


 Cite this: *RSC Adv.*, 2021, 11, 28643

# Fabrication of patterned calcium carbonate materials through template-assisted microbially induced calcium carbonate precipitation†

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Patterned calcium carbonate materials with controlled morphologies have broad applications in both environmental and engineering fields. However, how to fabricate such materials through environmental-friendly methods under ambient conditions is still challenging. Here, we report a green approach for fabricating patterned calcium carbonate materials. This eco-friendly approach is based on template-assisted microbially induced calcium carbonate precipitation. As a proof of concept, by varying the templates and optimizing fabrication parameters, different patterned calcium carbonate materials were obtained. The optimized parameters include  $C_{Ca^{2+}} = 80$  mM,  $T_i = 15$  °C, and templates made of small-sized  $CaCO_3$  particles with a concentration of  $1.5$  mg mL<sup>-1</sup>, under which better and more sharp patterns were obtained. Materials with periodic patterns were also fabricated through a periodic template, showing good scalability of this approach. The results of this study could mean great potential in applications where spatially controlled calcium carbonate depositions with user-designed patterns are needed.

 Received 25th May 2021  
 Accepted 18th August 2021

DOI: 10.1039/d1ra04072c

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## Introduction

Calcium carbonate is one of the most abundant biominerals in nature,<sup>1</sup> and has broad technological applications, for example, as coating materials in fabricating light-weight ceramics and catalysis support materials,<sup>2</sup> as well as bone-regeneration materials for biomedical implants.<sup>3</sup> For such applications, the techniques to deposit directly the patterned calcium carbonate films with controlled morphologies through environmental-friendly methods under ambient conditions are ideal and in high demand.

For chemical synthesis of patterned calcium carbonate materials, techniques based on templated organic surfaces such as Langmuir monolayers,<sup>4–6</sup> self-assembled monolayers (SAMs)<sup>7–11</sup> and polyelectrolyte multilayer film<sup>12</sup> *etc.*, have been developed. Particularly, the SAM method has been shown to be able to form ordered ceramic films with a high spatial resolution and controllable crystal morphologies.<sup>8–11</sup> Compared with such chemical synthesis methods, techniques based on

microbially induced calcium carbonate precipitation (MICP)<sup>13,14</sup> are green and eco-friendly, and they are performed under ambient conditions. Thus, fabrication of calcium carbonate through MICP techniques is a promising way to meet the increasingly high requirement of aforementioned applications.

MICP is a common phenomenon in nature observed in a variety of microorganisms including the urease producer bacterium – *Sporosarcina pasteurii* (*S. pasteurii*),<sup>15–18</sup> which can be performed by ureolysis<sup>19</sup> or by denitrification.<sup>20</sup> Ureolytic MICP<sup>13</sup> is one of the widely used environmental-friendly biomineralization techniques due to its simple hydrolysis mechanism and high reaction activity. Many studies on MICP have been focused on polymorphs of precipitated calcium carbonates and the dependence of MICP activities on environmental factors such as pH, temperature, and calcium concentrations *etc.*<sup>21–28</sup> However, compared with the aforementioned abundant reports on chemically synthesis of patterned calcium carbonate materials, there has been no study, to the best of our knowledge, reported on the fine spatial control of calcium carbonate precipitation during MICP, which is the key for applying MICP techniques into the fabrication of patterned calcium carbonate materials.

In an earlier work,<sup>29</sup> Zhang *et al.* observed that  $CaCO_3$  particles obtained from precipitation in previous MICP runs can act as nucleating sites to support the growth of newly precipitated calcium carbonate in fresh MICP runs. Inspired by this observation, in this work, we reported an approach for the fabrication of patterned calcium carbonate materials using the MICP technique *via* heterogenous template-promoted

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† Electronic supplementary information (ESI) available. See DOI: 10.1039/d1ra04072c

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precipitation. The aim of this study is to show whether and how  $\text{CaCO}_3$  particles can be used to pattern MICP precipitations. The templates were formed by  $\text{CaCO}_3$  particles obtained from MICP precipitates, which resulted in a promoted growth of calcium carbonate on templated regions when they were immersed in MICP cultures. Such promoted growth finally led to patterned calcium carbonate materials whose spatial distribution on the substrate is governed by the template patterns. The MICP process was also optimized by tuning environmental factors such as the concentration and size of  $\text{CaCO}_3$  particles used for making templates,  $\text{Ca}^{2+}$  concentration and cultural temperature.

