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# Readily-fabricated supported MgO catalysts for efficient and green synthesis of diethyl carbonate from ethyl carbamate and ethanol

 Fengjiao Li,<sup>id</sup>\*<sup>ab</sup> Ligu Wang,<sup>id</sup>\*<sup>c</sup> Shuang Xu,<sup>c</sup> Shuting Liang<sup>d</sup> and Ningning Zhang<sup>a</sup>

Developing cost-effective, high-efficiency and heterogeneous catalysts is of prime importance for the green synthesis of diethyl carbonate (DEC) from ethyl carbamate (EC) and ethanol. Herein, a series of MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalysts were readily fabricated by an impregnation method for DEC synthesis from EC and ethanol. The activities of the as-prepared MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalysts as well as the individual MgO or  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> were first tested in the batch reactor. Among the investigated samples, the MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> with a MgO loading of 10 wt% (denoted as 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>) exhibited the largest amount of stronger basic sites, and the highest activities with EC conversion of 41.8% and DEC yield of 30.4%, respectively. Furthermore, the DEC yield was greatly boosted to 52.1% with a high DEC selectivity of 93.8% over the 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst under the optimized reaction conditions in the fixed bed reactor, outperforming most of the reported catalysts.

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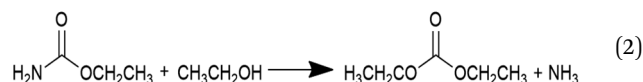
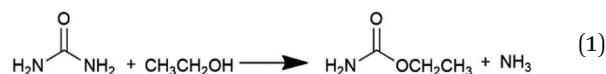
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## 1. Introduction

Diethyl carbonate (DEC) is an important linear carbonate in the 21st century, which can be widely used as a carbonylating reagent, alkylating reagent, solvent, electrolyte, fuel additive, *etc.*<sup>1–3</sup> Various methods have been adopted to produce DEC. The earliest one is the phosgenation of ethanol to synthesize DEC in 1941, which involved an extremely hazardous raw material such as phosgene.<sup>4</sup> To avoid the usage of the poisonous phosgene, a number of phosgene-free routes such as transesterification of carbonate,<sup>5–8</sup> carbonation of ethanol,<sup>9,10</sup> coupling reaction from CO<sub>2</sub>, epoxides and ethanol,<sup>11</sup> ethanolysis of CO<sub>2</sub>,<sup>12–16</sup> ethanolysis of urea,<sup>17–24</sup> and ethanolysis of ethyl carbamate (EC)<sup>24–33</sup> have been developed in the past years. It is worth noting that ethanolysis of urea or EC to produce DEC, which is considered as indirect utilization of CO<sub>2</sub> to high value-added products, has been attracting wide attention and interest in the recent years.

As shown in eqn (1) and (2), ethanolysis of urea to DEC actually occurs in two steps: (i) ethanolysis of urea to EC intermediate and NH<sub>3</sub> by-product, (ii) ethanolysis of EC intermediate to DEC product and NH<sub>3</sub> by-product. The latter one is well

known as the rate-determining step, which has dominant impacts on DEC synthesis and strongly calls for the development of efficient catalysts. Urea is easy to decompose at high reaction temperatures, usually causing unsatisfactory DEC yield and selectivity *via* direct ethanolysis of urea. However, the more stable EC intermediate can be easily prepared by ethanolysis of urea with high yield and selectivity even without any catalysts.<sup>17</sup> Therefore, ethanolysis of EC is a more economical and promising route for large-scale production of DEC when compared with the direct ethanolysis of urea to DEC.



The ethanolysis of EC to DEC is very sluggish, and the obtained DEC yield under conventional conditions is usually less than 5% without the presence of catalysts.<sup>26–28,31–33</sup> Actually, the DEC yield could be improved to 22.9% with a DEC selectivity of 48.0% from EC in supercritical ethanol, but the extremely harsh conditions of 573 K and 13.2 MPa will inevitably increase the investment costs on reactors.<sup>12</sup> Therefore, the research work is more focused on developing efficient catalysts for DEC synthesis from EC and ethanol. For instance, Zhao *et al.* applied different transition metal chlorides to investigate the catalysis effects in the batch reactor, and found that the activities

<sup>a</sup>Shenzhen Automotive Research Institute, Beijing Institute of Technology, Shenzhen 518118, Guangdong, China. E-mail: lifengjiao@szari.ac.cn

<sup>b</sup>College of Chemistry and Environmental Engineering, Shenzhen University, Shenzhen 518060, Guangdong, China

<sup>c</sup>Key Laboratory for Green Process and Engineering, National Engineering Laboratory for Hydrometallurgical Cleaner Production Technology, Institute of Process Engineering, Chinese Academy of Sciences, Beijing 100190, China. E-mail: lgwang@ipe.ac.cn

<sup>d</sup>College of Chemical and Environmental Engineering, Chongqing University of Arts and Sciences, Yongchuan, Chongqing 402160, China



followed the sequence of  $\text{MnCl}_2 > \text{CoCl}_2 > \text{ZnCl}_2 > \text{CdCl}_2 > \text{NiCl}_2$ .<sup>33</sup> However, the EC conversion and DEC yield over the highest  $\text{MnCl}_2$  is only 23% and 11%, respectively. In addition, these transition metal chlorides were homogeneous and normally suffered from the difficulties in separating from the products. In contrast, single or mixed metal oxides such as  $\text{PbO}$ ,<sup>25</sup>  $\text{ZnO}$ <sup>24</sup> and zinc-based mixed oxides (e.g.,  $\text{ZnO-PbO}$ ,<sup>26</sup> and  $\text{Zn-Al-M}$  based oxides ( $\text{M} = \text{Ca}, \text{Mg}, \text{La}$  and  $\text{Y}$ )<sup>30</sup>),  $\text{MgO}$ <sup>28</sup> and magnesium-based mixed oxides (e.g., waste slag derived oxides,<sup>27</sup> transition metal-modified mesoporous  $\text{Mg-Al}$  mixed oxides,<sup>29</sup> and  $\text{Mg-Al-Y}$  mixed oxides<sup>31</sup>), and  $\text{CeO}_2$ <sup>32</sup> were more frequently employed in the batch reactors. In general, the DEC yields over the Pb-containing oxides are lower than 21%.<sup>25,26</sup> In addition, the post-treatment of the non-environment-friendly Pb element is another challenge for green and large-scale synthesis of DEC. As for the single  $\text{ZnO}$  or  $\text{ZnO}$ -containing mixed oxides, the  $\text{ZnO}$  component was converted to the homogenous  $\text{Zn}(\text{NH}_3)_2(\text{NCO})_2$  during the reaction, which functioned as the real active composition for DEC synthesis,<sup>24,26</sup> and thus would also lead to the problems of separating catalysts. Recently, the Mg-containing oxides have shown great potentials as heterogeneous catalysts for efficient DEC synthesis in the batch reactors.<sup>27-29,31</sup> It was discovered that the activity of  $\text{MgO}$  is strongly dependent on the preparation method, and the  $\text{MgO}$  nanosheet ( $\text{MgO-SC-450}$ ) exhibited the highest catalytic activities among the investigated  $\text{MgO}$  samples prepared by different methods.<sup>28</sup> However, these methods to obtain  $\text{MgO}$ -based materials appear to be expensive and complicated for practical applications of DEC synthesis. Furthermore, the mechanical strength of  $\text{MgO}$  is relatively low, and shaping of  $\text{MgO}$ -based materials is also complex. It can be also noted that the above-mentioned catalysts were used in the batch reactors. Therefore, it still remains a formidable challenge to develop highly effective, low-cost, and readily-fabricated  $\text{MgO}$ -based catalysts with strong mechanical strength for continuous synthesis of DEC *via* ethanolysis of EC in the fixed bed reactors.

