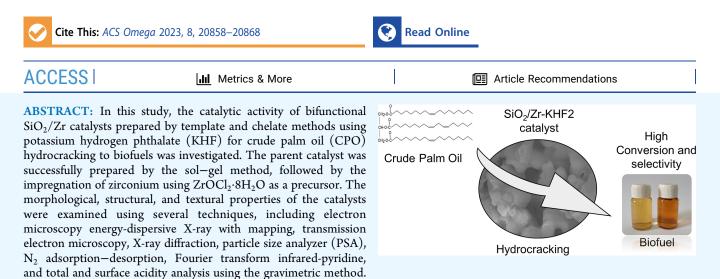


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Enhancement of Catalytic Activity on Crude Palm Oil Hydrocracking over SiO₂/Zr Assisted with Potassium Hydrogen Phthalate

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The results showed that the physicochemical properties of SiO₂/Zr were affected by different preparation methods. The template method assisted by KHF (SiO₂/Zr-KHF2 and SiO₂-KHF catalysts) provides a porous structure and high catalyst acidity. The catalyst prepared by the chelate method assisted by KHF (SiO₂/Zr-KHF1) exhibited excellent Zr dispersion toward the SiO₂ surface. The modification remarkably enhanced the catalytic activity of the parent catalyst in the order SiO₂/Zr-KHF2 > SiO₂/Zr-KHF1 > SiO₂/Zr > SiO₂-KHF > SiO₂, with sufficient CPO conversion. The modified catalysts also suppressed coke formation and resulted in a high liquid yield. The catalyst features of SiO₂/Zr-KHF1 promoted high-selectivity biofuel toward biogasoline, whereas SiO₂/Zr-KHF2 led to an increase in the selectivity toward biojet. Reusability studies showed that the prepared catalysts were adequately stable over three consecutive runs for CPO conversion. Overall, SiO₂/Zr prepared by the template method assisted by KHF was chosen as the most prominent catalyst for CPO hydrocracking.

1. INTRODUCTION

Global population expansion has resulted in a decline in the petroleum supply as a vital energy source. This is primarily due to the non-renewable nature of petroleum fuels, which require an extended period for recharge.¹ Worldwide energy consumption has risen in parallel with the expansion of the industrial sector, thus encouraging the necessary exploration of renewable and environmentally acceptable alternative energy sources.² Biofuels are among the most intriguing alternative energy sources currently being explored because they are ecofriendly and sustainable. They are broadly extracted from a clean energy source such as vegetable oil which provides noncontaining nitrogen and sulfur chemicals.³ Vegetable oil-based feedstocks consist predominantly of triglycerides, which can be easily transformed into liquid biofuels compared to other existing biomasses.⁴ Specifically, Indonesia produces a considerable amount of crude palm oil (CPO) and has an extremely high yield per hectare compared to other vegetable oils. Given its quantity and importance to the Indonesian economy, CPO is both promising and cost-effective as a raw material for manufacturing biofuels. Various energy conversion technologies have been developed to transform triglyceride feedstock into biofuels. Pyrolysis and transesterification are the most commonly used methods for producing biofuels. Nevertheless, when used in engines, the high oxygen content and acidity biofuels produced by the pyrolysis method, as well as other shortcomings produced by the transesterification method, such as high viscosity and low energy content, cause difficulties and are relatively not suitable for long-term production.⁵ In these circumstances, the catalytic hydrocracking process provides benefits such as low operational cost, high conversion, and yields toward biofuels.⁶ Hydrocracking is a process that involves the successive breaking of

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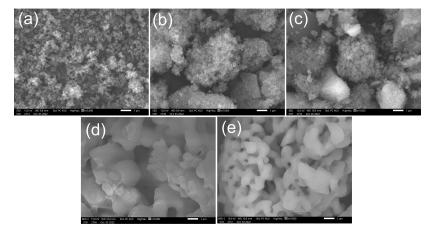


Figure 1. SEM micrographs of (a) SiO₂, (b) SiO₂/Zr, (c) SiO₂/Zr-KHF1, (d) SiO₂/Zr-KHF2, and (e) SiO₂-KHF at 10,000× magnification.

carbon bonds and hydrogenation of bigger hydrocarbon molecules, resulting in smaller ones. 7

The development of a selective hydrocracking reaction catalyst is critical for ensuring that the process is efficient and profitable. This poses a challenge in producing synthesis processes with controlled features that promote high catalytic activity. Catalysts for hydrocracking processes are typically metal dispersed on the acid support. The metal function involves hydro/dehydrogenation reactions, and in acid supports, the cracking reaction is performed via a bifunctional system.⁸ NiMo/Al₂O₃ is a commonly utilized conventional hydrotreating catalyst. Bentonites, zeolites, amorphous silica-alumina, mesoporous silica (such as SBA-15 and MCM 41), metal oxides, and mixed oxides have also been investigated.⁹