## Results

### Fabrication of patterned $\text{CaCO}_3$ through template-assisted MICP

To test whether the spatial distribution of MICP can be controlled through a template consisting of  $\text{CaCO}_3$  precipitates, we first patterned the bottom glass surface of a Petri dish using colloidal suspensions consisting of precipitates collected from MICP process (Fig. 1(a), see Methods and ESI† for more details). After the pattern had been air-dried and UV-sterilized, fresh liquid culture of *S. pasteurii* containing urea was filled into the dish. As bacterial cells grew and multiplied, MICP process was continued, during which urea was hydrolyzed by urease produced by cells to generate ammonium and carbonate ions, which led to an increased pH in the local environment. The rise in pH then induced the precipitation of  $\text{CaCO}_3$  in the presence

of  $\text{Ca}^{2+}$ . After 48 h-incubation, a clear pattern having the same shape as the template but with a more solid and bolded appearance formed. Fig. 1(b) shows a disk pattern from a disk template. Different spatial patterns can also be obtained using different designed templates (see one example in Fig. S1†). A quantitative measurement of the surface density of  $\text{CaCO}_3$  precipitates,  $\rho_s$ , along the radial direction shows that  $\rho_s$  is over five times higher at the template region than at the template-free region (Fig. 1(c)), implying that there is much more accumulation of precipitates over the template than other places. This preferred precipitation at the template region also causes  $\rho_s$  of the template-free region to be even lower than that when there is no template used in control samples under otherwise same conditions. Together, these results clearly demonstrate the successful control of the spatial distribution of MICP through a template-based approach.

### $\text{CaCO}_3$ is the main component of the template responsible for the preferred MICP on template

The XPS measurement of precipitates used for making the template shows that besides Ca, C and O, N and P are also detected (Fig. 2(a)). Such elements are most likely from bacteria associated sources. To determine the main component of the template that is responsible for its promoting effect for MICP, we first checked the role of organic materials contained in precipitates. Using both pure heat-killed *S. pasteurii* cells and heat-treated MICP-induced  $\text{CaCO}_3$  particles (to burn out the possible attached organic materials on particles, if they have) as template materials, we repeated the above experiments of MICP

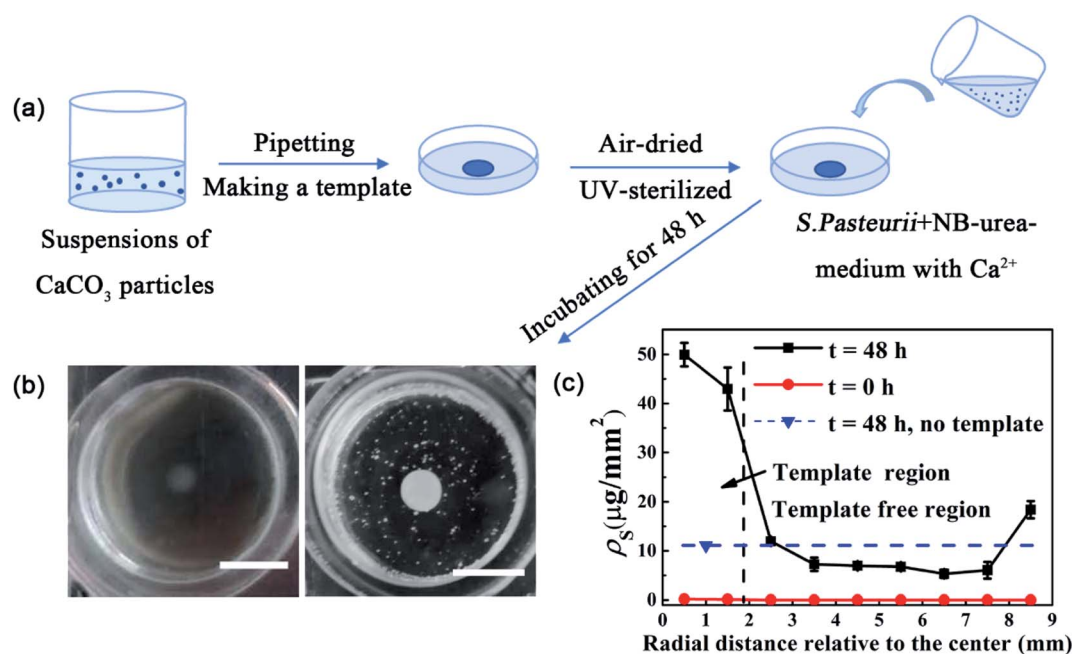


Fig. 1 Schematic illustration of the fabrication of patterned MICP through a template-based approach. (a) Scheme of the approach. (b) Photographs of a templated (disk-shape) glass surface at  $t = 0$  h and  $t = 48$  h after incubated in bacterial culture. The disk-shaped template is made of a suspension of MICP-induced  $\text{CaCO}_3$  particles with a concentration of  $1.5 \text{ mg mL}^{-1}$ . Scale bars are 6 mm. (c) The surface density of  $\text{CaCO}_3$  precipitates,  $\rho_s$ , along the radial direction. The rise at the largest radius is likely due to the boundary effect of container walls. Error bars show the standard deviations from three repeats.

