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**Cite this article:** Brüningk S, Powathil G, Ziegenhein P, Ijaz J, Rivens I, Nill S, Chaplain M, Oelfke U, ter Haar G. 2018 Combining radiation with hyperthermia: a multiscale model informed by *in vitro* experiments. *J. R. Soc. Interface* **15**: 20170681. <http://dx.doi.org/10.1098/rsif.2017.0681>

Received: 18 September 2017

Accepted: 18 December 2017

### Subject Category:

Life Sciences—Physics interface

### Subject Areas:

systems biology, computational biology, biophysics

### Keywords:

hybrid multiscale model, radiotherapy, hyperthermia, cell cycle, cancer, tumour

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Electronic supplementary material is available online at <http://dx.doi.org/10.6084/m9.figshare.c.3970839>.

# Combining radiation with hyperthermia: a multiscale model informed by *in vitro* experiments

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Combined radiotherapy and hyperthermia offer great potential for the successful treatment of radio-resistant tumours through thermo-radiosensitization. Tumour response heterogeneity, due to intrinsic, or micro-environmentally induced factors, may greatly influence treatment outcome, but is difficult to account for using traditional treatment planning approaches. Systems oncology simulation, using mathematical models designed to predict tumour growth and treatment response, provides a powerful tool for analysis and optimization of combined treatments. We present a framework that simulates such combination treatments on a cellular level. This multiscale hybrid cellular automaton simulates large cell populations (up to  $10^7$  cells) *in vitro*, while allowing individual cell-cycle progression, and treatment response by modelling radiation-induced mitotic cell death, and immediate cell kill in response to heating. Based on a calibration using a number of experimental growth, cell cycle and survival datasets for HCT116 cells, model predictions agreed well ( $R^2 > 0.95$ ) with experimental data within the range of (thermal and radiation) doses tested (0–40 CEM43, 0–5 Gy). The proposed framework offers flexibility for modelling multimodality treatment combinations in different scenarios. It may therefore provide an important step towards the modelling of personalized therapies using a virtual patient tumour.

## 1. Introduction

Cancer is a complex disease, with a variety of approaches available for its treatment. Treatment modalities are often combined to maximize response and to overcome the limitations of individual modalities when used alone. One such example is the combination of radiotherapy (RT) with hyperthermia (HT), i.e. non-ablative sustained heating (41–50°C applied for times up to  $\approx 1$  h) for the treatment of radiation-resistant tumours, or tumour sub-regions. Heat has a radio-sensitizing effect on cell lines of both normal and malignant origin [1–3]. Heating applied locally to a tumour may therefore enhance treatment outcome without increasing the risk of normal tissue complications. The intra-cellular mechanisms involved in thermo-radiosensitization are still subject to investigation. However, it is believed that a major cause of this synergism is an inhibition of DNA repair mechanisms by heat, leaving them more vulnerable to radiation-induced DNA strand breaks [4–6]. Radiation induced cell death is a highly regulated cellular process. Depending on factors such as the severity of the damage, cell-cycle stage and cell type, a response cascade, which will not only drive pro-survival repair pathways, but also trigger programmed cell death, is activated [4,7–9]. Once DNA damage is recognized, cell-cycle

checkpoint inhibition will prevent cycle progression to allow time for damage repair. Depending on the cell's current stage in its cycle, the allowed duration of cell-cycle arrest, as well as the availability of different DNA repair pathways, varies, leading to differences in repair capacity between cell-cycle stages. However, prolonged activation of repair and cell-cycle arrest drive prodeath pathways, resulting, if repair is unsuccessful, in cell kill via apoptosis, necroptosis or autophagy depending on both the cell type and the severity of the damage [4,7]. If the cell-cycle checkpoint functionality is compromised, unrepaired DNA damage will be inherited by daughter cells and may result in the formation of highly aneuploid cells with abnormal phenotype (giant cells) that eventually die or are unable to reproduce (mitotic catastrophe). This mitotic cell death is therefore not instantaneous but may take several cycles to manifest itself. Cellular senescence, i.e. irreversible cell-cycle arrest, is another potential result of severe DNA damage. Senescent cells do not proliferate but remain metabolically active [4,7]. In order to predict the dynamic treatment response of a tumour, or of a cell population, in general, it is therefore important to consider these various reaction pathways.

Systems oncology simulations [10–14] provide a powerful tool for analysis and optimization of treatment combinations, and make it possible to take inhomogeneities in the delivered heating profiles into account. In general, two types of simulation approaches, continuum and discrete models, are considered. Continuum-based approaches describe macroscopic cell densities and substrate concentrations according to reaction–diffusion processes using sets of partial and ordinary differential equations (PDEs and ODEs) [11]. Discrete approaches, such as cellular automaton models, track individual cells or even sub-cellular elements [11]. These are usually represented as lattice points on a simulation grid with all actions being governed by a set of predefined rules. Hybrid models combine both approaches and model biophysical processes on scales ranging from cellular to macroscopic using a mix of predefined transition rules and PDE-driven processes, such as the diffusion of nutrients or messaging molecules. Recent publications in the field of computational modelling of cancer therapies span a broad range, from modelling cell response *in vitro* [15–17] to modelling angiogenesis and tumour vasculature effects [18,19], the prediction of treatment outcome for patients [20,21] treated with a variety of approaches, and even to describing the evolution of different cancer types [22].

Although several studies have looked into modelling radio- and chemo-therapy response [10,18,23], studies reporting the effects of combination treatments of radiation and heat are few. Several groups have investigated the mathematical modelling of therapy outcome in terms of cell surviving fractions [3,24–26].

We here present an implementation of a hybrid cellular automaton model which simulates the response of cells to heat, RT or combinations of the two, on several different spatio-temporal scales. Temporally, the simulation covers modelling a cell's cycle progression (minutes), cellular division and treatment response (hours), up to the modelling of the growth of the whole population over the course of a treatment (days). Spatially, the simulation ranges from simulating individual cells ( $\mu\text{m}$ ) to dealing with macroscopic cell culture dishes ( $\approx 10^7$  cells, cm scale). The multiscale nature of the model therefore requires analysis of the effects of single

and combination treatments on individual cells, and on the cell population as a whole. The aim of this model was the prediction of response to the treatment of a large-cell population *in vitro*, i.e. to predict the number and distribution of viable cells over time, in order to provide an important first step towards more complex modelling of tumours *in vivo*. This requires finding a compromise between the simplest model that summarizes a cascade of complex biological processes, and a model that is sufficiently complex to describe the observed biological behaviour and is based on known key response pathways.

## 2. Methods

### 2.1. Model implementation

The model presented here is a significant development of the previous model of Powathil *et al.* [23,27], with new implementation in C++. This is a cellular automaton model for the simulation of response to therapy using the recently developed AlphaR survival model designed specifically for calculating cell surviving fractions after multimodality treatments [26]. Besides enabling the introduction of heat as a second treatment modality, the simulation framework has been extended to include dynamic modelling of mitotic cell kill after irradiation. Optimization of the implementation has further allowed an extension of the simulation to large cell populations (of the order of several million cells). This is required for direct comparison between experimental and simulated data. We show that our model can predict the dynamic growth of a treated cell population once key model parameters have been adjusted using experimentally derived *in vitro* data.

#### 2.1.1. Growth modelling

Digital cells are represented as voxels on a two- or three-dimensional lattice depending on the experimental set-up to be simulated. Thus, the diameter of a cell corresponds to the edge length of a voxel. The following discussion of *in vitro* experiments is restricted to the representation of cell monolayers in culture dishes, which are simulated as flat, two-dimensional lattices.

