Modelling the factors that influence exposure to SARS-CoV-2 on a subway train carriage

Supplementary Material

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13 Abstract

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In this supplementary material, we provide details on how the representative carriage is chosen when simulating passengers trips and estimating exposure to SARS-CoV-2 within the TVC model. We also show how passengers are allocated within 2m of an infected passenger during their journey, and give an overview of the method used in order to adjust the surface area in 0-1m and 1-2m of the infected passenger to account for possible positions of this passenger within the carriage. We estimate the surface area within the carriage as a whole and the region of the carriage within 2m of an infectious passenger. Finally, precise details on the implementation of the different droplet models and droplet evaporation calculations are provided, and a comprehensive list of parameter values within the TVC model is given.

14 1. Representative carriage selection

Instead of considering different carriage journeys as a stochastic element in the TVC model, which would be computationally prohibitive, a single carriage was selected, to represent an *average* or *rep-**resentative behaviour, for our numerical results. This representative carriage is depicted as a solid black line in Figure 2 in the main paper. In particular, the following approach was used to choose this representative carriage journey:

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• Only southbound (SB) routes were considered to represent travel into the city.

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- The total number of passengers carried over the trip in the representative carriage must be within 10% of the mean across all the carriages on the SB route.
- The integrated occupancy over all stops must be with 10% of the mean over all carriages on the SB route.
- We compare the boarding numbers at each station (normalised by total passengers on the journey)
 to the averages amongst the SB carriages, and select the carriage with the lowest error via an R^2 value.
 - We visually check the route against occupancy patterns, and against stops travelled.
- We check linearity of carriage at different loading percentages is sufficient. In particular, the loading percentages for the selected carriage were found to be linear with an R2 value of 0.97.

2. Process of allocating passengers to be within 2m of an infectious passenger

- In order to calculate a passenger's exposure as a result of being within 2m of an infectious passenger, a method for allocating passengers within the carriage is needed. This process occurs every time the passengers board and alight in each station, and is as follows:
- 1. When passengers board, the number of passengers on board, N_P is calculated. Passengers are initially assumed to be uniformly spread across the carriage, and classified to be within 0-1m, 1-2m or further than 2m away from infectious passengers.
- 2. The proportion of carriage floor area within 0-1m $(A_{01} [m^2])$ and 1-2m $(A_{12} [m^2])$ of an infectious passenger, and the total carriage floor surface area $(A_F [m^2])$ are used together with the number of passengers on board N_P to generate a target (rounded to an integer) number of passengers within 0-1m, T_{01} , and 1-2m, T_{02} , of an infectious passenger, as follows:

$$T_{01} = N_P \frac{A_{01}}{A_F}, \quad T_{12} = N_P \frac{A_{12}}{A_F}.$$

3. If the number of passengers initially allocated in 0-1m of an infectious passenger is less than T_{01} then, if possible, passengers are moved from the 1-2m region into the 0-1m region. If this is not possible then they are taken at random from the rest of the carriage.

- 4. If the number of passengers initially allocated in the 1-2m region is less than T_{12} then the spaces are filled by passengers from the rest of the carriage.
- 5. If the number of passengers within 0-1m of the infectious passenger is greater than T_{01} then the excess passengers are moved to the 1-2m region.
 - 6. If the number of passengers in the 1-2m region is greater than T_{12} then passengers are moved out of the region into the rest of the carriage. Passengers moved into this region within the previous step are chosen last from the list of passengers eligible to be moved out of the region.

3. Adjustment of proportion of carriage within 2m of an infectious passenger

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Here, we give an overview of the method used in order to adjust the surface area and available 53 volume in 0-1m and 1-2m of the infectious passenger to account for possible positions of this passenger 54 within the carriage; see Figure 1 which has been generated from available information in [1]. To begin, 55 a rectangular grid is generated with the same dimensions as the width and length of the carriage. At each grid point, a random sample is generated from a uniform distribution for a 1m disc and for an 57 annulus between 1m and 2m radii, see Figure 2. Then, the number of points that lie inside the carriage 58 is counted and divided by the total number of points to yield a proportion of the disc/annulus that lies 59 inside the carriage at a given point within the carriage. The proportion of the disc and the proportion of the annulus at a given point will be linked (Figure 1) and it is therefore necessary to consider what 61 the proportion at 1-2m is, given the proportion at 0-1m.