In this work, using the common  $\gamma\text{-Al}_2\text{O}_3$  with strong mechanical strength as the support, a series of  $\text{MgO}/\gamma\text{-Al}_2\text{O}_3$  catalysts with different  $\text{MgO}$  loadings (e.g., 5 wt%, 10 wt% and 15 wt%) were readily prepared by a facile impregnation method for the synthesis of DEC from EC and ethanol. The structures and physicochemical properties of the above supported catalysts, the  $\gamma\text{-Al}_2\text{O}_3$  support and the pure  $\text{MgO}$  sample were systematically characterized by X-ray diffraction (XRD), X-ray photoelectron spectra (XPS), field-emission scanning electron microscope (FE-SEM), Fourier transform infrared (FTIR) spectra,  $\text{N}_2$  sorption, and temperature programmed desorption of  $\text{CO}_2$  ( $\text{CO}_2$ -TPD). The screening and reusability of catalysts was first evaluated in the batch reactor. Afterwards, the effects of reaction conditions on the performances over the most active catalyst were investigated in the fixed bed reactor for continuous synthesis of DEC from EC and ethanol. This work provides a comprehensive insight into a very cost-effective and highly efficient heterogeneous catalyst system of  $\text{MgO}/\gamma\text{-Al}_2\text{O}_3$  for continuously manufacturing DEC *via* the reaction of EC and ethanol.

## 2. Experimental

### 2.1 Materials

EC ( $\geq 98.0\%$  purity), ethanol (99.7% purity), cyclohexanol ( $\geq 99.0\%$  purity),  $\text{Mg}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  ( $\geq 99.0\%$  purity) and quartz sand (20–40 mesh) were commercially purchased from Sino-pharm Chemical Reagent Co., Ltd., China.  $\gamma\text{-Al}_2\text{O}_3$  (20–40 mesh) was obtained from Aladdin Industrial Corporation, China.

### 2.2 Catalyst preparation

The  $\gamma\text{-Al}_2\text{O}_3$  was pre-treated at 873 K for 2 h prior to use. Various  $\text{MgO}$  supported on  $\gamma\text{-Al}_2\text{O}_3$  catalysts with different  $\text{MgO}$  loadings of 5 wt%, 10 wt%, and 15 wt% were prepared by an impregnation method. First, the  $\gamma\text{-Al}_2\text{O}_3$  support was impregnated with a desired amount of magnesium nitrate solution for 18 h at room temperature, followed by drying at 383 K for 12 h and calcination in air at 673 K for 3 h. The obtained catalysts were denoted as 5%  $\text{MgO}/\gamma\text{-Al}_2\text{O}_3$ , 10%  $\text{MgO}/\gamma\text{-Al}_2\text{O}_3$  and 15%  $\text{MgO}/\gamma\text{-Al}_2\text{O}_3$ , respectively. Pure  $\text{MgO}$  employed in this paper was also prepared by calcining  $\text{Mg}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  at 673 K in air for 3 h for comparison.

### 2.3 Catalyst characterization

X-ray diffraction (XRD) patterns were acquired with a PANalytical Empyrean diffractometer using  $\text{Cu K}\alpha$  radiation at 40 kV, 40 mA.

Field-emission scanning electron microscopy (FE-SEM) images were collected on an FEI Quanta 250 FEG microscope.

X-ray photoelectron spectra (XPS) tests were conducted on an ESCALAB 250Xi spectrometer with  $\text{Al K}\alpha$  radiation (1486.6 eV). The C 1 s peak at 284.8 eV was applied as a reference to calibrate all the peaks.

Fourier transform infrared (FTIR) spectra were recorded on a Tensor 27 Fourier-transform infrared spectrometer from 4000 to 400  $\text{cm}^{-1}$ .

$\text{N}_2$  sorption analysis experiments were carried out on a Quantachrome Autosorb-1 instrument at 77 K. Prior to the measurements, all the samples were outgassed in vacuum at 573 K for 3 h. The specific surface areas ( $S_{\text{BET}}$ ) of the samples were determined using the  $\text{N}_2$  adsorption data at a relative pressure ( $P/P_0$ ) from 0.05 to 0.30 according to the Barrett-Emmett-Teller (BET) method. The total pore volume ( $V_{\text{p}}$ ) and the average pore diameter ( $D_{\text{p}}$ ) of the samples were obtained by analyzing the desorption branch of the isotherms based on the Barrett-Joyner-Halenda (BJH) model.

The  $\text{CO}_2$  temperature program desorption ( $\text{CO}_2$ -TPD) experiments were performed on an AutoChem II 2920 with a thermal conductivity detector (TCD). Typically, the sample was pre-heated in helium (25  $\text{mL min}^{-1}$ ) at 393 K for 60 min, and then cooled to 323 K. Afterwards, the sample was saturated with a mixture of 10 vol%  $\text{CO}_2/\text{He}$  (25  $\text{mL min}^{-1}$ ) for 1 h. The physically-adsorbed  $\text{CO}_2$  was removed by flushing with helium (25  $\text{mL min}^{-1}$ ) at 323 K for 30 min. Finally, the temperature was increased to 923 K at a heating rate of 10  $\text{K min}^{-1}$ .

## 2.4 Catalytic tests

**2.4.1 DEC synthesis in the batch reactor.** The reactions in the batch reactor were conducted in a 100 mL-stainless-steel autoclave with a magnetic stirrer and a temperature controller. A typical reaction procedure is as follows: first, 34 mmol of EC, 0.34 mol of ethanol, and 10 wt% catalyst (based on the weight of EC) were added into the autoclave. Then the autoclave was sealed, heated to 473 K and retained at 473 K for 3 h under vigorous stirring. After the reaction was finished, the autoclave was cooled to room temperature and depressurized. After the catalyst was separated by centrifugation, the resulting liquid mixtures with cyclohexanol as the internal standard were analyzed on GC-2014 (Shimadzu, Japan) with an Rtx-5 capillary column (30 m  $\times$  0.25 mm  $\times$  0.25  $\mu$ m), an autosampler and a flame ionization detector (FID). For the recycling experiments, the used catalyst was separated by centrifugation, washed thoroughly with ethanol, and directly added into the autoclave with fresh EC and ethanol for the next cycle. For clarity, the 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst after the fifth cycle was denoted as 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>-reused. The EC conversion (shorted as EC conv.), DEC yield, DEC selectivity (shorted as DEC sel.) and the yield of *N*-ethyl ethyl carbamate (NEEC) were calculated according to the previous literature.<sup>28</sup>

**2.4.2 DEC synthesis in the fixed bed reactor.** Continuous synthesis of DEC *via* ethanolysis of EC was carried out in a bench-scale fixed bed reactor with a single stainless-steel tube. The length and inner diameter of the tube are 0.90 m and 1.2  $\times$  10<sup>-2</sup> m, respectively. The reactor was heated to the desired reaction temperature by three independently controlled tubular furnaces. The reactor was provided with mass flow controllers,

pressure indicator, controller devices and four thermocouples to measure the temperatures at four different points. A stuff storage vessel of 3 L capacity was connected to the constant-flux pump through a volumetric buret to measure the liquid flow rate, followed by a preheater. The pump possessed a maximum capacity of 1.2  $\times$  10<sup>-4</sup> m<sup>3</sup> h<sup>-1</sup> under a pressure of 200 bar. The product stuff storage vessel of 3 L capacity was connected to the other end of the reactor through a product condenser, which also functioned as a separator for products.

