistically regulate the d-band center ( $-2.86$  eV), balancing adsorption/desorption kinetics ( $\Delta G_3 = 0.194$  eV) to meet “volcano-type” activity requirements, while maintaining dynamic stability at 600 K.



**Fig. 5** The stress distribution and atomic strain field maps of Ir<sub>38</sub>, Pd<sub>38</sub>, Pd<sub>19</sub>Ir<sub>19</sub> Janus, Pd<sub>20</sub>Ir<sub>18</sub> sandwich, and Pd<sub>32</sub>Ir<sub>6</sub> core-shell nanoalloys. (a) and (b) The x-direction, (c) and (d) y-direction, and (e) and (f) z-direction for surface and cross-sectional stress. (g) and (h) The atomic strain at the surface and in the cross-section. The Pd<sub>19</sub>Ir<sub>19</sub> Janus and Pd<sub>20</sub>Ir<sub>18</sub> sandwich nanoalloys exhibit compressive strain at the Ir–Pd interface. The unit of measurement for stress is bar.

Based on the presented calculation results, it can be inferred that Pd<sub>30</sub>Ir<sub>6</sub> core-shell, Pd<sub>60</sub>Ir<sub>19</sub> core-shell, Pd<sub>19</sub>Ag<sub>19</sub> Janus and Pd<sub>34</sub>Ag<sub>45</sub> Janus nanoalloys exhibit superior catalytic activities for FDH and FOR. This can be attributed to the strain present on the surface of nanoalloy, which directly modulates the d-band center (Fig. S10†) as evidenced by: (1)  $-0.75\%$  compressive strain in Pd<sub>19</sub>Ag<sub>19</sub> Janus lowering the d-band center to  $-2.855$  eV, (2) corresponding  $\Delta G_{\text{H}}$  reduction to  $0.194$  eV (Fig. 2(e)), and (3) simultaneous FOR overpotential minimization to  $0.515$  V (Fig. 3(e)). The complete strain  $\rightarrow$  d-band  $\rightarrow \Delta G_{\text{H}} \rightarrow$  activity pathway is quantitatively validated through cross-referencing Fig. 5, 6, S10 with 2e, 3e. The Pd<sub>30</sub>Ir<sub>6</sub> core-shell and Pd<sub>60</sub>Ir<sub>19</sub> core-shell nanoalloys is the optimal catalyst

candidate for FDH and FOR due to its maximum tensile strain on its surface. The Pd<sub>19</sub>Ag<sub>19</sub> Janus and Pd<sub>34</sub>Ag<sub>45</sub> Janus nanoalloys is the optimal catalyst candidate for FDH and FOR due to its maximum compressive strain on its surface. These findings are consistent with a previous theoretical study<sup>54</sup> on the formic acid dehydrogenation activity of PdAu nanoalloys, which showed that Janus-shaped PdAu nanoalloys have better formic acid dehydrogenation selectivity and activity. In practical FDH and FOR conditions, Ir atoms originally positioned in the core may undergo segregation towards the shell, while PdAg Janus nanoalloys exhibit the capability to sustain their structural stability. Segregation in nanoalloys can be attributed to the interplay between variations in binding energy for H and O,



**Fig. 6** The stress distribution and atomic strain field maps of  $\text{Ag}_{38}$ ,  $\text{Pd}_{38}$ ,  $\text{Pd}_{19}\text{Ag}_{19}$  Janus,  $\text{Pd}_{20}\text{Ag}_{18}$  sandwich, and  $\text{Pd}_{32}\text{Ag}_6$  core-shell nanoalloys. (a) and (b) The  $x$ -direction, (c) and (d)  $y$ -direction for surface and cross-sectional stress. (e) and (f) The  $z$ -direction for surface and cross-sectional stress. (g) and (h) The atomic strain at the surface and in the cross-section. In the  $\text{Pd}_{19}\text{Ag}_{19}$  Janus and  $\text{Pd}_{20}\text{Ag}_{18}$  sandwich nanoalloys, the Ag atoms experience tensile strain while the Pd atoms experience compressive strain. The unit of measurement for stress is bar.

differences in surface energy, and the alleviation of internal stress.

## 4. Conclusions

In this work, we utilized the Birmingham Nanoalloy Genetic Algorithm software to obtain atomic structures of  $\text{PdM}_{38}$  and  $\text{PdM}_{79}$  ( $M = \text{Ir}, \text{Ag}$ ) nanoalloys. Three representative atomic arrangements, including Janus, sandwich, and core-shell structures, were considered. The results show that compressive stress is present inside both  $\text{PdM}_{38}$  and  $\text{PdM}_{79}$  ( $M = \text{Ir}, \text{Ag}$ ) nanoalloys. The atomic strain distribution in Janus and sandwich structures is element dependent, with tensile strain

present in the Ag atoms region and compressive strain present in the Pd atoms region. In addition, our calculations reveal that as the size of the nanoalloy increases, the compressive atomic strain on the surface becomes more increased, while the tensile strain remains constant. Density functional theory (DFT) calculations suggest that PdIr nanoalloys with core-shell structures exhibit optimal formate dehydrogenation (FDH) and oxidation reactions (FOR) catalytic activity, while PdAg nanoalloys with Janus structures exhibit optimal FDH and FOR catalytic activity due to the excessive H adsorption free energy of Ir elements on the Janus and sandwich surfaces. Our calculations demonstrate that decreasing the adsorption free energy of H intermediates can improve FDH and FOR catalytic activity.

Based on the segregation energy and *ab initio* molecular dynamics (AIMD) simulations, it is observed that Ag segregates to the shell under vacuum conditions, whereas Ir segregates to the shell under H and O conditions. Overall, this work provides valuable theoretical insights for the design and development of efficient formate dehydrogenation catalysts and anode catalysts for direct formate fuel cells.

## Data availability

The data underlying this study are available in the published article and its online ESI.†

## Author contribution

J. W. and T. J. contributed equally to this work. J. W.: data curation, project administration, validation, writing manuscript. T. J.: figures prepared, data curation, project administration, validation. L. G.: project administration. Z. L. and C. W.: validation, experimental design. S. S. and Q. T.: validation. B. P.: figures prepared. F. C.: project administration, funding acquisition, writing manuscript. All the authors have approved the final manuscript.

## Conflicts of interest

There are no conflicts to declare.

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