

# Imaging and Dosimetric Study on Direct Flat-Panel Detector-Based Digital Mammography System

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## Abstract

**Introduction:** Image quality of digital mammography system is generally defined by three primary physical parameters, namely, contrast, resolution, and noise. Quantification of these metrics can be done by measuring objective image quality parameters defined as contrast-to-noise ratio (CNR), modulation transfer function (MTF), and noise power spectra (NPS). **Materials and Methods:** In the present study, various imaging metrics such as CNR, contrast detail resolution, MTF, and NPS were evaluated for a direct flat-panel detector-based digital mammography system following the European Guidelines. Furthermore, system performance relating to both image quality and doses were evaluated using figure of merit (FOM) in terms of CNR<sup>2</sup>/mean glandular dose (MGD) under automatic exposure control (AEC) and clinically used OPDOSE operating mode. **Results and Conclusion:** Under AEC mode, FOM values for the 4.5 cm thick BARC polymethyl methacrylate (PMMA) phantom were found to be 15.02, 15.88, and 19.82 at Mo/Mo, Mo/Rh, and W/Rh target/filter (T/F), respectively. Under OPDOSE mode, FOM values were found to be 65.32, 11.80, and 1.14 for the BARC PMMA phantom thickness of 2, 4.5, and 8 cm, respectively. Under OPDOSE mode, the calculated MGD values for three Computerized Imaging Reference Systems slab phantoms having total thickness of 7 cm were observed to be 3.03, 2.32, and 1.75 mGy with glandular/adipose tissue compositions of 70/30, 50/50, and 30/70, respectively, whereas for the 2–8-cm thick BARC PMMA phantom, the calculated MGDs were found to be in the range of 0.57–3.32 mGy. All the calculated MGDs values were found to be lower than the acceptable level of dose limits provided in European Guidelines.

**Keywords:** Contrast-to-noise ratio, contrast-detail mammography, digital mammography, mean glandular dose, modulation transfer function, noise power spectra, phantoms, X-ray

Received on: 08-06-2018

Review completed on: 08-10-2018

Accepted on: 09-10-2018

## INTRODUCTION

In India, use of digital mammography has increased rapidly due to its several advantages over screen-film-based mammography. Digital mammography technology offers simplified archival, retrieval and transmission of images, reduction in mean glandular dose (MGD), higher patient workflow, and improved diagnostic accuracy.<sup>[1,2]</sup> Digital mammography utilizes digital detectors having the wider dynamic range and is categorized on the basis of direct and indirect flat-panel detector technology. Digital detectors (even with a lower spatial resolution than film) also appear to improve lesion conspicuity through their improved efficiency of absorption of X-ray photons, a linear response over a wide range of radiation intensities and low system noise.<sup>[2]</sup> In addition, postprocessing software can be utilized to assist the radiologist in evaluating the images for suspicious findings by altering contrast and brightness

automatically or manually. Also in digital mammography system, the images can be displayed in hard and soft copy formats. Other advantage of using digital mammography is that computer-aided detection software can be utilized to highlight the abnormal areas of density, mass, or calcification on the mammogram image.

Image quality characterization of any X-ray-based imaging system is evaluated by measuring three primary physical parameters: contrast, resolution, and noise.<sup>[3]</sup> Practically, quantification of these metrics can be done by evaluating

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**How to cite this article:** Sharma R, Sharma SD, Sarkar PS, Datta D. Imaging and dosimetric study on direct flat-panel detector-based digital mammography system. *J Med Phys* 2018;43:255-63.

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10.4103/jmp.JMP\_64\_18

objective image quality parameters defined as contrast-to-noise ratio (CNR), modulation transfer function (MTF), and noise power spectra (NPS).<sup>[3]</sup> CNR defines the image contrast of a digital imaging system. In addition, CNR measurement is very useful for assessing the performance of automatic exposure control (AEC) system that can be related to the effect on threshold object thickness of a given system.<sup>[4]</sup> In the present study, we have evaluated the image quality of direct flat-panel-based mammography systems by measuring CNR values under clinically used operating conditions following the European protocol.<sup>[5,6]</sup> Present days, a new concept called as figure of merit (FOM) is used as a tool in digital mammography to assess the performance in terms of image quality and patient doses.<sup>[7,8]</sup> FOM of digital mammography system was evaluated in terms of  $CNR^2/MGD$  under AEC and clinically used OPDOSE mode using indigenously made polymethyl methacrylate (PMMA) phantom having different thicknesses.<sup>[7-9]</sup> OPDOSE mode selects the best target/filter combination depending on breast thickness, density, whereas AEC mode selects optimized exposure parameters for each individual breast size and composition and determines the dose based on the contrast needed for the image. European guidelines for quality control (QC) in full-field digital mammography recommends to measure the threshold contrast (i.e., the lowest contrast value for which the objects are visible) visibility under clinical conditions which is used to express the image quality.<sup>[10]</sup> Furthermore, several studies have also reported that measurement of contrast detail (CD) resolution of the digital mammography system is also an essential part as it helps to visualize the objects with very small contrast and diameter from the background.<sup>[11-20]</sup> CD resolution studies on the digital mammography system simulating the clinical operating conditions were carried out using the Artinis make contrast-detail mammography (CDMAM 3.4) phantom.