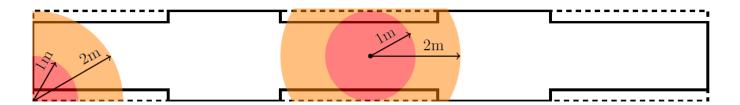


Figure 1: Depiction of 0-1m and 1-2m regions for different potential locations of the infectious passenger within the subway train carriage.

The array of proportions for 0-1m is then sorted from smallest to largest with the associated array of 1-2m values sorted according to the 0-1m value at that carriage position. The 0-1m values are then binned, the number of values in each bin counted and divided by the total number of points to generate a probability of the 0-1m value lying in that bin. An array of bin midpoints is also generated. We then

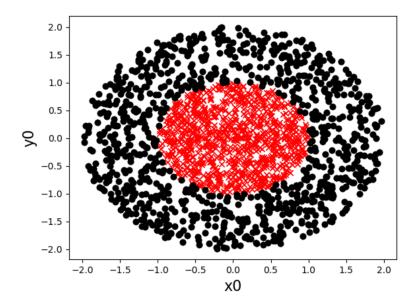


Figure 2: Uniform distribution of points within disc and annulus.

generate a sample of 0-1m carriage proportions (from the bin midpoints) with a weighting dictated by
the probability of a value lying in that bin.

A probability distribution for the 1-2m values is then generated as follows. The 1-2m values for a given 0-1m bin are binned using the same bin edges and widths as the 0-1m bins. As before, the number of values in each bin is counted and used to generate the probability of the 1-2m value lying in a given bin. These can then be used in conjunction with the bin midpoints to generate a random sample of 1-2m values if the 0-1m lies in the associated bin. This means that there are as many 1-2m probability distributions as there are 0-1m bins.

For each passenger that boards the carriage, instead of estimating their 0-1m and 1-2m proportions 75 (i.e., adjusted surface areas) by randomly allocating the passenger within the carriage and following the 76 approach above, their 0-1m and 1-2m proportions are directly sampled from the distributions computed 77 a priori as described above. This decreases computational cost of running stochastic simulations of the 78 carriage trip. In Figure 3 we carry out some numerical experiments to confirm that the resulting 0-1m and 1-2m proportions for any passenger are appropriately estimated in this way. In this figure, green 80 points result from randomly selecting a position in the carriage, red from regularly separated points 81 (at 0.1m distance) organised in a rectangular grid, and grey are points sampled from our distributions 82 with their size linearly related to the number of points overlapping at a given point on the plot. As 83 one can notice, and for a large number of estimates, these approaches are in agreement.

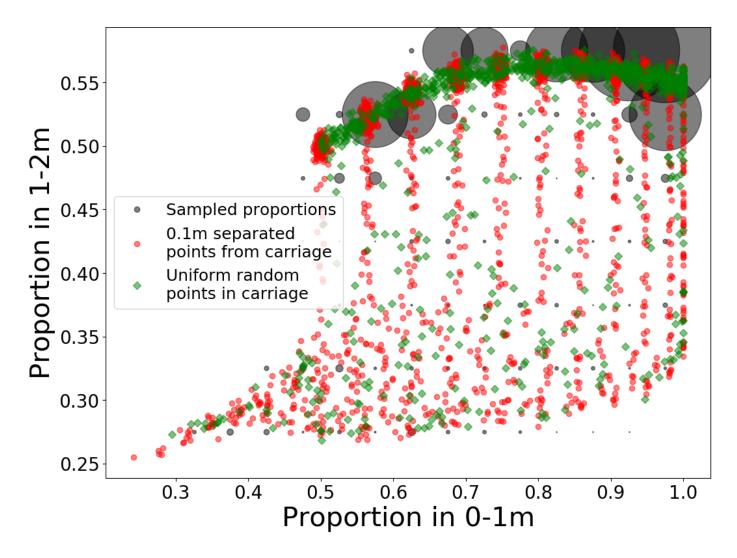


Figure 3: Position of sampled values relative to proportions directly from the carriage.

