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Efficient Electrochemical Hydrogenation of Furfural to Furfuryl Alcohol Using an Anion-Exchange Membrane Electrolysis Cell

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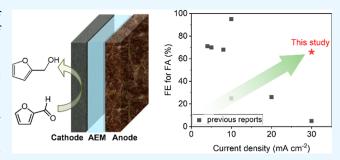
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ABSTRACT: The electrochemical hydrogenation (ECH) of furfural (FF) offers a promising pathway for the production of furfuryl alcohol (FA) while aligning with sustainability and environmental considerations. However, this technology has primarily been studied in half-cell configurations operating at high cell voltages and low current densities. Herein, we employ a membrane electrode assembly (MEA) system with an anionexchange membrane for the ECH of FF and systematically investigate various parameters, including the ionomer content in the cathode catalyst, electrolyte type, electrolyte concentration, and flow rate. Under optimal conditions, our MEA system with non-



noble metal-based catalysts exhibits a current density of 30 mA cm⁻² with a Faradaic efficiency for FA production of 66% at a cell voltage of 2 V, maintaining operational durability for 5 h. This study highlights the potential of electrochemical FA production for practical applications to realize the decarbonization of the hydrogenation industry.

■ INTRODUCTION

The direct conversion of biomass into valuable chemicals is being intensively pursued to reduce the dependency on petroleum-derived resources amidst the growing environmental and economic concerns. 1-6 Furfural (FF), which is produced from agricultural waste treatment at a commercial scale of 250,000 tons per year, 1,7 stands among the top 12 biomass-derived platform molecules crucial for fuel production.8 The valorization of FF yields various chemicals, with furfuryl alcohol (FA) as the main derivative accounting for roughly 60% of the FF feedstock due to its extensive demand in the foundry industry for binder production. 1,7,9-12 Conventionally, FA is mainly produced from FF using thermocatalytic hydrogenation methods, exhibiting high selectivity. 13-16 However, these techniques require high temperature (>400 K) and pressure (>5 MPa). 1,12,17,18 Hence, a more sustainable and environmentally friendly approach to upgrading FF into FA is highly desirable.

Electrochemical hydrogenation (ECH) has emerged as an alternative method for converting FF to FA. 19-25 ECH operates under mild conditions without the need for hydrogen gas, utilizing electricity that can be sourced from renewable energy. However, despite its technological potential, the ECH of FF suffers from a series of drawbacks that hinder its practical application. First, most studies on electrochemical FA production predominantly rely on half-cell systems, achieving limited current densities (~20 mA cm⁻²). 9,10,19,20,23,26-30 Low current densities (\sim 20 mA cm $^{-2}$) at elevated cell voltages (>2 V) have also been reported in a few studies on FA production using membrane electrode assembly (MEA) cells;^{8,31} thus,

further understanding and optimization of MEA systems are required. Second, discovering an optimal electrolyte for FA production is imperative to ensure an enhanced selectivity and economic viability. Initially, research on the ECH of FF focused on acidic conditions; 9,11,25,28,32-36 however, acidic electrolytes are prone to side reactions such as hydrogen evolution, 2-methylfuran production, and polymerization and require noble metals such as Pt and Ir for durability. 1,7,17 Therefore, identifying the optimal electrolyte and parameters for the electrochemical production of FA in the MEA systems is crucial.

Herein, we employed a MEA system with an anion-exchange membrane (AEM) for the ECH of FF and systematically investigated various parameters under alkaline conditions. A Cu catalyst was employed as a cathode catalyst due to its exceptional selectivity for FA production, 11,17,19,29 and an electrodeposited FeCo-based catalyst was used as an anode catalyst. Various parameters, including the ionomer content in the Cu catalyst, electrolyte type, electrolyte concentration, and flow rate, were systematically investigated under alkaline conditions, and the optimal conditions in terms of FA production performance and selectivity were identified.

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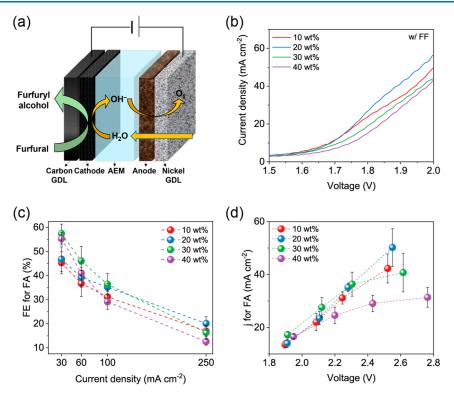


Figure 1. (a) Schematic of the ECH of FF to FA in a MEA system. (b) Polarization curves, (c) FE for FA production, and (d) current density for FA production in the MEA systems with Cu electrodes at varying ionomer contents from 10 to 40 wt % in a solution containing 1 M K_2CO_3 and 0.1 M FF (w/FF).