MTF measurement describes the sharpness of digital imaging detector at different spatial frequencies and gives the quantitative analysis of spatial resolution.<sup>[21]</sup> Various methods have been employed for deriving MTF quantity which is based on slit, edge, and bar pattern.<sup>[21-23]</sup> In this paper, we report an edge method which was used for deriving MTF of a direct digital mammography imaging system. NPS measurement of digital mammography system describes the noise amplitude and texture observed in images obtained with a uniform field of radiation.<sup>[24-30]</sup> Under NPS measurement, variance of image intensity divided among its frequency components is calculated from region of interest (ROI) taken from a region of a uniformly exposed image. In the present study, we have evaluated NPS from the uniformly exposed digital mammography images following the European Guidelines.<sup>[23]</sup>

Estimation and optimization of MGD is an important component of the QC program in mammography due to associated risk of radiation-induced carcinogenesis.<sup>[31]</sup> Furthermore, in the case of digital mammography, single-dose measurement at one thickness is not sufficient and it requires different PMMA thicknesses and breast-simulating phantoms

to measure the radiation doses.<sup>[9,32]</sup> Hence, MGDs for the digital mammography system was measured using different breast tissue-simulating phantoms.

## MATERIALS AND METHODS

### Digital mammography X-ray machine

Mammomat Inspiration digital mammography machine (Siemens Medical Systems, Germany) was employed for all the measurements. The Mammomat Inspiration is DR-based mammography machine which contains Molybdenum (Mo) and Tungsten (W) targets. This machine also contains different filters, namely, 30  $\mu\text{m}$  Mo for Mo target, 25  $\mu\text{m}$  rhodium (Rh) for Mo target, and 50  $\mu\text{m}$  Rh for W target. The operating kilovoltage of the machine is in the range of 23–35 kV at an increment of 1 kV and the focus-to-imager distances are 65.0 cm and 65.55 cm for Mo and W targets, respectively. Exposure modes available with the machine are OPDOSE, AEC, and manual. The image receiver of the machine contains solid-state amorphous selenium (a-Se) detector with pixel size of 85  $\mu\text{m}$ . The detector size is 24 cm  $\times$  30 cm, but the irradiation field is automatically collimated to 18 cm  $\times$  24 cm when the smaller compression paddle is fitted.

### Mammography phantoms

Computerized Imaging Reference Systems (CIRS) mammography research set (012A), CIRS mammography accreditation phantom (015A) supplied by CIRS, Norfolk, Virginia, USA, and in-house developed PMMA phantom (Referred as Bhabha Atomic Research Centre [BARC] PMMA phantom) were used to carry out the dosimetry measurements with digital mammography systems.<sup>[9,33]</sup> Physical and dimensional details of these phantoms are given in Table 1. The CIRS mammography research set contains three different breast tissue equivalent phantoms having semispherical shapes and total thicknesses of 4, 5, and 6 cm. The relative contents of the glandular and adipose tissues of these phantoms are 50/50%, 30/70%, and 20/80%, respectively. CIRS research set also includes 10 cm  $\times$  12.5 cm photo timer compensation plates with varying thicknesses (0.5 cm to 7 cm) and varying relative contents of glandular and adipose tissues (30/70%, 50/50%, and 70/30%). The material used in the CIRS phantoms is epoxy resin which mimics the photon attenuation coefficients of a range of breast tissues. The BARC mammography phantom is made up of PMMA and was used for measuring CNR of the digital mammography system at various thicknesses. The BARC mammography phantom is equivalent to commercially available mammography phantoms and considered to be suitable for measuring radiation doses in different breast equivalent thicknesses.<sup>[9]</sup>

For CD resolution study of digital mammography machine, CDMAM phantom (CDMAM 3.4) along with automated CDMAM Analyzer software V 1.2 (Artinis Medical Systems, The Netherlands) was used.<sup>[10]</sup> The phantom is delivered with set of five PMMA blocks of different thicknesses ranging from 5 mm to 10 mm and physical dimensions of 180 mm  $\times$  240 mm. The CDMAM phantom

**Table 1: Physical and dimensional details of different mammography imaging and dosimetry phantoms**

Phantom type (glandular/adipose)	Descriptions	Quantity (nos)	Material
CIRS mammography research set (012A)			
CIRS 30/70 slabs (cm <sup>3</sup> )	Slab dimensions: 10×12.5×0.5	2	Epoxy resin
	Slab dimensions: 10×12.5×1.0	2	
	Slab dimensions: 10×12.5×2.0	2	
CIRS 50/50 slabs (cm <sup>3</sup> )	Slab dimensions: 10×12.5×0.5	2	
	Slab dimensions: 10×12.5×1.0	2	
	Slab dimensions: 10×12.5×2.0	2	
CIRS 70/30 slabs (cm <sup>3</sup> )	Slab dimensions: 10×12.5×0.5	2	
	Slab dimensions: 10×12.5×1.0	2	
	Slab dimensions: 10×12.5×2.0	2	
CIRS 10 B	Tissue equivalent mammography phantom, 4 cm thickness having 50% glandular tissue and 50% adipose tissue	1	
CIRS 10 A	Tissue equivalent mammography phantom, 5 cm thickness having 30% glandular tissue and 70% adipose tissue	1	
CIRS 10 C	Tissue equivalent mammography phantom, 6 cm thickness having 20% glandular tissue and 80% adipose tissue	1	
CIRS mammography accreditation phantom (015A) (cm <sup>3</sup> )	Dimensions: 10.8×10.2×4.4	1	PMMA
BARC-PMMA phantom	Semispherical phantom with the length and radius of the central slab of 21 and 10 cm respectively	1	PMMA