Particularly, various metal-supported catalysts have been employed for biofuel production through CPO hydroconversion. Subsadsana et al.¹⁰ reported that ZSM-5/MCM-41 loaded with NiMoW promoted conversion up to 62.60 with 9.23% gasoline yield under 2 h reaction at 400 °C for 2 h. Utami et al.⁷ reported that the Cr/ZrO₂ catalyst exhibits selectivity toward 65.85% of the gasoline fraction. Among other supports, SiO₂ offers a high specific surface area, excellent thermal stability, and tunable porosity, making it appropriate for the catalyst support.¹¹ The metal catalysts are often based on noble metals; however, they are exceedingly expensive and susceptible to poisoning and deactivation during their application in hydroconversion reactions.¹² The selection of an adequate non-noble metal-based catalyst for the hydrocracking process is necessary. Various active metals, such as nickel, copper, zirconia, and zinc,¹³⁻¹⁵ have been combined with SiO₂ supports. On the other hand, zirconia has been recognized as a comparatively affordable, low toxicity, green, and efficient catalyst for numerous main chemical transformations due to its Lewis acid behavior and high catalytic abilities.¹⁶ Ma et al.¹⁷ discovered that Zr species might improve the acidity characteristics of $MoS_2/SiO_2-Al_2O_2$, resulting in increased catalytic activity for heavy-oil hydrocracking. Another study revealed that the association between Zr loading and catalyst selectivity is consistent with the enhancement of active site formation at the interface between the metal atoms of the Co and Zr promoter species under the SiO₂ support. This catalyst significantly improves propane dehydrogenation compared to the parent Co/SiO₂ catalyst.¹⁸ As a result, there is a compelling motivation for SiO_2/Zr to evaluate its potential as an effective hydrocracking catalyst.

To tune the metal–support interaction, modifications such as morphology, acidity, and structural features of the catalysts are essential aspects that directly affect the catalytic activity. Various additive chemicals have been employed as chelating and templating agents to generate the desired structure.^{19–21} Wijaya et al.²² proposed NaHCO₃ as a template for monodisperse hierarchical silica. This method promotes the formation of a NiMo/SiO₂ catalyst toward a high liquid product yield in waste frying oil hydrocracking. Ren et al.²³ proposed glycine as a complexing agent to produce a well-dispersed metal-supported Ni/SiO₂ catalyst. Other complexing agents, such as ETDA, citric acid, and ethylene diamine, have been employed to enhance the SiO₂ catalyst by providing excellent catalytic features.^{24–26}

In this context, for the first time, potassium hydrogen phthalate (KHF) was employed as a chelating and templating agent for SiO₂/Zr preparation. These methods promote different characteristics that affect the properties of the catalyst as well as the performance of CPO hydrocracking in biofuels. KHF compounds are inexpensive, abundant, and easy to maintain. According to the literature review, neither exploration nor study has been reported yet to compare different preparation methods using KHF as a chelating and templating agent for SiO₂/Zr. The catalyst characteristics were assessed using several techniques. Furthermore, the reusability of the catalyst was evaluated to determine its stability in CPO conversion.

2. RESULTS AND DISCUSSION

2.1. Characterization of Catalysts. Several analyses were conducted to characterize the morphological, structural, and textural properties of the catalysts. Figure 1 depicts the scanning electron microscopy (SEM) micrographs of the parent SiO₂, SiO₂/Zr, and their different modifications involving KHF, that is, the chelating (SiO₂/Zr-KHF1) and templating (SiO₂/Zr-KHF2) methods. It is apparent that the parent SiO₂ (Figure 1a) has a surface morphology with small particles distributed uniformly and exhibits a relative absence of aggregation. After impregnation with Zr (Figure 1b), the surface morphology of SiO₂ tended to agglomerate, indicating the formation of a metal-supported phase. According to Nadia et al.,²² the formation of agglomerates during the impregnation process suggests that the metal species were successfully loaded onto the supported surface material. The SiO₂/Zr-KHF1 (Figure 1c) catalysts exhibit irregular shapes, suggesting

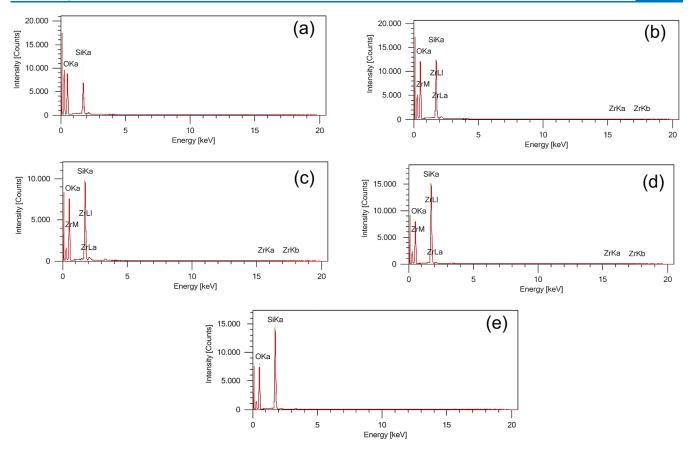


Figure 2. EDX spectra of (a) SiO₂, (b) SiO₂/Zr, (c) SiO₂/Zr-KHF1, (d) SiO₂/Zr-KHF2, and (e) SiO₂-KHF.

Table 1. Elemental Composition of the Catalyst Determined by EDX

	atomic (wt %)				
elements	SiO ₂	SiO ₂ /Zr	SiO ₂ /Zr-KHF1	SiO ₂ /Zr-KHF2	SiO ₂ -KHF
Si	18.21 ± 0.12	22.3 ± 0.10	22.46 ± 0.12	29.35 ± 0.02	30.20 ± 0.13
0	81.75 ± 0.33	77.47 ± 0.27	76.78 ± 0.33	70.36 ± 0.29	69.80 ± 0.30
Zr		0.15 ± 0.02	0.76 ± 0.03	0.29 ± 0.02	

that the chelating agent of KHF randomly increases the dispersion of Zr on the SiO₂ surface. Notably, SiO₂/Zr-KHF2 (Figure 1d) exhibits a different surface morphology compared to SiO₂/Zr-KHF1. SiO₂/Zr prepared by the template method assisted by KHF exhibited a porous surface morphology. In this case, the KHF species were eliminated during calcination, leading to the formation of pores. Similarly, SiO₂-KHF displayed a porous surface morphology but with a more ordered structure.

