

Article

Thermodynamics Analysis and Removal of P in a P-(M)-H₂O System

Hao Peng , Jing Guo, Hongzhi Qiu, Caiqiong Wang, Chenyu Zhang, Zhihui Hao, Yating Rao and Yanhong Gong

Chongqing Key Laboratory of Inorganic Special Functional Materials, College of Chemistry and Chemical Engineering, Yangtze Normal University, Fuling, Chongqing 408100, China; 20171110@yznu.edu.cn (J.G.); q780173781@126.com (H.Q.); wqc18290390314@163.com (C.W.); hzh3229224722@126.com (C.Z.); zcy20010126@126.com (Z.H.); rytill@163.com (Y.R.); scarlett20001212@163.com (Y.G.)

* Correspondence: penghao@yznu.edu.cn; Tel.: +86-151-2303-1643

Abstract: In order to efficiently remove phosphorus, thermodynamic equilibrium diagrams of the P-H₂O system and P-M-H₂O system (M stands for Fe, Al, Ca, Mg) were analyzed by software from Visual MINTEQ to identify the existence of phosphorus ions and metal ions as pH ranged from 1 to 14. The results showed that the phosphorus ions existed in the form of H₃PO₄, H₂PO₄[−], HPO₄^{2−}, and PO₄^{3−}. Among them, H₂PO₄[−] and HPO₄^{2−} were the main species in the acidic medium (99% at pH = 5) and alkaline medium (97.9% at pH = 10). In the P-Fe-H₂O system ((P) = 0.01 mol/L, (Fe³⁺) = 0.01 mol/L), H₂PO₄[−] was transformed to FeHPO₄⁺ at pH = 0–7 due to the existence of Fe³⁺ and then transformed to HPO₄^{2−} at pH > 6 as the Fe³⁺ was mostly precipitated. In the P-Ca-H₂O system ((P) = 0.01 mol/L, (Ca²⁺) = 0.015 mol/L), the main species in the acidic medium was CaH₂PO₄⁺ and HPO₄^{2−}, and then transformed to CaPO₄[−] at pH > 7. In the P-Mg-H₂O system ((P) = 0.01 mol/L, (Mg²⁺) = 0.015 mol/L), the main species in the acidic medium was H₂PO₄[−] and then transformed to MgHPO₄ at pH = 5–10, and finally transformed to MgPO₄[−] as pH increased. The verification experiments (precipitation experiments) with single metal ions confirmed that the theoretical analysis could be used to guide the actual experiments.

Keywords: thermodynamics; removal; phosphorus



Citation: Peng, H.; Guo, J.; Qiu, H.; Wang, C.; Zhang, C.; Hao, Z.; Rao, Y.; Gong, Y. Thermodynamics Analysis and Removal of P in a P-(M)-H₂O System. *Molecules* **2021**, *26*, 3342. <https://doi.org/10.3390/molecules26113342>

Academic Editors: Ramesh Gardas and Riccardo Chelli

Received: 20 April 2021

Accepted: 30 May 2021

Published: 2 June 2021

Publisher's Note: MDPI stays neutral with regard to jurisdictional claims in published maps and institutional affiliations.



Copyright: © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (<https://creativecommons.org/licenses/by/4.0/>).

1. Introduction

Phosphorus plays an important role in living organisms as it is one of the main components of cell structure [1]. Usually, phosphorus exists in three species (orthophosphate, polyphosphate, and organic phosphorus) in solution. Furthermore, the primary phosphorus compounds are generally orthophosphates [2]. The overuse and inefficient use of phosphorus lead to the eutrophication problem in natural water, which is a serious global problem that needs to be treated [3,4].

Phosphorus mitigation is expensive and difficult in the waste stream. Many methods have been developed for phosphorus removal. The conventional biological methods have difficulty in removing phosphorus due to the inherent limitations of the activated sludge method. The removal efficiency of phosphorus is less than 30%, and the residual phosphorus concentration is still over the wastewater discharge guideline [5]. As a result of catastrophic environmental implications, including eutrophication and red tide, the governments have established some biological wastewater treatment systems to treat the wastewater containing phosphorus and limited the emission standard for residual phosphorus concentration (0.5–1 mg TP/L in the USA, <0.2 mg TP/L in South Korea, and 1–2 mg TP/L in France) [6]. The conventional biological treatment processes can only achieve low removal efficiency of phosphorus due to large volume requirements and long hydraulic retention time. Thus, the development of advanced technology to improve phosphorus removal efficiency is needed, including easy installation, short intention time, little space, low operation cost, and low capital investment [2,7–10]. Enhanced biological phosphorus removal processes have attracted much more attention [11–15]. The key

factor in the enhanced biological phosphorus removal process is the use of phosphorus accumulating organisms. Under anaerobic conditions, the stored poly-phosphate (poly-P) is hydrolyzed to supply energy for the polyhydroxyalkanoates uptake. During the subsequent aerobic process, phosphorus accumulating organisms absorb the excessive amounts of phosphorus for poly-P. Finally, the phosphorus is removed when the waste-activated sludge is separated from the treated wastewater at the end of the aerobic stage. In the whole process, stable phosphorus removal efficiency is hard to maintain. Thus, some physicochemical treatments have come to the forefront [16–18]. Among them, chemical precipitation methods are widely used for phosphorus removal with metal ion salts. Calcium salts, such as CaCl_2 , $\text{Ca}(\text{NO}_3)_2$, are often added for the removal of phosphorus as calcium and phosphorus have a strong affinity and could form insoluble $\text{Ca}_3(\text{PO}_4)_2$ [19]. The concentration of phosphorus can be reduced from 15.1 ppmw to 0.2 ppmw with the addition of magnesium in acidic conditions [20]. Commonly, magnesium is used with ammonium for phosphorus removal called the magnesium ammonium phosphate method [21–24], but it is limited by co-precipitation, low separation efficiency caused by the separation equipment, serious ammonia wastewater, and ammonia gas pollution [25]. Ferric and aluminum are also used for phosphorus removal as they can generate co-precipitates with phosphate, and the hydroxyl complexes formed by hydrolyzing of Fe^{3+} and Al^{3+} show great adsorption performance for orthophosphate [26–28].

From the above analysis, the existing form of phosphorus and the metal ion in the solution has a great influence on phosphorus removal efficiency. Thus, the present work focuses on the existence of phosphorus ions and metal ions in solution at different pH ranges by employing the Visual MINTEQ software. This work aims to provide a theoretical basis for efficient phosphorus removal from wastewater.