CIRS: Computerized Imaging Reference Systems, BARC: Bhabha Atomic Research Centre, PMMA: Polymethylmethacrylate

consists of a 16 cm × 24 cm × 0.3 mm aluminum (Al) plate with 205 square cells (arranged in 16 rows × 16 columns) with gold disks of various thicknesses (0.03 μm to 2.00 μm) and diameters (0.06 mm to 2.00 mm). These disks are aligned on a two-dimensional grid where two disks can be found in each cell, one in the center and another in one of the four cell corners. Columns have equal gold disc thickness whereas rows have equal gold disc diameters. The CDMAM 3.4 phantom was positioned on the bucky of the mammography machine. The structures with the smallest diameter were located closest to the chest wall side of the bucky. PMMA blocks supplied along with CDMAM phantom were used to increase the total thickness of the phantom. CDMAM Analyzer software was used for computing the CD curve, the inverse image quality figure (IQF<sub>inv</sub>) and % detected gold disks, which offers the various functionality test on the exposed CDMAM 3.4 phantom images which should be DICOM (digital imaging and communications in medicine) tagged.<sup>[10]</sup> CDMAM analyzer software offers the possibility to analyze more than one CDMAM image into one result thus reducing the influence of image noise.<sup>[10]</sup> For image quality evaluation, smallest thickness of the disks just visible for each diameter called the threshold contrast was measured using automatic software analyzer and same was plotted in CD curve for the various clinically used operating conditions. The IQF<sub>inv</sub> numbers were obtained from the analyzed CDMAM phantom images which determines the contrast (thickness) threshold in the image of the object as a function of the detail (diameter) and is calculated using given equation 1.

$$IQF_{inv} = \frac{100}{\sum_{i=1}^{16} C_{i,th} \times D_i} \quad (1)$$



**Figure 1:** Experimental set up for measurement of breast entrance exposure in mammography phantom

where  $C_{i,th}$  denotes the threshold thickness in diameter-column  $i$  and  $D_i$  denotes the threshold diameter in contrast column  $i$ . The contrast is given in “μm” whereas the diameter is taken in “mm.” Furthermore, % detected disks were obtained from the analyzed CDMAM phantom image which is also used as the image quality indicator. Higher the IQF<sub>inv</sub>, better the low contrast visibility.

### Half value layer (HVL), radiation output, breast entrance exposure, and mean glandular dose measurements

Beam quality (HVL) and radiation output (mGy) measurements at different kVp stations and target/filter combinations were carried out using Raysafe X2 base unit along with Raysafe X2 MAM sensor (Fluke Biomedical, USA) having measurable

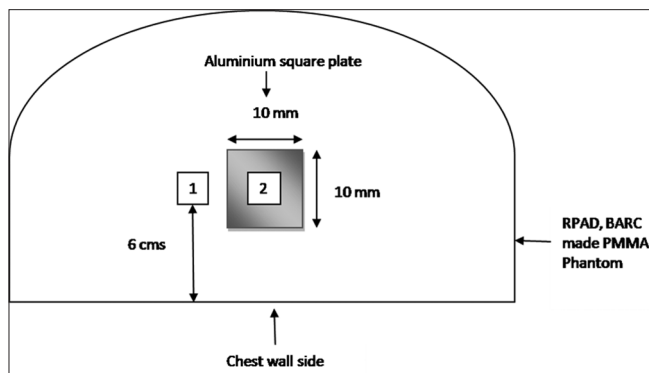
dose range of 1  $\mu$ Gy to 99.99 Gy with uncertainty of 5%. All these measurements were performed using manual mode digital mammography machine. Raysafe X2 base unit along with Raysafe X2 MAM sensor was also used for measuring breast entrance exposure (BEE) while exposing different mammography phantoms. During BEE measurement, Raysafe X2 MAM sensor was placed at one side of the phantom and compression plate was used in contact of phantom to simulate clinical exposure conditions as shown in Figure 1. The MGD values were calculated from the measured BEEs by applying multiple conversion factors using equation 2.<sup>[31,34]</sup>

$$MGD = K \cdot g \cdot c \cdot s \tag{2}$$

where *K* represents the BEE (i.e., incident air kerma) at the upper surface of the breast, *g* is the incident air kerma to MGD conversion factor corresponding the glandularity of 50%, *c* is the correction factor for difference in breast composition from 50% glandularity, and *s* is the correction factor for difference in X-ray spectra. Dance *et al.* have given *g* and *c* values against HVL of the X-ray beams in the tabulated form.<sup>[31,34]</sup> Using these standard tables, data points were plotted and same were used to derive the values of *g* and *c* factors corresponding to the HVL values measured for different mammography phantoms for the studied digital mammography system in the present study.

