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Carbon dioxide capture and conversion by an acid-base resistant metal-organic framework

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Considering the rapid increase of CO_2 emission, especially from power plants, there is a constant need for materials which can effectively eliminate post-combustion CO_2 (the main component: $CO_2/N_2 = 15/85$). Here, we show the design and synthesis of a Cu(II) metalorganic framework (**FJI-H14**) with a high density of active sites, which displays unusual acid and base stability and high volumetric uptake (171 cm³ cm⁻³) of CO_2 under ambient conditions (298 K, 1 atm), making it a potential adsorbing agent for post-combustion CO_2 . Moreover, CO_2 from simulated post-combustion flue gas can be smoothly converted into corresponding cyclic carbonates by the **FJI-H14** catalyst. Such high CO_2 adsorption capacity and moderate catalytic activity may result from the synergistic effect of multiple active sites.

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ue to the dependence on fossil fuels to meet the world's growing energy demand, the concentration of CO₂ in the atmosphere has increased from 310 p.p.m. to over 380 p.p.m. during the last half century, and it continues to rise ¹⁻³. Some 60% of the total CO₂ emission worldwide is attributable to electricity generation⁴. The installation of effective CO₂ capture systems that can selectively remove the CO₂ component of the exhaust gas emitted by coal- or gas-fired power plants would extremely reduce the global annual emissions. Current technologies involving aqueous amine absorbents for the capture of CO₂ from a gas mixture are usually themselves significant consumers of energy and a source of corrosion problems in equipment⁵⁻⁷. Thus, exploration of new materials that can selectively and efficiently eliminate combustion-generated CO₂ is urgent.

Due to their large capacity for the adsorption of gases and their chemical tunability⁸⁻²¹, the emerging porous metal-organic frameworks (MOFs) could serve as promising cost-effective and efficient materials for CO₂ capture and separation, but development of practically useful MOF materials for CO₂ capture directly from power plants remains a challenge. The flue gas generated from coal-fired power plant, released at a total pressure of approximately 1 atm., contains 15-16% CO₂, 73-77% N₂, 5-7% H_2O , 3-4% O_2 and a small amount of acid gas²²⁻²⁴. An ideal MOF material for CO₂ capture should exhibit extraordinarily high CO2 uptake and selectivity at ambient pressures; furthermore, it should also be resistant to water and acid gas, can be prepared on a large scale and is reusable. Moreover, in terms of practical applications, high volumetric CO₂ adsorption capacity seems even more important than gravimetric CO₂ adsorption capacity, since the capture and separation of post-combustion CO₂ is often carried out in a fixed-bed reactor⁵.

Generally, open metal sites (OMS) and Lewis basic sites (LBS) are favorable for interaction with CO_2 and various types of OMS and LBS have been introduced into MOFs in an effort to improve their adsorption capacity^{25–32}. To adsorb CO_2 effectively under ambient conditions, one would seek to prepare an MOF with high densities of OMS and LBS, in which the OMS and LBS could synergistically capture CO_2 molecules in the pores. Such a potential synergy effect from the OMS and LBS can improve the adsorption capacity more effectively than a single OMS or LBS.

In this paper, we describe the design and synthesis of a Cu(II)-MOF, **FJI-H14** with a high density of OMS and LBS, which shows extraordinary high volumetric uptake of CO₂ at ambient conditions and excellent selectivity for CO₂ over N₂. Remarkably, it is highly stable in a water and acid/base environment and can be reused without loss of adsorption capacity; furthermore, it can be easily synthesized in large quantities. Experiments with simulated post-combustion flue gas have shown that **FJI-H14** can smoothly catalyze the chemical transformation of CO₂ into the corresponding cyclic carbonates.

Results

Synthesis and structure analysis. The reaction of 2,5-di(1*H*-1,2,4-triazol-1-yl)terephthalic acid (H₂BTTA, Fig. 1a) with Cu (NO₃)₂ in H₂O at 120 °C for 3 days affords rod-shaped blue crystals of **FJI-H14** ([Cu(BTTA)H₂O]_n·6nH₂O) in 73% yield. Single-crystal X-ray structure analysis shows that **FJI-H14** crystallizes in trigonal space group *R*-3 (for more details see Supplementary Table 1). The crystallographic asymmetric unit contains one BTTA^{2−}ligand, one Cu(II) ion and one coordinate water. As shown in Fig. 1b, each Cu(II) ion has a square-pyramidal coordination geometry, and is surrounded by two imine N atoms from two different 1,2,4-triazole groups and two O atoms from two different carboxylate groups in the equatorial plane, together with one O atom of the water molecule in the

vertex (Supplementary Fig. 1). Topologically, the Cu(II) ion is a planar 4-connected node, further linked by four tetradentate BTTA²⁻ ligands into a three-dimensional network with Kagomelike **USF** topology (Fig. 1d). Consequently, there are hexagonal one-dimensional channels along the c direction (Fig. 1c). The pore limiting diameter and the maximum pore diameter predicted by the program Poreblazer³³ for the fully evacuated **FJI-H14** are 5.95 and 7.62 Å, respectively. The evacuated **FJI-H14** has a theoretical porosity of 44.4% according to PLATON calculations with a probe radius of 1.65 Å. **FJI-H14** has a total concentration of active sites as high as 9.22 mol l⁻¹ (the total of Cu (II) OMS is 3.07 mol l⁻¹ and free N LBS is 6.15 mol l⁻¹), which is higher than in many well-known MOFs for CO₂ capture (Supplementary Table 2).