Typically, 2.0 g catalyst (20–40 mesh, about 2.6 mL) was charged into the fixed bed reactor and the residue zone of the reactor was filled with quartz sand (20–40 mesh). Then, the reactor was heated to the expected reaction temperature after being pressured with N<sub>2</sub> to the desired pressure. Afterwards, the solution containing EC and ethanol was continuously introduced into the reactor after being pre-heated to 333 K. After the reaction was finished, the products were cooled in a product condenser at 323 K, in order to avoid the formation of ammonium carbonate from the reaction of carbon dioxide and ammonia. Simultaneously, at the top of the condenser, the gas products were released through the pipeline. The liquid products were introduced into the product storage vessel at the bottom of the condenser. Liquid samples were analyzed by the method similar to those in the batch reactor.

## 3. Results and discussion

### 3.1 Catalyst characterization

**3.1.1 XRD and XPS.** Fig. 1a and b shows XRD patterns of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support, the three supported MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples,

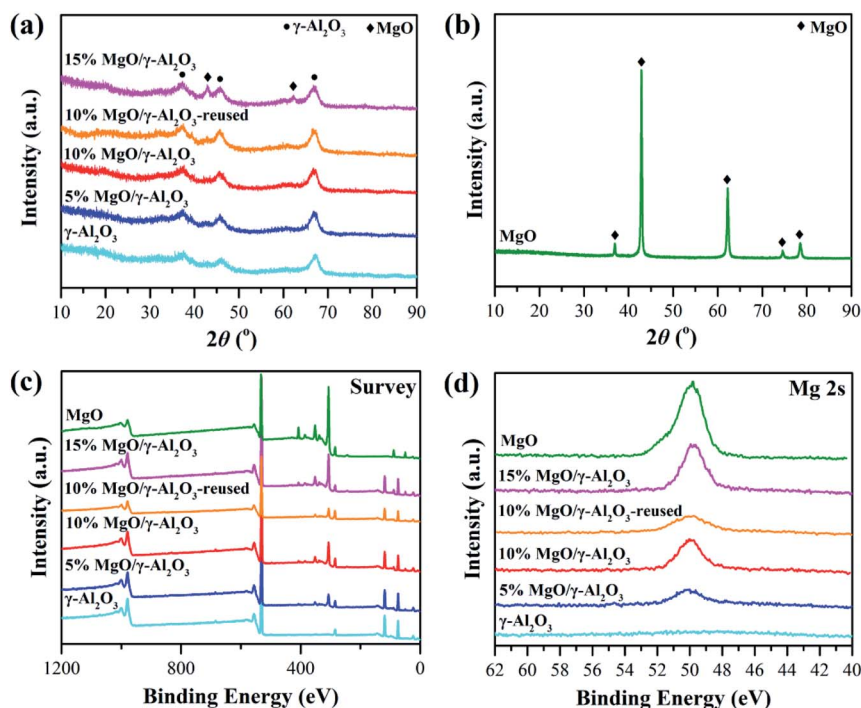


Fig. 1 XRD patterns (a and b), XPS survey spectra (c) and Mg 2s high resolution XPS spectra (d) of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, 5% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, 15% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, MgO and 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>-reused samples.



the pure MgO sample and the 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>-reused sample. As shown in Fig. 1a, all the MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples present the typical diffraction peaks of  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> with  $2\theta$  values of 37.6°, 45.8° and 67.3° (JCPDS 01-1308). In addition, when the MgO loading is lower than 10 wt%, no crystalline phase of MgO can be found in the 5% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples, suggesting that MgO was highly dispersed as a monolayer on the surface of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support. In contrast, the peak intensities of the crystalline MgO dramatically increases with the MgO loading increasing to 15 wt%, as evidenced by the distinct diffraction peaks of the crystalline MgO in the 15% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> sample. It was reported that MgO can react with  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> to generate Mg–Al spinel when the calcination temperature is higher than 843 K, while no obvious reaction occurs between MgO and  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> at a lower calcination temperature of 723 K.<sup>34</sup> Therefore, the reaction of MgO with  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> to Mg–Al spinel can be neglected in all the three supported MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples, as those supported samples were obtained at a relatively lower calcination temperature of 673 K in this work. Highly crystallized MgO was obviously obtained by calcining Mg(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O at 673 K in air, as proved by the typical diffraction peaks of MgO (JCPDS 79-0612) in the pure MgO sample (Fig. 1b). The following XPS results (Fig. 1c and d) confirmed that MgO was highly enriched on the surfaces of the MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples, also proving that no Mg–Al spinel formed in the three supported MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples.

**3.1.2 SEM.** Fig. 2 presents the SEM images of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support, the three supported MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples, the pure MgO sample and the 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>-reused sample. As presented in Fig. 2a, the pure MgO sample is composed of nanoplates with a thickness of *ca.* 0.12  $\mu$ m. The  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support is consisted of stacked nano-sized particles with average sizes of *ca.* 30 nm (Fig. 2b). All the three MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples

possessed similar morphologies with the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support, and no obvious nanoplates derived from MgO were found in the above supported MgO samples (Fig. 2c–e), also confirming that MgO was highly dispersed on the surfaces of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support.

**3.1.3 FTIR.** Fig. 3 displays the FTIR spectra of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support, the three supported MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples, and the pure MgO sample. The absorption band around 1633 cm<sup>-1</sup> is observed in all the above samples, which is well-known as the H–O–H angle bending vibration band of weakly bound molecular water. As for the three supported MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples, two broad bands around 780 and 580 cm<sup>-1</sup> were detected, which corresponded to Al–O–Al bending mode and Al–O stretching mode, respectively, while the band at  $\sim$ 3470 cm<sup>-1</sup>

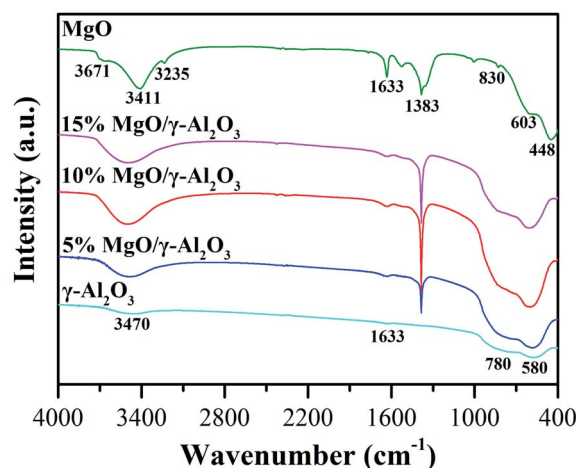


Fig. 3 FTIR of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, 5% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, 15% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and MgO samples.