### Contrast-to-noise ratio measurement

For CNR measurements, a square plate of aluminum (Al) of dimension 10 mm  $\times$  10 mm and thickness 0.2 mm was placed on different thickness of PMMA phantom which ranges from 2 to 8 cm as shown in Figure 2. While carrying out the CNR measurements, BEE was measured using Raysafe X2 MAM sensor positioned by the side of PMMA phantom of different thicknesses and compression paddle in contact of phantom to derive the actual MGD. The images of the different PMMA phantom thicknesses obtained during the dose measurement were analyzed to obtain the CNR values using Image J software.<sup>[35]</sup> A 5 mm  $\times$  5 mm square ROI was used to determine the average signal pixel value ( $PV_{\text{signal}}$  at location 2, Al) and the standard deviation (SD) in the signal within the image of the Al square and the surrounding background (ROI) at location 1 (PMMA) as



**Figure 2:** Set up for contrast-to-noise ratio measurement with different BARC polymethyl methacrylate phantom thicknesses

shown in Figure 3. The CNR was calculated for each image as defined in the European protocol using the following equation 3.

$$CNR = \frac{PV_{\text{Signal}} - PV_{\text{Bkg}}}{\sqrt{\frac{(SD_{\text{Signal}})^2 + (SD_{\text{Bkg}})^2}{2}}} \tag{3}$$

where  $PV_{\text{signal}}$  is the average pixel value of the signal,  $PV_{\text{bkg}}$  is the average pixel value of background,  $SD_{\text{signal}}$  is the SD in the signal area 2, and  $SD_{\text{bkg}}$  is the SDs in the background area 1.

### Figure of merit measurements

FOM for the digital mammography system was evaluated using the measured CNR values and corresponding MGDs in BARC mammography PMMA phantom. Equation 4 was used for all the FOM calculation.

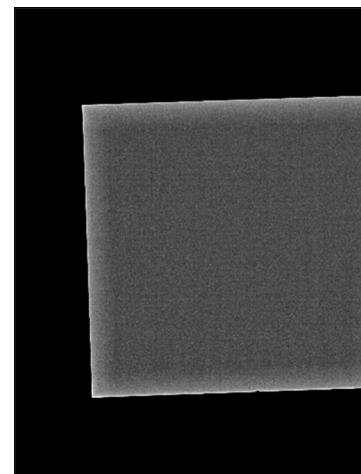
$$FOM = \frac{CNR^2}{MGD} \tag{4}$$

Furthermore, percentage change (%) was calculated in terms of increased or decreased value for the three measured parameters called CNR, MGD, and FOM using the formula given by equation 5.

$$\text{Percentage change (\%)} = \frac{[\text{Reference}_{\text{value}} - \text{Observed}_{\text{value}}]}{\text{Reference}_{\text{value}}} \times 100 \tag{5}$$

### Modulation transfer function and noise power spectra measurements

MTF of the digital mammography system was measured using a slanted radiopaque edge placed at the detector input plane with grid in position.<sup>[21-23]</sup> Image of the exposed radiopaque plate is shown in Figure 3. Radiopaque plate was made up of tantalum having sharp and straight edge with dimensions 10 cm  $\times$  10 cm and thickness of 100  $\mu$ m. The edge spread function (ESF) was obtained using Image J software from the image of tantalum



**Figure 3:** Image of exposed radiopaque tantalum plate used for modulation transfer function measurement

plate. Derivative of the ESF was calculated to generate line spread function (LSF) as given by the following equation.

$$LSF(X) = \frac{d}{dx}ESF(x) \tag{6}$$

The presampled MTF was obtained from the LSF using fast Fourier transform (FFT) and by calculating the magnitude as given by the following equation.

$$MTF = |FFT[LSF(x)]| \tag{7}$$

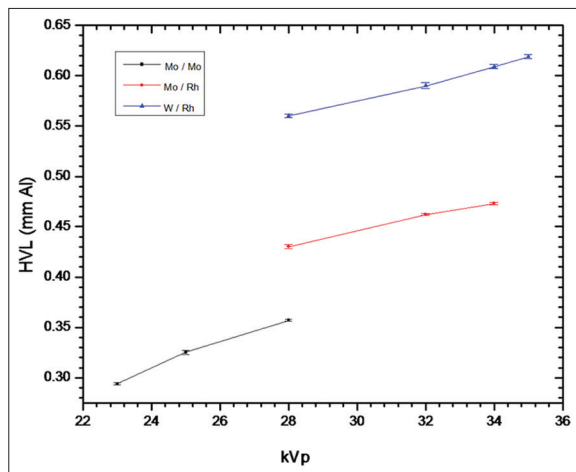
NPS of the digital mammography system was calculated from a series of flat-field images acquired at radiation dose of ~100 μ Gy using the following equation:<sup>[23-30]</sup>

$$NPS(u, v) = \frac{\Delta x \Delta y}{M \cdot 256 \cdot 256} \sum_{m=1}^M \left| \sum_{i=1}^{256} \sum_{j=1}^{256} (I(x_i, y_j) - S(x, y)) e^{-2\pi i(u x_i + v y_j)} \right|^2 \tag{8}$$

where an ROI dimension of 256 × 256 pixels has been used, M is the number of ROIs, Δx is the pixel spacing in the x-direction, Δy is the pixel spacing in the y-direction, I (x, y) are the pixel value data, S (x, y) is a two-dimensional polynomial function used to the entire extracted region used of NPS analysis.

## RESULTS AND DISCUSSION

For the studied digital mammography machine, measured HVL values for the different T/F combinations are shown in Figure 4. Before measuring HVL values, accuracy of all the kVp stations and different T/F combinations were evaluated which were found to be <±1 kVp. At Mo/Mo setup, the measured HVL range was found to be 0.294 ± 1E-3–0.357 ± 1E-3 for the applied kVp of 23, 25, and 28. At Mo/Rh set up, HVL range was found to be 0.43 ± 0.002–0.473 ± 1E-3 for the applied kVp of 28, 32, and 34. At W/Rh set up, HVL range was found to be 0.56 ± 0.002–0.62 ± 0.002 for the applied kVp of 28, 32, 34, and 35 kVp.