Stability. The flue gas from power plants contains moisture and acid gas, suggesting that the practical adsorbents of postcombustion CO₂ should be sufficiently stable toward heat, water and acid. This led us to investigate both the chemical stability and thermal stability of FJI-H14 before the CO₂ adsorption test. Powder X-ray diffraction pattern (PXRD) analyses reveal that FJI-H14 is very stable not only in boiling water but also in both acid and base environments at pH = 2 to pH = 12 and at temperatures as high as 373 K (Fig. 2a). However, the framework of FII-H14 collapses when it is immersed for 24 h in solution at pH = 1 or pH = 13 (Supplementary Fig. 2). Thermogravimetric analysis (TGA) studies (Supplementary Fig. 3) indicate that the as-synthesized FJI-H14 sample is thermally stable up to 230 °C, and this is confirmed by temperature-dependent PXRD studies (Fig. 2b and Supplementary Fig. 4). Generally, MOFs based on Cu ions and organic carboxylates are usually subject to hydrolysis in the presence of moisture and only a few known MOFs show such excellent chemical stability 16, 34-38. The unusual chemical stability of FJI-H14 may result from its unique structure because the penta-coordinated Cu(II) ion subunit should be more stable than

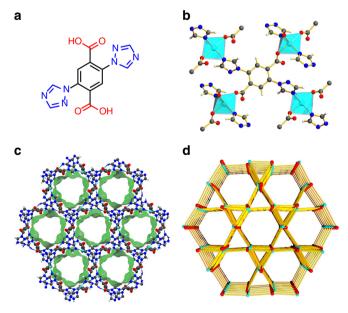


Fig. 1 Structural illustration of FJI-H14. **a** The selected ligand H_2BTTA for the construction of **FJI-H14. b** The coordination environment of the Cu(II) ions as four-connected nodes and BTTA also as a four-connected node. **c** The one-dimensional nanoporous channels along the crystallographic *c* direction. **d** The framework of **USF** topology. (Cu atom, cyan; C atom, gray; O atom, red; N atom, blue; H atom, white)

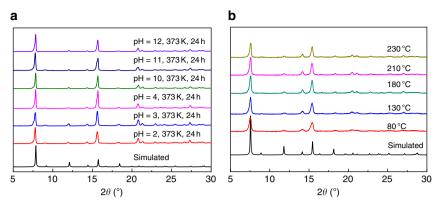


Fig. 2 Stability of FJI-H14. a PXRD patterns after treatment with boiling water, acid/base environment from pH = 2 to 12 at 373 K. b Temperature-dependent PXRD patterns

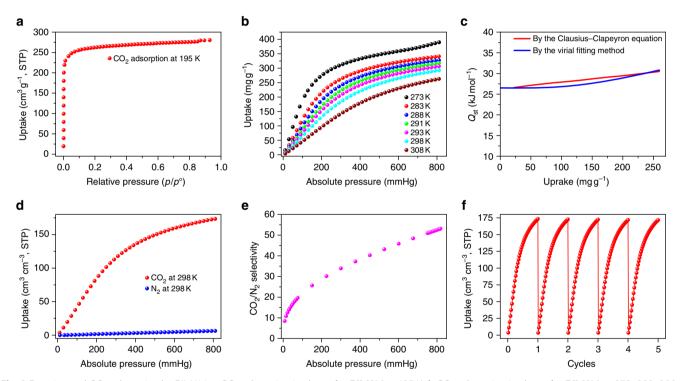


Fig. 3 Experimental CO_2 adsorption by FJI-H14. **a** CO_2 adsorption isotherm for **FJI-H14** at 195 K. **b** CO_2 adsorption isotherm for **FJI-H14** at 273, 283, 288, 291, 293, 298 and 308 K. **c** The isosteric heat of CO_2 adsorption (Q_{st}) for **FJI-H14** calculated by the Clausius-Clapeyron equation and the Virial fitting method. **d** N_2 and CO_2 adsorption isotherms for **FJI-H14** at 298 K. **e** CO_2/N_2 selectivity for the 15/85 CO_2/N_2 mixture at 298 K. **f** Cycles of CO_2 adsorption for **FJI-H14** at 298 K

traditional paddle-wheel structure due to the Cu–N coordination interaction, which is stronger than the Cu–O interaction. Furthermore, the abundant free N atoms could also prevent the destruction caused by acids.

Porosity and CO₂ adsorption capacity. The **FJI-H14** sample for adsorption testing was pre-activated under dynamic vacuum at 100 °C for 10 h after exchanged by acetone for 3 days. PXRD data displayed that the crystallinity was retained after activation (Supplementary Fig. 5). N₂ adsorption at 77 K was much lower than expected (Supplementary Fig. 6), and consequently, the porosity of activated **FJI-H14** was examined by CO₂ adsorption experiments at 195 K. A CO₂ uptake of 279 cm³ g⁻¹ was obtained (Fig. 3a), corresponding to a formula [Cu(BTTA)]_n·4.5nCO₂. A

phenomenon that restricted N_2 uptake at 77 K but supported type-I CO_2 uptake at 195 K has been observed in several reported MOF materials (Supplementary Table 3). However, **FJI-H14** has a low N_2 uptake of 170 cm₃ g⁻¹ at 77 K and 1 atm, which is different from the reported MOFs which exhibit almost zero N_2 adsorption at 77 K. The much lower N_2 adsorption at 77 K of **FJI-H14** may be a consequence of the relatively narrow pores in **FJI-H14** being easily blocked by the relatively large N_2 molecule at 77 K, so hindering further diffusion of N_2 into the framework of **FJI-H14**. The typical type-I isotherm observed indicates that only micropores are formed in the framework of activated **FJI-H14**. The Brunauer–Emmett–Teller (BET) -specific surface area of **FJI-H14** is calculated to be 904 m² g⁻¹ and its Langmuir-specific surface area is $1004 \text{ m}^2 \text{ g}^{-1}$. The total pore volume estimated from the experimental CO_2 isotherm is $0.45 \text{ cm}^3 \text{ g}^{-1}$ at $P/P_0 = 0.92$,

which is slightly higher than the theoretical value of $0.39 \text{ cm}^3 \text{ g}^{-1}$ derived from the solvent accessible volume and the crystal density through PLATON calculations with a probe radius of 1.65 Å. The comparable values of the pore volume indicate that the activated **FJI-H14** remains permanently porous.