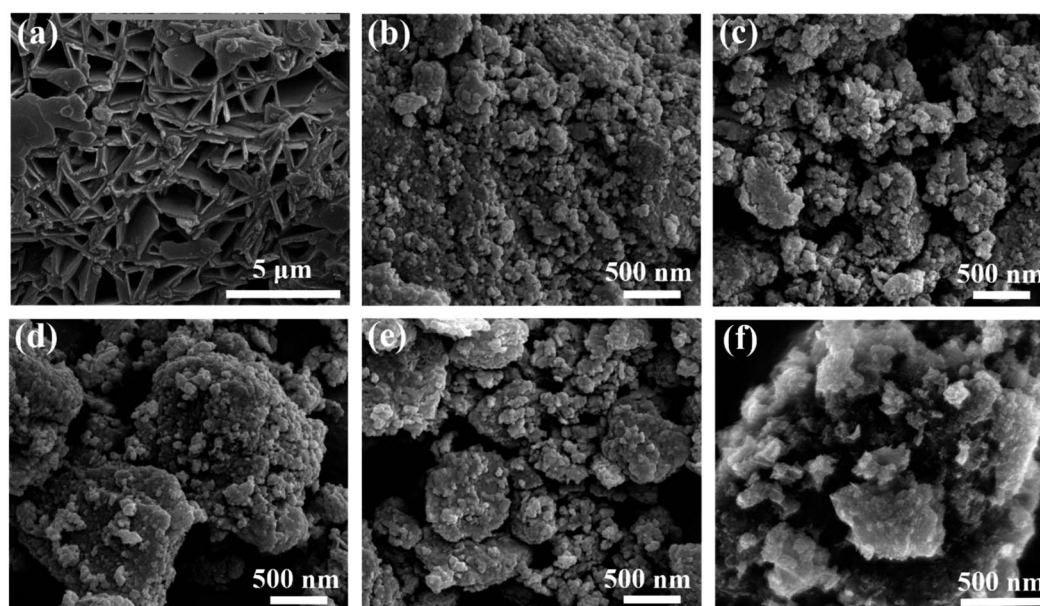


Fig. 2 SEM images of (a) MgO, (b)  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, (c) 5% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, (d) 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, (e) 15% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and (f) 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>-reused samples.

could be attributed to the presence of the Al–OH bond, all of which are derived from the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support.<sup>35,36</sup> In addition, the peaks around 1383, 830, 603 and 448 cm<sup>-1</sup> in all the three supported MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples were assigned to the stretching vibration of Mg–O–Mg bonding,<sup>37,38</sup> also confirming the successful formation of MgO on the surfaces of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support for the three supported MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples.

**3.1.4 Nitrogen adsorption/desorption.** The N<sub>2</sub> adsorption/desorption isotherms and the corresponding pore size distributions of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, the three supported MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and pure MgO samples are shown in Fig. 4, and their corresponding pore structure parameters are summarized in Table 1. As displayed in Fig. 4a, the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support and the three MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples present typical type IV isotherms with obvious hysteresis loops, suggesting that the mesopores of the three MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples are derived from the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support. In addition, the pore sizes of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support and the three supported MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples mainly center at 7–8 nm (Fig. 4b). As listed in Table 1, the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support possesses the largest surface area and pore volume (203.0 m<sup>2</sup> g<sup>-1</sup> and 0.59 cm<sup>3</sup> g<sup>-1</sup>, respectively) with an average pore diameter of 11.6 nm, while MgO has a negligible number of pores with the

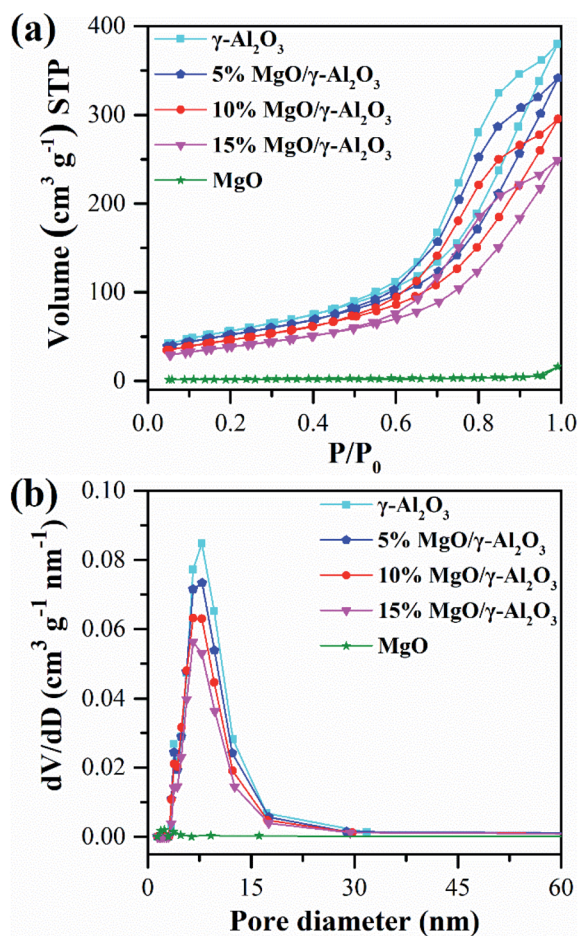
**Table 1** Textural and structural properties of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, 5% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, 15% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and MgO samples

Sample	$S_{\text{BET}}$ (m <sup>2</sup> g <sup>-1</sup> )	$V_{\text{p}}$ (cm <sup>3</sup> g <sup>-1</sup> )	$D_{\text{p}}$ (nm)
$\gamma$ -Al <sub>2</sub> O <sub>3</sub>	203.0	0.59	11.6
5% MgO/ $\gamma$ -Al <sub>2</sub> O <sub>3</sub>	187.5	0.53	11.3
10% MgO/ $\gamma$ -Al <sub>2</sub> O <sub>3</sub>	167.3	0.46	11.0
15% MgO/ $\gamma$ -Al <sub>2</sub> O <sub>3</sub>	138.3	0.39	11.2
MgO	5.5	0.02	—

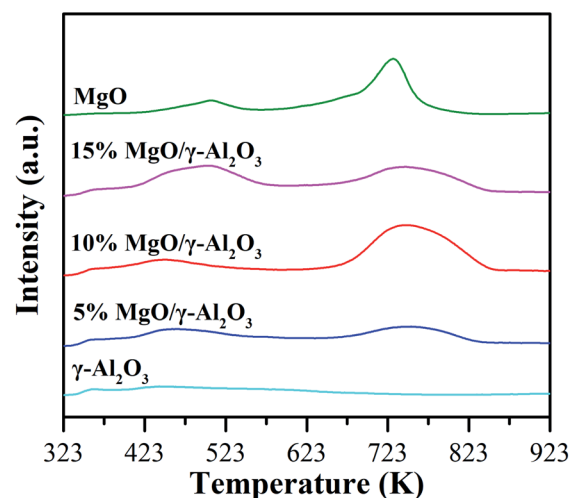
smallest surface area of 5.5 m<sup>2</sup> g<sup>-1</sup>. After introducing MgO onto the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support, both the surface areas and pore volumes of the three supported MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples decrease with the increasing MgO loadings. However, high specific surface areas (>130 m<sup>2</sup> g<sup>-1</sup>) and large pore volume (>0.3 cm<sup>3</sup> g<sup>-1</sup>) are still obtained in the three supported MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples due to the high dispersion of MgO on the surface of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support.