Under optimum conditions, our system using non-noble-metal-based catalysts attained a current density of 30 mA cm⁻² at a cell voltage of 2 V with a Faradaic efficiency (FE) of 66%. Moreover, it demonstrated notable durability for 5 h of operation at a constant current density of 30 mA cm⁻². These results underscore the promising prospects of electrochemical FA production for practical applications.

■ EXPERIMENTAL SECTION

Electrocatalyst Preparation. For the cathode catalysts, Cu nanoparticles were prepared via the liquid-phase reduction of NaBH₄. First, 0.1 g of carbon black powder was added to 100 mL of deionized water (18.2 M Ω cm, Milli-Q Direct 8 system, Merck Millipore, MA, USA), and the mixture was sonicated for 30 min. Subsequently, CuCl₂ (99.9%, Sigma-Aldrich) was added at a concentration of 5 mM, and the mixture was stirred for 1 h. NaOH (98%, Alfa Aesar) was employed to attain a pH of 12, followed by the addition of 10 mL of 0.5 M NaBH₄ (99.9%, Sigma-Aldrich). After the solution was stirred for more than 20 h, the Cu nanoparticles were isolated via filtration. The Cu cathode electrode was fabricated by using the spray-coating technique. Briefly, a cathodic ink slurry comprising the synthesized Cu nanoparticles, XB-7 ionomer (Dioxide Materials), water, and isopropyl alcohol, was sonicated for 1 h and then subjected to the spray-coating process, achieving a loading density of 5 mg cm⁻² on carbon paper (10BC, Sigracet). The ionomer content relative to Cu was adjusted within the range of 10-40 wt %. For the anode catalyst, a FeCo-based catalyst was fabricated via electrodeposition of Fe and Co from a solution containing 25 mM FeCl₃ (99.9%, Sigma-Aldrich) and 25 mM of CoCl₂ (99.9%, Sigma-Aldrich) on Ni felt (NF, 2Ni18-025, Bekaert) at -0.95 V (vs SCE) for 5 min using a conventional

three-electrode electrochemical cell with NF, platinum foil, and a saturated calomel electrode (SCE) as the working, counter, and reference electrodes, respectively.

Electrochemical Evaluation of MEA Systems. The electrochemical assessment of the MEA system was performed using the established AEM water electrolysis single-cell system.^{37–39} The single cell consists of a 1 cm² Cu cathode, the FeCo-based anode, and an X37-50 grade RT (Dioxide Materials) AEM. Pt-coated Ti flow fields and end plates were provided by the CNL Energy company. A 1 M K₂CO₃ (99.0%, Sigma-Aldrich) solution was supplied to the anode. For the cathode, Li₂CO₃ (99.0%, Sigma-Aldrich), Na₂CO₃ (99.5%, Sigma-Aldrich), or K₂CO₃ solutions were used as electrolytes with and without 0.1 M FF (99.0%, Sigma-Aldrich). All experiments were performed at room temperature. Linear sweep voltammetry (LSV) curves were obtained in the range of 1.0-2.0 V using a scan rate of 10 mV s⁻¹. To ascertain the industrial applicability of FA production, we quantified the FA production amount at high current densities ranging from 30 to 250 mA cm⁻². The quantity of FA produced was measured after a constant current density was applied for 3 min. For a durability test, the AEMWE system was operated at 30 mA cm⁻² for 5 h. Electrochemical impedance spectroscopy (EIS) measurements were conducted at a cell voltage of 1.7 V and an applied amplitude of 10 mV, spanning a frequency range of 10 kHz to 1 Hz.