The incorporation of high porosity and the high concentration of open active sites in the framework are expected to lead to high CO₂ uptake. Indeed, activated FII-H14 exhibits remarkable CO₂ volumetric adsorption capacities of 171 cm³ cm⁻³ at 298 K and 1 atm (Fig. 3d), and the capacity is only lower than that of MAF-X25ox (203 cm³ cm⁻³)³⁶, MAF-X27ox (196 cm³ cm⁻³)³⁶ and Co₂(dobdc) (184 cm³ cm⁻³) under the same conditions³⁶, ³⁹, exceeding that in almost all well-known MOFs such as Mg-MOF-74 (162 cm³ cm⁻³)^{6, 40}, UTSA-16 (160 cm³ cm⁻³)^{6, 41}, SIFSIX-2-Cu-i $(151 \text{ cm}^3 \text{ cm}^{-3})^{42}$, MPM-1-TIFSIX $(115.7 \text{ cm}^3 \text{ cm}^{-3})^{43}$, Bio-MOF-11(113 cm³ cm⁻³)⁶, ⁴⁴, Cu-tdpat(103 cm³ cm⁻³)⁶, ⁴⁵ and Mmen–CuBTTri (83 cm⁻³)⁶, ³⁰ (Supplementary Table 2). The formula of CO₂ adsorbed FJI-H14 at room temperature is [Cu(BTTA)]_n·2.4nCO₂ and there is a 53% CO₂ occupancy at room temperature compared with the maximal uptake at 195 K, which is rather high compared with reported MOFs such as SMT- $1 (27\%)^{46}$, [Cu(L)] $(31\%)^{47}$ and MPM-1-Cl $(29\%)^{43}$. It should be noted that although volumetric adsorption capacity is more practical for stationary CO₂ capture and separation applications, the gravimetric adsorption capacity is also an important parameter for CO₂ capture. Although the gravimetric CO₂ uptake of FJI-H14 (146 cm³ g⁻¹) is lower than that of Mg-MOF-74 (176 cm³ g⁻¹) due to the considerably lighter weight of Mg⁴⁰, it can be comparable to that in other familiar MOF materials such as MAF-X25ox $(160 \text{ cm}^3 \text{ g}^{-1})^{36}$, $[\text{Co}_2(\text{dobdc})]$ $(154 \text{ cm}^3 \text{ g}^{-1})^{39}$ or MAF-X27ox $(150 \text{ cm}^3 \text{ g}^{-1})^{36}$. Another challenging issue is the uptake of CO₂ at low pressure, which can be highly improved by chemisorption due to the stronger interactions. For instance, the hydrazine functionalized MOF $[Mg_2(dobdc)(N_2H_4)_{1.8}]$ (137 cm³ cm⁻³) developed by Zhang et al. shows the highest volumetric CO2 adsorption capacities at

298 K and 0.15 bar³¹, and the second highest is MAF-X27ox (124 cm³ cm⁻³)³⁶, which was also prepared by Zhang et al. Based on physisorption, FJI-H14 displays a volumetric capacity of 60 cm³ cm⁻³ at 298 K and 0.15 atm, which makes it comparable to SIFSIX-2-Cu-i (63 cm³ cm⁻³). In order to evaluate the affinity of the pore surface of activated FII-H14 toward CO₂, the isosteric heat of adsorption (Q_{st}) of activated FJI-H14 was calculated using the Clausius-Clapevron equation based on the CO₂ isotherms at seven different temperatures without data fitting (Fig. 3b, Supplementary Fig. 7 and Supplementary Table 4). As shown in Fig. 3c, the Q_{st} at low coverage is 26.6 kJ mol⁻¹ and then slightly increases to 30.5 kJ mol⁻¹ with CO_2 loading increasing to 260 mg g⁻¹. The $Q_{\rm st}$ with an increasing slope is unusual^{9, 36, 43, 48}, and reveals the possible formation of CO₂ clusters inside the pores. Such phenomena have been previously observed in other porous MOFs materials^{41, 49}. The $Q_{\rm st}$, confirmed by the Virial fitting method⁵⁰, also slowly increases from 26.5 to 30.8 kJ mol⁻¹ with increasing CO₂ loading from lower coverage to 260 mg g⁻¹ (Fig. 3c and Supplementary Fig. 8). Such similar trends in the two methods confirm the unusual increasing slope in $Q_{\rm st}$.

Because flue gas from power plants contains a large amount of N_2 , the CO_2/N_2 selectivity is a crucial parameter in CO_2 capture applications. For comparison, N_2 sorption isotherms were also measured at 298 K, and showed an uptake of 6.5 cm³ cm⁻³ at 1 atm (Fig. 3d). By the ideal adsorbed solution theory (IAST)⁵¹, the CO_2/N_2 selectivity for the 15/85 CO_2/N_2 mixture at 1 atm is calculated to be 51 at 298 K (Fig. 3e). The highly selective adsorption of CO_2 over N_2 further suggests that the densely populated open active sites in the framework have a positive effect on CO_2 adsorption. The possibility of reuse of an adsorbent is also an important aspect of the practical application. Further research demonstrates that activated **FJI-H14** can be recycled without losing its adsorption capacity. Even after five cycles, it still maintains 100% adsorption capacity as shown in Fig. 3f, indicating that **FJI-H14** is highly suitable for CO_2 capture.