Specifically, the 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> sample possesses a moderate surface area of 167.3 m<sup>2</sup> g<sup>-1</sup> with a pore volume of 0.46 cm<sup>3</sup> g<sup>-1</sup> and an average pore diameter of 11.0 nm. The enlarged specific surface areas of the supported MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples were beneficial for the active sites to access to the reactants, thus facilitating the enhancement of the EC conversion and DEC yield over the supported MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> samples.

**3.1.5 CO<sub>2</sub>-TPD.** Basic strength and total basicity (*i.e.*, the number of basic sites per unit weight of catalyst) are two crucial parameters to evaluate the basic properties of solid base catalysts.<sup>27,28,31,39</sup> Therefore, to enclose the differences among the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, the three supported MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and the pure MgO samples, the basic strength and the number of different kinds of basic sites of these oxide catalysts were further investigated by CO<sub>2</sub>-TPD. The CO<sub>2</sub>-TPD profiles of the above samples are displayed in Fig. 5. In general, the CO<sub>2</sub> desorption peaks represents three kinds of basic sites based on the desorption



**Fig. 4** N<sub>2</sub> adsorption and desorption isotherms (a) and the corresponding pore size distributions (b) of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, 5% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, 15% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and MgO samples.



**Fig. 5** CO<sub>2</sub>-TPD profiles of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, 5% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, 15% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and MgO samples.

temperatures, *i.e.*, the weak basic sites ( $\text{CO}_2$  desorption temperature below 473 K), the medium basic sites ( $\text{CO}_2$  desorption temperature between 473 K and 673 K), and the strong basic sites ( $\text{CO}_2$  desorption temperature higher than 673 K).<sup>27,31</sup> The corresponding distribution of basic sites on the above samples was listed in Table 2. Among the investigated samples, the  $\gamma\text{-Al}_2\text{O}_3$  possessed the lowest amount of total basic sites and strong basic sites ( $520.5 \mu\text{mol g}^{-1}$  and  $22.1 \mu\text{mol g}^{-1}$ , respectively), while the pure MgO had the smallest amount of weak basic sites ( $72.6 \mu\text{mol g}^{-1}$ ) with a moderate amount of medium and strong basic sites. After introducing MgO onto the  $\gamma\text{-Al}_2\text{O}_3$  support, the number of total basic sites increased with the increasing MgO loadings, and reached a maximum value of  $2196.7 \mu\text{mol g}^{-1}$  over the 15% MgO/ $\gamma\text{-Al}_2\text{O}_3$  sample. In addition, in the region of  $\text{CO}_2$  desorption temperature higher than 673 K, the three supported MgO samples definitely required higher temperature for  $\text{CO}_2$  to desorb from their surfaces than the pure MgO sample, indicating that the three supported MgO samples possessed stronger basicity in the region of strong basic sites than pure MgO. Importantly, the amount of strong basic sites followed the order of 10% MgO/ $\gamma\text{-Al}_2\text{O}_3$  > 15% MgO/ $\gamma\text{-Al}_2\text{O}_3$  > 5% MgO/ $\gamma\text{-Al}_2\text{O}_3$ .

### 3.2 DEC synthesis in the batch reactor

The performances of the  $\gamma\text{-Al}_2\text{O}_3$  support, the three supported MgO catalysts, and the individual MgO sample for DEC synthesis from EC and ethanol were first evaluated in the batch reactor, and the results are summarized in Table 3. The EC conversion and DEC yield over the  $\gamma\text{-Al}_2\text{O}_3$  support are 8.3% and 3.6%, respectively (entry 2), which are very close to those in the blank experiment (entry 1), indicating that the  $\gamma\text{-Al}_2\text{O}_3$  support was quite inert for DEC synthesis from EC and ethanol. In addition, the pure MgO sample obtained by simple calcination of  $\text{Mg}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  at 673 K in air also showed inferior activities towards this reaction (9.5% of EC conversion and 4.0% of DEC yield, entry 6), which is worse than the reported MgO catalysts by thermal decomposition (*i.e.*, MgO-MCBP-450 and MgO-MH-450) and precipitation methods (*i.e.*, MgO-SC-450, MgO-SH-450 and MgO-NH-450),<sup>28</sup> also suggesting that the preparation method had a significant impact on the activities of MgO. However, the three supported MgO/ $\gamma\text{-Al}_2\text{O}_3$  catalysts obtained by the facile impregnation method exhibited much higher catalytic abilities than the  $\gamma\text{-Al}_2\text{O}_3$  support or the pure MgO

**Table 2** The basicities and the distribution of basic sites determined by  $\text{CO}_2$ -TPD of the  $\gamma\text{-Al}_2\text{O}_3$ , 5% MgO/ $\gamma\text{-Al}_2\text{O}_3$ , 10% MgO/ $\gamma\text{-Al}_2\text{O}_3$ , 15% MgO/ $\gamma\text{-Al}_2\text{O}_3$  and MgO samples

Sample	Number of basic sites ( $\mu\text{mol g}^{-1}$ )			
	Weak	Medium	Strong	Total
$\gamma\text{-Al}_2\text{O}_3$	221.5	276.9	22.1	520.5
5% MgO/ $\gamma\text{-Al}_2\text{O}_3$	380.4	538.1	617.1	1535.6
10% MgO/ $\gamma\text{-Al}_2\text{O}_3$	270.5	301.9	1054.3	1626.7
15% MgO/ $\gamma\text{-Al}_2\text{O}_3$	426.6	881.7	888.4	2196.7
MgO	72.6	334.5	593.2	1000.3

**Table 3** The catalytic performances of different catalysts on the DEC synthesis from EC and ethanol in the batch reactor<sup>a</sup>

Entry	Catalyst	EC conv. (%)	DEC yield (%)	DEC sel. (%)	NEEC yield (%)
1	None	6.1	4.4	72.1	—
2	$\gamma\text{-Al}_2\text{O}_3$	8.3	3.6	43.6	1.4
3	5% MgO/ $\gamma\text{-Al}_2\text{O}_3$	25.0	10.6	42.5	2.5
4	10% MgO/ $\gamma\text{-Al}_2\text{O}_3$	41.8	30.4	72.6	1.6
5	15% MgO/ $\gamma\text{-Al}_2\text{O}_3$	32.2	19.3	59.9	2.5
6	MgO	9.5	4.0	41.5	1.3

<sup>a</sup> Reaction conditions: 473 K, 34 mmol of EC, 0.34 mol of ethanol, 10 wt% of catalyst amount (based on the weight of EC), and 3 h.

