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Letter

# HCl Treatment of Mixed-Phase MoVTeNbO<sub>x</sub> Catalysts for Enhanced Performance in Selective Oxidation of Propane

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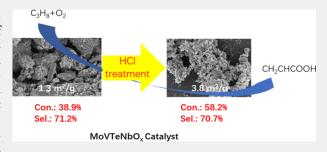
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ABSTRACT: Hydrothermally synthesized mixed-phase MoVTeNbOx catalysts are active for catalyzing the selective oxidation of propane to acrylic acid but suffer from the presence of the amorphous phase and low specific surface areas. Herein we report that HCl treatment preferentially dissolves the amorphous phase in hydrothermally synthesized mixed-phase MoVTeNbOx catalysts and increases the catalytic performance. An optimal HCl treatment significantly increases the C<sub>3</sub>H<sub>8</sub> conversion from 38.9% to 58.2% without changing the acrylic acid selectivity in the selective oxidation of propane to acrylic acid at 380 °C. The original and HCl treated



catalysts exhibit similar apparent activation energies, while HCl treatment increases the specific surface area, surface acid sites, surface  $V^{5+}$  density, and  $C_3H_8$  and  $C_3H_6$  irreversible adsorption amounts but decreases the  $C_3H_8$  and  $C_3H_6$  irreversible adsorption heats. The C<sub>3</sub>H<sub>8</sub> conversion rate is proportional to the surface V<sup>5+</sup> density and C<sub>3</sub>H<sub>8</sub> irreversible adsorption amount, and the TOF is measured as  $3.31 \pm 0.08 \times 10^{-5}$  s<sup>-1</sup> at 340 °C. Thus, HCl treatment enhances the catalytic performance of mixed-phase MoVTeNbO, catalysts mainly by increasing the active site density rather than by increasing the active site activity. Our results provide an effective approach to prepare highly active mixed-phase MoVTeNbO<sub>x</sub> catalysts for the selective oxidation of propane to

KEYWORDS: MoVTeNbO,, selective oxidation of propane, acrylic acid, active site, microcalorimetry

 $\bigcap$  ith the shortage of oil and the shale gas revolution, the selective oxidation of propane becomes an alternative to produce acrylic acid, an important chemical widely used to synthesize acrylic paints, acrylic adhesives, superabsorbent polymers, and other products,<sup>2</sup> in addition to the currently adopted two-step propene partial oxidation,<sup>3</sup> in which propene is mainly produced by the intensive energy-consuming and thermodynamically controlled naphtha cracking process.<sup>4,5</sup> To date, MoVTeNbO<sub>x</sub> mixed oxide is the most promising catalyst for the selective oxidation of propane to acrylic acid.6-MoVTeNbO<sub>r</sub> has the orthorhombic M1 phase and pseudohexagonal M2 phase, <sup>13–15</sup> and many strategies, including different synthesis methods, <sup>16–22</sup> doping, <sup>23–29</sup> and modulation of the phase composition,  $30^{\circ}-32$  were developed to optimize the catalyst performance. An interesting phase synergy between the M1 and M2 phases of MoVTeNbO, catalysts was observed in the selective oxidation of propane to acrylic acid by mechanical mixtures of the pure phases.<sup>30</sup> We recently found a novel one-pot hydrothermal synthesis assisted by sodium citrate and citric acid to fabricate mixed-phase MoVTeNbO<sub>x</sub> catalysts with tunable phase compositions of the M1 and M2 phases to optimize the synergetic effect in catalyzing the selective oxidation of propane to acrylic acid. 33 However, the hydrothermally synthesized mixed-phase MoVTeNbO<sub>x</sub> catalysts suffer from the presence of an amorphous phase and low specific surface areas. Herein we report that HCl treatment

preferentially dissolves the amorphous phase in hydrothermally synthesized mixed-phase MoVTeNbOx catalysts and significantly increases the  $C_3H_8$  conversion from 38.9% to 58.2% without changing the acrylic acid selectivity. The active site is precisely identified, and the underlying mechanism is also established.