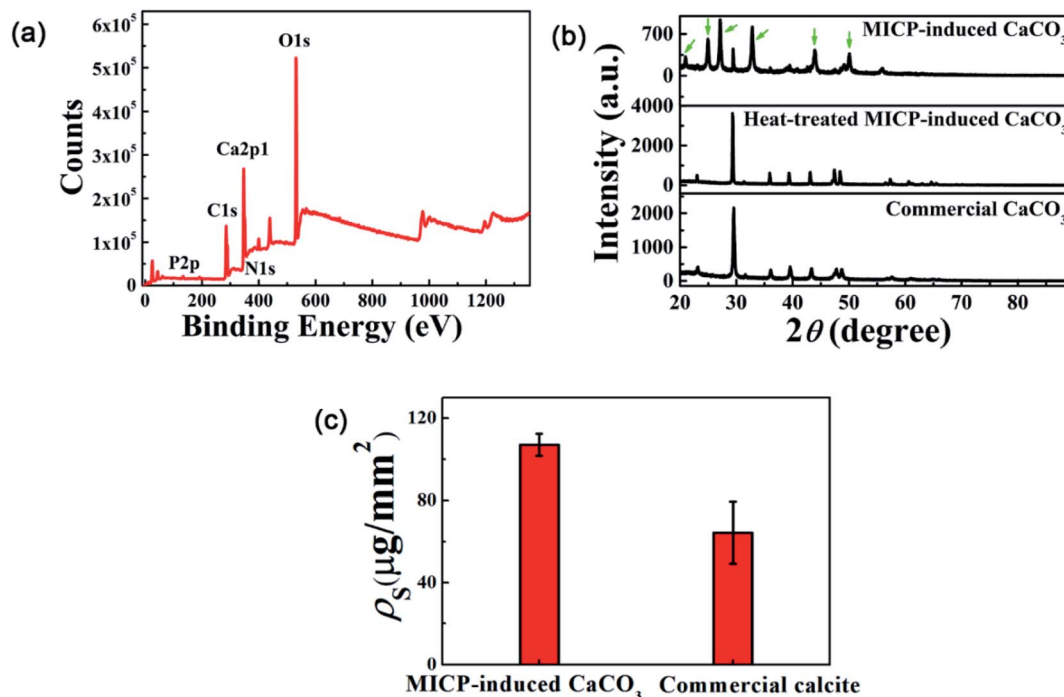


Fig. 2 Characterization of MICP precipitates. (a) XPS measurement of MICP-induced CaCO<sub>3</sub> particles. (b) XRD measurements of three types of CaCO<sub>3</sub> particles used in the study, including MICP-induced (green arrows point to characteristic peaks of vaterite, and the other peaks are for calcite), heat-treated MICP-induced, and commercial CaCO<sub>3</sub> particles. (c)  $\rho_s$  after 48 h incubation. Error bars show the standard deviations from three repeats.

precipitation on templated glass surfaces. The results show a preferred deposition of MICP at the template region for the latter case but not for the former case (Fig. S2(a), (e), (c) and (g)†), which excludes the possibility of the organic material contained in the template to be the main factor for the resulted preferential deposition of MICP. To see whether the negative-charged surface can lead to such phenomena, sulfonic group modified polystyrene (PS) particles having negative-charged surfaces, were also tested as a template, and no preferential deposition of MICP was observed (Fig. S2(b) and (f)†). This result agrees with observations in an earlier report.<sup>29</sup> Next, we used commercial CaCO<sub>3</sub> particles to make a template, and the preferred growth of precipitates at the template region was again observed (Fig. S2(d) and (h)†). Taken together, these results show that CaCO<sub>3</sub> of the template is the key ingredient responsible for the preferred deposition of MICP at the template region.