sample. As shown in entries 3–5, both the EC conversion and the DEC yield increased with the MgO loading increasing to 10 wt%, and then dropped when the MgO loading was further increased to 15 wt%. It can be clearly found that in the batch reactor, the activities of the supported MgO catalysts follow the similar order with the total amount of strong basic sites. Specifically, the 10% MgO/ $\gamma\text{-Al}_2\text{O}_3$  catalyst with the largest total amount of strong basic sites exhibited the highest EC conversion of 41.8% and the highest DEC yield of 30.4%, respectively, while the 5% MgO/ $\gamma\text{-Al}_2\text{O}_3$  catalyst with the smallest total amount of strong basic sites showed the lowest activities. The total amount of strong basic sites over the pure MgO sample is close to that over the 5% MgO/ $\gamma\text{-Al}_2\text{O}_3$  catalyst, but the activities of the former one is much lower than the latter one, indicating that the high dispersion of MgO on the  $\gamma\text{-Al}_2\text{O}_3$  support and the enlarged surface area were also beneficial for the enhanced activities of the supported MgO catalysts. More importantly, the supported MgO catalysts obviously possessed stronger basic sites than the pure MgO sample in the region of desorption temperature higher than 673 K (Fig. 5), therefore, it can be concluded that larger amount of stronger basic sites of the supported MgO catalysts actually played the very crucial role in the DEC synthesis from EC and ethanol.

In a word, the above results suggested that the outstanding activities of the supported MgO catalysts could be attributed to the co-contribution of the high dispersion of MgO on the  $\gamma\text{-Al}_2\text{O}_3$  support, the enlarged surface area, and larger amount of stronger basic sites.

The reusability of the 10% MgO/ $\gamma\text{-Al}_2\text{O}_3$  catalyst for DEC synthesis in the batch reactor was also investigated for practical application. After the reaction, the catalyst was centrifuged, washed, and directly reused for the next cycle, and the results are shown in Fig. 6. Obviously, the 10% MgO/ $\gamma\text{-Al}_2\text{O}_3$  catalyst could be recycled and reused at least five times without significant variation in the activity. Furthermore, XRD, XPS and SEM studies of the 10% MgO/ $\gamma\text{-Al}_2\text{O}_3$  catalyst after the fifth cycle (denoted as 10% MgO/ $\gamma\text{-Al}_2\text{O}_3$ -reused) were also performed, in order to gain a deep insight into the stability of the 10% MgO/ $\gamma\text{-Al}_2\text{O}_3$  catalyst. As exhibited in Fig. 1a, compared with the fresh 10% MgO/ $\gamma\text{-Al}_2\text{O}_3$  catalyst, there were no obvious changes to the crystallite size and crystal phase after the fifth reuse.



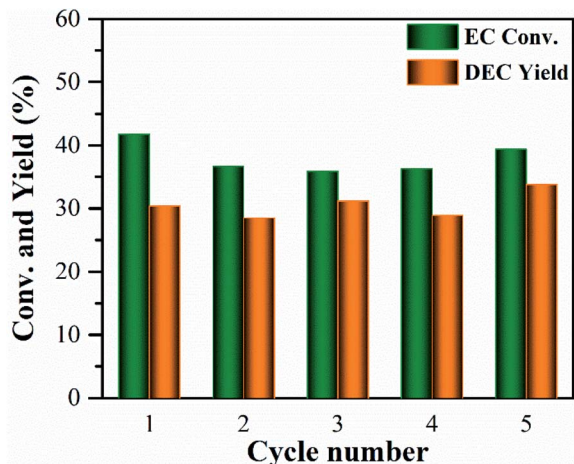


Fig. 6 The reusability of the 10% MgO/γ-Al<sub>2</sub>O<sub>3</sub> catalyst for DEC synthesis from EC and ethanol in the batch reactor. Reaction conditions: 473 K, 34 mmol of EC, 0.34 mol of ethanol, 10 wt% of catalyst amount (based on the weight of EC), and 3 h.

XPS also shows no distinct changes between the fresh and the reused 10% MgO/γ-Al<sub>2</sub>O<sub>3</sub> catalyst, indicating that no new species were formed after reuse (Fig. 1c and d). In addition, the 10% MgO/γ-Al<sub>2</sub>O<sub>3</sub>-reused catalyst showed similar morphologies

(Fig. 3f) in comparison with the fresh one. Therefore, it could be concluded that the 10% MgO/γ-Al<sub>2</sub>O<sub>3</sub> catalyst has a remarkable structure stability and reusability for DEC synthesis from EC and ethanol.

### 3.3 DEC synthesis in the fixed-bed reactor

Despite of the high activities of the 10% MgO/γ-Al<sub>2</sub>O<sub>3</sub> catalyst in the batch reactor, the NH<sub>3</sub> by-product was accumulated in the batch reactor and would restrict the shift of the reaction equilibrium to DEC synthesis, which is disadvantageous to the improvement of DEC yield. Therefore, the performances of the 10% MgO/γ-Al<sub>2</sub>O<sub>3</sub> catalyst for continuous synthesis of DEC from EC and ethanol were further investigated in the fixed-bed reactor, which could efficiently shift the reaction equilibrium to the side of DEC synthesis by removing the ammonia by-product simultaneously from the reactor. In addition, this reactor would also alleviate the problems of the undesirable side reactions, thus helping to improve the DEC yield and selectivity.

At first, the experiment only with quartz sand filled into the whole tube of the fixed bed reactor was conducted under the reaction condition of 463 K, 1.6 MPa, EC solution liquid hourly space velocity (LHSV) of 2.02 h<sup>-1</sup>, and the molar ratio of ethanol to EC (shorted as  $n(\text{EtOH})/n(\text{EC})$ ) of 10. As shown in Fig. 7a, in the absence of the 10% MgO/γ-Al<sub>2</sub>O<sub>3</sub> catalyst, both the EC conversion and the DEC yield are extremely low, which are 3.7%