A mixed-phase MoVTeNbO<sub>x</sub> catalyst (denoted as Cat-0) was hydrothermally synthesized using ammonium heptamolybdate, vanadyl sulfate, telluric acid, and ammonium niobium oxalate with an addition of citric acid.<sup>33</sup> Then, Cat-0 was treated in HCl aqueous solutions with concentrations of 3, 6, or 12 wt % at 60 °C for 2 h, respectively, to obtain the catalysts denoted as Cat-3, Cat-6, or Cat-12. Figure 1 compares the catalytic performance of various catalysts in the selective oxidation of propane at different temperatures. At 340 °C, C<sub>3</sub>H<sub>8</sub> conversion increases from 18.3% for Cat-0 to 23.1% for Cat-3, 36.0% for Cat-6, and 59.0% for Cat-12, while acrylic acid selectivity is around 70% for Cat-0, Cat-3, and Cat-6 but

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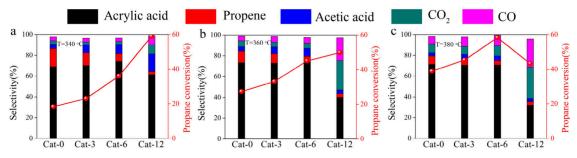


Figure 1. Catalytic performance of Cat-0, Cat-3, Cat-6, and Cat-12 in selective oxidation of propane to acrylic acid at (a) 340, (b) 360, and (c) 380 °C. Reaction conditions: 5%  $C_3H_8$ -10%  $O_2$ -40%  $H_2O$ -45%  $H_9$ , GHSV = 3000 mL  $g^{-1}$   $h^{-1}$ .

Table 1. Compositions and Properties of Various MoVTeNbO, Catalysts

	Cat-0	Cat-3	Cat-6	Cat-12
bulk composition <sup>a</sup>	$MoV_{0.27}Te_{0.26}Nb_{0.20}$	$MoV_{0.28}Te_{0.19}Nb_{0.22} \\$	$MoV_{0.27}Te_{0.16}Nb_{0.24} \\$	$MoV_{0.26}Te_{0.11}Nb_{0.28} \\$
surface composition <sup>b</sup>	$MoV_{0.13}Te_{0.20}Nb_{0.18} \\$	$MoV_{0.13}Te_{0.20}Nb_{0.18} \\$	$MoV_{0.12}Te_{0.17}Nb_{0.19} \\$	$MoV_{0.11}Te_{0.12}Nb_{0.26}$
surface area $(m^2/g)$	1.3	2.5	3.8	8.7
pore size (nm)	85.6	52.4	49.7	27.9
pore volume (cm <sup>3</sup> /g)	0.0107	0.0323	0.0439	0.0606
crystalline size (nm) <sup>c</sup>	33.1	31.7	31.1	29.0
amount and heat of C3H8 irreversible adsorption	$5.0 \ \mu \text{mol/g}$	$6.8 \mu \text{mol/g}$	11.1 $\mu$ mol/g	22.3 $\mu$ mol/g
	84.7 kJ/mol	74.0 kJ/mol	70.2 kJ/mol	64.3 kJ/mol
amount and heat of C3H6 irreversible adsorption	$1.8 \ \mu \text{mol/g}$	$10.8 \ \mu \text{mol/g}$	$20.4 \ \mu \text{mol/g}$	31.1 $\mu$ mol/g
	99.1 kJ/mol	74.6 kJ/mol	59.6 kJ/mol	46.4 kJ/mol
M1 phase content (wt %) <sup>d</sup>	35.3	44.0	50.2	58.3
M2 phase content (wt %) <sup>d</sup>	19.0	21.1	21.0	26.2
amorphous content (wt $\%$ ) <sup>d</sup>	45.7	34.9	28.8	15.5
M2/(M2 + M1) (%)	35.0	32.4	29.5	31.0

<sup>&</sup>lt;sup>a</sup>Measured by ICP-AES. <sup>b</sup>Measured by XPS. <sup>c</sup>Calculated using the (200) diffraction peak at 7.7° of XRD patterns by the Scherrer equation. <sup>36</sup>
<sup>d</sup>Phase content calculated from Rietveld refinement analysis of XRD patterns. <sup>35</sup>

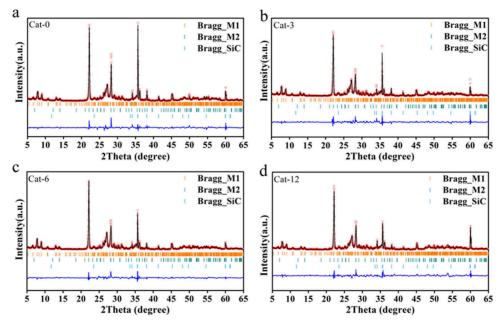


Figure 2. XRD patterns of Cat-0 (a), Cat-3 (b), Cat-6 (c), and Cat-12 (d), refined using the Rietveld method. The catalysts were thoroughly mixed with 20 wt % of a fully crystalline SiC standard material during the XRD measurements to quantify the amorphous content.