CaCO<sub>3</sub> has three different types of crystal structures, which are vaterite, calcite and aragonite.<sup>30</sup> The XRD measurements of the MICP-induced CaCO<sub>3</sub> particles show characteristic peaks of both calcite and vaterite with higher intensity peaks of vaterite than calcite (green arrows in Fig. 2(b)), indicating that MICP-induced CaCO<sub>3</sub> particles used in this study are mostly vaterite but also contain a less amount of calcite. By contrast, heat-treated MICP-induced CaCO<sub>3</sub> particles, show only peaks of calcite, same as commercial CaCO<sub>3</sub> particles do (Fig. 2(b)). This result consists with a previous report that vaterite is not stable and easily transformed into calcite at high temperature.<sup>31</sup> Interestingly, by making two templates side by side on the same

glass surface, which are made of MICP-induced and commercial CaCO<sub>3</sub> particles, respectively, the results show that the pattern formed at the former template region is much denser and clearer than that at the latter one (Fig. S3†), indicating that vaterite may have a stronger promoting effect for the deposition of MICP than calcite does. Such difference in the promoting effect of template can be seen more clearly from  $\rho_s$  measurements, which show that  $\rho_s$  of the template of MICP-induced CaCO<sub>3</sub> particles is about 1.7 times as big as that of the one formed by commercial CaCO<sub>3</sub> particles (Fig. 2(c) and S4†). In the following text, if not specified otherwise, the template is made of MICP-induced CaCO<sub>3</sub> particles.

### Parameter optimization

To improve the promoting efficiency of template for MICP, several parameters including the concentration of calcium ions  $C_{Ca^{2+}}$ , incubation temperature  $T_i$ , as well as the properties of template,<sup>27,28</sup> were optimized. The results are shown in Fig. 3. We can see that  $\rho_s$  first increases with  $C_{Ca^{2+}}$  and then reaches a plateau when  $C_{Ca^{2+}} > 80$  mM under our conditions (Fig. 3(a)). MICP process is highly influenced by cultural temperature, and lowering temperature would decrease the urease activities,<sup>23</sup> which has also been confirmed in this study (Fig. S5†). However, under our conditions, we find that  $\rho_s$  first increases as  $T_i$  decreases from 30 °C to 15 °C and then decreases as  $T_i$  continues to drop down to 10 °C (Fig. 3(b), also see Fig. S6† for typical images obtained at different  $T_i$ ). Since the template acts as growth sites for MICP process,  $\rho_s$  will also depend on the