The energy-dispersive X-ray (EDX) spectra of the modified catalysts and their elemental compositions are shown in Figure 2 and Table 1, respectively. Undoubtedly, the parent SiO₂ and both SiO₂-KHF consisted of Si and O atoms with no impurities, whereas the Zr element was observed in the SiO₂/Zr catalyst, suggesting that the Zr species was successfully incorporated with SiO₂. The Zr content on both modified catalysts prepared by the template and chelate methods varied due to the uneven metal distribution on the SiO₂.²⁷

The EDX mapping (Figure 3) shows that the Si and Zr distributions are affected differently depending on the preparation method. Under the chelating method of KHF, Zr is homogeneously distributed toward the SiO₂ surface

owing to the strong interaction between the metal and KHF. In this case, the calcination process caused each particle to incline closer. Meanwhile, the templating method caused the catalyst to form an irregular metal distribution. The same elemental distribution feature was also revealed for the parent SiO_2 prepared by the templating methods.

The transmission electron microscopy (TEM) images of the parent SiO₂, SiO₂/Zr, and their modifications using different methods are presented in Figure 4. The parent SiO₂ catalyst (Figure 4a) generally exhibits a spherical particle in nature, whereas semispherical particle agglomerates are formed on the SiO_2/Zr catalyst (Figure 4b). Compared with the parent SiO_2/Zr Zr, the SiO₂/Zr-KHF1 (Figure 4c) shows an increase in tiny black spots, presumably originating from the impregnated species.²⁸ This suggests that the chelate methods enhance the metal dispersion toward the SiO₂ surface. Distinctive images from SiO₂/Zr-KHF2 (Figure 4d) and SiO₂-KHF were observed because of the preparation of the template method using KHF as an agent. The dark field characteristics with no obvious clear-light patches suggest the presence of a mesoporous structure.²⁹ Meanwhile, Zr species were not well noticed in the SiO₂/Zr-KHF2. Overall, the TEM image analysis corroborated the SEM-EDX results.

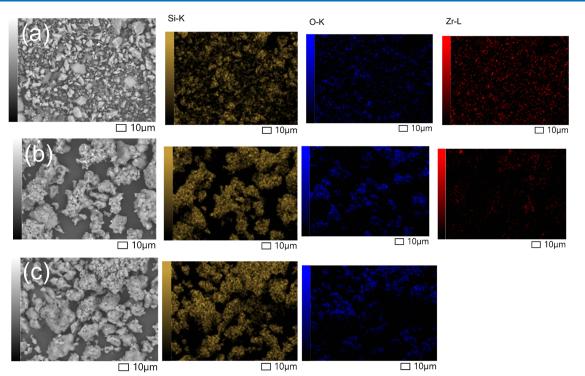


Figure 3. EDX mapping of (a) SiO₂/Zr-KHF1, (b) SiO₂/Zr-KHF2, and (c) SiO₂-KHF.

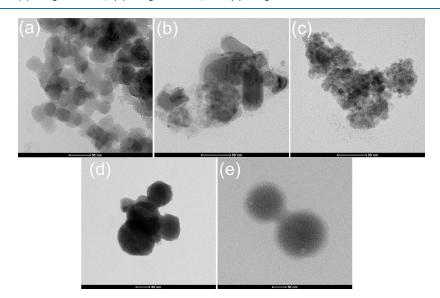


Figure 4. TEM images of (a) SiO₂, (b) SiO₂/Zr, (c) SiO₂/Zr-KHF1, (d) SiO₂/Zr-KHF2, and (e) SiO₂-KHF.

The diffractograms of the parent SiO₂ and SiO₂/Zr and their modifications were assessed to determine the crystal structures of the catalysts. The SiO₂ catalyst (Figure 5a) exhibits a broad diffraction peak 2θ at 22° , suggesting the formation of an amorphous structure.³⁰ This typical SiO₂ peak is also consistently reported by other studies.^{19,31} The diffraction peaks at $2\theta = 30$, 35.83, 50.28, and 60.08° from SiO₂/Zr (Figure 5b) were ascribed to ZrO₂ with a tetragonal phase (ICDD no. 80-2155).³² A broad peak was also observed at low 2θ values, indicating that the amorphous silica was retained during impregnation. Meanwhile, no zirconia phase was discerned in SiO₂/Zr-KHF1, indicating good dispersion on the surface of SiO₂, which is presumably less than the detection limit of the X-ray diffraction (XRD).²² A similar result was also

reported by Majewski et al.³³ when preparing the Ni@SiO₂ catalyst, which showed that the unobserved XRD peaks were due to the amorphous phase or the presence of highly dispersed Ni. Furthermore, an appreciable change in the diffractograms can be observed for both SiO₂/Zr-KHF2 and SiO₂-KHF. The 2 θ peaks of SiO₂/Zr-KHF2 (Figure 5d) reveal a highly crystalline structure attributed to the formation of quartz and cristobalite mixes that overlapped with the ZrO₂ phases. The template method assisted by KHF (Figure 5e) provides a highly ordered silica structure, thus transforming the amorphous phase into the crystalline phase.