61.3% for Cat-12. With the reaction temperature increasing,  $C_3H_8$  conversion increases for Cat-0, Cat-3, and Cat-6, and acrylic acid selectivity remains around 70%. However,  $C_3H_8$  conversion decreases for Cat-12, and  $CO_x$  selectivity increases at the expense of acrylic acid selectivity. The different catalytic

behavior of Cat-12 from that of the other catalysts results from the full consumption of  $O_2$  that occurred in the selective oxidation of propane catalyzed by Cat-12 already at 360  $^{\circ}$ C but not for the other catalysts (Figure S1), suggesting the much higher catalytic activity for propane combustion of Cat-12 than

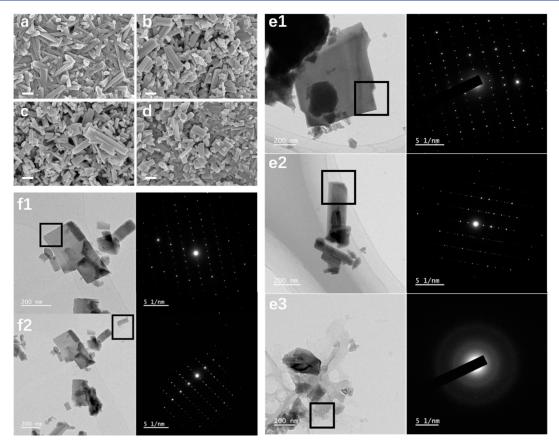


Figure 3. SEM images of Cat-0 (a), Cat-3 (b), Cat-6 (c), and Cat-12 (d). TEM images and selective area electron diffraction patterns (in [010] direction for M1 phase and in [100] direction for M2 phase) of the M2 phase (e1), M1 phase (e2), and amorphous phase (e3) in Cat-0 and the M2 phase (f1) and M1 phase (f2) in Cat-12.

of the other catalysts. These results demonstrate that HCl treatment strongly affects the catalytic performance of hydrothermally synthesized mixed-phase MoVTeNbO<sub>x</sub> catalysts in the selective oxidation of propane. An optimal HCl treatment leads to the best Cat-6 catalyst exhibiting a C<sub>3</sub>H<sub>8</sub> conversion of 58.2% and an acrylic acid selectivity of 70.7% at 380 °C, better than most previously reported results in the literature (Table S1). Cat-6 also shows good catalytic stability in the selective oxidation of propane at 380 °C (Figure S2). Reaction kinetics of the selective oxidation of propane catalyzed by various catalysts were measured under kinetically controlled reaction conditions (Figure S3). The resulting Arrhenius plots (Figure S4) show that the apparent activation energy is around 85.9 kJ/mol for Cat-0 and slightly increased to around 90.1 kJ/mol for Cat-3, Cat-6, and Cat-9, suggesting that the active site structure is not much affected by HCl

As summarized in Table 1, the bulk composition is MoV<sub>0.27</sub>Te<sub>0.26</sub>Nb<sub>0.20</sub> for Cat-0, MoV<sub>0.28</sub>Te<sub>0.19</sub>Nb<sub>0.22</sub> for Cat-3, MoV<sub>0.27</sub>Te<sub>0.16</sub>Nb<sub>0.24</sub> for Cat-6, and MoV<sub>0.26</sub>Te<sub>0.11</sub>Nb<sub>0.28</sub> for Cat-12. Thus, the HCl treatment preferentially dissolves Te and then Mo. Phase compositions of various catalysts were quantitatively analyzed using XRD patterns with Rietveld refinement analysis<sup>35</sup> (Figure 2). All catalysts show the diffraction peaks arising from the M1 phase at 6.5°, 7.8°, 8.9°, 22.0°, 27.1°, 35.0°, and 45.0° and from the M2 phase at 22.0°, 28.3°, 36.1°, 45.0°, and 50.1°. <sup>26,37,38</sup> As summarized in Table 1, the M1 phase percentage increases from 35.3% for Cat-0 to 44.0% for Cat-3, 50.2% for Cat-6, and 58.3% for Cat-

12, and the M2 phase percentage slightly increases from 19.0% for Cat-0 to around 21.0% for Cat-3 and Cat-6 and to 26.2% for Cat-12. The amorphous phase percentage decreases from 45.7% for Cat-0 to 34.9% for Cat-3, 28.8% for Cat-6, and 15.5% for Cat-12. The M2/(M1 + M2) percentage does not change much, being 35.0%, 32.4%, 29.5% and 31.0% for Cat-0, Cat-3, Cat-6, and Cat-12, respectively. A further quantitative analysis of the mass loss of each phase during HCl treatment (Table S2) demonstrates that the amorphous phase is largely dissolved and the M2 phase is also dissolved, but the M1 phase is barely dissolved. Therefore, HCl treatment preferentially dissolves the amorphous phase in the Cat-0 mixed-phase MoVTeNbO, catalyst, which is enriched with the Te element.