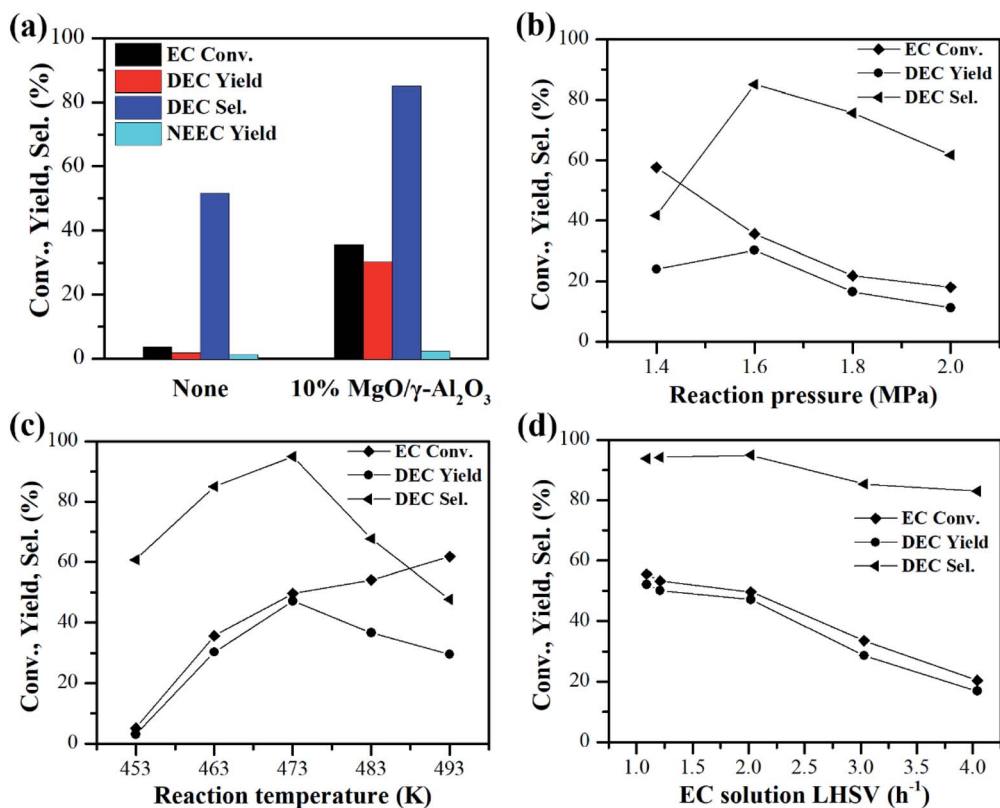


Fig. 7 Effects of reaction conditions on the performances of the 10% MgO/γ-Al<sub>2</sub>O<sub>3</sub> catalyst for continuous synthesis of DEC from EC and ethanol in the fixed bed reactor, 2 g of catalyst,  $n(\text{EtOH})/n(\text{EC})$  of 10. (a) Comparison before and after the addition of the 10% MgO/γ-Al<sub>2</sub>O<sub>3</sub> catalyst. Reaction conditions: 463 K, 1.6 MPa, EC solution LHSV of 2.02 h<sup>-1</sup>; (b) effect of reaction pressure. Reaction conditions: 463 K, EC solution LHSV of 2.02 h<sup>-1</sup>; (c) effect of reaction temperature. Reaction conditions: 1.6 MPa, EC solution LHSV of 2.02 h<sup>-1</sup>; (d) effect of EC solution LHSV. Reaction conditions: 473 K, 1.6 MPa.

and 1.9%, respectively, demonstrating that the quartz sand is inactive towards this reaction. However, after the 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst was loaded into the reaction zone in the fixed bed reactor, the EC conversion and the DEC yield were greatly boosted to 35.6% and 30.3% under the same reaction conditions, also re-confirming the superior activities of the 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst (Fig. 7a). Furthermore, the effects of reaction conditions such as reaction pressure, reaction temperature, and EC solution LHSV on the catalytic performances of the 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst for continuous synthesis of DEC from EC and ethanol in the fixed-bed reactor were also investigated.

The effect of reaction pressure is shown in Fig. 7b. Theoretically, low pressure is beneficial for the ammonia by-product to escape from the reaction system.<sup>40</sup> As a result, the EC conversion gradually increased with the reaction pressure decreasing from 2.0 MPa to 1.4 MPa. However, the DEC yield first increased with the reaction pressure increasing from 1.4 MPa to 1.6 MPa, and then dropped from 1.6 MPa to 2.0 MPa. In addition, 85.0% of DEC selectivity was obtained at 1.6 MPa, which was higher than that in the batch reactor at a higher reaction temperature of 473 K (72.6% of DEC selectivity, entry 4 in Table 3). Therefore, the suitable reaction pressure for the DEC synthesis in the fixed bed reactor should be 1.6 MPa.

The effect of reaction temperature is displayed in Fig. 7c. The EC conversion increased with the reaction temperature increasing from 453 K to 493 K. In contrast, the DEC yield first increased with the reaction temperature increasing from 453 K to 473 K, and then dropped after 473 K. As disclosed by previous work, DEC could be decomposed into CO<sub>2</sub> and diethyl ether at temperatures of 453–513 K over catalysts.<sup>41</sup> Therefore, the rapid drop of DEC yields from 483 to 493 K is largely ascribed to the decomposition of the DEC to carbon dioxide and diethyl ether at too high temperatures. It should be noted that the maximal DEC yield of 47.1% with a DEC selectivity higher than 90% was achieved at 473 K. Therefore, the optimized reaction temperature for the DEC synthesis in the fixed-bed reactor was 473 K.

The effect of EC solution LHSV on the continuous synthesis of DEC from EC and ethanol over the 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst was displayed in Fig. 7d. Both the EC conversion and the DEC yield decreased with the EC solution LHSV increasing from 1.09 h<sup>-1</sup> to 4.04 h<sup>-1</sup>. A higher EC solution LHSV indicated that a larger amount of EC was used. As the amount of catalyst is constant, the low EC solution LHSV of 1.09 h<sup>-1</sup> was advantageous to obtain high DEC yield.

It should be noted that under the optimized reaction conditions of 473 K, 1.6 MPa, EC solution LHSV of 1.09 h<sup>-1</sup>,  $n(\text{EtOH})/n(\text{EC})$  of 10, 2 g of 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst, EC conversion of 55.5%, a maximum DEC yield of 52.1% and a high DEC selectivity of 93.8% were achieved in the fixed bed reactor, which are superior to most of the reported catalysts.<sup>24–27,30,32,33</sup>

The catalytic stability of the 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst was also tested in the fixed-bed reactor. As presented in Fig. 8, with the reactants continuously pumping into the fixed bed reactor, no obvious changes in EC conversion and DEC yield were observed after 7 h of test over the 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst, also indicative of the outstanding stability of the 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst for DEC synthesis from EC and ethanol.

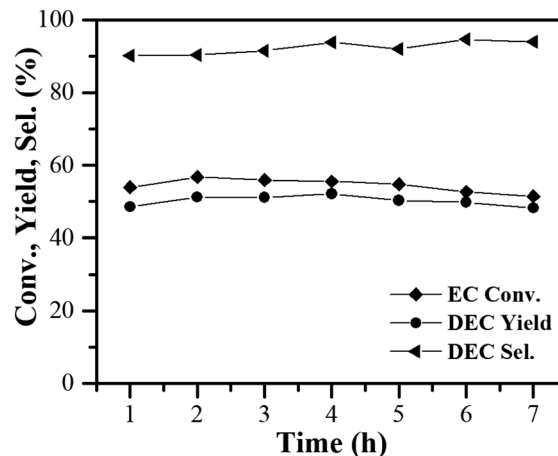


Fig. 8 Continuous synthesis of DEC from EC and ethanol over time using the 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst. Reaction conditions: 473 K, 1.6 MPa, EC solution LHSV of 1.09 h<sup>-1</sup>,  $n(\text{EtOH})/n(\text{EC})$  of 10, 2 g catalyst.

Based on the above results, it could be concluded that the readily-fabricated 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst was a very promising candidate as a highly-efficient, cost-effective and heterogeneous catalyst for green and continuous synthesis of DEC using low-cost and environmental-benign EC and ethanol as raw materials, which is also an efficient way to indirectly utilize CO<sub>2</sub> to synthesize high value-added chemicals.