4. Surface area within the carriage

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To calculate the fraction of deposited droplets that deposits onto mucosal membranes, it is required to obtain an estimate of the surface area (SA) within the carriage as a whole and the region of the carriage within 2m of an infectious passenger.

The total surface area within the carriage has the following components: the carriage floor surface area, the ceiling surface area, the four walls areas, the number of internal surfaces multiplied by their surface area (see Table 2 in this Supplementary Material), the number of passengers on board at any given time multiplied by their surface area (see Table 2 in this Supplementary Material). On the other hand, the components of the surface area within 2m of an infectious passenger are: the floor area within 2m (computed following methodology in Section 3 in this Supplementary Material), the number of surfaces within 2m (estimated by multiplying the total number of surfaces in the carriage by the

fraction of floor area within 2m) multiplied by their surface area, the number of passengers within 2m multiplied by their surface area, and an estimate of the wall surface area within 2m of the passenger ($13.05m^3$, estimated by performing Monte Carlo simulations of the positions within the carriage and calculating the mean).

5. Droplet size distribution

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There is no current consensus on which droplet size distribution best fits human behaviour for the 101 activities which are of most interest (coughing, speaking, breathing). As such, choice of droplet size 102 distribution varies significantly within the literature. One common choice is to use the data given by 103 Duguid [2] or Loudon and Roberts [3, 4], with the data on number of droplets and droplet diameter for 104 coughing therein being widely referenced. Another approach is to use the bronchiolar/laryngeal/oral 105 (BLO) model which is used within [5] and which models the number concentration of droplets in a 106 given size bin via a lognormal distribution. Another common choice is that proposed by Nicas et al. 107 [4, 6], which is to use a probability distribution function (PDF) generated by summing two lognormal 108 distributions. This approach is not used here but is used in, for example, [7]. 109

We have implemented approaches based on droplet data [2, 3] and the BLO model [5] into the TVC 110 model, and explore their impact on our exposure estimates. The main model variables/parameters 111 related to this are dropletModel, exhaleType, largeDropletMin and largeDropletMax. If one chooses 112 "Duguid" as the droplet Model parameter, the TVC model considers the midpoints of the droplet diam-113 eter from the cough data within [2], and the number of droplets in the bin along with the number of 114 coughs per second and the viral load to generate a list of (wet) droplet diameters and an associated 115 source term Ω_i [PFU·s⁻¹] for each droplet diameter, for droplet sizes $j=1,\ldots,M$. The largeDroplet-116 Min and largeDropletMax parameters then provide upper and lower bounds on which of these droplet 117 sizes are considered as "large droplets" in the model (this is the same for all of the distributions). The 118 same process occurs if "LR" is selected as the droplet Model. In this case the data is taken from the 119 paper [4] but originally reported in [3]. We follow the same procedure as [4] and double the droplet 120 diameters as it was assumed that the droplet sizes reported in [3] were evaporated sizes. 121

If "BLO" is selected as the *dropletType* then the BLO model [5] is used. This is implemented using the approach within [8]. Given a bin j, its minimum and maximum values $(x_{j_{start}}$ and $x_{j_{stop}})$ and its midpoint (x_j) , the number concentration (number of droplets per m^3) inside the bin is given by the 125 following sum of lognormal distributions:

$$\begin{array}{lcl} \frac{dCn_j}{dLogx_j} & = & ln10\sum_{i=1}^{3}\left(\frac{Cn_i}{\sqrt{2\pi}ln(GSD_i)}\right)e^{-\frac{(ln(x_j)-ln(CMD_i))^2}{2\cdot(ln(GSD_i))^2}},\\ dLogx_j & = & logx_{j_{stop}}-logx_{j_{start}}, \end{array}$$

with the parameters in Table 1.

| | Parameter | Coughing | Speaking | Breathing |
|--------|-----------------|----------|----------|-----------|
| | $Cn_1 [m^{-3}]$ | 9.03E4 | 5.4E4 | 5.4E4 |
| B mode | $CMD_1[m]$ | 1.57E-6 | 1.61E-6 | 1.61E-6 |
| | GSD_1 [-] | 1.25 | 1.30 | 1.3 |
| L mode | $Cn_2 [m^{-3}]$ | 1.42E5 | 6.8E4 | N/A |
| | $CMD_2 [m]$ | 1.60E-6 | 2.40E-6 | N/A |
| | GSD_2 [-] | 1.68 | 1.66 | N/A |
| | $Cn_3 [m^{-3}]$ | 1.60E4 | 1.26E3 | N/A |
| O mode | $CMD_3 [m]$ | 1.23E-4 | 1.44E-4 | N/A |
| | GSD_3 [-] | 1.84 | 1.80 | N/A |

Table 1: BLO model input parameters [5]. Breathing only uses the B mode.