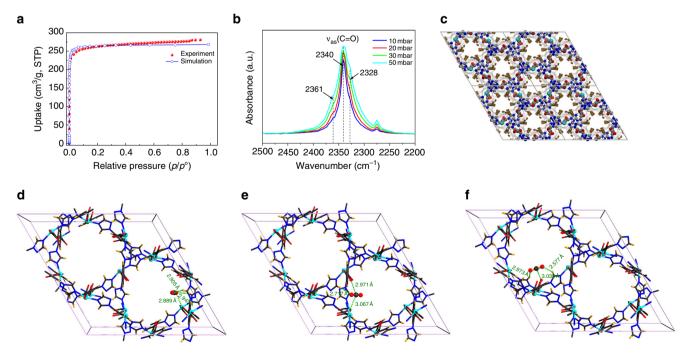


Fig. 4 Mechanism of CO₂ adsorption of FJI-H14. **a** Experimental and simulated excess CO₂ adsorption isotherms at 195 K. **b** Background-subtracted FTIR spectra of CO₂ adsorbed on **FJI-H14** at decreasing equilibrium pressure. **c** Density picture of adsorbed CO₂ (1 CO₂ at 273 K), which is shown as a volume rendered mode. **d-f** represent three preferential CO₂ locations in **FJI-14** obtained from GCMC simulation and DFT optimization

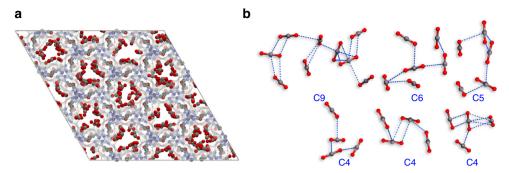


Fig. 5 The snapshot for CO_2 -loaded FJI-H14. **a** The snapshot of CO_2 adsorption for **FJI-H14** at 11.2 kPa and 273.15 K calculated using the GCMC method. **b** The representative CO_2 clusters including nine (C9), six (C6), five (C5) and four (C4) CO_2 molecules. The blue dashed line represents weak interactions between neighboring CO_2 molecules with a short $C\cdots O$ separation (from 2.71 to 3.50 Å) for adjacent CO_2 molecules

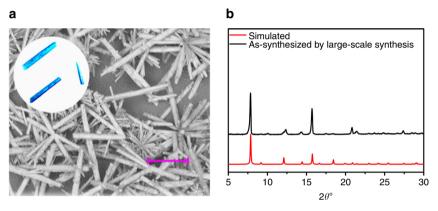


Fig. 6 Large-scale synthesis of FJI-H14 microcrystals. **a** Morphology comparison between SEM image of **FJI-H14** microcrystals and of **FJI-H14** single crystals (inset). Scale bars, 10 μm. **b** PXRD patterns comparison: black represents simulated **FJI-H14**; red represents **FJI-H14** microcrystals

Revealing the CO₂ adsorption sites in FJI-H14. The extraordinary CO₂ capture performance of FJI-H14 under ambient conditions has motivated us to rationalize the crucial factors supporting the high CO₂ adsorption capacity. To understand the sorption behavior of FJI-H14, both grand canonical Monte Carlo (GCMC) simulations and density functional theory (DFT) calculations have been carried out and are shown in Fig. 4. The GCMC simulations show that the theoretical CO₂ adsorption isotherms of FJI-H14 are basically consistent with the experimental data at different temperatures (195, 273 and 298 K) (Fig. 4a, Supplementary Fig. 9). The simulated CO₂ concentration loaded into FJI-H14 is about 4.3, 3.1 and 2.5 CO2 per ligand molecule at 195, 273 and 298 K, respectively. These figures are close to the experimental values of 4.5, 3.1 and 2.4 CO₂ per ligand molecule at 195, 273 and 298 K. As shown in Fig. 4c, the adsorbed CO₂ molecules at low coverage prefer to locate the corners of hexagonal channels. Combining the density plots and a snapshot of the adsorbed CO2 molecules, three typical preferential CO2 adsorption sites can be observed. These three adsorption sites were further optimized by DFT methods using the Dmol³ module. Site I (Fig. 4d) shows that CO₂ molecules prefer to coordinate with open Cu(II) ions through Cu-O interaction, with a Cu-O distance of about 2.889 Å, and each copper site binding only one CO₂⁵². In Site II (Fig. 4e), the two closest C–O distances are about 2.971 and 3.067 Å, indicating that O atoms of carboxyl group could also interact as a Lewis base with CO2. It is also interesting to find that positively charged H atoms could further promote CO₂ adsorption, with the shortest O-H distances about 2.577 Å as shown in Site III (Fig. 4f). The calculated static CO₂ binding energy of the above three different preferential CO_2 adsorption sites are ~43.71, 38.94, 32.82 kJ mol^{-1} , respectively, indicating that the open copper sites could play a leading role in CO_2 adsorption.