As summarized in Table 1, the specific surface area increases from 1.3 m<sup>2</sup>/g for Cat-0 to 2.5 m<sup>2</sup>/g for Cat-3, 3.8 m<sup>2</sup>/g for Cat-6, and 8.7 m<sup>2</sup>/g for Cat-12. The average pore size keeps decreasing from Cat-0 to Cat-12, while the pore volume keeps increasing. SEM images (Figure 3a-d and Figure S5) display rod-shaped and plate-shaped particles, which are the typical morphologies of M1-phase MoVTeNb oxide and M2-phase MoVTeNb oxide, respectively. 13,39 Size distributions counted from the SEM images of the M1 phase particles in Cat-0 and Cat-12 (Figure S6) show a decrease in the average length from around 231.0 nm for Cat-0 to around 185.6 nm for Cat-12; meanwhile, the average crystalline size of the M1 phase calculated from the XRD patterns<sup>36</sup> (Table 1) shows a gradual decrease from Cat-0 to Cat-12. TEM images of Cat-0 (Figure 3e1-e3) identify the presence of the M1 phase, M2 phase, and amorphous phase, whereas TEM images of Cat-12 (Figure

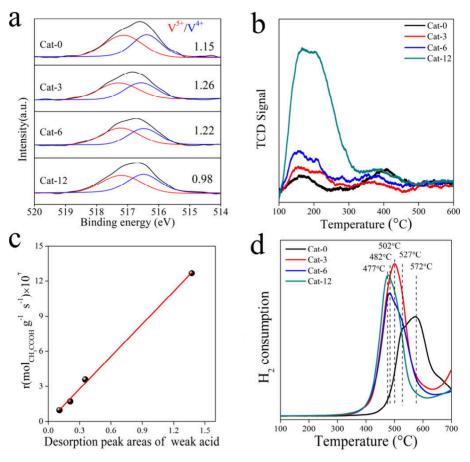


Figure 4. (a) V 2p XPS spectra and (b) NH<sub>3</sub>-TPD profiles of various mixed-phase MoVTeNbO<sub>x</sub> catalysts. (c) Acetic acid production rate of the selective oxidation of propane catalyzed by various mixed-phase MoVTeNbO<sub>x</sub> catalysts as a function of their desorption peak areas of weak acid in the NH<sub>3</sub>-TPR profiles. (d) H<sub>2</sub>-TPR profiles of various mixed-phase MoVTeNbO<sub>x</sub> catalysts.

3f1,f2) mainly identify the presence of the M1 phase and M2 phase, supporting the preferential dissolution of the amorphous phase by HCl treatment. The TEM images also show that the particle sizes of the M1 phase and M2 phase in Cat-0 are larger than those in Cat-12. All these results demonstrate that HCl treatment of Cat-0 decreases the particle size of the M1 phase and M2 phase, which contributes to the increase of catalyst surface area, beneficial for the catalytic activity.

Surface compositions of various mixed-phase MoVTeNbO<sub>x</sub> catalysts were characterized using XPS as MoV<sub>0.13</sub>Te<sub>0.20</sub>Nb<sub>0.18</sub> for Cat-0,  $MoV_{0.13}Te_{0.20}Nb_{0.18}$  for Cat-3,  $MoV_{0.12}Te_{0.17}Nb_{0.19}$ for Cat-6, and  $MoV_{0.11}Te_{0.12}Nb_{0.26}$  for Cat-12 (Table 1). Compared to the surface content of Mo, HCl treatment slightly decreases the surface contents of V and Te and increases the surface content of Nb in Cat-3 and Cat-6 but significantly decreases the surface content of Te and increases the surface content of Nb in Cat-12. The Mo 3d, Nb 3d, and Te 3d XPS spectra (Figure S7a-c) all exhibit a single component with the binding energies of Mo  $3d_{5/2}$ , Nb  $3d_{5/2}$ , and Te  $3d_{5/2}$  features at 232.9  $\pm$  0.2, 207.2  $\pm$  0.2, and 576.5  $\pm$ 0.1 eV, respectively, suggesting the presence of Mo<sup>6+</sup>, Nb<sup>5+</sup>, and Te<sup>4+</sup> cations in all catalysts. No Cl signals were observed in the Cl 2p XPS spectra (Figure S7d). Two components were well resolved in the V 2p XPS spectra with the V  $2p_{3/2}$  binding energies at 561.3 and 571.1 eV, respectively, arising from  $V^{4+}$  and  $V^{5+}$  cations (Figure 4a).  $^{36,46,47}$  The calculated surface  $V^{5+}/V^{4+}$  ratio is 1.15 for