By assuming an homogeneous viral load per unit volume across droplet sizes, and for a particular droplet size j = 1, ..., M, the volume concentration $[m^3 \cdot m^{-3}]$ is then calculated using the formula

$$dC_{vol_j} = \frac{4}{3} \cdot \pi \cdot \left(\frac{x_j}{2}\right)^3 \cdot dCn_j,$$

and the source term $[PFU \cdot s^{-1}]$ for coughing is found via

$$\Omega_j = \frac{dC_{vol_j} \cdot V_{air} \cdot \omega}{T_c},$$

where ω is the viral load $[PFU \cdot m^{-3}]$, V_{air} is the volume of air exhaled during a cough $[m^3]$ and T_c is
the time between coughs $[s^{-1}]$. For speaking and breathing the source term is given by

$$\Omega_j = dC_{vol_i} \cdot BR \cdot \omega,$$

where BR is the breathing rate $[m^3 \cdot s^{-1}]$.

Finally, within the TVC model individual passengers may or may not be wearing a mask. The percentage of passengers whom are wearing a mask is denoted by $Mask_{\%}$. This parameter's value is

between 0 and 100, with 100 denoting all passengers wearing masks and 0 indicating that no passengers are wearing masks. The impact of wearing a mask for infectious individuals is a reduction in their release of small aerosol and droplets. In particular, it is assumed that masks block all large droplets, while a 50% filtration efficacy is assumed for small aerosols [9, 10]. This filtration efficacy is also applied to reduce the exposure of susceptible passengers who are wearing a mask.

In Figures 4 and 5, we explore the impact that the interaction between the droplet model under 140 consideration and the values of the key parameters varied in Section 3 within the main manuscript has 141 on exposure. We note that Duguid's droplet model predicts consistently higher median values than any 142 of the others, particularly when comparing BLO breathing or coughing model (e.g. Figure 4a). Duguid's 143 droplet model also predicts a relatively larger contribution of the long range airborne route, although the highest doses are still predicted to occur via the close range and fomite routes. Interestingly, 145 the BLO speaking typically predicts higher median values than the BLO coughing model whereas 146 this trend is reversed when analysing the mean values. As a result, it suggests that there may be less opportunistic events when the infectious person is speaking rather than coughing, under these 148 viral loads. However, we note here that while speaking happens in our model continuously during 149 the infectious passenger trip, coughing is assumed to occur at a given frequency instead. It is to be 150 expected that if an assumption about the fraction of the journey where the passenger is speaking 151 was incorporated, this relationship could change. The effect of mask wearing compliance in Figure 5a 152 shows how the variability in the predicted mean between droplet models is reduced to the same order 153 of magnitude when all passengers comply with mask wearing at 100%. 154

6. Evaporation of respiratory droplets

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Evaporation of respiratory droplets affects the resulting particle size. The act of drying is also 156 believed to affect viral viability. The majority of the initial droplets produced dry rapidly and for 157 the purposes of calculating deposition rates within the concentration and exposure calculations, it 158 is assumed that all droplets rapidly dry to their final size. This is likely to slightly underestimate 159 deposition rates for the largest droplet sizes. However, deposition rates for these sizes are high (even 160 when dry) so this does not introduce a large source of error. The dry size is also used for any removal 161 due to face coverings worn by exposed individuals, while wet droplet sizes are used for estimating 162 source reduction by face coverings of infected individuals. 163

However, so as not to underestimate the effect of larger droplets, the loss of viability due to drying