In agreement with the known cell-cycle progression of real cells [28,29], each virtual cell follows the well-known four-stage cycle through  $G_1$ ,  $S$ ,  $G_2$  and  $M$ -phases. Cycle stages are assigned according to an individual cell-cycle timer that is incremented in each time frame according to the predefined growth rate of that cell type. To account for variation in cycle duration for cells within a population, growth rates are assigned using a normal distribution, with a mean growth rate corresponding to the experimentally determined rate for the specific cell type, and a standard deviation of 5% of this value. Upon division, a cell's neighbourhood (i.e. Von Neumann (directly adjacent voxels), or Moore (directly and diagonally adjacent voxels) neighbourhoods) is scanned for free spaces up to third-order neighbours. Moore and Von Neumann neighbourhoods are applied alternately to give circular growth of the cell colony. From all free spaces, an empty voxel is randomly selected for the new position of the daughter cell, with positions closest to the parental cell being occupied first. For simplicity, during these relatively short-term studies (up to two weeks), all cells are assumed to have an infinite life span and unlimited division potential in the absence of external damage, resulting in exponential population growth. However, experimental cellular growth curves *in vitro* (i.e. number of cells present as a function of time) are characterized by an initial lag period during which the cells attach and adapt to their new environment, followed by exponential growth. A lag phase of 2 h was therefore introduced into our simulations. During this

phase, digital cells do not progress through their cycle, but may die if treatment is delivered during this time.

In a culture dish, a cell population eventually reaches confluence, and proliferation decreases due to a lack of space and increased competition for nutrients. This results in a plateau in the growth curve. A fifth stage,  $G_0$ , is introduced to account for this behaviour.  $G_0$  represents a reversible resting stage (quiescence). It is entered if a cell is no longer able to divide due to a lack of free space nearby. Quiescent cells arrest their cycle until neighbouring spaces are vacated, or the cell is killed. For a simulated culture dish of a predefined geometry, the number of cells at which the plateau is reached depends only on the number of voxels present, thus making it necessary to adapt the voxel size to model the shape of a simulated plateauing growth curve correctly. This will be described in detail in §3.1.1. Figure 1 shows a flow chart which describes the simulation of normal cell growth.

## 2.2. Treatment response modelling

### 2.2.1. Radiotherapy

Radiation is simulated as being delivered homogeneously to all cells in each fraction. Cell survival after radiation,  $S_{RT}$ , is estimated as a function of dose  $d$  using the AlphaR model [26], extended by a cycle stage-dependent weighting factor  $\gamma$  to account for differences in radiation sensitivity at each stage [23].

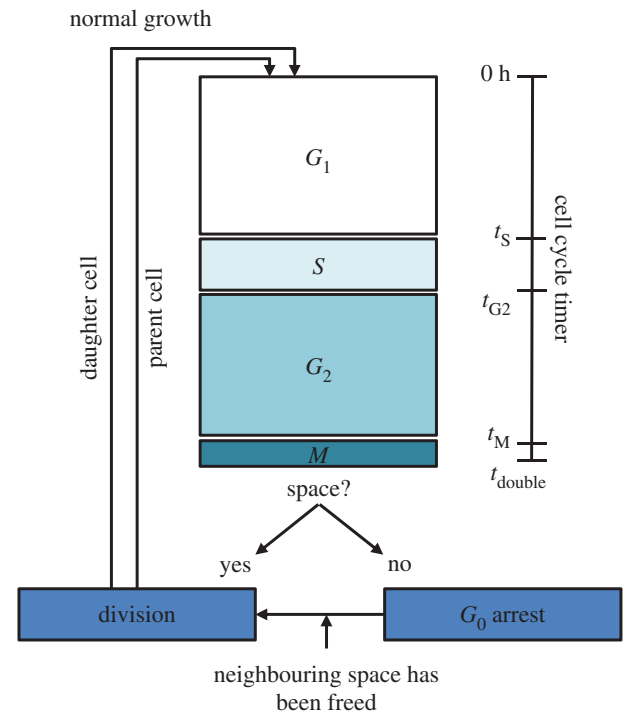
$$-\log(S_{RT}) = \begin{cases} \gamma(\alpha_0 - \alpha_R)d + \beta d^2 & d \leq D_T = \frac{\alpha_R}{2\beta} \\ \gamma(\alpha_0 d - \frac{\alpha_R^2}{4\beta}) & d > D_T. \end{cases} \quad (2.1)$$

The AlphaR model uses three cell line and treatment-dependent parameters:  $\alpha_0$ ,  $\alpha_R$  and  $\beta$ . These describe a combination of cellular damage ( $\alpha_0$ ), damage repair ( $\alpha_R$ ) and reduction of the repair capacity with increasing dose ( $\beta$ ).  $D_T$  represents a threshold dose above which no damage repair is possible. Whereas for doses lower than  $D_T$ , survival is described by a linear-quadratic (LQ) exponential function, the cell survival curve is described by a single exponential for doses exceeding this threshold.

The advantage of the AlphaR model over others, such as the LQ model [30], is its applicability to multimodality therapies. In particular, HT cell survival curves, which are characterized by a strong shoulder followed by an exponentially linear decay, are well described by this model. More information on the cell survival model used is provided in [26].

As for most cell survival models, the AlphaR model relates to survival as measured by clonogenic assays [31]. This assay is conducted several days post treatment, and therefore does not give information about the dynamics of cell damage and repair. In the range of doses used therapeutically, radiation-induced cell killing is not instantaneous, but occurs as a consequence of the cell's inability to undergo division successfully [4,7,8]. This means that irradiated cells may continue to proliferate, become senescent or form giant cells with multiple nuclei (mitotic catastrophe) before undergoing apoptosis. It is important to take this into account as growth restrictions due to space or nutrient limitations, as well as processes such as re-oxygenation (where three-dimensional growth is considered) will be affected by these dying cells.

Previous simulations have accounted for this observation by artificially increasing the surviving fraction predicted by the cell survival model (e.g. [23,27,32]). However, such an implementation does not reflect actual cellular behaviour, and has not been verified experimentally. In our model, we approximate the dynamics of radiation-induced cell killing using a series of random events as outlined in the decision tree shown in figure 2. Each cell that receives radiation in the simulation, will die with a probability  $1-S_{RT}$  ( $S_{RT}$  being the calculated surviving fraction). However, radiation-induced cell kill is not simulated