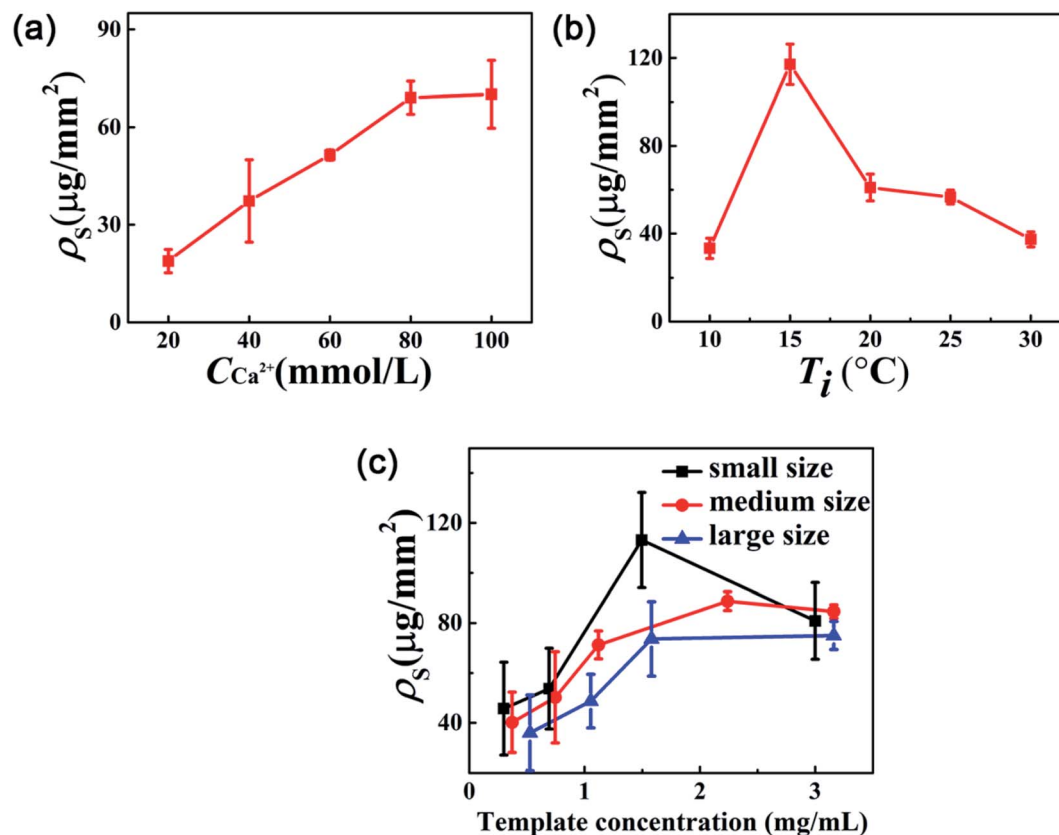


Fig. 3 Optimization of the fabrication parameters. Template promoting efficiency changes with (a)  $\text{Ca}^{2+}$  concentration (with small-sized  $\text{CaCO}_3$  particles), (b) cultural temperature (with small-sized  $\text{CaCO}_3$  particles), and (c) template concentration for different sized  $\text{CaCO}_3$  particles. Error bars show the standard deviations from three repeats.

properties of template. Fig. 3(c) shows the measured  $\rho_s$  vs. the template concentration (*i.e.*, the mass concentration of  $\text{CaCO}_3$  particles used to make templates) at  $15\text{ }^{\circ}\text{C}$ . Three different sized MICP-induced  $\text{CaCO}_3$  particles were tested, which have a size distribution peaked at  $\sim 1\text{ }\mu\text{m}$  (small-size),  $4.5\text{ }\mu\text{m}$  (medium-size), and  $6\text{ }\mu\text{m}$  (large-size) (Fig. S7†), respectively. From the figure, we can see that for each sized  $\text{CaCO}_3$  particles,  $\rho_s$  first increases relatively rapidly with the template concentration and then changes gradually when the concentration is higher than  $1.5\text{ mg mL}^{-1}$ . Moreover, by comparing the  $\rho_s$  of the small-size ( $\rho_s^{\text{small}}$ ), medium-size ( $\rho_s^{\text{medium}}$ ), and large-size ( $\rho_s^{\text{large}}$ )  $\text{CaCO}_3$  particles, we can see that before  $1.5\text{ mg mL}^{-1}$ ,  $\rho_s$  at the same mass concentration of  $\text{CaCO}_3$  particles shows a trend of  $\rho_s^{\text{small}} > \rho_s^{\text{medium}} > \rho_s^{\text{large}}$ , *i.e.*,  $\rho_s$  decreases with the size of  $\text{CaCO}_3$  particles. The observed dependence of  $\rho_s$  on the template concentration can be understood in terms of the exposed surface areas of  $\text{CaCO}_3$  particles. When the template concentration increases from a very dilute value, the total exposed surface area of  $\text{CaCO}_3$  particles in the template also increases, *i.e.*, there are more available growth sites, which then leads to a higher promoting efficiency of the template. But after the template concentration reaches to a value (about  $1.5\text{ mg mL}^{-1}$  under our conditions) where the whole template region is fully covered by a monolayer of  $\text{CaCO}_3$  particles, the total exposed surface area of  $\text{CaCO}_3$  particles would be saturated, and thus the deposition density roughly reaches a plateau. Similarly,

one may also imagine that by reducing the size of  $\text{CaCO}_3$  particles, the total exposed surface area of these particles can also be increased given the same total mass of particles, therefore,  $\rho_s$  would increase when smaller sized  $\text{CaCO}_3$  particles are used, which are exactly what we observed in the experiments.

By employing these optimized conditions, *i.e.*, when  $\text{Ca}^{2+} = 80\text{ mM}$ ,  $T_i = 15\text{ }^{\circ}\text{C}$ , and using the template made of small-sized  $\text{CaCO}_3$  particles with a concentration of  $1.5\text{ mg mL}^{-1}$ , better patterns were obtained (Fig. 4), which display more sharpened edges and have higher contrast with the non-template region than the pattern shown in Fig. 1 (or Fig. S1†) which was formed under non-optimized conditions. Moreover, by employing a template array of disks, a periodically patterned  $\text{CaCO}_3$  material was successfully fabricated (see one example of  $4 \times 4$  array in Fig. 4), indicating the scalability of this method in fabricating large-scale  $\text{CaCO}_3$  materials with controlled spatial arrangement.