2. Results

2.1. Thermodynamic Analysis of the P-H₂O System

In the P-H₂O system, the phosphorus existed in the form of HPO_4^{2-} , H_2PO_4^- , H_3PO_4 , and PO_4^{3-} . These four species were interchangeable with changed pH according to Equations (1)–(3).

$$[\text{PO}_4^{3-}][\text{H}^+]^2 = 10^{-17.650}[\text{H}_2\text{PO}_4^-] \quad (1)$$

$$[\text{HPO}_4^{2-}][\text{H}^+] = 10^{-6.418}[\text{H}_2\text{PO}_4^-] \quad (2)$$

$$[\text{H}_3\text{PO}_4] = 10^{1.772}[\text{H}^+][\text{H}_2\text{PO}_4^-] \quad (3)$$

Based on the above equations, thermodynamic studies of the P-H₂O system were performed to determine the chemical state of ions in the wastewater. A mole fraction of different phosphorus species in the P-H₂O system was plotted as the pH ranged from 1 to 14 and (P) = 0.01 mol/L to 0.09 mol/L. The results are shown in Figure 1.

It can be seen that the phosphorus mainly existed in the form of H_3PO_4 , H_2PO_4^- , HPO_4^{2-} , and PO_4^{3-} . With the increase in pH value, the phosphorus transformed to H_2PO_4^- , HPO_4^{2-} , and PO_4^{3-} . The maximum percentage of H_3PO_4 , H_2PO_4^- , HPO_4^{2-} , PO_4^{3-} was, respectively, 26.8% (at pH = 2), 99% (at pH = 5), 97.9% (when pH = 10), and 23.1% (at pH = 12). With the increase in phosphorus concentration, the percentage of H_2PO_4^- and HPO_4^{2-} had no obvious change, while the maximum percentage of H_3PO_4 and PO_4^{3-} increased with the increase in phosphorus concentration, but the pH was kept constant.

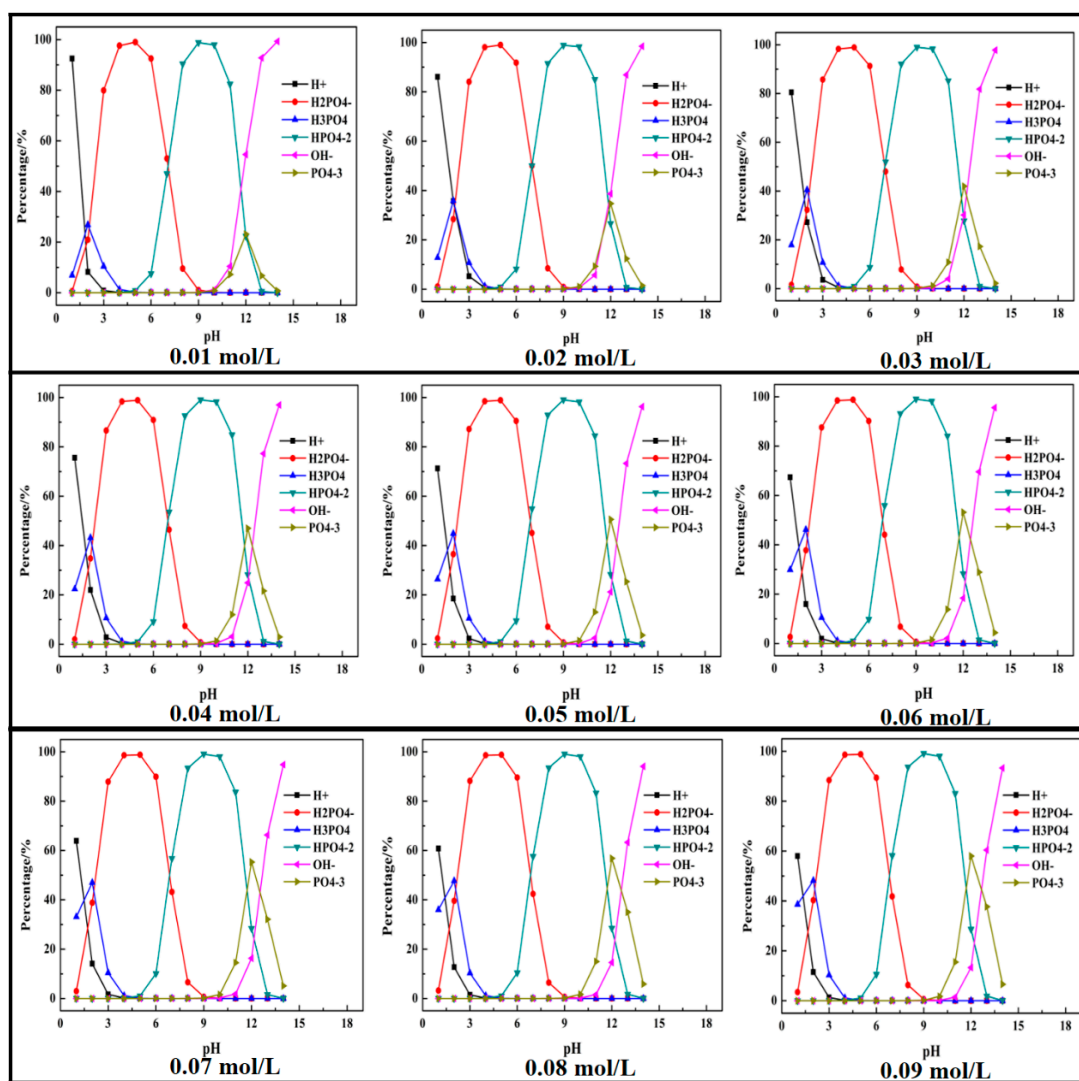


Figure 1. Mole fraction diagram of phosphorus species in the P-H₂O system at 298 K at various pH (P) = 0.01 to 0.90 mol/L).

2.2. Thermodynamic Analysis of M-P-H₂O System

2.2.1. Fe (Ca, Mg)-P-H₂O System

In this section, a single metal salt was used to remove phosphorus from the wastewater, and Fe^{3+} , Ca^{2+} , and Mg^{2+} were selected. The composition in the phosphorus solution with single metal salt was simulated by Visual MINTEQ software. The results are shown in Figures 2–4.