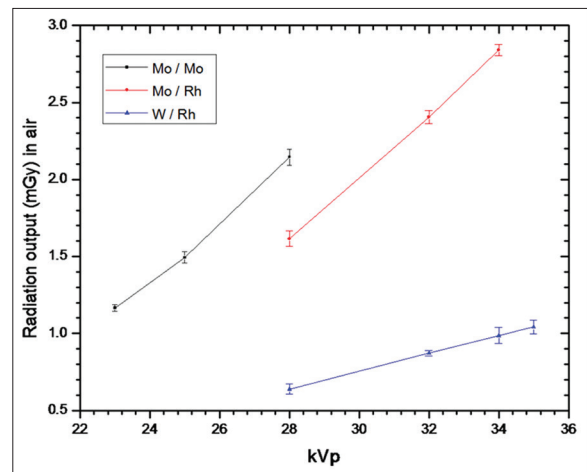


**Figure 4:** Measured HVL values (mm Al) at different kVp settings for the various target/filter combinations (Mo/Mo, Mo/Rh, W/Rh)

Results of radiation output (mGy) measured at different T/F combinations for the various kVp stations are shown in Figure 5. Radiation output consistency at all kVp stations and different T/F combinations was calculated in terms of coefficient of variation and was found to be < 0.05. For Mo/Mo and T/F, the radiation output was found to be in the range of 1.16–2.15 mGy at 23, 25, and 28 kVp. For Mo/Rh, measured radiation output range was observed to be 1.62–2.84 mGy at 28, 32, and 34 kVp, and for W/Rh, it was found to be 0.639–1.04 mGy at 28, 32, 34, and 35 kVp.

Figure 6 shows the FOM values in terms of CNR<sup>2</sup>/MGD for the 4.5 cm thick BARC PMMA phantom exposed under AEC mode at three different T/F combinations. CNR values for the BARC PMMA phantom with total thickness of 4.5 cm were found to be 6.71, 6.17, and 5.27 with MGD values of 3, 2.4, and 1.4 mGy at T/F of Mo/Mo, Mo/Rh, and W/Rh, respectively. These measured CNR values are found to be within the European limiting CNR values.<sup>[5,10]</sup> Corresponding calculated FOM values were 15.02, 15.88, and 19.82 for these three T/F combinations, respectively. Percentage decreases in MGD values were found to be 20 and 53.33% when T/F was changed from Mo/Mo to Mo/Rh and W/Rh, respectively. Also for comparing two clinical operating mode, that is, AEC (T/F = W/Rh) and OPDOSE (T/F = W/Rh), % change in MGD, CNR, and FOM for the 4.5 cm BARC PMMA phantom were calculated. It is seen from the compared values that percentage increase of 21.43 was found in MGD value for the AEC than OPDOSE mode, whereas in CNR values, % increase of 31.5 was observed for OPDOSE than AEC mode. Furthermore, percentage increase of 40.46 was found in FOM value for the AEC than the OPDOSE mode at same T/F combination. Hence, it is concluded that for the 4.5 cm thick PMMA phantom, AEC mode provides the better image quality and dose performance.

Calculated FOM values for BARC PMMA phantom of different thicknesses and exposed under OPDOSE mode are shown in Figure 7. It is observed that highest CNR



**Figure 5:** Measured radiation output (mGy) in air at different kVp settings for the various target/filter combinations (Mo/Mo, Mo/Rh, W/Rh)

value with lowest MGD was achieved for 2 cm thick BARC PMMA phantom and lowest CNR with highest MGD value was found to be for 8 cm thick phantom. Correspondingly, highest FOM values were achieved for 2 cm and lowest for 8 cm thick BARC PMMA phantom. The outcome of this analysis suggests that when the breast thicknesses are small, detectability of any mass, or microcalcification will be higher due to higher CNR value observed at lower thickness.

Calculated MGD values for digital mammography system for different breast tissue-simulating phantoms and for different BARC PMMA phantom thickness are given in Tables 2 and 3, respectively. It incorporates the displayed compressed breast thickness (CBT in cm), machine-selected parameters such

as T/F combination, applied kVp, mAs, and MGDs. It also include the values of other parameters measured by dosimeter X2 MAM, for example, BEE, HVL, exposure time, and exposure rate. MGD ratio between machine displayed and calculated MGD values using the appropriate conversion factors are also given in Tables 2 and 3. The outcome of the study also show that for the CIRS slabs phantom of different glandular/adipose tissue compositions and physical thickness of 7 cm, the calculated maximum MGD value was found to be of 3.03 for 70/30, 2.32 for 50/50, and 1.75 mGy for the 30/70 glandular/adipose tissue compositions. Furthermore, fitting equation was achieved for the calculated MGD values at different thicknesses of BARC PMMA phantom. The

**Table 2: Measured mean glandular dose values under clinically operated OPODSE mode (target/filter=tungsten/rhodium) for digital mammography system using different breast tissue simulating mammography phantoms**