## Discussion

For successfully patterned MICP precipitation at the template region, it is ideal to have promoted heterogeneous nucleation and growth at the template region but suppressed homogeneous nucleation in solution. According to classical crystallization theories,<sup>32–34</sup> the free energy for formation of stable nuclei ( $\Delta G$ ) at an interface can be expressed as

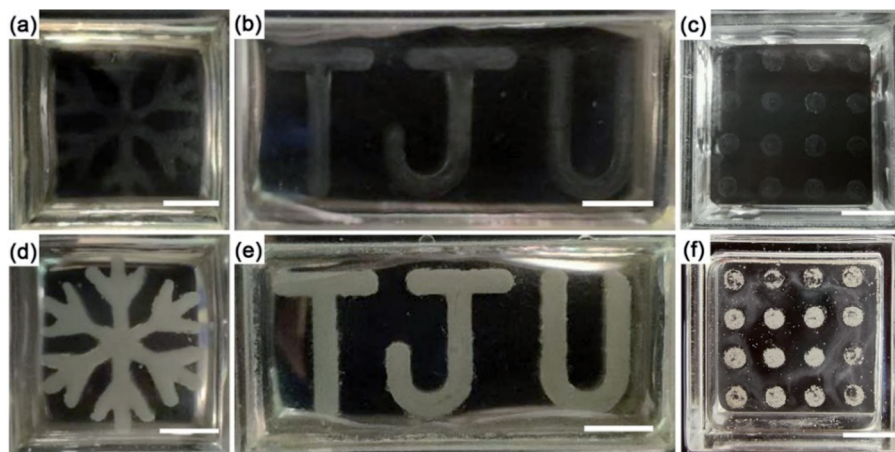


Fig. 4 MICP precipitates with different patterns obtained under optimized conditions. (a–c) At  $t = 0$  h, and (d–f) at  $t = 48$  h. Scale bars are 6 mm.

$$\Delta G = -RT \ln S + \sigma_{cl}A_{cl} + (\sigma_{cs} - \sigma_{sl})A_{cs} \quad (1)$$

where,  $R$  is the ideal gas constant,  $T$  is the temperature,  $S$  is the degree of supersaturation,  $\sigma$  is the interfacial energy,  $A$  is the particle surface area. The subscripts c, l, s refer to crystalline particle, the liquid phase and the substrate, respectively. It has been shown that the template can greatly promote heterogenous nucleation by having a lower net interfacial energy than particle-solution interfacial energy, and thus under the same supersaturation conditions, the nucleus formed by heterogenous nucleation can be about one order of magnitude bigger than that formed by homogenous one.<sup>34</sup> In this work, by using the MICP precipitates as the template material, the net interfacial energy is lowered not only when compared with that of homogenous nucleation in solution, but also when compared with that of heterogeneous nucleation at other non-templated glass surface, as  $\sigma_{cs}$  is essentially zero when MICP precipitates used as the template material whereas  $\sigma_{cs}$  of glass and  $\text{CaCO}_3$  is larger than zero. Thus the template region will show promoted precipitation.

During MICP process, it has been suggested that the less stable, amorphous calcium carbonate (ACC) nanoparticles are first formed and then crystallize into crystalline calcium carbonate polymorphs.<sup>35–37</sup> The interfacial energy between ACC and vaterite will be less than that between ACC and calcite since vaterite is less stable than calcite. This can explain why the promoting efficiency of MICP-induced precipitates (which are mainly vaterite) is higher than commercial ones (which are calcite).

In this work, we observed that the promoting efficiency of template for MICP is optimized at  $T_i = 15$  °C within the tested temperature range of 10–30 °C. However, the bacterial growth curves show that bacteria grow faster and better as  $T_i$  increases (Fig. S5(a)†). Correspondingly, for bacterial cultures which start with a similar cell concentration, their urease activities also display a better performance at higher temperatures (Fig. S5(b)†). These results indicate that besides the urease activity of bacterial culture, there are also other temperature-associated factors that would contribute to the observed maximum  $\rho_s$  at  $T_i = 15$  °C.

One such possible factor would be the diffusion of calcium and carbonate ions (*i.e.*, the influence of mass transport) during

MICP. With the continuation of MICP precipitation at the template region, calcium and carbonate ions over this region would be depleted to the point of undersaturation, which can then be supplemented by the diffusion of ions from nearby regions under no flow conditions. Thus, by tuning the relative ratio of the consuming rate and the diffusion rate of calcium and carbonate ions over the template region through temperature (as these two rates are both affected by temperature), the efficiency of the template can be controlled. Specifically, in our case, what we think have happened is the following. At high  $T_i = 30$  °C, the urease activity is strong and induces a high concentration of carbonate ions, which changes the tested bacterial solution quickly into a supersaturated state for  $\text{CaCO}_3$ . Although the precipitation in the template region starts relatively easily due to the lower net interfacial energy for the nucleation of precipitates on  $\text{CaCO}_3$  particles, the rapid supersaturation in the non-template region can also induce the precipitation of  $\text{CaCO}_3$ . As a consequence, the precipitation will happen not only in the template region but also in the non-template region, thus the precipitated  $\text{CaCO}_3$  in the template region is reduced (under the same total amount of calcium ions). When  $T_i$  decreases from 30 °C to 15 °C, the urease activity goes down (Fig. S5(b)†) so the concentration of carbonate ions increases but slowly. As soon as the concentration of carbonate ions reaches to a certain level, the preferred precipitation in the template region would happen, which then will deplete the concentration of calcium and carbonate ions to the point of undersaturation in the template region and cause a concentration gradient to drive the diffusion of ions from nearby regions to the template region. Because the consuming rate of calcium and carbonate ions would be slowed down as  $T_i$  decreases, the diffusion of ions from nearby regions could be relatively easily to maintain the level of calcium and carbonate ions and keep the preferred precipitation continuing over the template region, thus the promoting efficiency is increased. But when  $T_i$  continues to drop down to 10 °C, the urease activity is reduced so much (Fig. S5(b)†) that the solution is deficient in the amount of carbonate ions and thus result in a large decrease in MICP. This diffusion-controlled process is similar to that