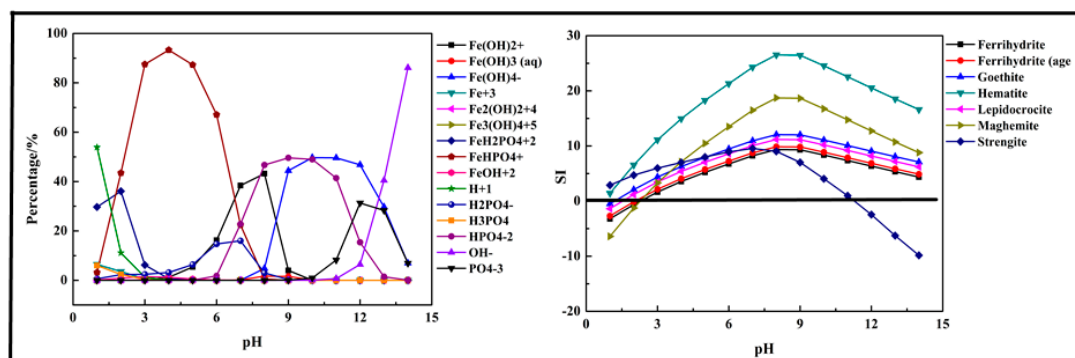


Figure 2. Percentage of species in the Fe-P-H₂O system at 298 K at ranged pH (P) = 0.01 mol/L, (Fe^{3+}) = 0.01 mol/L).

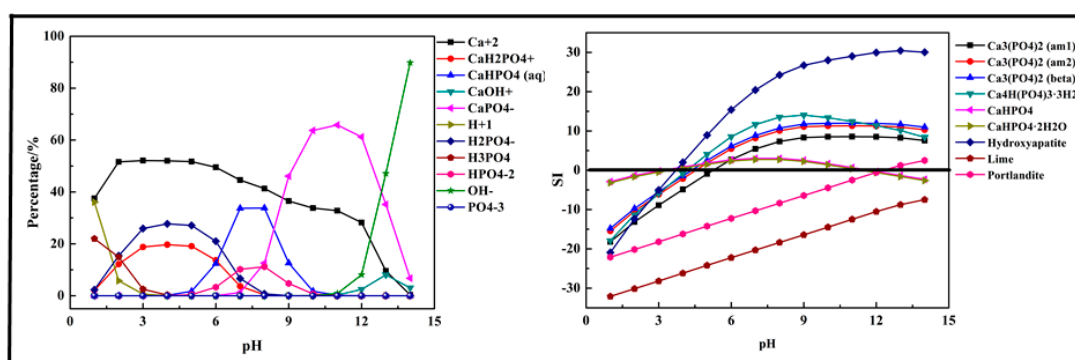


Figure 3. Percentage of species in the Ca-P-H₂O system at 298 K at ranged pH ($P = 0.01$ mol/L, $(Ca^{2+}) = 0.015$ mol/L).

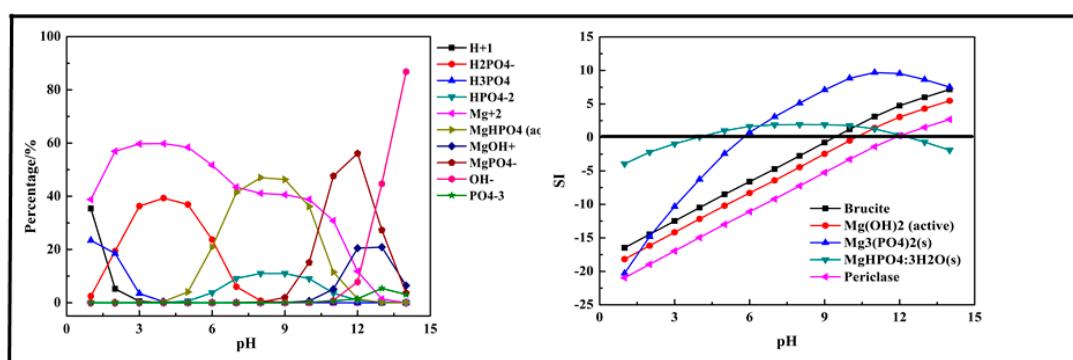


Figure 4. Percentage of species in the Mg-P-H₂O system at 298 K at ranged pH ($P = 0.01$ mol/L, $(Mg^{2+}) = 0.015$ mol/L).

The results shown in Figure 2 indicated that the main species in the Fe-P-H₂O system were $Fe(OH)_2^+$, $Fe(OH)_3(aq)$, $Fe(OH)_4^-$, Fe^{3+} , $Fe_2(OH)_2^{4+}$, $Fe_3(OH)_4^{5+}$, $FeH_2PO_4^{2+}$, $FeHPO_4^+$, $FeOH^{2+}$, H^+ , $H_2PO_4^-$, H_3PO_4 , HPO_4^{2-} , OH^- , and PO_4^{3-} . Due to the existence of Fe^{3+} , phosphorus first transformed into $FeH_2PO_4^{2+}$ at $pH < 2$ and then transformed into $FeHPO_4^+$ at $pH = 2-7$. In an alkaline medium ($pH > 7$), the phosphorus and Fe^{3+} mainly existed in the form of HPO_4^{2-} and $Fe(OH)_4^-$. The results shown in Figure 2 also display the predicted precipitation products. The main products of the reaction were Ferrihydrite ($Fe_5HO_8 \cdot 4H_2O$), Goethite ($HFeO_2$), Hematite (Fe_2O_3), Lepidocrocite ($FeO(OH)$), Maghemite ($\gamma-Fe_2O_3$), and Strengite ($FePO_4 \cdot 2H_2O$). Almost all the precipitation products were hydrolyzed Fe^{3+} , but only Strengite is our aim. The suitable pH for precipitation of phosphorus with Fe^{3+} was below 11.

The results displayed in Figure 3 show that the main species in the Ca-P-H₂O system were quite different from the Fe-P system. In the acidic medium ($pH < 7$), the phosphorus existed in the form of HPO_4^{2-} , $H_2PO_4^-$. As pH value increased, it transformed into $CaHPO_4(aq)$ and $CaH_2PO_4^+$. When $pH > 7$, it mainly existed in the form of $CaPO_4^-$. During the phosphorus removal process, there was no precipitation formed at $pH < 4$ because the SI of all predicted products was below 0. The first precipitation product, also the main product, was Hydroxyapatite ($Ca_5(PO_4)_3(OH)$). As pH value increased, some other products might be generated, such as $Ca_3(PO_4)_2$, $Ca_4H(PO_4)_3 \cdot 3H_2O$, $CaHPO_4$, and $CaHPO_4 \cdot 2H_2O$. But $CaHPO_4$ and $CaHPO_4 \cdot 2H_2O$ dissolved again at $pH > 11$. Above all, Ca^{2+} salts were used efficiently for phosphorus removal.