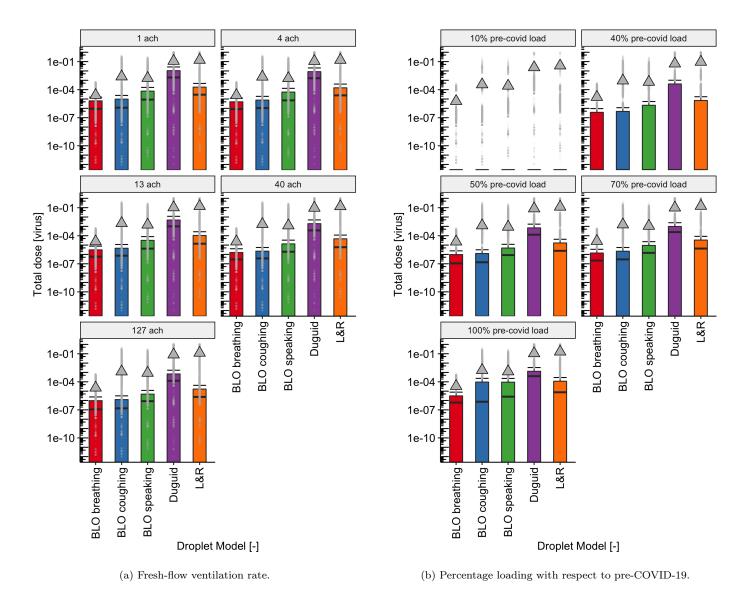


Figure 4: Boxplots showing the effect of the five droplet models varying disease and individual parameters one at a time on total dose received.

is determined following the approach of [7]. In particular, we define an evaporation time

$$T_e = \beta \cdot r_0^2,$$

where β [$s \cdot m^{-2}$] is a fitting parameter and r_0^2 is the wet droplet radius squared. We also define a travel time for a droplet to be

$$T_s = \frac{s}{v_m}$$

where s is the distance travelled and v_m the droplet speed $[m \cdot s^{-1}]$. The distance s takes the value 0.5m (T_{05}) or 1.5m (T_{15}) depending on the distance of the susceptible passenger to the infectious passenger

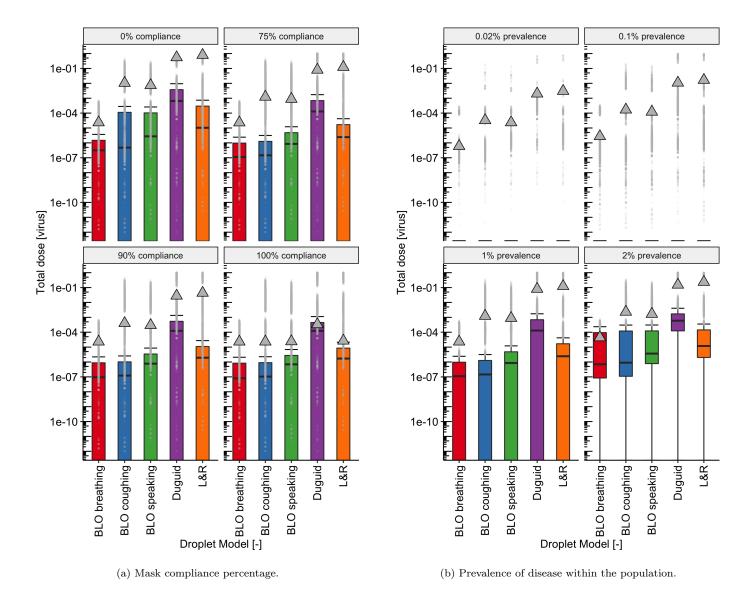


Figure 5: Boxplots showing the effect of the five droplet models varying disease and individual parameters one at a time on total dose received.

(either within 1m or 1-2m away). We then have the following scenarios for a droplet of a given wet size:

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- If $T_e < T_{05}$ then the droplet has dried before reaching any passengers. In this scenario the close range exposure for all passengers within 2m is reduced by a factor of 4 to represent the loss of viability [7].
- If $T_{05} < T_e < T_{15}$ then passengers within 1m of the infectious passenger receive the full close range exposure but passengers within 1-2m have theirs reduced by a factor of 4.
- If $T_e > T_{15}$ then the droplet is assumed to still be wet for all passengers within 2m and they thus

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receive the full exposure.

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We note that the exposures and doses due to small aerosol are all multiplied by 0.25 before being used to calculate final exposure upon alighting as the drying time for the small aerosol is assumed to be smaller than the distance to all passengers.