Figure 6 shows the particle size distributions of all the catalysts. The particle size distribution of the parent SiO_2 catalyst (Figure 6a) can be seen to be relatively uniform with a

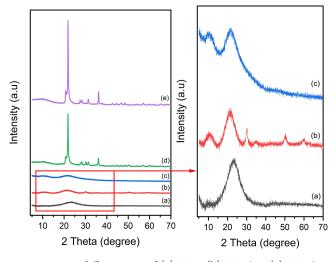


Figure 5. XRD diffractogram of (a) SiO_2 , (b) SiO_2/Zr , (c) SiO_2/Zr -KHF1, (d) SiO_2/Zr -KHF2, and (e) SiO_2 -KHF.

narrow size distribution, whereas the SiO₂/Zr catalyst (Figure 6b) exhibits a non-uniform particle size distribution owing to the effect of the impregnation process. Gel formation occurs uniformly in the unmodified SiO₂ catalyst because no molecules interfere with gelation. In this case, Si(OH)₄ from tetraethyl orthosilicate (TEOS) led to a uniform SiO₂ particle distribution. The SiO₂/Zr-KHF1 catalyst (Figure 6c) showed a particle size distribution similar to that of the parent SiO₂ catalyst, suggesting that the chelating effect of KHF enhanced the particle size distribution of the catalysts. In contrast, the SiO₂/Zr-KHF2 catalyst (Figure 6d) exhibited a wide particle size distribution, suggesting that the template method increased the particle size distribution of SiO₂-KHF also revealed properties similar to those of SiO₂/Zr-KHF2 catalysts. When KHF is

added during the gelatinization process, KHF interacts with the Si species from TEOS before gel formation so that part of the Si species is bound to four acetate groups while others are bound to KHF, which will eventually change the features of the $Si(OH)_4$ gel, thereby changing the particle size distribution.

The average particle size of the catalysts is listed in Table 2. It is clear that the SiO_2/Zr catalyst exhibited a larger average

Table 2. Average Particle Size of Catalysts Determined by PSA

catalysts	average particle size (μm)
SiO ₂	22.65 ± 0.35
SiO ₂ /Zr	49.49 ± 0.04
SiO ₂ /Zr-KHF1	14.55 ± 0.35
SiO ₂ /Zr-KHF2	38.61 ± 0.07
SiO ₂ /KHF	31.49 ± 0.07

particle size than the parent SiO_2 . This is presumably due to the formation of agglomerated SiO_2 particles.¹⁶ It is apparent that the template method assisted by KHF increased the average particle size relative to the parent SiO_2 , whereas it decreased the average particle size of the SiO_2/Zr catalyst. The chelate method assisted by KHF (SiO_2/Zr -KHF1) promoted a decrease in the average particle size of the catalyst, presumably owing to the complex interaction between KHF and Zr.

The acidity properties of all prepared catalysts are shown in Figure 7. It is noticeable that the parent SiO_2 catalyst had the lowest acidity property from the low Lewis acid sites from Si^{4+} ions.²⁷ An increase in the total and surface acidity was observed in SiO_2/Zr due to the addition of new Lewis acid sites from Zr^{4+} ions.³⁴ Furthermore, chelate and template methods assisted by KHF successfully enhanced the acidity of the parent catalysts. The KHF-assisted chelate and template methods successfully enhanced the acidity of the parent

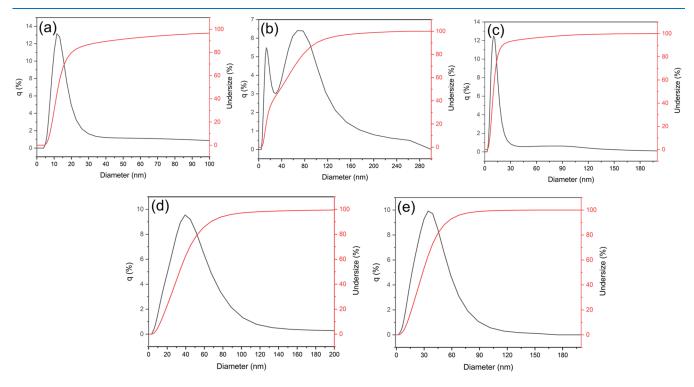


Figure 6. Particle size distribution of (a) SiO₂, (b) SiO₂/Zr, (c) SiO₂/Zr-KHF1, (d) SiO₂/Zr-KHF2, and (e) SiO₂-KHF.

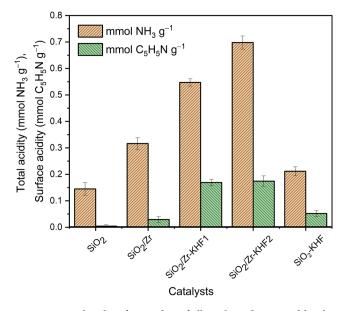


Figure 7. Total and surface acidity of all catalysts determined by the gravimetric methods using NH_3 and C_6H_5N as probes.

catalysts. SiO₂/Zr-KHF2 had a higher total acidity than SiO₂/Zr-KHF1, but the surface acidity remained relatively constant, suggesting the same acidity features on the surface of the catalysts. The pores provided by the template methods might predominantly promote efficient adsorption of the probes toward the acidic sites, thereby increasing the acidity of the catalysts. Similarly, the SiO₂-KHF had a higher total acidity value than the parent SiO₂, suggesting that the pores generated by the KHF template provided efficient base adsorption toward the Si⁴⁺ sites.

The Fourier transform infrared (FTIR)-pyridine spectra of the catalysts are shown in Figure 8. These spectra distinguish between the Brønsted and Lewis acid sites contained in the catalyst. The absorption peak at ~1625 cm⁻¹ is attributed to the presence of Bronsted acid sites from the pyridinium ion.³⁵ The absorption band at ~1430 cm⁻¹ corresponds to coordinated pyridine with Lewis acid sites.³⁶ It can be seen that the absorption band in both regions increased after the

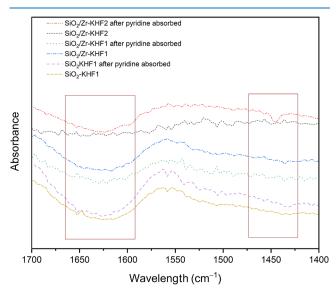


Figure 8. FTIR-pyridine spectra of all catalysts.

adsorption of pyridine by the catalyst. SiO_2/Zr -KHF2 exhibited the highest intensity compared to the other catalysts, which is consistent with the acidity results analyzed by the gravimetric method.