The results shown in Figure 4 indicate that the main species in the Mg-P-H₂O system were $H_2PO_4^-$, H_3PO_4 , HPO_4^{2-} , Mg^{2+} , $MgHPO_4(aq)$, $MgOH^+$, $MgPO_4^-$, OH^- , and PO_4^{3-} . Phosphorus existing as H_3PO_4 first transformed into $H_2PO_4^-$ at $pH < 7$ and then transformed into $MgHPO_4(aq)$ and HPO_4^{2-} at $pH = 4-12$, owing to the existence of Mg^{2+} . As pH value increased to 9, $MgPO_4^-$ was the main form of phosphorus and up to 56.1% at $pH = 12$. The main products of the reaction were predicted as brucite ($Mg(OH)_2$), $Mg(OH)_2$, $Mg_3(PO_4)_2$, $MgHPO_4 \cdot 3H_2O$, and Periclase (MgO). The removal of phosphorus

with Mg^{2+} should be conducted at $\text{pH} > 6$ and especially at $\text{pH} > 10$ as there was no precipitation generated at $\text{pH} < 5$ and only $\text{Mg}_3(\text{PO}_4)_2$, $\text{MgHPO}_4 \cdot 3\text{H}_2\text{O}$ generated after $\text{pH} = 5$. After $\text{pH} = 11$, almost all the predicted products generated except $\text{MgHPO}_4 \cdot 3\text{H}_2\text{O}$, which dissolved again. The optimal pH ranged from 7 to 14.

In conclusion, the removal of phosphorus could achieve high efficiency in an alkaline medium. Using Fe^{3+} salts and Ca^{2+} salts more easily generated phosphorus precipitation and were more efficient in removing phosphorus.

2.2.2. Two Salts System

The results shown in Figure 5 indicate that the main species in the Fe-Ca-P- H_2O system could be divided into three sections. At $\text{pH} = 1\text{--}6$, $\text{CaH}_2\text{PO}_4^+$, H_2PO_4^- , FeHPO_4^+ , and Ca^{2+} were the main species in the solution. As pH value increased, the above ions transformed into CaHPO_4 (aq), HPO_4^{2-} , and $\text{Fe}(\text{OH})^{2+}$ at $\text{pH} = 6\text{--}9$. At $\text{pH} > 9$, the main species ions were CaPO_4^- , $\text{Fe}(\text{OH})_4^-$, HPO_4^{2-} , OH^- , and PO_4^{3-} . Strengite was the first predicted precipitation product generated in the precipitation process, and it dissolved again after $\text{pH} > 11$. Other precipitation products were generated after $\text{pH} > 3$, and the main phosphorus precipitation products were Hydroxyapatite, three kinds of $\text{Ca}_3(\text{PO}_4)_2$ and $\text{Ca}_4\text{H}(\text{PO}_4)_3 \cdot 3\text{H}_2\text{O}$. CaHPO_4 , CaHPO_4 generated at $\text{pH} = 5\text{--}10$ and then dissolved after $\text{pH} > 11$.

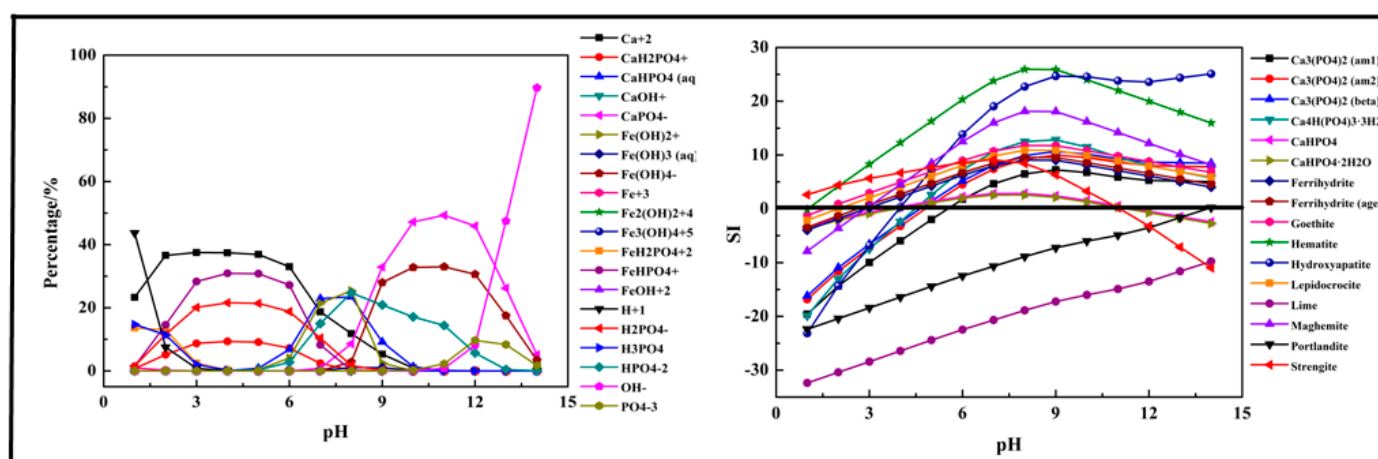


Figure 5. Percentage of species in the Fe-Ca-P- H_2O system at 298 K at ranged pH ($(\text{P}) = 0.01 \text{ mol/L}$, $(\text{Fe}^{3+}) = 0.005 \text{ mol/L}$, $(\text{Ca}^{2+}) = 0.0075 \text{ mol/L}$).

The results shown in Figure 6 indicate that the main species in Ca-Mg-P- H_2O system could be divided into three sections. At $\text{pH} = 1\text{--}6$, H_2PO_4^- , Ca^{2+} , $\text{CaH}_2\text{PO}_4^+$, and Mg^{2+} were the main species in the solution. As pH value increased, above ions transformed into CaHPO_4 (aq), MgHPO_4 (aq), HPO_4^{2-} at $\text{pH} = 6\text{--}9$. At $\text{pH} > 9$, the main species ions were CaPO_4^- , MgOH^+ , and MgPO_4^- , $\text{Fe}(\text{OH})_4^-$, OH^- , and PO_4^{3-} . Hydroxyapatite ($\text{Ca}_5(\text{PO}_4)_3(\text{OH})$) was first precipitated at $\text{pH} > 4$, then $\text{Ca}_4\text{H}(\text{PO}_4)_3 \cdot 3\text{H}_2\text{O}$, $\text{Ca}_3(\text{PO}_4)_2$ followed. The precipitation containing Mg, such as $\text{Mg}_3(\text{PO}_4)_2$, was formed after $\text{pH} > 7$. For the Ca-Mg-P system, the suitable pH for phosphorus removal was after 5.