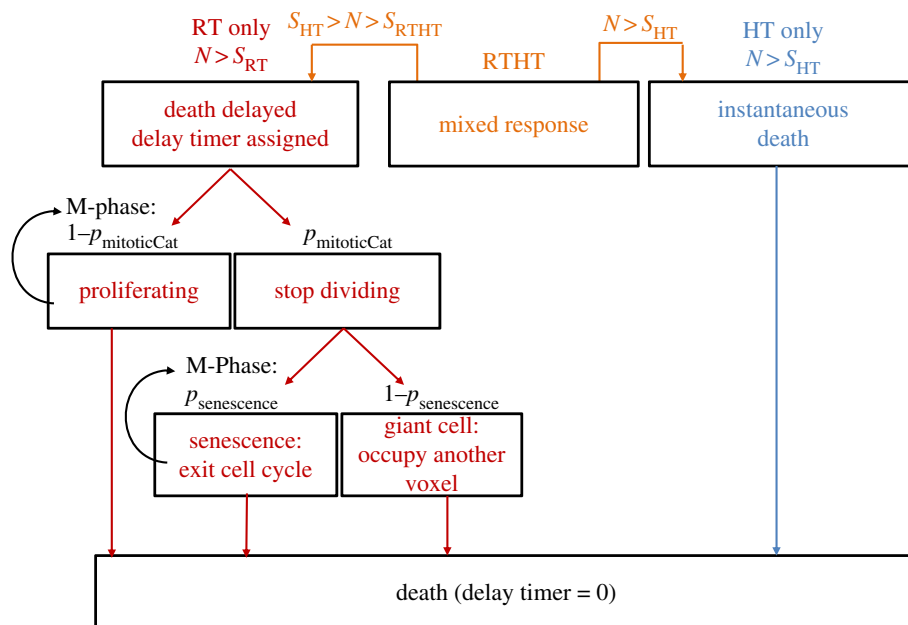


**Figure 1.** Flow chart showing the implementation of normal cell growth. According to its cycle timer a virtual cell follows a four-stage cycle consisting of  $G_1$ ,  $S$ ,  $G_2$  and  $M$ -phases. Once the cycle timer exceeds the threshold time  $t_{stage}$ , the cell is assigned to a new cycle stage. Once the cycle timer reaches the doubling time  $t_{double}$ , the cell will either divide into two cells in stage  $G_1$  or enter the reversible quiescent stage  $G_0$ , if no free neighbouring spaces are available. (Online version in colour.)

as being instantaneous, rather, the dying cells are assigned a randomly selected delay period between irradiation and time of death. These delays to cell death are sampled from an exponential distribution with exponent  $k_{delay}$  which has to be determined from experimental data (see §2.4). During the delay period, cells keep proliferating, but any daughter cells created will die at the same time as their parent. Besides normal proliferation, dying cells can also enter mitotic catastrophe at the end of  $M$ -phase, with a probability  $p_{mitoticCat}$ . Cells undergoing mitotic cell death either form giant cells with their size increasing at each attempted division, or they become senescent with probability  $p_{senescence}$ , i.e. they cease to proliferate but are still viable. This allows for a small population of surviving, but non-proliferating cells. It should be stressed that, although motivated by experimental observations, this simulation provides a mathematical construct that provided the best balance between a biologically motivated description and simplifying approximations to build a time efficient simulation. The actual underlying biological processes may, however, be far more complex, and it was the aim of this study to provide a deliberately simple implementation with few model parameters to vary.

### 2.2.2. Cellular heat response

For the experimental procedure described below, heat treatments are simulated as temporally homogeneous exposures, such as are performed in a thermal cycler. The biological effect of these treatments depends on treatment temperature and duration. To compare different heating profiles, and to quantify the effects of the applied heat distribution at a cellular level, the 'thermal dose' concept [33] is used. Thermal dose is defined in terms of the equivalent time at a constant temperature of 43°C (measured in units described as CEM43) required to yield the same number of surviving cells as from a different arbitrary combination of



**Figure 2.** Decision tree used to simulate treatment response to radiation, heat and combination treatments for each individual cell. According to a random number  $N[0, 1]$  drawn for each cell, a decision is made whether the cell lives ( $N \leq S$ ) or dies. The respective surviving fractions after heat alone,  $S_{HT}$ , radiation alone,  $S_{RT}$ , or combination treatment,  $S_{RTHT}$ , were calculated using equations (2.1), (2.3) and (2.4). Whereas heated cells (HT) are assumed to die instantaneously, irradiated cells (RT) are assigned a time delay before death which is sampled from an exponential distribution. Until this time point is reached, dying cells either keep dividing (with probability  $1 - p_{mitoticCat}$ ), or undergo mitotic catastrophe and become either a giant cell (with probability  $1 - p_{senescence}$ ) or a senescent cell (with probability  $p_{senescence}$ ). For combination treatments (RTHT), cells die instantaneously if  $N > S_{HT}$ , or follow radiation-induced delayed cell death if  $S_{HT} > N > S_{RTHT}$ . (Online version in colour.)

heating time and temperature. It is calculated using a two-case model distinguishing between heating above and below a threshold temperature of  $43^\circ\text{C}$  to account for the activation of different biological processes at these temperature levels: for a number of heating steps  $i$ , heating times  $t_i$  at a temperature  $T_i$  are expressed in terms of equivalent heating time at  $43^\circ\text{C}$ ,  $t_{43}$ .

$$t_{43} = \sum_i t_i \cdot R^{43-T_i} \quad \text{with } R = \begin{cases} 0.25 & T_X \leq 43^\circ\text{C} \\ 0.5 & T_X > 43^\circ\text{C}. \end{cases} \quad (2.2)$$

For the calculation of the total thermal dose from a treatment, time steps  $t_i$  with temperatures exceeding  $40^\circ\text{C}$  are taken into account. In a similar manner to the implementation of the cellular response to radiation, the AlphaR model surviving fraction is used to evaluate the fate of an HT as a function of thermal dose,  $S_{HT}(t_{43})$ . For this, the dose parameter  $d$  in equation (2.1) is replaced by the total thermal dose,  $t_{43}$ , according to equation (2.2).

$$-\log(S_{HT}(t_{43})) = \begin{cases} \gamma((\alpha_{0,HT} - \alpha_{R,HT})t_{43} + \beta_{HT}t_{43}^2) & t_{43} \leq D_T = \frac{\alpha_{R,HT}}{2\beta_{HT}} \\ \gamma\left(\alpha_{0,HT}t_{43} - \frac{\alpha_{R,HT}^2}{4\beta_{HT}}\right) & t_{43} > D_T. \end{cases} \quad (2.3)$$

The model parameters  $\alpha_0$ ,  $\alpha_R$  and  $\beta$  are replaced by the cell line-specific parameters determined from HT cell survival curves,  $\alpha_{0,HT}$ ,  $\alpha_{R,HT}$  and  $\beta_{HT}$ . In the simulation, HT-induced cell killing is modelled to occur instantaneously, and no further cell-cycle delay is applied.

### 2.2.3. Combination treatments

Similar to the implementation of heat alone, and radiation alone induced cell killing, cell surviving fractions resulting from combined RT and HT treatments,  $S_{RTHT}(d, t_{43})$ , with thermal dose  $t_{43}$ , and radiation dose  $d$ , are first calculated. As reference data were only available for the LQ branch of the AlphaR model in

this case, surviving fractions are calculated as follows:

$$\left. \begin{aligned} S_{RTHT}(d, t_{43}) &= S_{HT}(t_{43}) \cdot e^{-(\alpha_{RTHT}(t_{43})d + \beta_{RTHT}(t_{43})d^2)}, \\ \alpha_{RTHT}(t_{43}) &= \alpha_{RT} + a \cdot t_{43} \\ \text{and } \beta_{RTHT} &= \beta_{RT}. \end{aligned} \right\} \quad (2.4)$$

Here,  $S_{HT}(t_{43})$  is the surviving fraction due solely to the heat treatment. Heat-induced radio-sensitization is described by a thermal dose-dependent parameter  $\alpha_{RTHT}$  that increases linearly with thermal dose according to a cell line-dependent slope  $a$ , whereas  $\beta_{RTHT}$  is assumed to be constant.  $\alpha_{RT}$  ( $\alpha_{RT} = \alpha_{0,RT} - \alpha_{R,RT}$ ), and  $\beta_{RT}$  refer to radiation only treatments. These thermal dose dependencies were analysed in detail in [26] for the cell line used here, and in [34–36] using a very similar parametrization for different cell lines.