The N_2 physisorption of all the catalysts is shown in Figure 9. It can be seen that all catalysts exhibit a type IV isotherm,

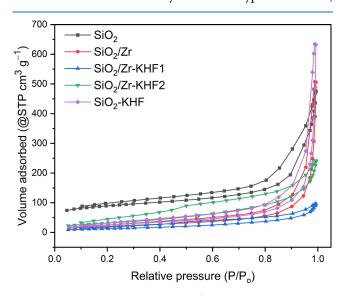


Figure 9. N_2 adsorption desorption of the parent SiO₂ and their modifications using different methods.

indicating a dominant mesoporous material.³⁷ The H_4 hysteresis was also observed on all catalysts, providing a narrow slit mesopore channel.³⁸ Sydorchuk et al.³⁹ stated that this type of loop hysteresis reflects the connectivity of pores of varying sizes, and the material develops noticeable micropores and mesopores. The catalyst's mesoporous characteristic might overcome the inadequate limitation of triglyceride diffusion.⁴⁰

The textural properties of the parent SiO_2 and its modifications are listed in Table 3. The S_{BET} of SiO_2/Zr was

Table 3. Textural Properties of All Catalysts

catalysts	$S_{\rm BET} \ ({\rm m}^2 \ {\rm g}^{-1})$	$V_{\rm p}~({\rm cc~g^{-1}})$	<i>d</i> (nm)
SiO ₂	294	0.73	9.92
SiO ₂ /Zr	76.43	0.76	39.77
SiO ₂ /Zr-KHF1	45.35	0.14	12.35
SiO ₂ /Zr-KHF2	220.5	0.80	14.51
SiO ₂ -KHF	90.7	0.92	40.57
SiO ₂ /Zr-KHF2	220.5	0.80	14.51

lower $S_{\rm BET}$ compared with the parent SiO₂ owing to the pore blocking of Zr species.⁴¹ Despite the fact that the SiO₂/Zr-KHF2 prepared by the template method exhibited a decrease in $S_{\rm BET}$, this method increased the total pore volume ($V_{\rm p}$), suggesting an enhancement in the pore features of the catalyst. Conversely, SiO₂/Zr-KHF1 prepared using the chelate method significantly decreased the pore volume. Meanwhile, an appreciable increase in pore diameter (*d*) in SiO₂-KHF is observed compared with the parent SiO₂ owing to the template-assisted effect of the KHF species, particularly the generation of pores with a high diameter.

2.2. Catalytic Test. The catalytic activities of the parent SiO_2 , SiO_2/Zr , and their modifications for CPO hydrocracking are shown in Figure 10. It is recognizable that SiO_2/Zr exhibits a higher conversion (86.37%) than the parent SiO_2 (70.42%)

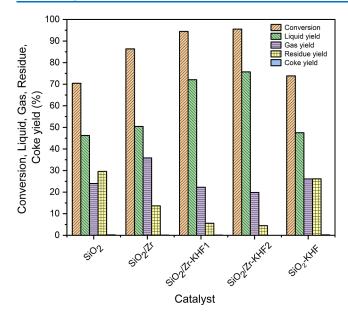


Figure 10. Catalytic activity of CPO hydrocracking over various catalysts.

owing to the presence of Zr Lewis acid sites that promote an increase in the CPO conversion. Similarly, Yongde et al.⁴⁴ reported that Zr species could enhance the hydrocracking catalytic activity of MoS₂/SiO₂-Al₂O₃-catalysts by increasing the sum of acidic sites. This treatment can improve both the hydrogenation and cracking activities of the bifunctional catalysts. Subsadsana et al.⁴³ observed the lowest conversion during CPO hydrocracking over ZSM-5, presumably because of the low acidity of the catalyst. The modification of both parent SiO₂ and SiO₂/Zr remarkably enhanced the CPO conversion in the following order: $SiO_2/Zr-KHF2$ (95.53%) > $SiO_2/Zr-KHF1$ (94.43%) > SiO_2-KHF (73.83%). This increase in conversion may be correlated with the high acidity of the corresponding catalyst, which is consistent with the results of the acidity measurements. In this respect, the template method using KHF promotes an increase in the acidity of the SiO_2/Zr catalyst compared with the chelate method. SiO₂/Zr-KHF2 promoted effective mass transport as a catalyst because of its efficient mass transport for interaction with the acid sites. Subsadsana et al.¹⁰ reported that the NiMoW-ZSM-5/MCM-41 catalyst exhibits 62.60-71.40% conversion of CPO during 4 h hydrocracking at 400 °C, whereas another study described that the CoMo/Al₂O₃ promotes the CPO conversion up to 64.21% under 1 h hydrocracking at 350° and 500 psi.⁴⁴

With regard to the liquid yield, it can be seen that indistinguishable trends are observed in Figure 10, in which the SiO_2/Zr -KHF2 (75.71%) exhibits the highest liquid yield compared with other catalysts. The greater the number of acid sites in the catalytic system, the greater the number of hydrogen radicals acquired and interacted with the feed, and as a consequence, increased the liquid yield.⁴⁵ The comparatively high gas yields generated by all catalysts range from 19.82–35.84%, which might be due to high-temperature hydrocracking. The SiO_2/Zr catalyst exhibited the highest gas yield, presumably attributed to successive CPO hydrocracking, leading to an increase in the gas yield. It was observed that both modified SiO_2/Zr -KH1 and SiO_2/Zr -KHF2 successfully promoted the hydrocracking reaction toward a high liquid yield with low residues, suggesting an effective catalyst for the