The results shown in Figure 7 indicate that the main species in the Fe-Mg-P- H_2O system could be divided into three sections. At $\text{pH} = 1\text{--}6$, H_2PO_4^- , FeHPO_4^+ , and Mg^{2+} were the main species in the solution. As pH value increased, the above ions transformed into MgHPO_4 (aq) ($\text{pH} = 6\text{--}11$), HPO_4^{2-} ($\text{pH} = 6\text{--}13$), $\text{Fe}(\text{OH})_4^-$ ($\text{pH} > 8$), and MgPO_4^- ($\text{pH} > 9$). Strengite was the first predicted precipitation product generated in the precipitation process, and it dissolved again after $\text{pH} > 11$. $\text{Mg}_3(\text{PO}_4)_2$, $\text{MgHPO}_4 \cdot 3\text{H}_2\text{O}$ generated after $\text{pH} = 6$. $\text{MgHPO}_4 \cdot 3\text{H}_2\text{O}$ was formed at $\text{pH} = 5$ and then dissolved after $\text{pH} > 12$.

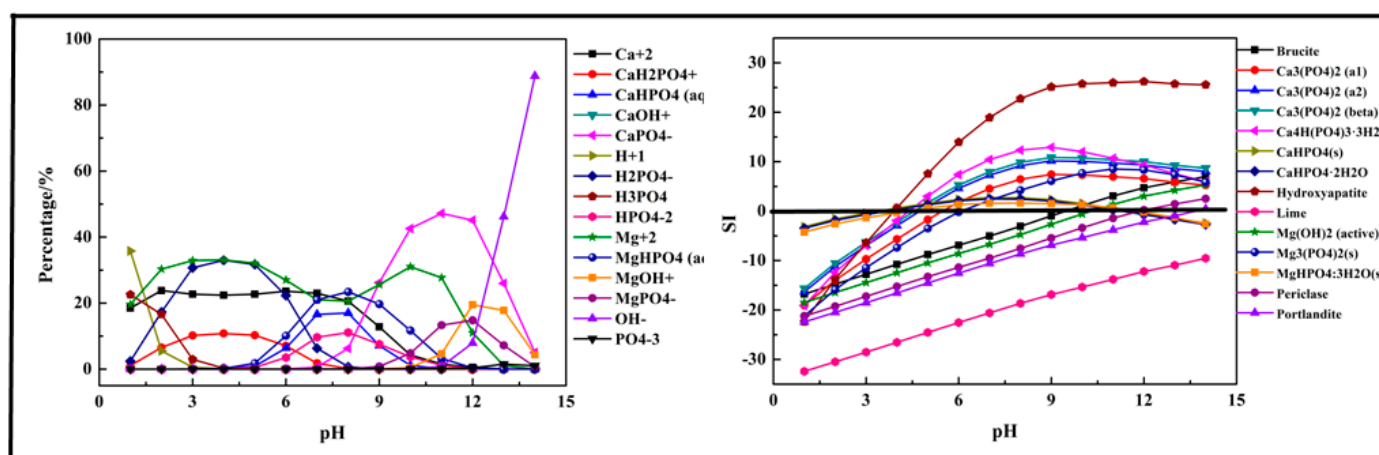


Figure 6. Percentage of species in the Ca-Mg-P-H₂O system at 298 K at ranged pH ($(P) = 0.01$ mol/L, $(Ca^{2+}) = 0.0075$ mol/L, $(Mg^{2+}) = 0.0075$ mol/L).

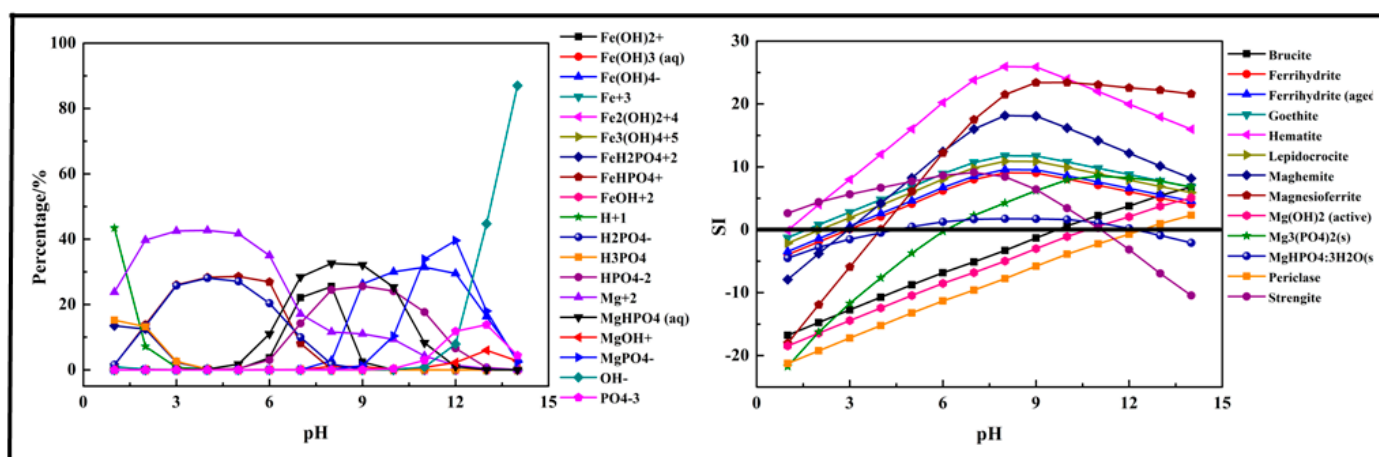


Figure 7. Percentage of species in the Fe-Mg-P-H₂O system at 298 K at ranged pH ($(P) = 0.01$ mol/L, $(Fe^{3+}) = 0.003$ mol/L, $(Mg^{2+}) = 0.0075$ mol/L).

2.2.3. Fe-Ca-Mg-P-H₂O System

The results shown in Figure 8 indicate that the main species in the Fe-Ca-Mg-P system could be divided into three sections. At pH = 1–6, $CaH_2PO_4^+$, $H_2PO_4^-$, Mg^{2+} , $FeHPO_4^+$, and Ca^{2+} were the main species in the solution. As pH value increased, above ions transformed into $MgHPO_4$ (aq) (pH = 5–13), $CaHPO_4$ (aq) (pH = 5–10), HPO_4^{2-} (5–13), $CaPO_4^-$ (pH = 8–14), $Fe(OH)^{2+}$ (pH = 5–12), and $MgPO_4^-$ (pH = 9–14). The first precipitation containing phosphorus was Strengite after pH > 2, while it occurred at pH = 0 in a single-salt system and two-salts system. Then other precipitations formed continually. The composition in the three salts system was more complex, and the precipitation was no more stable than the single salt system.