The simulated Q_{st} from the GCMC simulations can be used to deduce the information on Q_{st} with an increasing slope for FJI-H14. As shown in Supplementary Fig. 10, the simulated Q_{st} of 30.7-34.6 kJ mol⁻¹ is slightly larger than suggested by experimental results and has a uniformly increasing trend with increasing CO2 loading. The contribution of the CO2···Framework interaction to the total Q_{st} decreases slightly with increasing loading, which is reasonable because CO2 molecules first occupied the more active sites. However, the contribution from the CO₂···CO₂ interactions shows a tendency to increase significantly from 0 to 7.0 kJ mol⁻¹, which is due to the closer packing of the CO2 molecules under the higher pressure in the relatively narrow pores. Hence, the behavior of the total Q_{st} is the result of the two cooperative contributions. The increasing contribution from the CO2···CO2 interactions indicates that the CO₂ clusters could have formed inside the pores. Hence, GCMC simulation was used to investigate the potential CO2 clusters. Some small CO₂ clusters can be found in the snapshot at 195 K and low pressure (~21 Pa) calculated using the GCMC method (Supplementary Fig. 11), but at 273 K, similar CO₂ clusters can only be observed under a relatively high pressure of 11 kPa. The snapshots of the framework of FJI-H14 with CO2 molecules adsorbed are shown in Fig. 5a. The weak interactions between neighboring CO2 molecules are found in terms of the short C···O separation (from 2.71 to 3.50 Å) for adjacent CO₂ molecules,

Table 1 Cyclic carbonates from epoxides and CO2a

| | $ \stackrel{\text{O}}{\longrightarrow} \frac{N_2/2}{N_2} $ | CO ₂ (0.85 atm/0.15 | | 040 |
|-------|--|---|---------|-----------------------|
| Entry | Substrates | Catalysts | t[h] | Yield(%) ^b |
| 1 | O | FJI-H14 | 24 | 86 |
| 2 | O | _ | 24 | 52 |
| 3 | O | Cu(OAc) ₂ | 24 | 45° |
| 4 | | Cu(NO ₃) ₂ + H ₂ BTTA | 24 | 70 |
| 5 | | HKUST-1 | 24 | 67 |
| 6 | $CI \searrow 0$ | FJI-H14 | 24 | 95 |
| 7 | \\\\ 0 | FJI-H14 | 24 | 27 |

aReaction conditions: styrene oxide (20.0 mmol), catalyst (0.48 mol% per Cu(II) units), TBAB (2.5 mol%) in a Schleck tube with condenser, 1 atm simulated post-combustion flue (CO₂ = 0.15 atm, N₂ = 0.85 atm) was bubbled at 80 °C for 24 h Potentials by 10 MAR.

^bDetermined by ¹H NMR.

^cSome by-products were found when Cu(OAc)₂ was used as a catalyst

which links those CO₂ molecules into small clusters (Fig. 5b and Supplementary Fig. 12).

To verify the preferential adsorption sites experimentally, in situ fourier transform infrared microscope (FT-IR) spectra of activated **FJI-H14** sample have been collected at increasing equilibrium pressure under a CO₂ atmosphere. Figure 4b shows the background-subtracted IR spectra obtained by the progressive lowering of equilibrium pressure at room temperature. The strong absorption bands at 2,340 and 2,328 cm $^{-1}$ red-shifted by $\Delta\nu$ of about -9 and -21 cm $^{-1}$ from gas phase CO₂ asymmetric stretch $(\nu_{as}=2349~{\rm cm}^{-1})$ might be attributed to the ν_{as} mode of

 $\rm CO_2$ (Supplementary Fig. 13) interacting with Cu(II) centers. The slightly blue-shifted band at 2,361 cm $^{-1}$ ($\Delta\nu=+12$ cm $^{-1}$ shift) can be readily assigned to the asymmetric ν_{as} stretch of $\rm CO_2$ interacting with the exposed Lewis base sites throughout the channel. On the low-frequency side of this main absorption, the less intense bands at 2,275 cm $^{-1}$ result from the interaction between Cu(II) center and $^{13}\rm CO_2$ which is present (1%) naturally in $^{12}\rm CO_2$. The stronger absorption bands at 2,340 cm $^{-1}$ and 2,328 cm $^{-1}$ also indicate that $\rm CO_2$ molecules tend to stack around the open Cu(II) sites, which is in accord with the above theoretical calculation.

Large-scale synthesis. For practical applications, efficient macroscopic preparation and purification are a bottleneck problem which must be solved. After many attempts, the following protocol for large-scale preparation of FJI-H14 has been established: by directly mixing H_2BTTA ligand and $Cu(NO_3)_2$ in water and then refluxing for 1 day, microcrystalline FJI-H14 can be obtained with a high yield of 90%, its purity confirmed by PXRD analysis (Fig. 6b). Scanning electron microscopy measurements demonstrate that the relatively uniform rod crystallites form on the scale of about $20~\mu m$, displaying a similar morphology with the single crystal (Fig. 6a) obtained from the hydrothermal reaction. Therefore, macroscopic samples of FJI-H14 even on a 10~g scale can be readily synthesized by this method, which makes its application more possible.