Finally, a solid fraction, α , is defined as an input parameter which represents the proportion of the droplet volume that is made of solid material. A fully evaporated droplet thus has volume $\alpha \cdot V_0$, where V_0 is the volume of the wet droplet. Assuming the remaining solid following full evaporation is spherical gives the expression

$$r_1 = \alpha^{\frac{1}{3}} \cdot r_0$$

for the evaporated droplets radius. As discussed above, it is this radius which is used within the TVC model wherever calculations of deposition, filtration or protection of exposed individuals by masks require the use of a droplet radius, with the exception of source reduction for infected individuals due to mask wearing.

7. Parameter values

A comprehensive list of default parameter values is given in Table 2.

| Related Route | Parameter | Description | Units | Default value | Source |
|---------------|-------------|----------------------------------|--------------------|-------------------------|----------|
| General | φ | Prevalence; the proportion | - | Varied | - |
| | | of passengers boarding who | | | |
| | | are infectious | | | |
| General | ρ | System loading percentage | - | Varied | - |
| General | BR | Rate at which passenger | $m^3 \cdot s^{-1}$ | $1.72454 \cdot 10^{-4}$ | [11] |
| | | breathes. | | | |
| General | ω | The viral load of SARS- | $PFU \cdot m^{-3}$ | $3.61 \cdot 10^{12}$ | [12, 13] |
| | | CoV-2 in respiratory fluid. | | | |
| | | Computed by dividing RNA | | | |
| | | copies per m^3 from [12] (4.7· | | | |
| | | $10^{14} RNA/m^3$) by number | | | |
| | | of RNA per PFU from [13] | | | |
| | | $(130 \; RNA/PFU)$ | | | |
| General | H | Height of the carriage | m | 2.148 | [1] |
| General | HSA | Human surface area. Used | m^2 | 1.75 | [7] |
| | | for total deposition surface | | | |
| | | area in carriage | | | |
| General | $Mask_{\%}$ | Percentage of passengers | - | Varied | - |
| | | who wear masks | | | |

| Close range | α | Fraction of the droplet volume which is solid | - | 0.25^{3} | [7] |
|--------------------|-------------------|--|-----------------------|-------------------------|---|
| Close range | β | Fitting parameter which is used to calculate a droplet's evaporation time | $s \cdot m^{-2}$ | 7 · 108 | [7] |
| Close range | v_m | The droplet speed. Used to calculate how long a droplet takes to travel a fixed distance | $m \cdot s^{-1}$ | 0.1 | [7] |
| Close range | large Droplet Min | The minimum droplet di- ameter considered for close range transmission as a "large" droplet | m | $2 \cdot 10^{-5}$ | Assumed |
| Close range | large Droplet Max | The maximum droplet di- ameter considered for close range transmission as a "large" droplet | m | $2 \cdot 10^{-3}$ | Assumed |
| Close range | V_{air} | The volume of air expelled during a cough. Only used with the BLO droplet model | m^3 | $1.69 \cdot 10^{-3}$ | [14] |
| Close range | k_d | Coefficient of particle deposition | $s^{-1} \cdot m^{-2}$ | $3.89\cdot10^7$ | [7] |
| Small aerosol | RF_{small} | Proportion of the small aerosol inhaled which is retained | - | 0.8 | [15] |
| Large aerosol | RF_{large} | Proportion of the large aerosol inhaled which is retained | - | 0.6 | [15] |
| Long range aerosol | V | Carriage volume | m^3 | 53.2 | Based on dimensions within [1] and adapted to account for seating and occupants. |
| Long range aerosol | r_v | Fresh air flow rate in the carriage | $m^3 \cdot s^{-1}$ | 1.9 | Based on passenger theoretical crush capacity within [1] and an assumed supply rate of 10 L/s/person. |
| Long range aerosol | r_i | Virus decay rate in aerosol, fractional loss per second of virus in the air due to inac- tivation | s ⁻¹ | 3.78 · 10 ⁻⁴ | [16] |