observed using SAM template.<sup>8</sup> This hypothesis is also consistent with the observation that there are more CaCO<sub>3</sub> precipitates in the non-templated region as  $T_i$  increases (Fig. S6†), but to quantitatively determine the relationship between  $T_i$  and the template efficiency for MICP needs further studies. In addition, as bacterial growth is temperature-dependent, it would be also interesting to see how the bacterial concentration affects the observed temperature-dependent promoting efficiency of template in future studies.

## Conclusion

In summary, as a proof of concept, this work demonstrated a simple and efficient way to control the spatial distribution of MICP-induced CaCO<sub>3</sub> precipitates with essentially arbitrary 2D patterns through a template-assisted approach. Parameters like  $C_{Ca^{2+}}$ ,  $T_i$ , the concentration and size of CaCO<sub>3</sub> particles used in templates were optimized, under which patterns with much better quality were obtained. Compared with traditional ceramic processing routes, this method is green, environmentally friendly, scale-upable and is also conducted under mild conditions, and thus has a great potential for applications in fabricating patterned calcium carbonate materials.

## Methods

### Bacterial strain and growth conditions

Bacteria *S. pasteurii* (ATCC 11859) was used in this study. Bacterial cells were cultured in YE-urea liquid medium (2% w/v urea, and YE for yeast extract 20 g L<sup>-1</sup>, ammonium sulfate 10 g L<sup>-1</sup>, Tris 0.13 M) at 30 °C, 220 rpm (rotations per minute) or on YE-urea plates containing 2% agar. MICP experiments were carried out in nutrient broth (NB)-urea medium (2% w/v urea, and NB for peptone 10 g L<sup>-1</sup>, beef extract 10 g L<sup>-1</sup>, NaCl 5 g L<sup>-1</sup>, ammonium sulfate 10 g L<sup>-1</sup>). Urea solution and CaCl<sub>2</sub>·2H<sub>2</sub>O solution were filter-sterilized through 0.22 μm pore size filters and added later. All other media components were autoclaved separately at 121 °C for 15 min and mixed together before inoculation. Heat-killed *S. pasteurii* cells were obtained by autoclaving cell suspensions for 30 min at 121 °C.

### Collecting CaCO<sub>3</sub> precipitates produced by MICP process

*S. pasteurii* cultures were grown overnight at 30 °C in YE-urea medium to an optical density at 600 nm (OD<sub>600</sub>) ~1.6. Then cells were harvested by centrifugation at ~2000 g for 5 min, and resuspended in NB-urea medium (Ca-free). Next, the resuspended bacteria were diluted in 100 mL NB-urea medium containing 25 mM CaCl<sub>2</sub> to a final OD<sub>600</sub> of 0.02, and were incubated on an orbital shaker at 30 °C for 10 h. After 10 h-incubation, precipitates were collected by centrifugation, which were then subject to ultrasonication and washed for three times using deionized (DI) water to remove attached bacteria cells. The cleaned CaCO<sub>3</sub> precipitates were dried at 60 °C for 24 h and then were ready for further use. The heat-treated MICP CaCO<sub>3</sub> particles were obtained by furnacing the above collected MICP CaCO<sub>3</sub> particles in a Muffle furnace (JXR1200-30, Shanghai Junke Instrument Technology Co., Ltd) at 450 °C for 3 h (Table S1†).