Catalyzed cycloaddition of CO₂ using flue gas as feedstock. Another attractive means of effective elimination of CO2 is the direct chemical conversion of CO2 into value-added chemicals, such as dimethyl carbonate, cyclic carbonates, N,N'-disubstituted ureas or formic acid. Given their wide applications in the pharmaceutical and fine chemical industries, cyclic carbonates formed by the coupling of epoxides with CO₂ have attracted intense interest. Although several existing MOFs have been shown to be excellent heterogeneous Lewis acid catalysts for chemical conversion of CO₂ either at high pressure or normal pressure^{53–56}, the exploration of practically useful MOF materials which can catalyze the conversion of CO₂ obtained directly from power plants remains a challenge to be addressed. The high density of OMSs and LBSs which are finely distributed throughout the channel pores of FJI-H14, are devoted to capturing CO2 effectively and selectively under ambient conditions. Such unusual synergistic effects may also improve chemical conversion of postcombustion CO₂ from the power plant. Here, we use a mixed gas which contains 0.15 atm CO₂ and 0.85 atm N₂ to simulate flue gas from the power plant. As expected, FJI-H14 displays a much higher catalytic activity for cycloaddition of styrene oxide with the simulated flue gas than other catalysts, such as homogeneous Cu(OAc)₂, heterogeneous HKUST-1 and a mixture of Cu(NO₃)₂ and free H₂BTTA ligand. As shown in Table 1, absence of extra Lewis acid catalysts only lead to a moderate yield (52%), while use of extra Cu(II) catalyst can improve their reaction activity, with the exception of Cu(OAc)₂. Catalyzed by FJI-H14, chemical conversion of diluted CO₂ with styrene oxide into corresponding cyclic carbonates gives a yield of 86% within 24 h, while use of homogeneous Cu(OAc)2 and the mixture of Cu(NO3)2 and H₂BTTA leads only to 45 and 70% yields respectively under the same reaction conditions. Further tests demonstrate that the FJI-H14 is more active than well-known HKUST-1 which leads to only 67% yield under the same conditions. All these results indicate that FJI-H14 is indeed an efficient catalyst for chemical conversion of CO₂ under practical conditions. In order to investigate the catalytic character of FJIH-14, another two different sized substrates have been selected. As shown in Table 1 entries 5-6, the smaller (chloromethyl)ethylene oxide gives a higher yield (95%), while 1,2-epoxyoctane leads to a lower yield (27%), indicating that the cycloaddition reaction may occur within the pores of FIJ-H14, into which smaller-sized substrates could easily diffuse and make contact with the active sites. To further prove that the reaction may occur in the pores of FJI-H14, uptake of different reactants has also been assessed. Further analysis demonstrates that (chloromethyl)ethylene oxide indeed diffuses into the pores of FJI-H14 more easily than 1,2-epoxyoctane and styrene oxide which apparently have similar diffusion rates. Considering the similar diffusion from 1,2epoxyoctane and styrene oxide, the higher activity of styrene oxide compared to 1,2-epoxyoctane may result from following two factors: first, a phenyl ring is an electron-withdrawing group, which can improve reaction activity, and second, the π - π interaction from the phenyl ring of styrene oxide and the aromatic rings of the **FJI-H14** framework also can improve reaction activity. This may provide a strategy for development of more practical catalysts for the conversion of CO_2 directly from flue gas.

Discussion

Considering that most of CO₂ emission is generated from power stations, direct elimination of such CO₂ should play an important role in the reduction of global CO₂ emissions. The characteristics and composition of post-combustion CO₂ determine that an ideal adsorbent for post-combustion CO2 capture should possess advantages such as high CO2 uptake and selectivity at ambient pressure, excellent chemical stability and thermal stability, good reusability and large-scale production with low cost. Porous MOFs have been proved to be effective adsorbents for CO₂ capture due to their large capacity for the adsorption of gases, but development of an ideal MOF for post-combustion CO₂ capture is still challenging. Although many different OMS and LBS have been introduced into MOFs to improve CO₂ capture, only very few porous MOFs have been realized for high CO2 capture at ambient conditions, and most of them are sensitive to water. FJI-H14 not only shows extraordinary high volumetric uptake of CO₂ with high selectivity under ambient conditions but is also highly resistant to water and an acid/base environment; furthermore, it also can be reused without loss of adsorption capacity and prepared on a large-scale with low cost. These advantages make FJI-H14 an ideal and practical adsorbent for postcombustion CO₂. An unusual synergistic effect from multiple active sites has also been observed, and may provide a strategy for the design of more effective adsorbents for CO2 capture. Further chemical conversion of captured CO₂ to high-value products, such as cyclic carbonate, is also attractive, and several existing MOFs have been proved to be excellent heterogeneous Lewis acid catalysts for chemical conversion of pure CO2. However, development of MOF materials which can catalyze the direct conversion of post-combustion CO2 still remains a challenge. It is shown here that FJI-H14 can directly and smoothly catalyze the chemical transformation of simulated post-combustion gas CO2 into corresponding cyclic carbonates. All these results should be instructive for the design and discovery of more effective and practical MOF materials for the elimination of post-combustion CO₂ in the near future.

Methods

Synthesis and scale up. A mixture of $Cu(NO_3)_2\cdot 3H_2O$ (0.05 mmol, 12 mg) and H_2BTTA (0.05 mmol, 15 mg) in H_2O (4 ml) was sealed in a 23 mL Teflon vial, which was heated at 120 °C for 3 days, then cooled to room temperature. After washing with fresh acetone, blue crystals of **FJI-H14** were obtained in 73% yield based on the organic ligand H_2BTTA . Elemental analysis was calculated for **FJI-H14**: C, 29.54%; H, 4.13%; N, 17.23%. Found: C, 29.35%; H, 4.12%; N, 17.29%. For scale up, a mixture of $Cu(NO_3)_2\cdot 3H_2O$ (1 mmol, 241.6 mg) and H_2BTTA (1 mmol, 300.1 mg) in H_2O (80 ml) was refluxed for 1 day, and then the blue powder of **FJI-H14** microcrystals could be obtained in 90% yield based on H_2BTTA . After three washings with water and two with acetone, the phase purity of the sample was confirmed by PXRD.