In simulating the dynamic cell kill in response to combination treatments, cells are immediately ‘killed’ according to the surviving fractions derived from the heat contribution of the treatment, i.e. a fraction of  $1 - S_{HT}$  cells is removed from the grid. Of the remaining cells,  $1 - S_{RTHT}(d, t_{43})/S_{HT}(t_{43})$  (equation (2.4)) are assigned a time delay before cell death sampled from an exponential distribution as described for the simulation of RT alone cell kill (see flow chart in figure 2).

## 2.3. Experimental procedure for calibration and validation experiments

A number of experiments were performed to calibrate the simulation framework used to model the response of the colorectal carcinoma cell line HCT116. These included growth curves, cell-cycle analysis and clonogenic cell survival assays (published in [26]).

For all experiments, HCT116 cell monolayers were grown at  $37^\circ\text{C}$  in McCoy’s 5A medium (Gibco, Paisley, UK) supplemented with 10% fetal bovine serum (PAN Biotech, UK) and 1% antibiotics ( $50 \text{ U ml}^{-1}$  each of penicillin, streptomycin B and amphotericin B (Sigma Aldrich, Poole, UK)) in a humidified atmosphere containing 5%  $\text{CO}_2$ . Cells were passaged twice

**Table 1.** AlphaR-model parameters (with their time and temperature dependence) used to simulate the treatment response of HCT116 cells.

	$\alpha = \alpha_0 - \alpha_R$	$\alpha_0$	$\beta$
RT	$0.5 \text{ Gy}^{-1}$	—	$0.042 \text{ Gy}^{-2}$
HT	0	$0.05 \cdot e^{0.67^\circ\text{C}^{-1} \cdot (T-43^\circ\text{C})} \text{ min}^{-1}$	$\frac{\alpha_0^2}{1.95} \text{ min}^{-2}$
RTHT	$0.5 \text{ Gy}^{-1} + 0.015 \cdot t_{43} \text{ Gy}^{-1} \text{ min}^{-1}$	—	$0.042 \text{ Gy}^{-2}$

weekly using the gentle detaching agent Accutase (Gibco, Paisley, UK). Regular screening for mycoplasma and bacterial contamination was undertaken, and cells in exponential growth phase between passages 10 and 20 were used for experiments.

For treatments, cells were detached, concentrated to give a suspension of  $5 \times 10^6$  cells  $\text{ml}^{-1}$  and transferred to sterile, thin-walled PCR tubes (VWR, Lutterworth, UK) in  $60 \mu\text{l}$  volumes. For irradiation, tubes containing cells were embedded in a solid water sample holder and irradiated using a small animal radiation research platform (SARRP, X-Strahl, Camberley, UK) at a dose rate of  $63 \text{ mGy s}^{-1}$ . Heating to  $46^\circ\text{C}$  for 5 min was performed in a Biorad Tetrad2 DNA Engine PCR thermal cycler (Hercules, CA, USA) using the techniques described in [26,37]. Cells were kept on ice before, between and after treatments to minimize cellular activity during waiting periods. For combination treatments, cells were first irradiated, and then heated within 20 min of this irradiation. It was confirmed experimentally that if heating was applied within 30 min, the delay between irradiation and heating made no difference to the subsequent clonogenic cell survival [26]. For fractionated treatments, plates seeded with the required number of cells were irradiated every 24 h using an X-ray cabinet (X-Strahl, Camberley, UK, dose rate  $63 \text{ mGy s}^{-1}$ ).

### 2.3.1. Growth curves

Cell growth curves were acquired by seeding triplicates of treated cells in 24- or six-well plates depending on the expected number of surviving cells. Seeding densities ranged from  $2 \times 10^4$  cells/24-well plate to  $5.4 \times 10^5$  cells/six-well plate depending on the treatment given. Cell number was determined at various time points (24–200 h) after treatment by counting detached cells in a haemocytometer. A minimum of 100 cells in a minimum of three  $1 \times 1 \text{ mm}^2$  were counted for each replicate. For each data point, the average cell count and corresponding standard deviations of three replicates were taken. Growth curves were also acquired at comparable cell densities in 96-well plates. Cells in 96-well plates were fixed with ice-cold 10% trichloroacetic acid, and subsequently stained with sulforhodamine B (Sigma Aldrich, Poole, UK) before being imaged with bright-field microscopy to study cell morphologies.

### 2.3.2. Cell-cycle analysis

For cell-cycle analysis, cells were detached, washed in ice-cold phosphate-buffered saline and fixed in ice-cold 70% ethanol. Fixed cells were treated with RNase to minimize non-specific background staining, and stained with the DNA-intercalating dye propidium iodide (PI, Sigma Aldrich, Poole, UK) for 15 min at room temperature in the dark prior to analysis using flow cytometry in an LSRII analyser (BD, Franklin Lakes, NJ). DNA content of at least  $10^4$  cells was measured in this way and data were collected using DiVa (BD, Franklin Lakes, NJ). The resultant histograms were fitted by the Watson pragmatic model in FlowJo<sup>®</sup> to obtain cell-cycle distribution proportions.

### 2.3.3. Clonogenic assays

Clonogenic cell survival data have been published in [26] for HCT116 cells. Table 1 summarizes all parameters used for calculating clonogenic surviving fractions for possible treatment

**Table 2.** Summary of all parameters used in this simulation framework together with the method used for parameter estimation.

parameter	calibration method
$\alpha, \alpha_0, \alpha_R, \beta$	clonogenic assay
growth rate	growth curve
number of cells in plateau phase	growth curve
cell-cycle distribution	flow cytometry
initial number of cells $N_0$	haemocytometer count
$p_{\text{mitoticCat}}, p_{\text{senescence}}, k_{\text{delay}}$	fit of $R^2$

scenarios for this cell line. For RT and RTHT treatments, the LQ arm of the AlphaR model was sufficient to describe the cell survival data obtained for the radiation doses used here. Therefore, no individual values for  $\alpha_0$ , and  $\alpha_R$  are needed, and the difference between these parameters, (i.e.  $\alpha = \alpha_0 - \alpha_R$ ), is given. For HT treatments  $\alpha_0 = \alpha_R$  (see [26] for details).

## 2.4. Parameter fitting upon model calibration

Where it was not possible to measure model parameters experimentally, these were adjusted to yield the best overall agreement in terms of coefficients of determination  $R^2$  between simulated and reference data during calibration of the model. For model validation, no further changes were made to the parameters used. Table 2 gives an overview of all parameters used in this simulation and the method used for their determination.