Numbers assigned to phantom types	Phantom type (glandular/adipose)	Quoted physical thickness (cm)	Machine displayed parameters					Dosimeter X2 MAM readings				Calculated MGD (mGy) <sup>[31,34]</sup>	MGD ratio (machine displayed vs. calculated)
			T/F	CBT (cm)	kVp	mAs	MGD (mGy)	BEE (mGy)	HVL (mm Al)	Exposure time (s)	Exposure rate (mGy/s)		
1	Slabs of CIRS (30/70)	7.0	W/Rh	6.7	30	182.2	1.9	8.53	0.538	2.229	3.825	1.75	1.09
2	Slabs of CIRS (50/50)	7.0	W/Rh	6.7	30	238.6	2.5	11.19	0.54	2.876	3.890	2.32	1.08
3	Slabs of CIRS (70/30)	7.0	W/Rh	6.8	30	311.5	3.3	14.6	0.54	3.360	4.358	3.03	1.09
4	CIRS 10 C	6.0	W/Rh	5.7	29	113.8	1.2	4.67	0.541	1.588	2.941	1.13	1.06
5	CIRS 10 A	5.0	W/Rh	4.7	28	90.4	1.0	3.29	0.537	1.429	2.299	0.96	1.05
6	CIRS 10 B	4.0	W/Rh	3.8	27	75.4	0.9	2.46	0.517	1.426	1.727	0.69	1.30
7	CIRS 015	4.4	W/Rh	4.2	28	81.4	1.2	2.91	0.532	1.417	2.056	1.02	1.18
8	BARC-PMMA	6.0	W/Rh	5.9	29	181	2.1	7.15	0.552	2.241	3.193	1.41	1.49
9	BARC-PMMA	4.5	W/Rh	4.1	28	93.3	1.2	3.35	0.521	1.443	2.322	0.89	1.34

CIRS: Computerized Imaging Reference Systems, BARC: Bhabha Atomic Research Centre, PMMA: Polymethylmethacrylate, T/F: Target/Filter, CBT: Compressed breast thickness, kVp: Kilovoltage peak, mAs: Milliampere second, MGD: Mean glandular dose, BEE: Breast entrance exposure, HVL: Half value layer, mGy: Milli gray, mm Al: Millimeter aluminium, W/Rh: Tungsten/rhodium

**Table 3: Measured mean glandular dose values under clinically operated OPODSE mode (target/filter=tungsten/rhodium) for digital mammography system using Bhabha Atomic Research Centre-polymethylmethacrylate phantom of different thicknesses**

BARCPMMA mammography phantom thickness (cms)	Machine displayed parameters			Dosimeter X2 MAM readings				Calculated MGD (mGy) <sup>[31,34]</sup>	MGD ratio (machine displayed vs. measured)	Acceptable level of dose limits in European guidelines (mGy) <sup>[5]</sup>
	kVp	mAs	MGD (mGy)	BEE (mGy)	HVL (mm Al)	Exposure time (sec)	Exposure rate (mGy/sec)			
2.0	24	50.7	0.7	1.01	0.490	1.450	0.699	0.57	1.24	<1.0
2.5	26	45.4	0.7	1.21	0.523	1.441	0.842	0.60	1.16	-
3.0	26	58.9	0.8	1.58	0.525	1.462	1.084	0.70	1.15	<1.5
3.5	27	66.9	0.9	2.04	0.535	1.471	1.385	0.81	1.12	-
4.0	27	87.2	1.1	2.71	0.532	1.446	1.875	0.95	1.16	<2.0
4.5	28	98.8	1.3	3.43	0.542	1.502	2.287	1.10	1.18	<2.5
5.0	28	126.8	1.5	4.47	0.543	1.900	2.352	1.31	1.14	<3.0
5.5	29	143.4	1.8	5.59	0.551	2.064	2.711	1.50	1.20	-
6.0	29	181.0	2.1	7.15	0.552	2.241	3.193	1.77	1.19	<4.5
7.0	30	268.9	2.9	11.97	0.557	3.118	3.840	2.58	1.12	<6.5
8.0	31	352.6	3.7	17.59	0.560	3.905	4.505	3.32	1.12	-

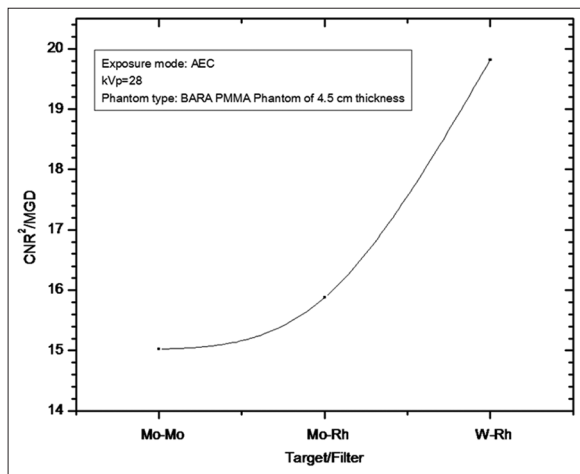
BARC: Bhabha Atomic Research Centre, PMMA: Polymethylmethacrylate, kVp: Kilovoltage peak, mAs: Milliampere second, MGD: Mean glandular dose, BEE: Breast entrance exposure, HVL: Half-value layer, mGy: Milligray, mm Al: Millimeter aluminum

variation of MGD with BARC PMMA phantom thickness can be represented by the following second-order polynomial fit equation 9.

$$\text{MGD (mGy)} = 0.83 + B_1 \times x + B_2 \times x^2 \quad (9)$$

where “x” represents the thickness of BARC PMAA phantom in centimeter. In equation 9,  $0.83 \pm 0.09$  represents the intercept value with associated standard error of 0.09;  $B_1$  has the value of  $-0.27 \pm 0.04$  and  $B_2$  has the value of  $+0.072 \pm 0.004$ . Adjusted R-squared value for the fitted data points is found to be 0.99. Establishing this fitted equation will be helpful in deriving the MGDs directly for any value of PMMA thicknesses rather calculating it using measured BEE and conversion factors.