CPO hydrocracking process. It is apparent that the coke yield generated by the parent SiO₂ catalyst decreased after Zr loading from 0.21 to 0.09%. Al-Marshed et al.⁴⁶ stated that the presence of metal dispersed could inhibit coke formation due to their hydrogen-transfer reactions. Moreover, the coke yield of SiO₂/Zr continuously decreased after modification by both the template and chelate methods-KHF, but the SiO₂-KHF catalyst remained the same as that of the parent SiO₂. The decreasing order was SiO₂/Zr < SiO₂/Zr-KHF1 < SiO₂/Zr-KHF2, suggesting that the SiO₂/Zr-KHF2 catalyst could effectively suppress the hydrocracking process toward low coke formation.

The effect of various catalysts on product selectivity toward biofuel fractions during CPO hydrocracking is presented in Figure 11. As expected, all catalysts provided different

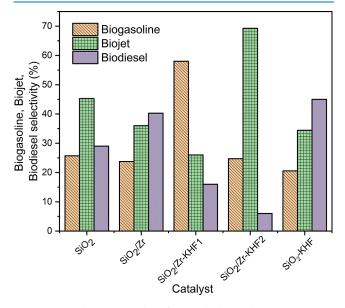


Figure 11. Selectivity results of CPO hydrocracking over various catalysts.

selectivities toward different biofuel fractions. The parent SiO_2 exhibited high selectivity toward biojet (45.28%), whereas the parent SiO₂/Zr promoted high selectivity toward biodiesel (40.25%). The biojet selectivity tends to increase up to 69.27% after modification by the template method $(SiO_2/$ Zr-KHF2) owing to the dominant effect of the mesopore structure. Hydroconversion in the mesopore cavity may hinder the formation of large intermediaries during the hydrocracking process, hence controlling the size of the preferred hydrocarbon molecule selective to the biojet. Meanwhile, SiO2-KHF dominantly generated a biofuel fraction selectivity toward biodiesel (45.01%) rather than the biojet (45.01%), presumably due to the effect of the porous structure provided by the template method assisted by KHF, thus promoting diffusion effectively. Interestingly, the SiO₂/Zr-KHF catalyst exhibited a higher selectivity toward biogasoline (58%) than the other catalysts. This may be due to the presence of dominant micropores provided by the chelate method assisted by the KHF catalyst.

Table 4 shows the catalytic activity of various catalysts during palm oil hydrocracking. It can be seen that the SiO_2/Zr modified by KHF using the chelate and template method exhibits an adequate performance during CPO hydroconversion compared with other reported catalysts (Table 4)

Table 4. Comparison of Catalytic Activity Using Various Catalysts on Palm Oil Hydrocracking

catalyst	reaction condition	results	references
zeolite Y	batch reactor, mass ratio of palm oil to catalyst = $20:1$, $T = 390^{\circ}C$	conversion = ca. 70 wt %, $Y_{\text{bio-jet}}$ = 42 wt %, $S_{\text{hydrocarbon}}$ = 91%	47
NiW-HY	batch reactor, $T = 400^{\circ}$ C, for 120 min, H ₂ flow rate = 500 cm ³ min ⁻¹ , $P = 3$ MPa for 30 min	conversion = 50.38%, $Y_{\text{biogasoline}}$ = 13.88%, $Y_{\text{biokerosene}}$ = 18.20%, $Y_{\text{biodiesel}}$ = 18.30%	48
Ni-SAPO-34	batch reactor, mass ratio of palm oil to catalysts = 20:1, T = 390°C for 8 h, P = 3 MPa	conversion = 97.5%, $Y_{\text{bio-jet}}$ = 42.03%, S_{alkene} = 65%, S_{arene} = 11%	49
NiW-HZSM-5	batch reactor, $T = 400^{\circ}$ C, $t = 120$ min, H ₂ flow rate = 500 cm ³ min ⁻¹ , $P = 3$ MPa for 30 min	conversion = 48.18%, $Y_{\text{biogasoline}}$ = 10.44%, $Y_{\text{biokerosene}}$ = 19.56%, $Y_{\text{biodiesel}}$ = 18.22%	48
Pd—Fe	batch reactor, palm oil = 100 mL, catalyst loading = 0.9 g, T = 400°C for 2 h, P = 60 bar	$\begin{array}{l} \text{conversion} = 94\%, \ S_{\text{gasoline}} = 62.20\%, \\ S_{\text{kerosene}} = 31.71\%, \ S_{\text{diesel}} = 6.63\%, \ Y_{\text{diesel}} = 62.20\%, \\ Y_{\text{kerosene}} = 31.71\% \end{array}$	40
MoN/bentonite	continuous fixed bed reactor, $T = 458^{\circ}$ C for 0.12 h, mass ratio of palm oil to catalyst = 0.12 w/w, flow rate palm oil = 11.94 g min ⁻¹ , H ₂ flow rate = 2 mL min ⁻¹	conversion = 78.33%, Y_{liquid} = 50.32%, Y_{gas} = 44%, biogasoline fraction = 28.7%, bioaviation fraction = 15.69%	3
$CoMo/Al_2O_3$	batch reactor, $T = 350^{\circ}$ C for 1 h, $P = 500$ psi	conversion = 64.21 wt %, $Y_{\rm liquid}$ = 90.56 wt %, $Y_{\rm gas}$ = 8.98 wt %	44
SiO ₂ /Zr-KHF1	continuous fixed bed reactor, catalyst weight = 0.5 g, CPO flow rate = 20 mL h^{-1} , $T = 500^{\circ}C$	$\begin{array}{l} \mbox{conversion}=94.43\%, S_{\rm biogasoline}=58\%, S_{\rm biojet}=26\%,\\ S_{\rm biodiesel}=16\%, \ Y_{\rm liquid}=72.08\% \end{array}$	this work
SiO ₂ /Zr-KHF2	continuous fixed bed reactor, catalyst weight = 0.5 g, CPO flow rate = 20 mL h^{-1} , T = 500°C	conversion = 95.53%, $S_{\text{biogasoline}}$ = 24.72%, S_{biojet} = 69.27%, $S_{\text{biodiesel}}$ = 6.01%, Y_{liquid} = 75.71%	this work
SiO ₂ -KHF	continuous fixed bed reactor, catalyst weight = 0.5 g, CPO flow rate = 20 mL h ⁻¹ , $T = 500^{\circ}$ C	conversion = 73.83%, $S_{\text{biogasoline}}$ = 20.56%, S_{biojet} = 34.43%, $S_{\text{biodiesel}}$ = 45.01%, Y_{liquid} = 47.52%	this work