## 4. Conclusions

In this work, low-cost and effective supported MgO catalysts readily fabricated by an impregnation method were employed for green synthesis of DEC from EC and ethanol. The 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst presented the highest activities in the fixed bed reactor with a maximum DEC yield of 52.1% and a high DEC selectivity of 93.8%, respectively, which are superior to the individual  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> or MgO, and most of the reported catalysts. The outstanding performances of the 10% MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst could be attributed to the co-contribution of the high dispersion of MgO on the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support, the enlarged surface area, and larger amount of stronger basic sites. This work has provided a readily-fabricated and economical catalyst system to efficiently synthesize high value-added DEC indirectly from CO<sub>2</sub>.

## Conflicts of interest

There are no conflicts to declare.

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## Notes and references

- 1 K. Shukla and V. C. Srivastava, *RSC Adv.*, 2016, **6**, 32624–32645.



- 2 K. Shukla and V. C. Srivastava, *Catal. Rev.*, 2017, **59**, 1–43.
- 3 S. Huang, B. Yan, S. Wang and X. Ma, *Chem. Soc. Rev.*, 2015, **44**, 3079–3116.
- 4 I. E. Muskat, F. Strain, *US Pat.*, 2379250, 1941.
- 5 H. Iida, R. Kawaguchi and K. Okumura, *Catal. Commun.*, 2018, **108**, 7–11.
- 6 S.-J. Wang, S.-H. Cheng, P.-H. Chiu and K. Huang, *Ind. Eng. Chem. Res.*, 2014, **53**, 5982–5995.
- 7 C. Murugan and H. C. Bajaj, *Fuel Process. Technol.*, 2011, **92**, 77–82.
- 8 K. Shukla and V. C. Srivastava, *Ind. Eng. Chem. Res.*, 2018, **57**, 12726–12735.
- 9 H. Wang, Y. Xiang, M. Guo, J. Su, G. Wang, W. Cui and Z. Deng, *Energy Fuels*, 2020, **34**, 8697–8706.
- 10 S. Huang, P. Chen, B. Yan, S. Wang, Y. Shen and X. Ma, *Ind. Eng. Chem. Res.*, 2013, **52**, 6349–6356.
- 11 L. Wang, H. Li, S. Xin, P. He, Y. Cao, F. Li and X. Hou, *Appl. Catal., A*, 2014, **471**, 19–27.
- 12 L.-C. Zhao, Z.-Q. Hou, C.-Z. Liu, Y.-Y. Wang and L.-Y. Dai, *Chin. Chem. Lett.*, 2014, **25**, 1395–1398.
- 13 B.-Y. Yu, P.-J. Wu, C.-C. Tsai and S.-T. Lin, *J. CO<sub>2</sub> Util.*, 2020, **41**, 101254.
- 14 O. Arbeláez, E. Hernández, L.-M. González, F. Bustamante and A.-L. Villa, *Chem. Eng. Technol.*, 2019, **42**, 1135–1143.
- 15 M. Buchmann, M. Lucas and M. Rose, *Catal. Sci. Technol.*, 2021, **11**, 1940–1948.
- 16 J. Wang, Z. Hao and S. Wohlrab, *Green Chem.*, 2017, **19**, 3595–3600.
- 17 S. Xin, L. Wang, H. Li, K. Huang and F. Li, *Fuel Process. Technol.*, 2014, **126**, 453–459.
- 18 P. Wang, S. Liu, F. Zhou, B. Yang, A. S. Alshammari and Y. Deng, *RSC Adv.*, 2015, **5**, 19534–19540.
- 19 K. Shukla and V. C. Srivastava, *Fuel Process. Technol.*, 2017, **161**, 116–124.
- 20 J. Zhang, T. Yan, Y. Yang, J. Sun, Y. Lin and M. Wei, *Chin. J. Catal.*, 2019, **40**, 515–522.
- 21 A. Angelini, A. Dibenedetto, D. Curulla-Ferré and M. Aresta, *RSC Adv.*, 2015, **5**, 88401–88408.
- 22 A. Dibenedetto, A. Angelini, M. Aresta, S. Fasciano, M. E. Cucciolito, F. Ruffo, B. M. Aresta, D. Curulla-Ferré and E. De Giglio, *Appl. Catal., A*, 2015, **493**, 1–7.
- 23 T. Yan, W. Bing, M. Xu, Y. Li, Y. Yang, G. Cui, L. Yang and M. Wei, *RSC Adv.*, 2018, **8**, 4695–4702.
- 24 W. Zhao, W. Peng, D. Wang, N. Zhao, J. Li, F. Xiao, W. Wei and Y. Sun, *Catal. Commun.*, 2009, **10**, 655–658.
- 25 L. Guo, X. Zhao, H. An and Y. Wang, *Chin. J. Catal.*, 2012, **33**, 595–600.
- 26 H. An, X. Zhao, L. Guo, C. Jia, B. Yuan and Y. Wang, *Appl. Catal., A*, 2012, **433**, 229–235.
- 27 L. Wang, H. Li, S. Xin and F. Li, *Catal. Commun.*, 2014, **50**, 49–53.
- 28 F. Li, H. Li, L. Wang, P. He and Y. Cao, *Catal. Sci. Technol.*, 2015, **5**, 1021–1034.
- 29 D. Wang, X. Zhang, C. Liu, T. Cheng, W. Wei and Y. Sun, *Appl. Catal., A*, 2015, **505**, 478–486.
- 30 K. Shukla and V. C. Srivastava, *Catal. Lett.*, 2017, **147**, 1891–1902.
- 31 D. Wang, X. Zhang, D. Zhou, S. Liu and W. Wei, *Fuel Process. Technol.*, 2017, **167**, 404–415.
- 32 Y. Ma, H. Wang, L. Wang and H. Li, *J. Environ. Manage.*, 2019, **232**, 952–956.
- 33 W. Zhao, D. Feng, J. Nong, G. Cao, X. Liu, Z. Tang and Y. Chen, *React. Kinet., Mech. Catal.*, 2016, **117**, 639–654.
- 34 D.-e. Jiang, B. Zhao, Y. Xie, G. Pan, G. Ran and E. Min, *Appl. Catal., A*, 2001, **219**, 69–78.
- 35 J. Gangwar, B. K. Gupta, S. K. Tripathi and A. K. Srivastava, *Nanoscale*, 2015, **7**, 13313–13344.
- 36 M. Aazza, H. Ahlafi, H. Moussout, C. Mounir, A. Fadel and A. Addad, *J. Environ. Chem. Eng.*, 2020, **8**, 103707–103718.
- 37 A. Ansari, A. Ali, M. Asif and Shamsuzzaman, *New J. Chem.*, 2018, **42**, 184–197.
- 38 J. P. Dhal, M. Sethi, B. G. Mishra and G. Hota, *Mater. Lett.*, 2015, **141**, 267–271.
- 39 H. Hattori, *Appl. Catal., A*, 2015, **504**, 103–109.
- 40 D. Wang, X. Zhang, W. Wei and Y. Sun, *Chem. Eng. Technol.*, 2012, **35**, 2183–2188.
- 41 M. Selva, M. Fabris and A. Perosa, *Green Chem.*, 2011, **13**, 863–872.