Characterization. Elemental analyses for C, H, N were carried out on a German Elementary Vario EL III instrument. The 1H NMR spectra were measured on an AVANCE III Bruker Biospin spectrometer, operating at 400 MHz. Thermogravimetric analyses (TGA) were recorded on an NETZSCH STA 449 C unit at a heating rate of 10 °C min $^{-1}$ under flowing nitrogen atmosphere. In situ FT-IR spectra were obtained using a NICOLET 6700 instrument at 298 K. The PXRD patterns were collected using a Rigaku MiniFlex 600 X-ray diffractometer with monochromatic Cu Kα radiation (λ = 1.54 Å). Simulations of the PXRD spectrum were carried out by the single-crystal data and diffraction-crystal module of the

Mercury program, available free of charge via the internet at https://www.ccdc.cam.ac.uk/solutions/csd-system/components/mercury/.

Single-crystal X-ray diffraction. The single-crystal data of FJI-H14 was collected on a SuperNova diffractometer at 100 K. The structure was solved using SHELXT-2014 and refined by full-matrix least squares on F^2 with SHELXL-2014⁵⁷. All the non-hydrogen atoms were refined anisotropically. Hydrogen atoms of the organic ligands were generated theoretically onto the specific atoms and refined isotropically. We employed $PLATON/SQUEEZE^{58}$ to calculate the contribution to the diffraction from the solvent region and thereby produced a set of solvent-free diffraction intensities. The final formula was calculated from the SQUEEZE results combined with elemental analysis data and TGA data. Crystallographic data and structure refinement parameters for this crystal are summarized in Supplementary Table 1.

Gas-adsorption. Low-pressure (<1 bar) adsorption measurements were performed using an Accelerated Surface Area and Porosimetry 2020-M System. Before the measurements, about 100 mg solvent-exchanged samples were loaded into the sample tube and then degassed under dynamic vacuum at 100 °C for 10 h to obtain fully desolvated samples. Low-pressure N2 adsorption isotherms were measured at 77 K in a liquid nitrogen bath (Supplementary Fig. 6). Low-pressure CO2 adsorption isotherms were measured at 195, 273, 283, 288, 291, 293, 298 and 308 K. The specific surface areas were determined using the BET model from the CO2 adsorption isotherm.

The isosteric heat of adsorption. Method 1: the isosteric heat of adsorption $Q_{\rm st}$ was calculated using the Clausius–Clapeyron equation (equation (1)).

$$\ln(P_i) = Q_{st} \times \frac{1}{RT_i} + C, \tag{1}$$

where P_i is the pressure of the isotherm i (kPa), T_i is the temperature of isotherm i (K), R is the gas constant and C is a constant. The Qst is subsequently obtained from the slope of plots of $\ln(P_i)$ as a function of 1/T (Supplementary Fig. 7 and Supplementary Table 4).

Method 2: the Qst was estimated from isotherms at different temperatures applying the Virial fitting method (equation (2) and Supplementary Fig. 8). The fitting parameters were then used to calculate the $Q_{\rm st}$ using equation (3).

$$\ln P = \ln N + \frac{1}{T} \sum_{i=0}^{m} a_i N^i + \sum_{i=0}^{n} b_i N^i, \tag{2}$$

$$Q_{\rm st} = -R \sum_{i=0}^{m} a_i N^i, \tag{3}$$

where P is the pressure (mmHg), N is the adsorbed quantity (mg g⁻¹), T is the temperature (K), R is the gas constant, a_i and b_i are virial coefficients and m and n represent the number of coefficients required to adequately describe the isotherms (herein, m = 5, n = 2).

Calculation of gas selectivity based on IAST. The gas adsorption isotherms were first fitted to a Langmuir-Freundlich model. IAST starts from the Raoults' Law type of relationship between fluid and adsorbed phase.

$$P_i = P y_i = P_i^o x_i, \tag{4}$$

$$\sum_{i=1}^{n} x_i = \sum_{i=1}^{n} \frac{P_i}{P_i^0} = 1, \tag{5}$$

where P_i is the partial pressure of component i (kPa), P is the total pressure (kPa), y_i and x_i represent mole fractions of component i in gas and adsorbed phase (dimensionless). P_i^0 is the equilibrium vapor pressure (kPa).

In IAST, P_i^0 is defined by relating to spreading pressure π ,

$$\frac{\pi S}{RT} = \int_{-}^{p_i^0} \frac{q_i(P_i)}{P_i} dP_i = \Pi \text{ (Constant)}, \tag{6}$$

where π is the spreading pressure, S is the specific surface area of adsorbent (m² g⁻¹), R is the gas constant, T is the temperature (K) and $q_i(P_i)$ is the single component equilibrium obtained from the isotherm (mg g⁻¹).

The isotherm parameters are known from the previous fitting. The adsorption selectivities S_{ads} were calculated using equation (7).

$$S_{ads} = \frac{q_1/q_2}{p_1/p_2}. (7)$$

In this study, IAST calculations were carried out assuming CO_2/N_2 (15/85) binary mixed gases at 298 K and pressure up to 1 bar to mimic the composition and condition of flue gas for post-combustion CO_2 capture.