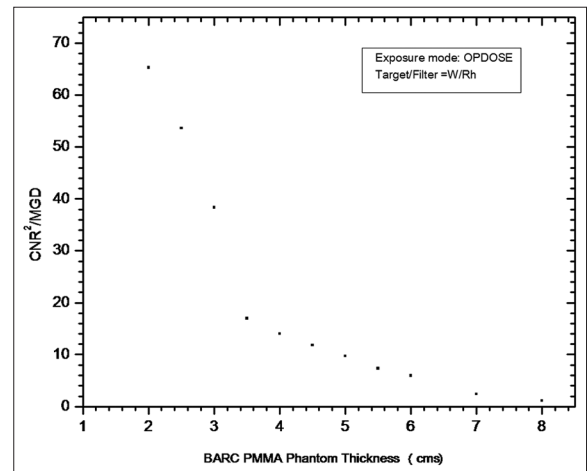
Results of the CD resolution study carried out on digital mammography system are shown in Figures 8 and 9 under



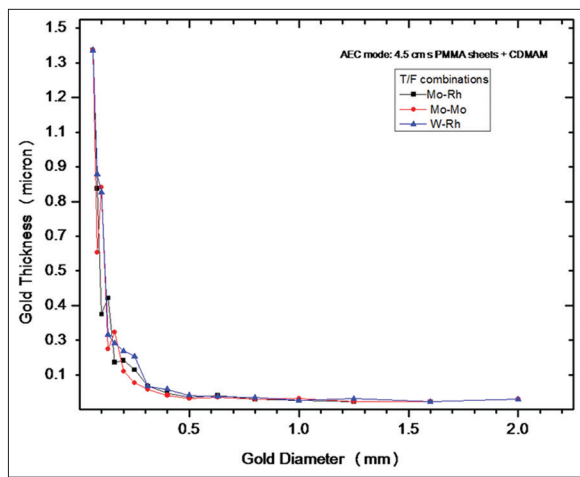
**Figure 6:** Plot for calculated figure of merit in terms of  $\text{CNR}^2/\text{mean glandular dose}$  values for the BARC polymethyl methacrylate phantom with a thickness of 4.5 cm and exposed under automatic exposure control mode

different clinical exposure conditions. Figure 8 shows the CD curve for the CDMAM phantom kept on top of the 4.5 cm PMMA sheets and exposed under AEC mode at different T/F combinations. Table 4 gives the detail of image quality parameters analyzed in terms of  $\text{IQF}_{\text{inv}}$  and % detected gold disks from the plotted CD curve along with machine selected and displayed parameters. Figure 9 shows the CD curve plotted for the CDMAM phantom in combination with PMMA sheets of various thicknesses to simulate clinical breast thicknesses in digital mammography. For different exposure conditions, under which CDMAM phantom was exposed, the measured  $\text{IQF}_{\text{inv}}$  numbers and % detected gold disks are presented in Table 5 along with machine selected and displayed parameters.

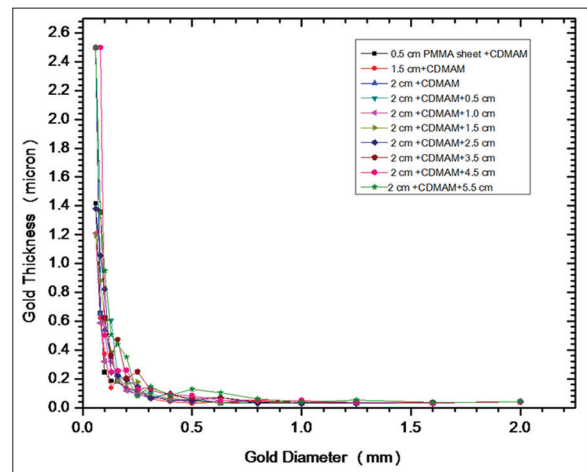
Figure 10 shows the calculated MTF values at different spatial frequencies from the image of exposed slanted edge device



**Figure 7:** Plot for calculated figure of merit in terms of  $\text{CNR}^2/\text{mean glandular dose}$  values for the BARC polymethyl methacrylate phantom having different thicknesses and exposed under clinically used OPDOSE mode



**Figure 8:** Plot of contrast detail performance for the digital mammography machine using contrast-detail mammography phantom kept on top of 4.5 cm polymethyl methacrylate sheets and exposed under automatic exposure control mode at different target/filter conditions (Mo/Mo, Mo/Rh, W/Rh)



**Figure 9:** Plot of contrast detail performance for the digital mammography machine using contrast-detail mammography phantom exposed in combination with polymethyl methacrylate sheets of various thicknesses to simulate clinical operating conditions under OPDOSE mode

**Table 4: The inverse image quality figure number and % detected gold disks for the contrast-detail mammography phantom which was kept on top of the 4.5 cm thick polymethylmethacrylate sheet and exposed at three different target/filter combinations using automatic exposure control mode**