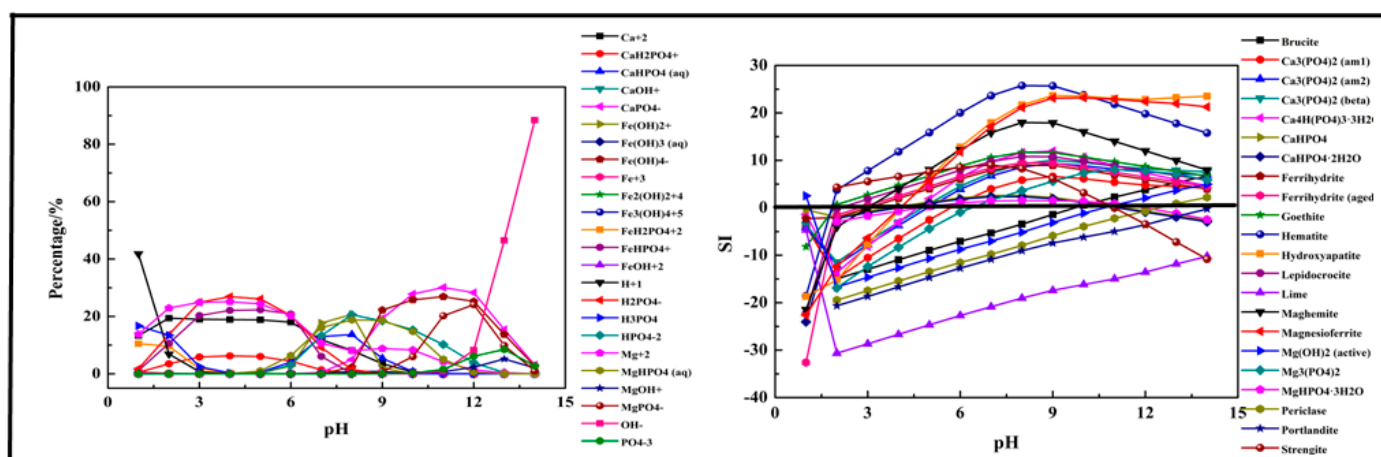


Figure 8. Percentage of species in the Fe-Ca-Mg-P-H₂O system at 298 K at ranged pH ((P) = 0.01 mol/L, (Fe³⁺) = 0.004 mol/L, (Ca²⁺) = 0.0045 mol/L, (Mg²⁺) = 0.0045 mol/L).

2.3. Phosphorous Removal Experiments

The phosphorous removal experiments were conducted with Ca²⁺, Al³⁺, and Fe³⁺. The results are shown in Figure 9. The phosphorus ion was precipitated under the selected reaction conditions. The dosage of metal ions had a significant effect on the removal efficiency of phosphorous. For Ca²⁺ salts, the high removal efficiency was 81.25% and achieved at n(Ca²⁺)/n(P) = 0.6. A further increase in Ca had no obvious effect on the removal efficiency. While for Al³⁺ salts, the removal efficiency was a step increase, and the highest was 80.13%. Great removal performance was achieved by Fe³⁺ at n(Fe)/n(P) = 1 with a removal efficiency of 91.54%. These actual experimental results are consistent with the analysis above, indicating that the theoretical analysis could be used to guide the actual experiments.

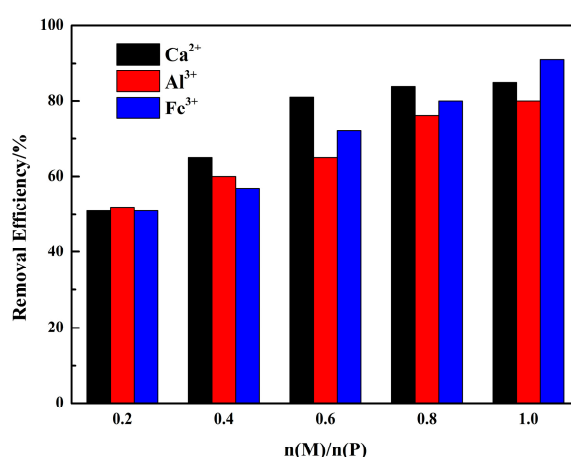


Figure 9. Phosphorous removal experiments ((P) = 0.01 mol/L, n(Ca)/n(P) = 0.2–1, n(Al)/n(P) = 0.2–1, n(Fe)/n(P) = 0.2–1).

3. Materials and Methods

The thermodynamic equilibrium diagrams of P-H₂O system and P-M-H₂O system (M stands for Fe, Al, Ca, Mg) were simulated by the VISUAL MINTEQ software. The concentration of P and M are detailed in Table 1. For the P-H₂O system, the concentration of phosphorus ranged from 0.01 mol/L to 0.09 mol/L. In the Fe-P-H₂O system, the concentration was (P) = 0.01 mol/L, (Fe³⁺) = 0.01 mol/L. For the Ca-P-H₂O system, the concentration was (P) = 0.01 mol/L, (Ca²⁺) = 0.015 mol/L. For the Mg-P-H₂O system, the concentration was

(P) = 0.01 mol/L, (Mg^{2+}) = 0.015 mol/L. For the Fe-Mg-P- H_2O system, the concentration was (P) = 0.01 mol/L, (Fe^{3+}) = 0.005 mol/L, (Mg^{2+}) = 0.0075 mol/L. For the Ca-Mg-P- H_2O system, the concentration was (P) = 0.01 mol/L, (Ca^{2+}) = 0.0075 mol/L, (Mg^{2+}) = 0.0075 mol/L. For the Fe-Ca-P- H_2O system, the concentration was (P) = 0.01 mol/L, (Fe^{3+}) = 0.003 mol/L, (Ca^{2+}) = 0.0075 mol/L. For Fe-Ca-Mg-P- H_2O system, the concentration was (P) = 0.01 mol/L, (Fe^{3+}) = 0.004 mol/L, (Ca^{2+}) = 0.0045 mol/L, (Mg^{2+}) = 0.0045 mol/L. The activity coefficients of the charged materials were calculated with the Davies equation. Meanwhile, the saturation index (SI) was used to predict the trend of precipitated and dissolved species and was calculated based on Equation (1). If $\text{SI} > 0$, the content was in oversaturation and might precipitate; $\text{SI} = 0$, the content was in an equilibrium state; $\text{SI} < 0$, the content existed in the form of ions in the solution.

$$\text{SI} = \log \text{IAP} - \log K_s \quad (4)$$

where IAP is the selected ion activity in the Visual MINTEQ software, and K_s is the solubility product constant.