with high conversion and liquid yield and promotes high selectivity toward biogasoline and biojet.

The reusability of the catalysts was assessed in three consecutive runs to evaluate their stability in the conversion of CPO. The spent catalyst was washed with hexane (50 mL), heated at 105 °C for 1 h, and subsequently subjected to heat treatment, including calcination at 850 °C for 3 h with an O₂ flow rate of 30 mL h⁻¹ and reduction at 600 °C for 3 h with a H₂ flow rate of 30 mL h⁻¹. As shown in Figure 12, generally, all

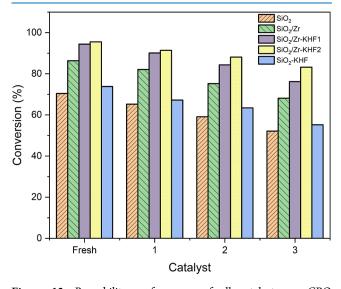


Figure 12. Reusability performance of all catalysts on CPO conversion.

catalysts showed a decrease in the catalytic performance, and a prolonged decrease was observed after three consecutive runs. This is due to the heavy product deposition on the catalyst, such as coke, which blocks the active sites of the catalyst.^{3,42}

Compared to the parent catalyst, a relatively insignificant decrease was observed for SiO_2/Zr -KHF2, followed by the SiO_2/Zr -KHF1 catalyst, suggesting that the modified catalyst could inhibit coke formation. Further analysis of coke yield on the spent catalyst emphasizes this notion. Based on Table 5,

Table 5. Coke Yield of Spent Catalysts

		coke yield (%)	
catalysts	1st	2nd	3rd
SiO ₂	0.21	0.51	1.03
SiO ₂ /Zr	0.09	0.32	0.83
SiO ₂ /Zr-KHF1	0.073	0.28	0.44
SiO ₂ /Zr-KHF2	0.001	0.10	0.35
SiO ₂ -KHF	0.21	0.32	0.67

 SiO_2 exhibited the highest increase in coke yield after a series of consecutive runs, suggesting a decrease in the catalytic performance. Meanwhile, the modified catalyst showed an insignificant increase in coke yield, with SiO_2/Zr -KHF2 showing the lowest coke yield after three consecutive runs. The modification of SiO_2/Zr using KHF as a templating agent successfully enhanced the properties of the catalyst, which inherently promoted hydrocracking catalytic activity toward high CPO conversion.

3. CONCLUSIONS

In this study, bifunctional SiO₂/Zr catalysts were synthesized by chelating and templating methods using KHF and were employed for hydrocracking CPO to biofuels. The physicochemical features of the parent and modified catalysts were assessed by several procedures including SEM-EDX with mapping, TEM, XRD, PSA, N₂ adsorption-desorption, FTIRpyridine, and total and surface acidity analysis using the gravimetric method. The empirical results revealed that the modification of the parent SiO_2 and SiO_2/Zr with both the template and chelate methods assisted by KHF significantly promoted CPO conversion and liquid products in the order SiO_2 -KHF > SiO_2/Zr -KHF1 > SiO_2/Zr -KHF2. Moreover, the difference in the preparation method using KHF also showed different catalyst properties that directly affected the catalytic activity toward a particular biofuel selectivity. SiO₂/Zr-KHF2 predominantly promoted selectivity toward high bio-jet, whereas SiO₂/Zr-KHF1 promoted selectivity toward biogasoline. Furthermore, a reusability study showed that the modified

catalysts were appreciably stable during the three reaction cycles and suppressed coke formation.

4. MATERIALS AND METHODS

4.1. Materials. TEOS $[Si(OC_2H_5)_4, 98\%]$, ammonia solution (NH₄OH, 28%), ethanol (CH₃OH, ≥99.5), KHF (C8H₅KO₄ ≥99.95%), zirconium(IV) oxide chloride octahydrate (ZrOCl₂·8H₂O, ≥97.0%), and pyridine (C₅H₅N, ≥99.9%) were obtained from Sigma-Aldrich without further purification.