| Long range aerosol | r_d | Deposition rate in carriage. | s^{-1} | $1.82 \cdot 10^{-4}$ | [2, 7, 17] |
|--------------------|------------|--------------------------------|--------------------|----------------------|----------------------|
| | | Assuming a factor of four | | | |
| | | for the drying ratio, using | | | |
| | | cough source data from [2]. | | | |
| | | Calculations performed us- | | | |
| | | ing model described in [7] | | | |
| | | from [17] | | | |
| Surface contact | N_T | Total number of surfaces in | - | 114 | [1] |
| | | the carriage. This consists | | | |
| | | of 57 touch points on poles | | | |
| | | and door handles, 25 touch | | | |
| | | points on chair handles and | | | |
| | | 32 touch points on horizon- | | | |
| | | tal railings. Surfaces are as- | | | |
| | | sumed to be hard and non- | | | |
| | | porous. | | | |
| Surface contact | N_{HS} | Number of surface touches | - | 3 | Assumed |
| | II S | when boarding and alighting | | | |
| Surface contact | $	au_{HS}$ | Transfer efficiency from | - | 0.27 | [7] |
| | | hand to surface | | | |
| Surface contact | $	au_{SH}$ | Transfer efficiency from sur- | - | 0.29 | [7] |
| | | face to hand | | | |
| Surface contact | $	au_{HM}$ | Transfer efficiency from | - | 0.36 | [7] |
| | 11111 | hand to mucous membrane | | | 1.1 |
| | | on face (eyes, mouth, lips) | | | |
| Surface contact | δ_H | Inactivation rate on hands | s^{-1} | $5.5 \cdot 10^{-5}$ | [18] |
| Surface contact | δ_S | Inactivation rate on surface | s^{-1} | $6.22 \cdot 10^{-5}$ | [19] |
| Surface contact | C_{H0} | Initial concentration on in- | $PFU \cdot m^{-2}$ | 1500 | [20] |
| | | fected passenger hands | | | |
| Surface contact | A_H | Area of full hand | m^2 | 0.042 | [21] |
| Surface contact | A_P | Area of front of hand | m^2 | 0.02016 | [21] |
| Surface contact | A_M | Area of mucous membranes | m^2 | $1 \cdot 10^{-3}$ | [7] |
| | | (lips+eyes+mouth) | | | |
| Surface contact | A_S | Area of surface, equal for all | m^2 | 0.04 | Assumed. Repre- |
| | | surfaces | | | sentative surface is |
| | | | | | a circular pole of |
| | | | | | diameter 25mm and |
| | | | | | length 50cm, leading |
| | | | | | to $0.04m^2$ |
| Surface contact | A_{HM} | Area of hand-membrane | m^2 | $1 \cdot 10^{-4}$ | [7] |
| | | contact area | | | |
| | | contact area | | | |

| Surface contact | A_{HS} | Area of hand-surface | m^2 | $6.216 \cdot 10^{-3}$ | [22] |
|-----------------|------------|------------------------------------|----------|--------------------------|------------------------|
| | | contact area. Obtained | | | |
| | | by multiplying A_H by | | | |
| | | HCF = 0.148 (fractional | | | |
| | | surface area; fraction of | | | |
| | | hand touching the surface), | | | |
| | | as measured in [22] | | | |
| Surface contact | ξ_m | Touches to mucous mem- | s^{-1} | $1.389 \cdot 10^{-3}$ (5 | [7] |
| | | branes per second | | per hour) | |
| Surface contact | T_a | Time after alighting that | s | 900 | Assumed. Represents |
| | | the passengers face touching | | | a situation where pas- |
| | | contamination transfer con- | | | sengers do not wash |
| | | tinues before hand washing | | | their hands during |
| | | | | | the first 15min after |
| | | | | | alighting. |
| Surface contact | T_c | Time between coughs | s | 60 (1 cough per | Assumed |
| | | | | minute) | |
| Surface contact | A_{proj} | Projected area of surface | m^2 | 0.0125 | Assumed |
| | | (equal to length \times width of | | | |
| | | the representative cylindri- | | | |
| | | cal surface) | | | |
| Surface contact | A_{depo} | Spread of droplets in the | m^2 | 0.25 | Assumed |
| | | air within the horizontal and | | | |
| | | vertical directions at a dis- | | | |
| | | tance $0.5m$ away from the | | | |
| | | coughing passenger | | | |
| | | | · | <u> </u> | |

Table 2: Default parameter values in the TVC model.

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