## 3. Results

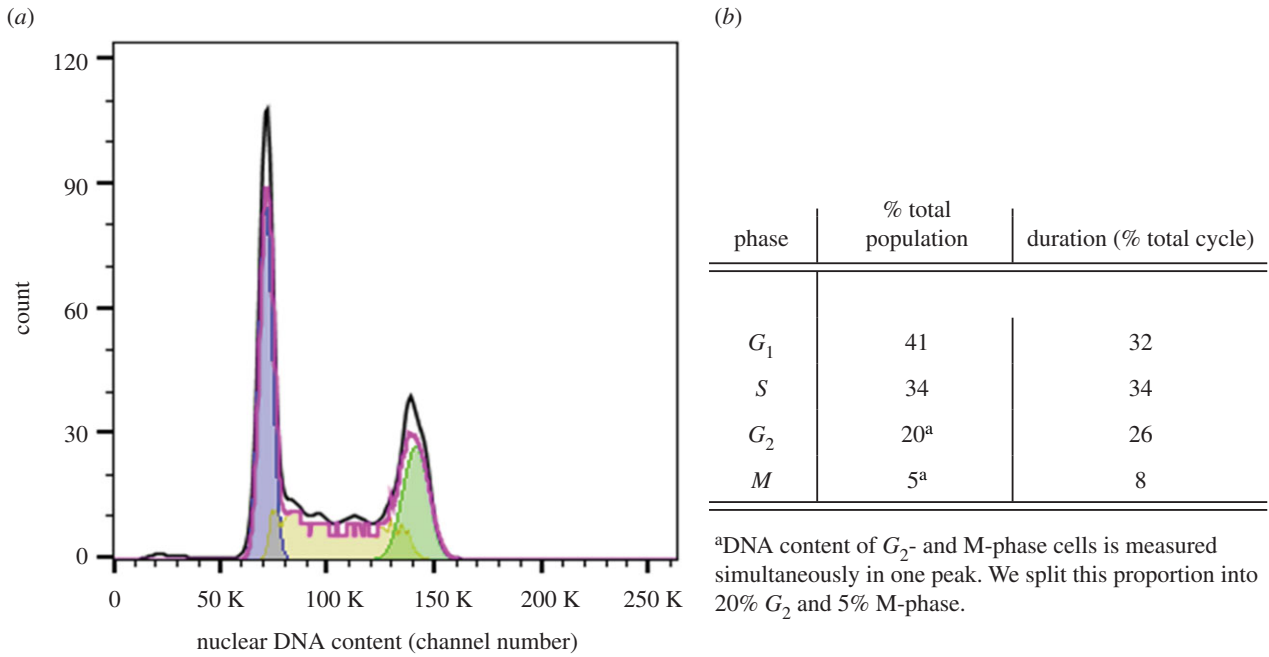
### 3.1. Model calibration

#### 3.1.1. Cell-cycle distribution and growth

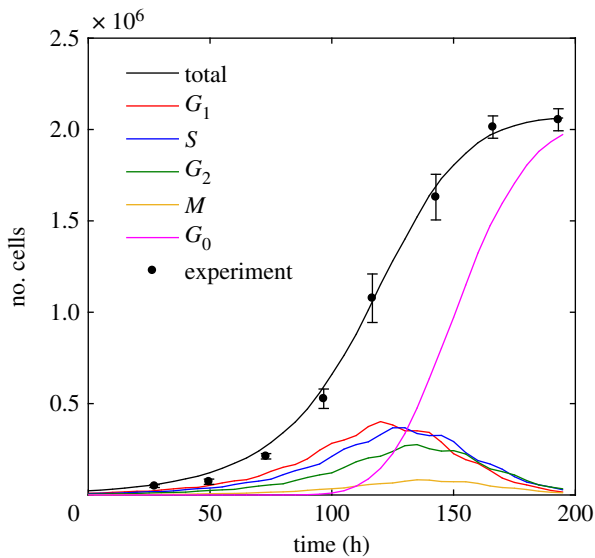
The simulation framework was first calibrated to model the growth and treatment response of the colorectal carcinoma cell line HCT116. Cellular growth curves were used to determine cell doubling time and voxel size, while flow cytometry was used to obtain information about the cell-cycle distribution.

Figure 3 shows the resulting histogram of the cellular DNA content separated into  $G_1$ ,  $S$  and  $G_2/M$  phase, as well as a table of the percentage of cells in, and duration of, each cycle phase. As flow cytometry cannot distinguish between cells in M- or  $G_2$ -phase (because they have the same DNA content), it was assumed that the 25% of cells in both phases is split into 20%  $G_2$ -, and 5% M-phase.

Figure 4 shows the corresponding growth curve for  $2.3 \times 10^4$  cells seeded in a 24-well plate (15.6 mm well diameter) along with the calibrated simulation. Data points and error bars correspond to mean and standard deviation values from three replicates of a single experiment. An average doubling time of  $19.5 \pm 1$  h was measured for HCT116 cells. A good simulation of the growth curve plateau was obtained for voxel sizes of  $9.6 \times 9.6 \mu\text{m}^2$  and  $12 \times 12 \mu\text{m}^2$  if cells in 24-well or six-well



**Figure 3.** (a) Histogram of the cellular DNA content obtained by flow cytometry. From a fit of the experimental data using the Watson pragmatic model, the proportions of singlets corresponding to cells in  $G_1$ -phase (first peak, purple), cells in the process of reproducing their DNA in S-phase (middle part, yellow), and doublets corresponding to cells in  $G_2$ - or M-phase are determined (second peak, green). The experimental data (black) and the model fit (pink) are shown. (b) Table of cell-cycle distribution, and cycle stage duration as obtained by flow cytometry analysis of untreated HCT116 cells. (Online version in colour.)



**Figure 4.** Simulated and experimentally determined growth curves for untreated HCT116 cells in 24-well plates;  $2.3 \times 10^4$  cells with a doubling time of 19.5 h on a 15.6 mm diameter circular two-dimensional grid (corresponding to a diameter of 1625 voxels) were simulated using the cell-cycle distribution information given in figure 3. The experimental data points (black circles, means and standard deviations), as well as the simulated total cell numbers and simulated contributions from the different cell-cycle stages (solid lines) are shown.

plates were simulated. Differences in voxel size determined from the plateau cell density in the two well types may be due to changes in nutrient medium volume-to-surface-ratios, as well as to variations in frequency of medium change for different samples.

### 3.1.2. Treatment response

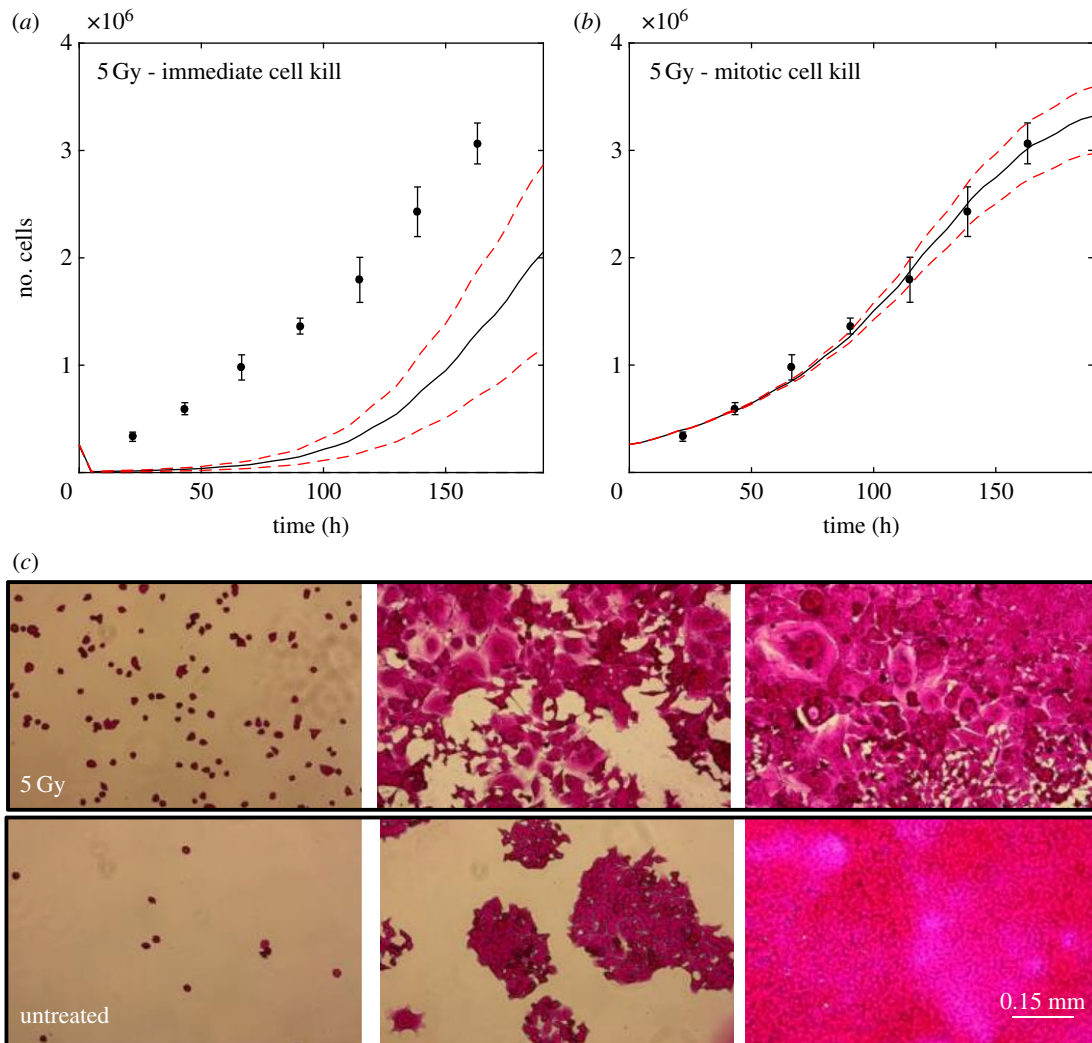
The simulation is first adapted to match the growth of HCT116 cells irradiated with 5 Gy. This was achieved by