### Template-assisted MICP

To make a template on a glass surface, a suspension of each specific material was first formed either by dispersing dried solid particles into water to the target concentration for MICP-induced, heat-treated MICP-induced, commercial CaCO<sub>3</sub> particles and sulfonic group modified PS particles, or by diluting the heat-killed *S. pasteurii* culture using NB-urea medium to an OD<sub>600</sub> of ~1. Next, to make a single disk-shaped template, a 2 μL drop of the suspension was pipetted onto the glass surface of a 18 mm glass-bottom Petri dish, which was then air-dried and treated with ultraviolet (UV) light. Other shaped templates were fabricated either by directly hand-drawing a pattern using a pipet or through an acrylic pattern obtained by laser-cutting (Yueming Laser, CMA6040). When an acrylic plate with a cut-out pattern was used to make a template, agar gel (1.5% w/v) was used to seal the gap between the acrylic plate and the glass first before the addition of CaCO<sub>3</sub> particle suspension, and once the added suspension dried, both the acrylic plate and the agar gel were removed to leave dried template only on the glass surface. Then a squared fence made of acrylic was glued onto the glass, which enclosed the template region to form a square well (with a size of 18 mm × 18 mm × 5 mm). Subsequently, the dish/square well was filled gently with 470–1200 μL (depending on the template) of diluted bacterial suspension with an OD<sub>600</sub> of 0.02 in NB-urea medium containing specified concentration of CaCl<sub>2</sub>. Then the dish/square well was sealed using parafilm and left still in an incubator at 15 °C for 48 h. After the incubation, the dish/square well was then placed on an optical microscope for imaging.

For the optimization of parameters to improve the promoting efficiency of template for MICP, disk-shaped templates were used.

### Microscopy and precipitation analysis

Images were captured using a sCMOS camera (Andor, Neo) on a Leica DMi8 inverted optical microscope with a 10× objective. XRD measurements were performed using a D8 Focus X-ray diffractometer (Bruker) in the diffraction angle range  $2\theta = 20\text{--}90^\circ$ , using Cu K $\alpha$  radiation (40 kV and 40 mA). XPS measurements were conducted using an X-ray photoelectron spectroscopy (XPS, Thermo Fisher Scientific) with an Al K $\alpha$  (150 eV) X-ray.

The surface density of precipitates  $\rho_s$  is determined as the following: after a specified period of incubation, e.g., 48 h, the Petri dish with the patterned glass bottom was washed gently for three times using DI water and then dried at 60 °C in an oven. For a typical measurement of  $\rho_s$  of the template region, the total mass of the dish with the dried MICP pattern on the glass bottom was first weighted to be  $m_1$ ; next, the precipitates at the template region were removed using a tweezer; after that, the whole dish was weighted again to get  $m_2$ , then the mass of precipitates was obtained by  $m_1 - m_2$ .  $\rho_s$  is obtained by dividing  $m_1 - m_2$  with the area of template region. We note that the mass of initial deposited precipitates used as the template is at least one order of magnitude smaller than that of final precipitates at the template region, and thus is neglected.

For measuring  $\rho_s$  along the radius direction of the Petri dish as shown in Fig. 1, we first split the round Petri dish area in the photo to 9 concentric annuli (Fig. S8†). Then, for each annular zone in the template region,  $\rho_s$  is calculated as described above. However, for each annular zone in the template free region, since the total mass of the precipitates in such zones is too small to be weighted accurately under our conditions, it was estimated by the sum of the mass of each precipitated particle in the zone. The mass of each particle is estimated as the product of  $\text{CaCO}_3$  density and the volume of the particle, which is assumed to be spherical and its diameter is measured by ImageJ.

### Urease activity measurement

Urease activity was determined by a conductivity method in the absence of calcium ions.<sup>38–40</sup> 1 mL of bacterial culture was added into 9 mL of 1.1 mol L<sup>-1</sup> urea solution, whose conductivity was then monitored for 5 min by a conductivity meter. The urease activity of the ureolytic bacteria can be calculated by multiplying the averaged variation rate of conductivity within 5 min (ms cm<sup>-1</sup> min<sup>-1</sup>) with the dilution factor (10 times) and 11.11, *i.e.*, the hydrolysis rate of urea (mmol L<sup>-1</sup> min<sup>-1</sup>) = the variation rate of conductivity (ms cm<sup>-1</sup> min<sup>-1</sup>) × 11.11.

### Author contributions

K. Z. conceived and designed the project. D. Y. and H. Z. performed experimental measurements. D. Y., H. Z., W. Z. and Y. Z. analyzed data. D. Y., H. Z. and K. Z. wrote the paper. All authors discussed the results and commented on the manuscript.

### Conflicts of interest

There are no conflicts to declare.

### Acknowledgements

This work is supported by the National Key R&D Program of China (2018YFA0902102), the National Natural Science Foundation of China (21621004 and 22006110). The funders had no role in the study design, data collection and interpretation, or the decision to submit the work for publication.

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