Product Analysis. The gas and liquid products were quantified via gas chromatography (GC; 7890B, Agilent) and high-performance liquid chromatography (HPLC; YL9100 HPLC system, YL Instrument), respectively, which are generally used to analyze both FF and FA. 9,19,40,41 For the analysis of the gas products, the cathode compartment of the flow cell was linked to a GC, directing the exit stream from the

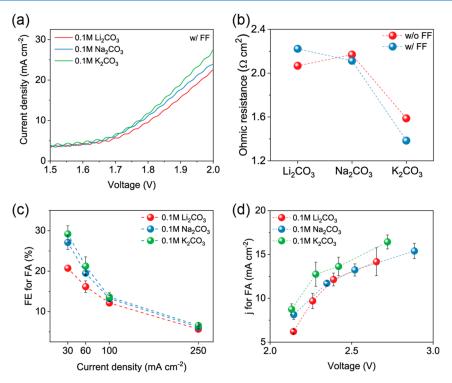


Figure 2. (a) LSV curves, (b) ohmic resistance, (c) FE for FA production, and (d) current density for FA production in MEA systems with solutions containing 0.1 M FF with 0.1 M Li₂CO₃, Na₂CO₃, or K₂CO₃.

ECH cell into the gas sampling loop of the GC. The gas products in the exit stream were analyzed by using a thermal conductivity detector. For the analysis of the liquid products, samples from the cathode reservoir were collected, 10-fold-diluted with acetonitrile (ACN; HPLC grade, 99.8+%, Thermo Scientific), and subsequently analyzed via HPLC. A mixture of ACN and DI in a ratio of 2:8 was employed as the eluent, and the resulting product was quantified by using a UV detector at 220 nm. Quantitative analysis was conducted through external calibration using standards at FF and FA concentrations ranging from 0.05 to 10 mM. The quantities of products obtained from the GC and HPLC analyses were employed to determine the FE of products according to eq 1

$$FE (\%) = \frac{n \times F \times m}{Q} \times 100$$
 (1)

where n represents the number of electrons involved in the ECH to produce one molecule, F is the Faraday constant (96,485 C mol⁻¹), m represents the amount of produced products in moles, and Q represents the total charge passed.

Materials Characterization. Surface morphology was evaluated via scanning electron microscopy (SEM) analysis using a JSM-7800F Prime microscope (JEOL, Japan) operating at 15 kV, conducted at the National Center for Inter-university Research Facilities (NCIRF) located at Seoul National University (SNU). X-ray photoelectron spectroscopy (XPS) analysis was conducted utilizing a K-alpha system (Thermo Fisher Scientific, UK) incorporating an Al Kα μ-focused monochromator operating at 1486.6 eV. The crystal structure was analyzed using X-ray diffraction (XRD) with a SmartLab system (Rigaku, Japan) employing Cu Kα radiation (40 kV, 250 mA) within the 2θ range of $30-80^\circ$, at a scan speed of 4° s⁻¹.

RESULTS AND DISCUSSION

Figure 1 depicts a schematic of the MEA system for electrochemical FA generation and shows the influence of the ionomer content in the Cu cathode on the FA production performance. In our MEA system, FA is produced via the reaction between FF and water at the cathode, and produced OH- migrates toward the anode across the AEM to generate O₂ (Figure 1a). A 1 M K₂CO₃ solution was employed in the anode, and a mixed solution containing 1 M K₂CO₃ and 0.1 M FF was used in the cathode. To explore whether ionomers play a comparable role in FA production systems as they do in water electrolysis, we conducted experiments varying ionomer content in the 1 M K₂CO₃ electrolytes with (w/FF) and without FF (w/o FF). Figure 1b illustrates the LSV curves of the MEA systems using Cu catalysts at varying ionomer contents ranging from 10 to 40 wt %. Among these systems, the MEA system with the Cu catalyst containing 20 wt % ionomer exhibited the highest current density of approximately 60 mA cm⁻² at a cell voltage of 2 V. Even in the absence of FF, the MEA system with the Cu catalyst containing 20 wt % of ionomer displayed superior performance to other systems (Figure S1). The FA produced at current densities of 30, 60, 100, and 250 mA cm⁻² was quantified via HPLC (Figure S2), and the FE was calculated (Figure 1c). At 30 mA cm⁻², the Cu system comprising 30 wt % of ionomer exhibited the highest FE of \sim 58%. However, at 250 mA cm⁻², the Cu system with an ionomer content of 20 wt % showed the highest FE of approximately 22%. For a comprehensive comparison of the performance and FE for FA production, the current density for FA versus cell voltage plots of each system is shown in Figure 1d. Each cell voltage represents the stabilized value obtained during the continuous operation under a constant current density. At around 1.9 V, all systems demonstrated similar current densities, while the system with the Cu catalyst