4.2. Preparation of SiO₂ Assisted with KHF as a Templating Agent. Briefly, 25 mL of TEOS was diluted with 50 mL of ethanol and stirred for 15 min at ambient temperature. Subsequently, 16.5 mL of KHF solution (10% w/v) was introduced and stirred for 3 h at ambient temperature, followed by gradual dripping of 2 mL of ammonia solution. Subsequently, the solution was aged at ambient temperature for 30 min and then dried at 85 °C for 1 day. The 60-mesh powder was calcined at 850 °C for 3 h at an O₂ flow rate of 30 mL h⁻¹, and the resulting powder was denoted as SiO₂-KHF. The catalyst was then washed with DI water and centrifuged at 3500 rpm for 10 min until the pH was close to neutral. The solution was heated until the water evaporated and then dried at 120 °C for 1 day. A SiO₂ catalyst, without the addition of KHF, was also prepared as a control.

4.3. Synthesis of SiO_2/Zr Assisted with KHF as a Templating Agent. The as-prepared SiO_2 -KHF described earlier was mixed with 200 mL of zirconium(IV) oxide chloride (0.04 mol L⁻¹) and stirred for 1 h at ambient temperature. Furthermore, the temperature was moderately increased to 85 °C, and the mixture was stirred for 3 h until a paste was formed. The paste was subsequently heated at 120 °C for 3 h, calcined at 850 °C for 3 h with an O₂ flow rate of 30 mL h⁻¹, and reduced at 600 °C for 3 h with an H₂ flow rate of 30 mL h⁻¹. The catalyst is denoted as SiO_2/Zr KHF2. A SiO_2/Zr catalyst, without the addition of KHF, was also prepared as a control.

4.4. Synthesis of SiO₂/Zr Assisted with KHF as a Chelating Agent. Briefly, 20 mL of ethanol was reacted with 25 μ L of TEOS with stirring for 15 min at ambient temperature. Next, 2.578 g of zirconium(IV) oxide chloride powder and a KHF solution (16.5 mL) were mixed and added to the previously prepared solution and stirred for 3 h. Subsequently, 2 mL of the ammonia solution was gradually dripped. The solution was aged at ambient temperature for 30 min and then dried at 85 °C for 1 day. The 60-mesh powder was calcined at 850 °C for 3 h at an O_2 flow rate of 30 mL h⁻¹, and the resulting powder was denoted as SiO₂/ZrO₂-KHF. Next, the catalyst was washed with DI water and centrifuged at 3500 rpm for 10 min until the pH closed to neutral. The solution was heated until the water evaporated and followed by drying at 120 °C for 1 day. The powder was subsequently calcined at 850 °C for 3 h at an O_2 flow rate of 30 mL h $^{-1}$ and reduced at 600 $^{\circ}\mathrm{C}$ for 3 h at an H_2 flow rate of 30 mL h^{-1}. The catalyst is denoted as SiO₂/Zr-KHF1.

4.5. Catalyst Characterization. SEM micrographs equipped with EDX were recorded using a JSM-IT200A/LA, JEOL (acceleration voltage of 20.00 kV and magnification of 10,000 times). TEM images were obtained using the Tecnai G2 20S-Twin function. A Rigaku Smart Lab X-ray powder diffractometer was used to analyze the diffractograms of the catalysts. The particle size distribution and average particle size of the catalysts were determined using a Horiba Partica LA-960

instrument. The measurements were calculated using the static light scattering method (0.01 to 5000 μ m). The total and surface acidity were assessed using the gravimetric methods with ammonia and pyridine as probes, as reported by others.⁵⁰ The catalyst containing pyridine was directly analyzed using an FT1R-8201PC infrared spectrophotometer (Shimadzu) to determine the acidic sites of the catalyst. The textural properties of the catalysts were analyzed by N₂ adsorption–desorption using NOVA Quantachrome at 77.35 K. The catalyst was outgassed at 275 °C prior to analysis. The surface area of the catalyst (S_{BET}) was determined using the Brunauer–Emmett–Teller (BET) multiplot method, whereas the properties of the catalyst pore were calculated by the Barrett–Joyner–Halenda method.

4.6. Catalytic Activity Test. A continuous system microcylindrical reactor was utilized to conduct the hydrocracking process with 0.5 g of the catalyst. The CPO feed with a flow rate of 20 mL h⁻¹ was injected into the reactor using a syringe pump. Hydrocracking was carried out at 500 °C for 1 h under a hydrogen atmosphere at a flow rate of 30 mL h⁻¹. The liquid product was analyzed using GC–MS (Thermo Scientific, TG-SMS column). The temperature was increased (5 °C min⁻¹) from 50 °C for 3 min to 300 °C for 10 min. The flow rate of helium as the carrier gas was 1 mL min⁻¹. Data analysis of the hydrocracking results was performed according to the following equations

conversion (% wt)
=
$$\frac{\text{CPO feed (g)} - \text{residue (g)}}{\text{CPO feed (g)}} \times 100\%$$
 (1)

$$Y_{\text{liquid}} (\% \text{ wt}) = \frac{\text{liquid product (g)}}{\text{CPO feed (g)}} \times 100\%$$
(2)

$$Y_{\text{coke}} (\% \text{ wt}) = \frac{\text{coke } (g)}{\text{CPO feed } (g)} \times 100\%$$
(3)

$$Y_{\text{residue}} (\% \text{ wt}) = \frac{\text{residue} (g)}{\text{CPO feed } (g)} \times 100\%$$
(4)

$$Y_{\text{gas}} (\% \text{ wt}) = 100\% - (Y_{\text{liqud product}} + Y_{\text{coke}} + Y_{\text{residue}})$$

$$\% \text{ wt}$$
(5)

$$S_{\text{liquid product}} (\%) = \frac{\% \text{ GCMS biofuel fraction area}}{\% \text{ GCMS total area}} \times 100\%$$
(6)

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Notes

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