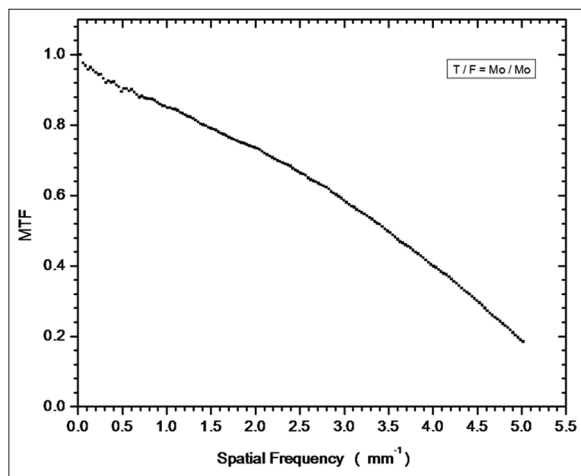
Target filter combination (T/F)	IQF <sub>inv</sub>	% detected gold disks	Operating parameters (kV/mAs) (average value for eight images)	Machine displayed MGD (mGy)
Mo/Mo	145.7	78.3	28/167.1	3.8
Mo/Rh	144.3	77.4	28/135.2	2.9
W/Rh	127.7	74.5	28/188.9	2.1

T/F: Target/filter, Mo/Mo: Molybdenum/molybdenum, Mo/Rh: Molybdenum/rhodium, W/Rh: Tungsten/rhodium, MGD: Mean glandular dose, mGy: Milligray, IQF<sub>inv</sub>: Inverse image quality figure, kV: Kilovoltage, mAs: Milliampere second

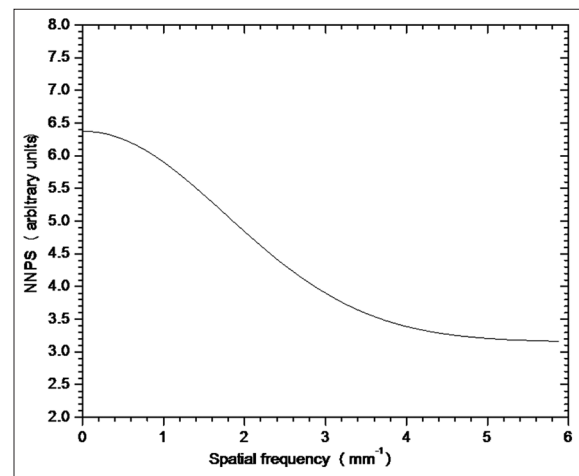
**Table 5: The inverse image quality figure number and percentage detected gold disks for the contrast-detail mammography phantom kept along with polymethylmethacrylate sheets to simulate different clinical breast thicknesses and exposed under clinically used OPDOSE mode**

Phantom thickness (cm)	IQF <sub>inv</sub>	Percentage detected gold disks	Operating parameters (kV/mAs) (average value for eight images)	Machine displayed MGD (mGy)
0.5 PMMA + CDMAM	171.9	81.6	24/41.1	0.6
1.5 PMMA + CDMAM	151.7	79	26/49.6	0.8
2.0 PMMA + CDMAM	144.4	78.7	26/63.2	0.9
2.0 PMMA + CDMAM + 0.5 PMMA	128.1	77.3	27/71.6	1.0
2.0 PMMA + CDMAM + 1.0 PMMA	168.2	79.1	27/97.45	1.25
2.0 PMMA + CDMAM + 1.5 PMMA	147.4	78.5	28/110.3	1.5
2.0 PMMA + CDMAM + 2.5 PMMA	135.6	75.5	29/152.4	2.0
2.0 PMMA + CDMAM + 3.5 PMMA	105.5	71.5	30/206.45	2.4
2.0 PMMA + CDMAM + 4.5 PMMA	102.8	72.0	31/361.3	3.8
2.0 PMMA + CDMAM + 5.5 PMMA	93.6	68.2	32/342.4	3.75

PMMA: Polymethylmethacrylate, CDMAM: Contrast-detail mammography phantom, MGD: Mean glandular dose, mGy: Milligray, IQF<sub>inv</sub>: Inverse image quality figure



**Figure 10:** Plot of calculated modulation transfer function values at different spatial frequencies for the digital mammography system



**Figure 11:** Plot of calculated normalized noise power spectrum for the different spatial frequency at entrance air kerma value of  $\sim 100 \mu\text{Gy}$

using Mo/Mo as T/F combination for the digital mammography system. Figure 11 shows the calculated normalized noise power spectrum versus spatial frequency for the digital mammography system at the entrance air kerma of  $100 \mu\text{Gy}$ . Both the MTF and the NPS are found to be falling off at higher spatial frequencies. However, at higher spatial frequencies, lower MTF values are observed when compared with reported values for the studied digital mammography machine.

### CONCLUSION

In the present study, various imaging metrics such as CNR, CD resolution, MTF, and NPS were evaluated for a direct flat-panel detector-based digital mammography system following the European Guidelines. As the studied digital mammography system has different exposure mode, a system performance study relating to both image quality and doses was carried out



by evaluating FOM in terms of  $CNR^2/MGD$  under AEC and clinically used OPDOSE operating mode. Under AEC mode of operation and for a given phantom thickness, the highest CNR and MGD values were observed for Mo/Mo, T/F combination, whereas W/Rh combination has provided the highest FOM value. Whereas, for clinically used OPDOSE mode, highest CNR, lowest MGD, and correspondingly highest FOM values were found for 2 cm thick BARC PMMA phantom. It was also concluded that as the phantom thickness increases, CNR and FOM value decreases. Detailed dosimetric studies were also performed on the digital mammography system by calculating MGDs using several mammography phantoms made up of breast tissue equivalent materials. However, all the calculated MGDs values were found to be lower than the acceptable level of dose limits provided in the European Guidelines.

### Financial support and sponsorship

Nil.

### Conflicts of interest

There are no conflicts of interest.

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