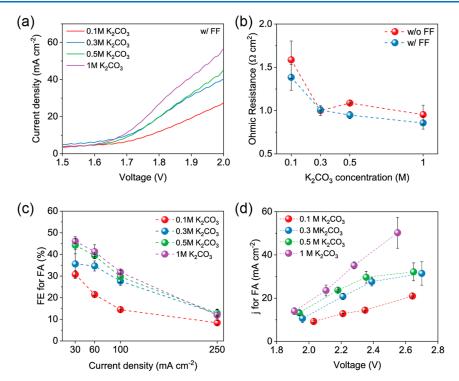


Figure 3. Comparison of (a) polarization curves, (b) ohmic resistance, (c) FE for FA production, and (d) current density for FA production in MEA systems with varying K_2CO_3 concentrations in the 0.1 M FF solution.

containing 20 wt % of ionomer showcased superior performance, delivering a current density of ~ 50 mA cm⁻² at approximately 2.5 V. Given that the performance trend based on ionomer content remains consistent regardless of the presence or absence of FF, it is posited that the observed trend, wherein optimal ionomer content enhances ion conduction and mass transfer in water electrolysis, $^{42-46}$ is also applicable to the ECH of FF. Accordingly, an ionomer concentration of 20 wt % was selected as the optimal condition for the subsequent experiments.

Next, the effect of the cation in the cathode electrolyte on the FA production performance was investigated by comparing 0.1 M Li₂CO₃, Na₂CO₃, and K₂CO₃ solutions (Figure 2). To minimize pH effects, the pH of all solutions was controlled at 12. Figure 2a shows that the MEA system with K₂CO₃ afforded the highest performance among others, exhibiting ~27 mA cm⁻² at 2 V. This trend, which was observed even in the absence of FF (Figure S3a), can be attributed to the lower ohmic resistance of the system with K2CO3 compared with other electrolytes (Figures 2b and S3b,c). In addition, the MEA system with a K₂CO₃ electrolyte exhibited the highest FE for FA among all of the systems at all current densities (Figure 2c). Among the electrolytes, Li₂CO₃ exhibited the lowest FE for FA. At all cell voltage ranges, the K₂CO₃ electrolyte consistently provided superior performance in terms of the current density for FA production (Figure 2d). These results demonstrate the pronounced influence of the cations in electrolytes on both the performance and selectivity for FA production. As established in the field of CO₂ reduction, this phenomenon can be attributed to the fact that with increasing cation size, the pK_a of cations diminished, and thereby the buffering capacity decreases in the order $K^+ > Na^+ > Li^+$, which resulted in diminishing the HER. 47,48 Consequently, K2CO3 was selected as the optimal electrolyte for electrochemical FA production in the MEA system.

Alkaline electrolytes can avoid the use of noble metal catalysts and reduce side reactions like hydrogen evolution, 2methylfuran production, and polymerization but may also induce the Cannizzaro reaction. 17,22,49-51 Thus, identifying the optimal molarity and pH for alkaline electrolytes is essential to minimize side reactions and ensure a high FA production performance. Figure 3 illustrates the FA production performance depending on the K2CO3 concentration at a constant FF concentration of 0.1 M. To mitigate the Cannizzaro reaction, which occurs at high pH and was confirmed even in 0.1 M KOH with 0.1 M FF in our experiments, we adjusted the pH to 12 for the K₂CO₃ electrolyte test. Figure 3a shows an obvious performance increase with increasing K₂CO₃ concentration irrespective of the presence of FF (Figure S4a). As observed in the LSV results, an increase in the K2CO3 concentration resulted in a decrease in the ohmic resistance of the system (Figures 3b and S4b,c). Notably, the electrolyte composed of 1 M K₂CO₃ and 0.1 M FF demonstrated the lowest ohmic resistance of 0.9 Ω cm². Furthermore, the MEA system with this electrolyte exhibited superior FE for FA production compared to other systems at all current density ranges (Figure 3c) and consistently demonstrated the highest FA production performance at all measured cell voltage ranges (Figure 3d). Given the observed correlation between the electrolyte concentration and FA production performance, electrolytes with higher concentrations of either K2CO3 or FF were also investigated. Three solutions, i.e., 1 M K₂CO₃ + 0.1 M FF, 1 M $K_2CO_3 + 0.2$ M FF, and 2 M $K_2CO_3 + 0.1$ M FF, were prepared and evaluated as electrolytes to determine the occurrence of spontaneous side reactions. Initially, all the three electrolytes exhibited a light brown color, which was retained for the 1 M K₂CO₃ + 0.1 M FF electrolyte after 20 h, whereas the 1 M K_2CO_3 + 0.2 M FF and 2 M K_2CO_3 + 0.1 M FF electrolytes turned darker (Figure S5a). This can be attributed to polymer formation via the Cannizzaro reaction. 17,22,49-51