adjusting the exponent  $k_{\text{delay}}$ , and the probability  $p_{\text{mitoticCat}}$  that characterize the distribution of delay times to cell death, and the probability of undergoing mitotic catastrophe after radiation treatments. Figure 5*a,b* shows the resulting growth of  $2.6 \times 10^5$  irradiated cells seeded in a six-well plate with the corresponding simulation assuming (a) instantaneous cell kill or (b) controlled delayed cell kill via mitotic catastrophe using  $k_{\text{delay}} = 0.009 \text{ h}^{-1}$ , and  $p_{\text{mitoticCat}} = 0.2$ . Neither  $p_{\text{senescence}}$  nor  $\gamma$  significantly changed the simulation result for these conditions. The probability of cellular senescence,  $p_{\text{senescence}}$ , was fixed at a value of 5% since we have assumed a small contribution from senescent cells. The sensitivity between different cycle stages was assumed to be a constant ratio of 1.5, meaning that surviving fractions  $S_{\text{phase}}$  differ by powers of 1.5 relative to each other:  $S_S = 1.5 \cdot S_{G1} = 1.5^2 \cdot S_{G2} = 1.5^3 \cdot S_M$ . This corresponds to factors,  $\gamma$ , ranging from 0.85 (least sensitive, S-phase) to 1.39 (most sensitive, M-phase).

It is clear that a simulation which assumes instantaneous cell death would greatly underestimate the total number of cells, whereas *in vitro* and *in silico* experiments are in very good agreement within the boundaries of the 95% confidence intervals of the calculated surviving fraction ( $S_{5\text{Gy}} = 0.04(0.03,0.05)$ ) when delayed cell kill is assumed. Photographs of fixed, irradiated and untreated cells at three different growth stages (initially seeded, subconfluent (96 h) and confluent wells (144 h)) are shown in figure 5*c*. In the irradiated samples, giant cells are clearly visible at the subconfluent, and confluent stages.

## 3.2. Model validation and application

HCT116 growth curves for heated (5 min at 46°C), irradiated (2 Gy, 5 × 2 Gy, 5 × 3 Gy), and combination treated cells (2 Gy irradiation, and heating for 5 min at 46°C) are simulated and compared to the corresponding experimental growth

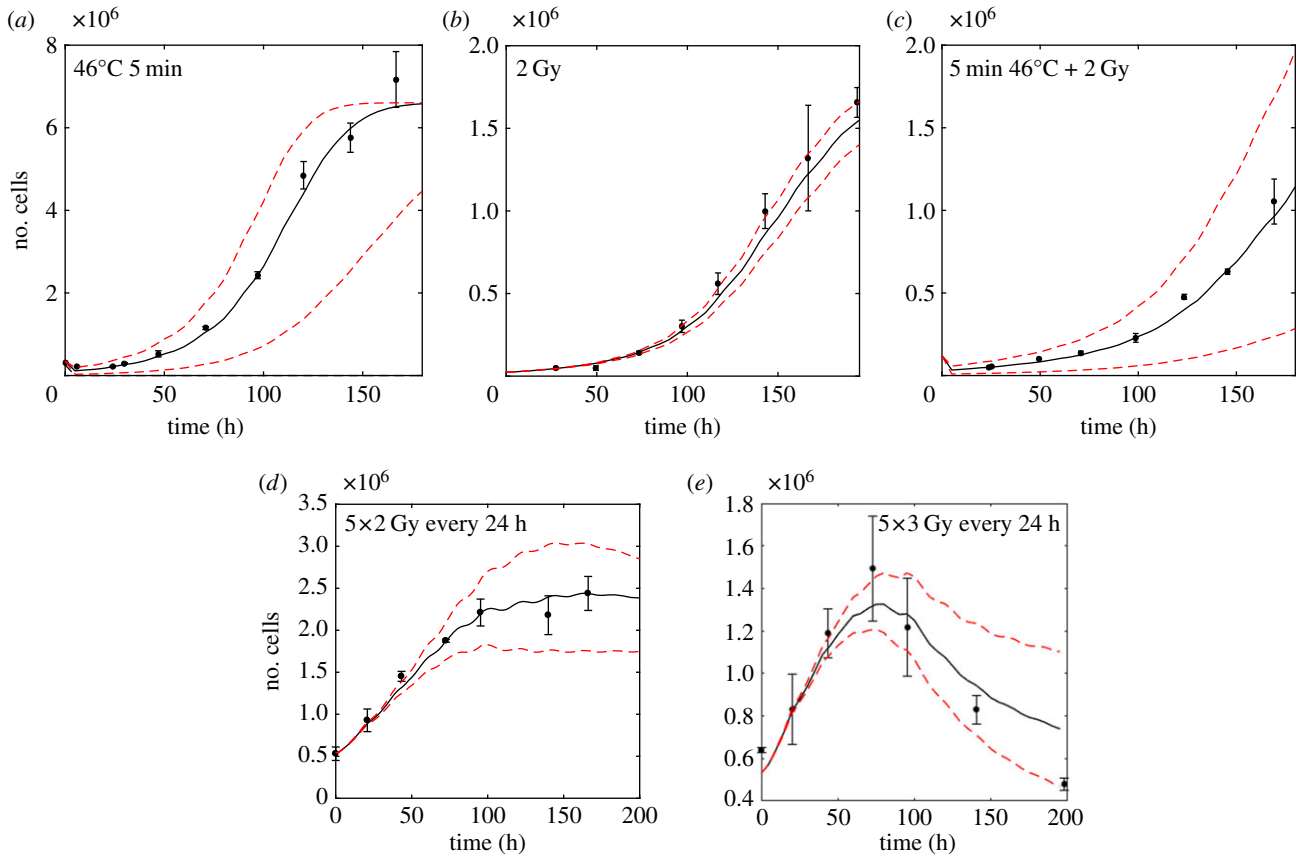


**Figure 5.** Calibrated simulation of a growth curve of  $2.6 \times 10^5$  irradiated (5 Gy) HCT116 cells seeded in six-well plates with a diameter of 34.8 mm (corresponding to a grid diameter of 2900 voxels). The experimental data points (black circles) are shown, as well as the simulated total cell numbers (solid lines) together with simulation of the 95% confidence bounds of the surviving fractions used (dashed lines,  $S_{5\text{Gy}} = 0.03$  (0.02, 0.04)). (a) Simulation assuming instantaneous cell kill greatly underestimated the total number of cells. (b) Simulation assuming controlled delayed cell kill via mitotic catastrophe was successfully calibrated to match the experimental data. (c) Photographs of fixed irradiated, and untreated cells at three different growth stages (initially seeded, sub-confluent (96 h) and confluent wells (144 h)). The pink stain corresponds to cellular protein stained by sulforhodamine B. A change in morphology from normal phenotype to a mixture of normal and aneuploid cells is seen for irradiated cells.