Table 1. The concentration for simulating process.

System	Concentration (mol/L)			
	P	Fe	Ca	Mg
P- H_2O	0.01–0.09			
Fe-P- H_2O	0.01	0.01		
Ca-P- H_2O	0.01		0.015	
Mg-P- H_2O	0.01			0.015
Fe-Mg-P- H_2O	0.01	0.005		0.0075
Ca-Mg-P- H_2O	0.01		0.0075	0.0075
Fe-Ca-P- H_2O	0.01	0.005	0.0075	
Fe-Ca-Mg-P- H_2O	0.01	0.004	0.0045	0.0045

4. Conclusions

Based on the results obtained in this study, the following conclusions can be obtained:

- (1) The phosphorus ions existed in the form of H_3PO_4 , H_2PO_4^- , HPO_4^{2-} , and PO_4^{3-} . Among them, H_2PO_4^- and HPO_4^{2-} were the main species in the acidic medium (99% at $\text{pH} = 5$) and alkaline medium (97.9% at $\text{pH} = 10$). In the P-Fe- H_2O System ((P) = 0.01 mol/L, (Fe^{3+}) = 0.01 mol/L), H_2PO_4^- was transformed to FeHPO_4^+ at $\text{pH} = 0\text{--}7$ due to the existence of Fe^{3+} and then transformed into HPO_4^{2-} at $\text{pH} > 6$ as the Fe^{3+} was mostly precipitated. In the P-Ca- H_2O System ((P) = 0.01 mol/L, (Ca^{2+}) = 0.015 mol/L), the main species in the acidic medium were $\text{CaH}_2\text{PO}_4^+$ and HPO_4^{2-} , and then transformed into CaPO_4^- at $\text{pH} > 7$. In the P-Mg- H_2O System ((P) = 0.01 mol/L, (Mg^{3+}) = 0.015 mol/L), the main species in the acidic medium was H_2PO_4^- and then transformed into MgHPO_4 at $\text{pH} = 5\text{--}10$, and finally transformed into MgPO_4^- as pH increased.
- (2) The phosphorus was more easily precipitated in the P-Fe- H_2O system than the P-Ca- H_2O system and P-Mg- H_2O system. The suitable pH of the solution for phosphorus precipitation was about 5–10 in all precipitation systems.
- (3) The verification experiments (precipitation experiments) with single metal ions confirm that the theoretical analysis can be used to guide the actual experiments.

Author Contributions: Conceptualization, H.P.; methodology, H.P.; software, H.P.; validation, H.P.; formal analysis, H.P.; investigation, H.Q., C.W. and J.G.; resources, H.P.; data curation, Z.H., C.Z., Y.G., Y.R. and J.G.; writing—original draft preparation, H.P.; writing—review and editing, H.P.; visualization, H.P.; supervision, H.P.; project administration, H.P.; funding acquisition, H.P. All authors have read and agreed to the published version of the manuscript.

Funding: This work was supported by the Science and Technology Research Program of Chongqing Municipal Education Commission (No. KJQN201901403 and No. CXQT20026) and Chongqing Science and Technology Commission (No. cstc2018jcyjAX0018).

Institutional Review Board Statement: Not applicable.

Informed Consent Statement: Not applicable.

Data Availability Statement: No new data were created or analyzed in this study. Data sharing is not applicable to this article

Conflicts of Interest: The authors declare no conflict of interest.

Sample Availability: Not available.