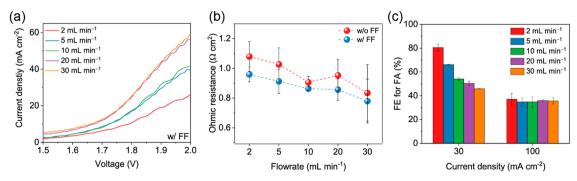


Figure 4. Comparison of (a) polarization curves, (b) ohmic resistance, and (c) FE for FA in MEA systems with varying flow rates from 2 to 30 mL min^{-1} in a solution containing 1 M K_2CO_3 and 0.1 M FF.

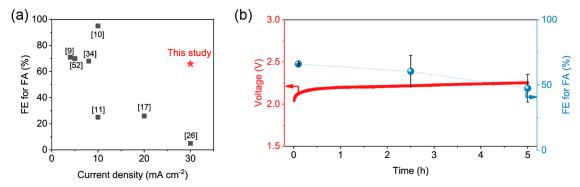


Figure 5. (a) Comparison of the performance of the Cu-based MEA system with previous state-of-the-art FF hydrogenation catalysts. $^{9-11,17,26,34,52}$ (b) Cell voltage and FE profiles for the ECH of FF to FA of the optimized MEA system at 30 mA cm⁻² for 5 h. Conditions: Cu cathode with an ionomer content of 20 wt %, 5 mL min⁻¹ of flow rate, and 1 M K₂CO₃ + 0.1 M FF solution.

To quantify the byproducts resulting from the Cannizzaro reaction, the products were measured over time. Due to the difficulties in polymer quantification via HPLC, the comparison primarily focused on FA production. For all electrolytes, FA was not detected within the first hour of the reaction. However, after 3 h, approximately 0.06 mM FA was produced in the 1 M $K_2CO_3 + 0.2$ M FF and 2 M $K_2CO_3 + 0.1$ M FF electrolytes but not in the 1 M K₂CO₃ + 0.1 M FF electrolyte (Figure S5b). After 20 h, approximately 0.2 mM FA was generated in the 1 M K₂CO₃ + 0.2 M FF and 2 M K₂CO₃ + 0.1 M FF electrolytes, while nearly half that amount was produced in the 1 M K₂CO₃ + 0.1 M FF electrolyte. These results demonstrate that excess K₂CO₃ or FF induces side reactions, such as the Cannizzaro reaction, highlighting the importance of controlling the pH and molarity of the electrolyte. Therefore, we selected the 1 M K₂CO₃ + 0.1 M FF solution as the optimal electrolyte composition and employed it in subsequent experiments.

Figure 4 shows the relationship between the FA production performance and the flow rate. The flow rate significantly influences mass transfer, thereby affecting both FA production rate and selectivity. Flow rates of 2, 5, 10, 20, and 30 mL min $^{-1}$ were evaluated using the 1 M $\rm K_2CO_3 + 0.1$ M FF electrolyte. The current densities of the systems at 2 V were improved with increasing flow rates and then stabilized at approximately 60 mA cm $^{-2}$ after reaching a plateau beyond a flow rate of 20 mL min $^{-1}$ (Figure 4a). The limited performance at lower flow rates stemmed from an insufficient reactant supply to the catalyst layer. 43 In this setup, a flow rate of around 20 mL min $^{-1}$ provided an adequate reactant supply. Along with the performance trend, a reduction in ohmic resistance irrespective of the presence of FF occurred with an increasing flow rate

(Figures 4b and S6). However, at a current density of 30 mA cm⁻², a noticeable increase in the FE for FA production was observed as the flow rate decreased (Figure 4c). At a flow rate of 2 mL min⁻¹, the MEA system displayed ~80% FE for FA at 30 mA cm⁻², representing the highest FE among the systems. However, this correlation was not verified at 100 mA cm⁻², where the FE remained consistently around 38% across all flow rates. Because FF inhibits the adsorption of the proton source at the catalyst surface, lower flow rates may impede the access of the proton source to the catalyst surface, enhancing the selectivity for FA production by inhibiting the HER. However, at high current densities, the depletion of FF on the catalyst surface enables water access, leading to diminished FE for FA regardless of flow rate. Considering both high performance and selectivity for FA production, a flow rate of 5 mL min⁻¹ was selected as the optimal condition, and the product analysis via HPLC and GC confirmed the exclusive presence of H2 and FA (Figure S7). Under the optimal conditions, our system demonstrated superior FE for FA production at a relatively high current density, outperforming state-of-the-art catalysts (Figure 5a and Table 1). 9-11,17,26,34,52 Moreover, in contrast with the majority of studies, which were conducted using halfcell systems requiring high cell voltages, our system exhibited a high performance at a cell voltage of approximately 2 V. We also compared our system with conventional thermocatalytic hydrogenation technologies, showing FA selectivity comparable to previous research under ambient conditions of temperature and pressure (Table S1). 13-16 To assess the economic viability of ECH of FF for the FA production process, a techno-economic analysis (TEA) was conducted based on the previous studies (see details in the Supporting Information). 53-55 Based on the TEA using our experimental