curves (figure 6). The calculated surviving fractions are shown with 95% confidence intervals:  $S_{2\text{Gy}} = 0.31$  (0.25, 0.37),  $S_{3\text{Gy}} = 0.15$  (0.10, 0.20),  $S_{5\text{ min}, 46\text{C}} = 0.26$  (0.07, 0.44),  $S_{2\text{Gy}+5\text{ min}, 46\text{C}} = 0.03$  (0.01, 0.05). For all treatment scenarios, simulation and experimental data are in good agreement. Although there seems to be a small offset between simulated and measured growth curves for cells treated with 2 Gy in a single fraction, this may be explained by a small deviation of the experimental surviving fraction from the average surviving fraction calculated by the AlphaR model. However, the experimental result lies well within the 95% confidence bounds of the predicted growth curves. In particular, for fractionated treatments, the overall shape of the growth response curve is well described for both 2 and 3 Gy fractions. Having shown that the simulation framework accurately predicts different homogeneous irradiation and heat treatments, it can now be used, for example, to predict the growth response to different fractionation combinations of radiation and heat. Since the simulation uses a stochastic succession of events, the average and standard deviations of 500 runs are taken

for each simulated treatment course. Figure 7 shows the influence of choosing a different time point for heat application within the overall treatment schedule involving 30 fractions of 2 Gy radiation in combination with a single combined treatment (thermal dose of 40 CEM43). Depending on the time of adding the heat fraction, the overall treatment success in terms of time until tumour regrowth may be changed slightly due to the alterations in the proportions of quiescent and proliferating cells. Based on this observation, this simulation framework may help to identify the best treatment order for RHT therapies for different proportions of proliferating and quiescent cells at treatment onset.

We also demonstrate that using instantaneous rather than delayed cell killing in response to RT may change the overall treatment outcome prediction of fractionated RT treatments alone (figure 7b) due to different numbers of regrowing cells in the two simulations. If instantaneous cell kill is considered, more space is available to allow cell division compared with the delayed cell kill simulation, where more cells remain quiescent for a longer period of time.



**Figure 6.** Comparison of experimental and simulated growth curves for HCT116 cells treated with different modalities: (a) heating at 46°C for 5 min ( $S_{5 \text{ min}, 46^\circ\text{C}} = 0.26$  (0.07, 0.44)),  $3 \times 10^5$  cells seeded in six-well plates. (b) 2 Gy radiation ( $S_{2\text{Gy}} = 0.31$  (0.25, 0.37)),  $2.4 \times 10^4$  cells seeded in 24-well plates. (c) Combination of 2 Gy radiation and heating for 5 min at 46°C ( $S_{2\text{Gy}+5 \text{ min}, 46^\circ\text{C}} = 0.03$  (0.01, 0.05)),  $1.2 \times 10^5$  cells seeded in six-well plates. (d) Five fractions of 2 Gy radiation given every 24 h ( $S_{2\text{Gy}} = 0.31$  (0.25, 0.37)),  $5.4 \times 10^5$  cells seeded in six-well plates. (e) Five 3 Gy fractions of radiation given every 24 h ( $S_{3\text{Gy}} = 0.15$  (0.11, 0.19)),  $5.4 \times 10^5$  cells seeded in six-well plates. Cells were simulated as having a mean doubling time of 19.5 h. The experimental data points (black circles, means and standard deviations) are shown, as well as the simulated total cell numbers (solid lines) and simulation of the 95% confidence bounds of the surviving fractions used (dashed lines). (Online version in colour.)

## 4. Discussion

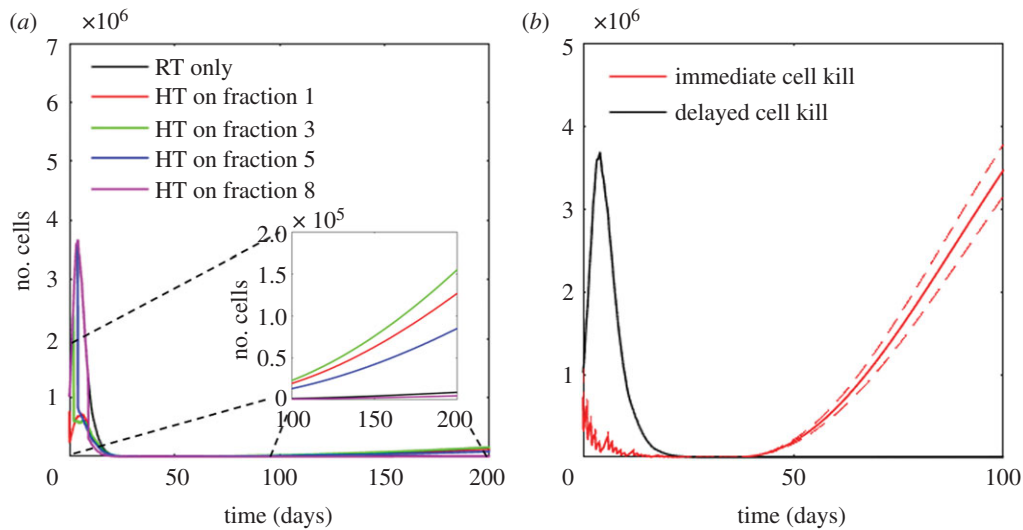
The cellular automaton model presented provides flexibility for application to the study of a number of different situations, both *in vivo* and *in vitro*. We have successfully calibrated the model for single and multimodality therapies of heat and ionizing radiation and could accurately predict treatment response for one particular cell line. This was achieved by introducing a delay before cell death, rather than solely instantaneous death, to describe the cellular response to irradiation. This is an important difference between our, and previous [27], implementations.

Cellular growth curves offer the possibility of testing the simulation in terms of the dynamic development of a treated population over time, rather than providing an absolute surviving fraction only at the fixed time point post treatment provided by clonogenic assays. Since most cell survival models, such as the AlphaR or the LQ, are based on clonogenic cell survival data, they predict the long-term surviving fraction, but cannot give any information on how the population develops towards this endpoint. Growth curves, on the other hand, provide dynamic information, but it can be difficult to extrapolate from them to the overall surviving fraction. Therefore, a combination of surviving fraction, as measured by clonogenic assays, and growth curve data captures a more complete picture. It is, however, difficult to measure cell growth within the first few hours after

cell seeding due to the lag between cell seeding, their attachment and exponential growth. Although there might well be differences in the lag time of treated and untreated cells, all experiments have here been allocated a constant lag period of 2 h, resulting in slight differences between experiment and simulation during the initial growth phase. While correct modelling of the initial growth phase may be difficult due to this lag time, the exponential and plateau phase of growth curves are accessible for model calibration. However, the plateau cell density depends strongly on the nutrients provided, i.e. the frequency of medium renewal and its overall volume. When fresh medium is continuously provided, cells in a confluent layer may continue to grow. These new cells may attach on top of other cells. As only a perfect monolayer of virtual cells of rigorously controlled size and shape is considered in this simulation, the voxel size used must be carefully adapted to the properties of the dishes. Although the voxel size, and therefore the maximum number of cells per well may be of importance for simulating fully confluent cells *in vitro*, the effects may be less important for tumours *in vivo*.