References

- Okano, K.; Yamamoto, Y.; Takano, H.; Aketo, T.; Honda, K.; Ohtake, H. A simple technology for phosphorus recovery using acid-treated concrete sludge. *Sep. Purif. Technol.* **2016**, *165*, 173–178. [\[CrossRef\]](#)
- Tran, N.; Drogui, P.; Blais, J.-F.; Mercier, G. Phosphorus removal from spiked municipal wastewater using either electrochemical coagulation or chemical coagulation as tertiary treatment. *Sep. Purif. Technol.* **2012**, *95*, 16–25. [\[CrossRef\]](#)
- Okano, K.; Uemoto, M.; Kagami, J.; Miura, K.; Aketo, T.; Toda, M.; Honda, K.; Ohtake, H. Novel technique for phosphorus recovery from aqueous solutions using amorphous calcium silicate hydrates (A-CSHs). *Water Res.* **2013**, *47*, 2251–2259. [\[CrossRef\]](#) [\[PubMed\]](#)
- Song, Y.; Weidler, P.G.; Berg, U.; Nüesch, R.; Donnert, D. Calcite-seeded crystallization of calcium phosphate for phosphorus recovery. *Chemosphere* **2006**, *63*, 236–243. [\[CrossRef\]](#) [\[PubMed\]](#)
- Hosni, K.; Ben Moussa, S.; Ben Amor, M. Conditions influencing the removal of phosphate from synthetic wastewater: Influence of the ionic composition. *Desalination* **2007**, *206*, 279–285. [\[CrossRef\]](#)
- Nguyen, D.D.; Ngo, H.H.; Guo, W.; Nguyen, T.T.; Chang, S.W.; Jang, A.; Yoon, Y.S. Can electrocoagulation process be an appropriate technology for phosphorus removal from municipal wastewater? *Sci. Total Environ.* **2016**, *563*–564, 549–556. [\[CrossRef\]](#)
- Asselin, M.; Drogui, P.; Benmoussa, H.; Blais, J.-F. Effectiveness of electrocoagulation process in removing organic compounds from slaughterhouse wastewater using monopolar and bipolar electrolytic cells. *Chemosphere* **2008**, *72*, 1727–1733. [\[CrossRef\]](#)
- Gatsios, E.; Hahladakis, J.N.; Gidarakos, E. Optimization of electrocoagulation (EC) process for the purification of a real industrial wastewater from toxic metals. *J. Environ. Manag.* **2015**, *154*, 117–127. [\[CrossRef\]](#) [\[PubMed\]](#)
- Wahab, M.A.; Hassine, R.B.; Jellali, S. Removal of phosphorus from aqueous solution by *Posidonia oceanica* fibers using continuous stirring tank reactor. *J. Hazard. Mater.* **2011**, *189*, 577–585. [\[CrossRef\]](#)
- Nguyen, D.D.; Ngo, H.H.; Yoon, Y.S. A new hybrid treatment system of bioreactors and electrocoagulation for superior removal of organic and nutrient pollutants from municipal wastewater. *Bioresour. Technol.* **2014**, *153*, 116–125. [\[CrossRef\]](#)
- Mandel, A.; Zekker, I.; Jaagura, M.; Tenno, T. Enhancement of anoxic phosphorus uptake of denitrifying phosphorus removal process by biomass adaption. *Int. J. Environ. Sci. Technol.* **2019**, *16*, 5965–5978. [\[CrossRef\]](#)
- Torresi, E.; Tang, K.; Deng, J.; Sund, C.; Smets, B.F.; Christensson, M.; Andersen, H.R. Removal of micropollutants during biological phosphorus removal: Impact of redox conditions in MBBR. *Sci. Total Environ.* **2019**, *663*, 496–506. [\[CrossRef\]](#)
- Lin, Z.; Wang, Y.; Huang, W.; Wang, J.; Chen, L.; Zhou, J.; He, Q. Single-stage denitrifying phosphorus removal biofilter utilizing intracellular carbon source for advanced nutrient removal and phosphorus recovery. *Bioresour. Technol.* **2019**, *277*, 27–36. [\[CrossRef\]](#)
- Ge, Y.; Lan, J.; Zhan, C.; Zhou, Y.; Ma, C.; Zhao, L. Biological removal of phosphorus and diversity analysis of microbial community in the enhanced biological phosphorus removal (EBPR) system. *Water Environ. J.* **2019**, *34*, 563–574. [\[CrossRef\]](#)
- Zou, H.; Wang, Y. Phosphorus removal and recovery from domestic wastewater in a novel process of enhanced biological phosphorus removal coupled with crystallization. *Bioresour. Technol.* **2016**, *211*, 87–92. [\[CrossRef\]](#) [\[PubMed\]](#)
- Qin, Z.; Shober, A.L.; Scheckel, K.G.; Penn, C.J.; Turner, K.C. Mechanisms of Phosphorus Removal by Phosphorus Sorbing Materials. *J. Environ. Qual.* **2018**, *47*, 1232–1241. [\[CrossRef\]](#)
- Shi, J.; Yin, D.; Xu, Z.; Song, D.; Cao, F. Fosfomycin removal and phosphorus recovery in a schorl/H₂O₂ system. *RSC Adv.* **2016**, *6*, 68185–68192. [\[CrossRef\]](#)
- Zhang, M.; Qiao, S.; Shao, D.; Jin, R.; Zhou, J. Simultaneous nitrogen and phosphorus removal by combined anammox and denitrifying phosphorus removal process. *J. Chem. Technol. Biotechnol.* **2018**, *93*, 94–104. [\[CrossRef\]](#)
- Shimpo, T.; Yoshikawa, T.; Morita, K. Thermodynamic study of the effect of calcium on removal of phosphorus from silicon by acid leaching treatment. *Metall. Mater. Trans. B* **2004**, *35*, 277–284. [\[CrossRef\]](#)
- Zhu, M.; Azarov, A.; Monakhov, E.; Tang, K.; Safarian, J. Phosphorus separation from metallurgical-grade silicon by magnesium alloying and acid leaching. *Sep. Purif. Technol.* **2020**, *240*, 116614. [\[CrossRef\]](#)
- Shu, J.; Wu, H.; Chen, M.; Peng, H.; Li, B.; Liu, R.; Liu, Z.; Wang, B.; Huang, T.; Hu, Z. Fractional removal of manganese and ammonia nitrogen from electrolytic metal manganese residue leachate using carbonate and struvite precipitation. *Water Res.* **2019**, *153*, 229–238. [\[CrossRef\]](#)
- Shu, J.; Liu, R.; Liu, Z.; Chen, H.; Tao, C. Simultaneous removal of ammonia and manganese from electrolytic metal manganese residue leachate using phosphate salt. *J. Clean. Prod.* **2016**, *135*, 468–475. [\[CrossRef\]](#)

23. Wang, R.; Shu, J.; Chen, M.; Wang, R.; He, D.; Wang, J.; Tang, C.; Han, Y.; Luo, Z. An innovative method for fractionally removing high concentrations of Ni^{2+} , PO_4^{3-} , TP, COD, and $\text{NH}_4^+\text{-N}$ from printed-circuit-board nickel plating wastewater. *Sep. Purif. Technol.* **2021**, *260*, 118241. [[CrossRef](#)]
24. Shu, J.; Chen, M.; Wu, H.; Li, B.; Wang, B.; Li, B.; Liu, R.; Liu, Z. An innovative method for synergistic stabilization/solidification of Mn^{2+} , $\text{NH}_4^+\text{-N}$, PO_4^{3-} and F^- in electrolytic manganese residue and phosphogypsum. *J. Hazard. Mater.* **2019**, *376*, 212–222. [[CrossRef](#)] [[PubMed](#)]
25. Yang, H.; Hu, Y.; Huang, D.; Xiong, T.; Li, M.; Balogun, M.S.; Tong, Y. Efficient hydrogen and oxygen evolution electrocatalysis by cobalt and phosphorus dual-doped vanadium nitride nanowires. *Mater. Today Chem.* **2019**, *11*, 1–7. [[CrossRef](#)]
26. Xiong, P.; Zhang, Y.; Bao, S.; Huang, J. Precipitation of vanadium using ammonium salt in alkaline and acidic media and the effect of sodium and phosphorus. *Hydrometallurgy* **2018**, *180*, 113–120. [[CrossRef](#)]
27. Yang, L.; Liang, X.; Han, Y.; Cai, Y.; Zhao, H.; Sheng, M.; Cao, G. The coupling use of advanced oxidation processes and sequencing batch reactor to reduce nitrification inhibition of industry wastewater: Characterization and optimization. *Chem. Eng. J.* **2019**, *360*, 1577–1586. [[CrossRef](#)]
28. Liu, B.; Liu, Z.; Yu, P.; Pan, S.; Xu, Y.; Sun, Y.; Pan, S.-Y.; Yu, Y.; Zheng, H. Enhanced removal of tris(2-chloroethyl) phosphate using a resin-based nanocomposite hydrated iron oxide through a Fenton-like process: Capacity evaluation and pathways. *Water Res.* **2020**, *175*, 115655. [[CrossRef](#)] [[PubMed](#)]