Computational methodologies. The GCMC simulations for CO₂ at 195, 273 and 298 K and up to 100 kPa were performed using with *RASPA* v2.03⁵⁹. The **FJI-H14s** framework was generated in the *R*3 space group based on the crystallographic data of **FJI-H14s** (2 × 2 × 3) were used to construct the simulation box of the GCMC run. The structural parameters of simulation box are a = b = 44.9714 Å and c = 33.1527 Å, as well as $\alpha = \beta = 90^{\circ}$ and $\gamma = 120^{\circ}$. The partial charges on the framework atoms were calculated by the Gaussian09 software at the B3LYP/6-31 G* level of theory⁶⁰. Partial atomic charges were extracted using the ChelpG method by fitting them to reproduce the electrostatic potential generated by the DFT calculations. The charge was adjusted slightly in order to result in a neutral framework. Resulting partial charges for **FJI-H14s** are given in Supplementary Table 5

CO2-CO2 and CO2-framework interactions were calculated using a Lennard-Jones (LJ) + Coulomb potential. LJ parameters for the framework atoms were taken from the Dreiding Force Field except for the copper atom, for which the parameters were taken from UFF (Supplementary Table 7). The CO₂ LJ parameters were taken from an empirical TraPPE force field with a partial charge on each atom (Supplementary Table 6). The mixing LJ parameters between different atomic types were calculated according to the Lorentz-Berthelot mixing rule. Lorentz-Berthelot mixing rules were used for all cross terms, and LJ interactions beyond 12.8 Å were neglected. The Ewald sum method was used to compute the electrostatic interactions. The fugacity of CO₂ was calculated using the Peng-Robinson equation of state with the corresponding parameters. Simulations for CO2 adsorption used 100,000 cycles for equilibration and 100,000 cycles for data collection. In a cycle, N Monte Carlo moves were performed, where N is whichever value is larger between 20 and the number of molecules in the system. Monte Carlo moves used with equal probability were translation, rotation, insertion, deletion, and random reinsertion of an existing molecule at a new position, while framework atoms remained fixed at their original positions.

The simulated isosteric heats of adsorption are computed from the GCMC simulations using the expression (equation (8)).

$$Q_{st} = RT - \frac{\langle U_{\rm gg}N\rangle - \langle U_{\rm gg}\rangle\langle N\rangle}{\langle N^2\rangle - \langle N\rangle^2} - \frac{\langle U_{\rm gf}N\rangle - \langle U_{\rm gf}\rangle\langle N\rangle}{\langle N^2\rangle - \langle N\rangle^2}, \tag{8}$$

where the brackets $\langle \ \rangle$ denote the ensemble average, R is the gas constant, N is the number of gas molecules in the system, $U_{\rm gg}$ is gas--gas interaction energy and $U_{\rm gh}$ is the gas---framework interaction energy. The second and third terms are the contributions to the simulated $Q_{\rm st}$ from the gas---gas interaction and the gas---framework interaction, respectively.

DFT methods help shed light on adsorption mechanisms by calculating the adsorption energy of CO₂ in MOF. Three possible main adsorption sites for adsorbed CO₂ in MOF were investigated by the Dmol³ module integrated into the Material Studio 7.0 program package⁶¹. The PBE-type exchange-correlation functional⁶² with a generalized gradient approximation and the Double Numerical plus polarization (DNP) basis sets⁶³ that include a d-type polarization function on all non-hydrogen atoms and a p-type polarization function on all hydrogen atoms were employed for all calculations⁶⁴. The FINE quality mesh size was employed in the calculations. During the CO₂-MOF structure optimization, the lattice parameters and the atomic fraction positions of the MOF crystal were kept immobile and the single CO₂ molecule was allowed to move during optimization. The possible adsorption sites are shown in the Fig. 4d–f. The adsorption energies were calculated in terms of equation (9)

$$E_{\text{ads}} = E_{\text{MOF-CO}_2} - E_{\text{MOF}} - E_{\text{CO}_2}, \tag{9}$$

where $E_{\rm MOF-CO_2}$ stands for the energy of the optimized adsorbate-MOF structure, and $E_{\rm MOF}$, and $E_{\rm CO_2}$ denote the energies of the bare MOF structure and the isolated CO₂ molecule, respectively. According to this equation, a more negative adsorption energy means more favorable binding.

Catalyzation of cycloaddition of simulated post-combustion CO₂. 20 mmol styrene oxide, 0.48 mol% per Cu(II) units (for example, 18 mg activated FJI-H14 (0.016 mmol), 8.7 mg Cu(OAc)₂ (0.048 mmol)), and 164 mg TBAB (0.5 mmol, 2.5 mol%) were placed in a 5 mL dry Schleck tube with condenser, then 1 atm simulated post-combustion flue gas (CO₂ = 0.15 atm, N₂ = 0.85 atm) was introduced by bubbling, and the reaction mixture was stirred at 80 °C for 24 h.

Uptake of different reactants. 10 mg of activated crystals of **FJI-H14** was placed in a dry 5 ml Schleck flask, the flask was then evacuated under dynamic vacuum at 80 °C for 2 h and filled with argon, then 1 ml reactant was injected and the reaction was kept under argon atmosphere. 10 min later, the inclusion crystals of **FJI-H14** were filtered, after removing surface reactant molecules; the inclusion reactants can be readily removed from inclusion crystals **FJI-H14** by ultrasonic processing in DMSO-d⁶ solution and further determined by ¹H NMR. Finally, about 2.78 µmol

of (chloromethyl)ethylene oxide, 1.2 μ mol of 1,2-epoxyoctane, or 1.1 μ mol of styrene oxide were added.

Data availability. The X-ray crystallographic coordinates for structure reported in this article have been deposited at the Cambridge Crystallographic Data Centre (CCDC), under deposition number CCDC 1517725. These data can be obtained free of charge from The Cambridge Crystallographic Data Centre via www.ccdc.cam.ac.uk/data_request/cif.

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Author contributions

Q.C., D.Y. and M.H. conceived and designed the experiments and co-wrote the paper. L.L. performed most of the experiments and analyzed data. C.L. worked on all computational simulations. H.X., J.Q. and L.Z. performed adsorption test. Q.C., D.Y., J.F., H. J., M.H. and L.L. analyzed the data and wrote the manuscript. All authors discussed the results and commented on the manuscript.

Additional information

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