Table 1. Comparison of the Performance of the Cu-Based MEA System with Reported FF Hydrogenation Systems 9-11,17,26,34,52

catalyst	FA selectivity (%)	current density (mA cm ⁻²)	references
Cu	66	30	this study
Cu	25	10	11
Cu	71	4	9
Cu/Cu-400 nm	5	30	20
AgPd	95	10	10
Cu ₁ /PC	70	5	52
Cu/NC900	26	20	17
$CuPd_{0.012}/C$	68	8	34

results, FA production via the ECH method with the MEA system (\$1076 per ton of FA) showed higher economic efficiency than conventional methods (\$1347 per ton of FA). This finding indicates the potential economic viability of the electrochemical FA production method, albeit necessitating further research on scale-up and enhancement of system performance and durability.

The optimized MEA system could be operated continuously at 30 mA cm⁻² for 5 h with an increase of approximately 0.2 V in the cell voltage, maintaining a FE of around 50% (Figure 5b). Our system demonstrates notable durability compared with previous reports describing shorter durability (~3 h) at low current densities (~15 mA cm⁻²).^{8,17,26,31} After the durability test, the ohmic resistance of the system increased by approximately 1.1 Ω cm², which can be attributed to membrane degradation or inadequate catalyst contact (Figure S8). To assess catalyst properties pre- and postdurability testing, XPS and SEM analyses were conducted. In the Cu 2p spectra, the peak around 932.5 eV indicates Cu⁰/Cu⁺, and the peak at approximately 933.8 eV corresponds to Cu²⁺ (Figure S9a). ⁵⁶ For O 1sp spectra, O₁ (lattice oxygen, ~529.7 eV) and O=C (~532.2 eV) peaks were shown (Figure S9c). S7 Initially, the Cu electrode exhibited dominance of the Cu²⁺ peak, yet postdurability testing, the prevalence shifts toward the Cu⁰/ Cu⁺ peak. Furthermore, following the durability test, the initially observed O_L peak was no longer observable. This result can be due to the electrochemical reduction of the Cu catalyst within the reducing atmosphere for FA formation. XRD analysis also revealed the transformation of the Cu catalyst from CuO to Cu/Cu₂O following the durability test (Figure S10). SEM analysis indicates that the Cu catalyst comprises nanoparticles on the order of tens of nanometers, with insignificant surface changes observed before and after the durability test (Figure S11). Overall, this study highlights the decent performance and durability of FA production in MEA systems using non-noble metal-based catalysts, demonstrating their potential for practical FA production. To enhance the FA production performance and durability in this MEA system, further research into catalyst and membrane development is required.

CONCLUSIONS

In conclusion, our extensive exploration of parameters for the ECH of FF employing a MEA system under alkaline conditions resulted in a notable FA production performance. A series of parameters, including the Cu catalyst ionomer content, electrolyte type, electrolyte concentration, and flow rate, were investigated, and the optimal condition in terms of

FA production performance and selectivity was identified. Under the optimal condition, our system achieved a current density of 30 mA cm⁻² with a FE of 66% for FA production at a cell voltage of 2 V. Furthermore, it exhibited remarkable durability during 5 h operation at a constant current density of 30 mA cm⁻². This study underscores the potential of electrochemical FA production for practical application, supporting the decarbonization of the hydrogenation industry.

ASSOCIATED CONTENT

Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acsomega.4c02107.

HPLC data; LSV and EIS plots in parametric MEA systems; FA production data according to electrolyte composition; Faraday efficiency for FA and H₂ during electrolysis; TEA analysis; EIS plots of the optimized MEA system at initial and after 5 h of operation; and XPS and SEM data for Cu electrodes (PDF)

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Notes

The authors declare no competing financial interest.

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