Figures 5 and 7b show that it is essential to consider the impact of delayed reproductive cell death, because instantaneous cell death greatly underestimates the number of living cells during the first days after treatment. This may influence simulation results, e.g. when studying the effects of tissue reoxygenation and tumour growth response, since immediate removal of all dying cells would allow faster





**Figure 7.** (a) Simulation results of fractionated treatments using 30 fractions of 2 Gy, of which one fraction is given in combination with a thermal dose treatment of 40 CEM43 at different days within the overall treatment period as indicated by the legend ( $5 \times 10^6$  cells initially). The means of 500 simulation runs are shown. Inset: expanded view of the population growth 100–200 days post treatment. Although the overall delivered radiation and thermal doses are the same, depending on the combination of the treatment fractions, the biological response may vary. (b) Fractionated RT treatment of 30 fractions of 2 Gy simulated using delayed (black lines) or instantaneous (red lines) cell kill ( $1 \times 10^6$  cells initially). Treatment was delivered 5 days a week, Monday to Friday, over a time course of 30 days. The means (solid lines) and standard deviations (dashed lines) of 500 simulation runs are shown. Whereas a simulation using delayed cell kill modelling predicts complete cell killing, a simulation that assumes immediate cell death would predict tumour regrowth.

repopulation and enhanced reoxygenation of the tumour compared to delayed cell kill simulations. For long-term studies of single treatment fractions, these delayed effects should be negligible since the surviving population will eventually provide the majority of proliferating cells. The parameters used to describe the dynamics of delayed cell kill ( $k_{\text{delay}}$ ,  $p_{\text{mitoticCat}}$  and  $p_{\text{senescence}}$ ) have here been customized to fit the data from HCT116 cells. Although it might be possible that some, or all, of these parameters are similar for other cell types, their accurate modelling would require re-calibration of these parameters.

The calculation of surviving fractions strongly depends on the biological model parameters used, i.e.  $\alpha_0$ ,  $\alpha_R$  and  $\beta$ , in the case of the AlphaR model. These parameters are subject to relatively large uncertainties and individual experiments often deviate from the predicted average surviving fraction. This may be a feature of clonogenic assays, which are very sensitive to experimental error (e.g. from cell counting and pipetting uncertainties), and strongly depend on the experimental conditions, such as incubation time, cell-cycle distribution and density, and cell health in general. This results in relatively large intra- and inter-experimental differences, leading to the large reported confidence bounds of the surviving fractions for HT and combination treatments.

All biological results presented were obtained for a commercially available human cancer cell line. As all reference experiments were performed by us on the same batch of cells, rather than using previously published data from a number of sources, our calibration benefits from a consistent dataset, which is immune to errors arising from differences in experimental techniques between different laboratories. Based on the current results, simulations of other cell types may either be calibrated using the techniques presented here, or a sensitivity analysis of the parameters used could be performed to understand the importance of individual parameters on the overall simulation outcome (see electronic supplementary material, appendix A). This would allow

study of the effects of heterogeneous cell populations such as seen in tumours *in vivo*.

Although the model provides good predictions within the calibrated dose range, it should be stressed that doses outside the range of standard therapies, in particular ablative thermal doses and large single fraction RT treatments, have not yet been studied, and may be subject to different cellular response mechanisms which are not captured by this implementation. Also, a number of other parameters that influence the overall cell surviving fraction, e.g. the irradiation RT dose rate or time interval between HT and RT treatments, are not yet included. A recent publication by van Leeuwen *et al.* [38] touched on this discussion and proposed an exponentially decaying influence of heat-induced radiosensitization as a function of time between HT and RT application. However, there is ongoing discussion concerning the decay rate of heat-induced radiosensitization which is considered to be cell line dependent, and may be greatly influenced by physiological factors such as blood flow leading to different parameter estimations between *in vivo* and *in vitro* applications even for the same tumour type. Van Leeuwen *et al.* recommended using a decay rate of the order of 2 h. Since in our simulation, RT and HT are considered to be given simultaneously, and consecutive radiation fractions are given at least 24 h apart from one another, we believe that our results remain valid, given we have included no time factor in the framework at this stage. Further experimental validation would be required if more complex heating and radiation schedules using shorter time intervals between treatment fractions, or longer time gaps between heat and radiation application, are of interest.

One particularly interesting application of the model is, therefore, the verification of the thermal dose concept for temperatures exceeding 48°C. Owing to the exponential relation of thermal dose on treatment temperature, even small deviations from the proposed mathematical descriptions translate into large differences in thermal dose and

cell survival in this temperature range. With uniform heating approaches, it is impossible to verify the thermal dose concept for very high temperatures accurately, since thermal dose uncertainties originating from heating and cooling gradients are difficult to account for in such cases. The proposed framework can be applied to the simulation of different cell distributions in order to calculate an overall probability for the expected cell survival.

Moreover, while the combination of focused ultrasound mediated heating [39,40] with RT provides a promising approach on paper, it is difficult to verify experimentally at a cellular level. For treatment and experiment planning, as well as for determining effective dose and exposure prescriptions, it is essential to first quantify the biological effects at a cellular level. Systems oncology simulations may provide a very useful tool for analysis of the effects of different, inhomogeneous (in space and time) heat and radiation distributions, for which the averaged cell surviving fractions for a subset of carefully selected scenarios can be verified experimentally. The simulation framework presented here was designed specifically for such applications. It is possible to simulate the whole experimental procedure of an *in vitro* focused ultrasound experiment, as well as to analyse the expected overall treatment response of the cell population.

## 5. Conclusion

We have demonstrated a cellular automaton model that is suitable for accurate modelling of the dynamic response to separate, or combined, heat and RT treatments. The inclusion

of delayed rather than instantaneous, cell kill after irradiation may impact on simulations which aim to study the effects of reoxygenation and tumour progression, and should therefore be taken into account. We have presented a simple implementation for enabling such modelling, and verified our framework against a consistent experimental dataset thus making this simulation framework a reliable basis for future applications where the effects and optimized treatment protocols for combination treatments *in vivo* are studied.

**Data accessibility.** The code for the framework is part of an ongoing PhD project, which will rely on its further development of the code. Making the code publicly available is an unacceptable risk to the novelty of the students project but we can provide copies to individuals upon request.

**Authors' contributions.** S.B. performed the majority of experiments, data analysis and model implementation, as well as drafting the article. G.P. assisted and advised on the model implementation. P.Z. helped in optimizing the simulation framework for a computationally effective implementation. J.I. conducted part of the biological experiments. G.P., M.C., I.R., S.N., U.O. and G.t.H. supervised the study and provided critical revision of the manuscript.

**Competing interests.** We declare we have no competing interests.

**Funding.** This work was financially supported by Cancer Research UK. Research at The Institute of Cancer Research is supported by Cancer Research UK under Programme C33589/A19727. P.Z. is supported by Cancer Research UK under Programme C33589/A19908. We thank the Focused Ultrasound Foundation for funding the work of Jannat Ijaz and Ian Rivens.

**Acknowledgements.** The authors thank Yuen-Li Chung for providing HCT116 cells. We acknowledge NHS funding to the NIHR Biomedical Research Centre at The Royal Marsden and The Institute of Cancer Research.

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