Cat-0, 1.26 for Cat-3, 1.22 for Cat-6, and 0.98 for Cat-12. Thus, HCl treatment affects the surface  $V^{5+}/V^{4+}$  ratio of various catalysts, while the surface  $V^{5+}$  site is considered as the active site on M1-phase MoVTeNbO $_x$  catalysts for propane activation. <sup>14,48,49</sup>

The surface acidity of various catalysts was probed by NH<sub>3</sub>-TPD (Figure 4b). The two NH<sub>3</sub> desorption peaks observed at around 150 and 400 °C in the NH3-TPD spectrum of Cat-0 could be assigned to the weak and strong acid sites, respectively.<sup>21</sup> HCl treatment greatly increases the amount of weak acid sites but seldom increases the amount of strong acid sites, particularly for Cat-12. The enhancement of weak surface acid sites in various catalysts seems to be related to the increasing surface content of Nb. Consistent with a previous report that weak acid sites on MoVTeNbO<sub>x</sub> catalysts favored the undesired C-C bond breaking reactions in the selective oxidation of propane, leading to the production of acetic acid and carbon oxides, 40 the production of acetic acid over various mixed-phase MoVTeNb catalysts correlates linearly with the integrated peak area of the NH3 desorption peak from the weak acid sites (Figure 4c).

The reducibility of various mixed-phase MoVTeNbO $_x$  catalysts was also examined by using H $_2$ -TPR (Figure 4d). Cat-0 exhibits two obvious reduction peaks at around 527 and 572 °C arising from the reduction of the M1 phase and M2 phase, respectively,<sup>33</sup> while Cat-3, Cat-6, and Cat-12 exhibit a dominant reduction peak at around 502, 482, and 477 °C, respectively. These observations suggest that HCl treatment

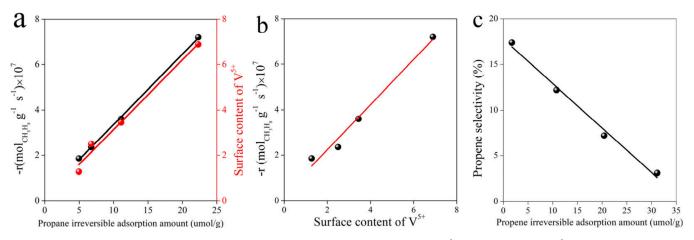


Figure 5. (a) Reaction rate of propane at the temperature of 340 °C and surface content of  $V^{5+}$  (surface content of  $V^{5+}$  = surface area × surface atomic percentage of  $V^{5+}$ ) as a function of the irreversible adsorption amount of propane on various mixed-phase MoVTeNbO<sub>x</sub> catalysts. (b) Reaction rate of propane at the temperature of 340 °C as a function of the surface content of  $V^{5+}$  (surface content of  $V^{5+}$  = surface area × surface atomic percentage of  $V^{5+}$ ) and (c) propene selectivity at the temperature of 340 °C as a function of the irreversible adsorption amount of propene on various mixed-phase MoVTeNbO<sub>x</sub> catalysts.

not only significantly promotes the reducibility of the M1 phase in the catalysts, beneficial for the catalytic activity, but also improves the M1-M2 phase synergy in the catalysts, beneficial for the acrylic acid selectivity.

Adsorptions of C<sub>3</sub>H<sub>8</sub>, the reactant, and C<sub>3</sub>H<sub>6</sub>, a primary product, on various catalysts at -30 °C were quantitatively studied using flow-adsorption microcalorimetry. 34,50-53 As shown in Figures S8-S11 and summarized in Table 1, the irreversible C<sub>3</sub>H<sub>8</sub> adsorption heat and amount are respectively around 84.7 kJ/mol and 5.0  $\mu$ mol<sub>C3H8</sub>/g (3.85  $\mu$ mol<sub>C3H8</sub>/m<sup>2</sup>) on Cat-0, 74.0 kJ/mol and 6.8  $\mu$ mol<sub>C3H8</sub>/g (2.72  $\mu$ mol<sub>C3H8</sub>/ m<sup>2</sup>) on Cat-3, 70.2 kJ/mol and 11.1  $\mu$ mol<sub>C3H8</sub>/g (2.92  $\mu$ mol<sub>C3H8</sub>/m<sup>2</sup>) on Cat-6, and 64.3 kJ/mol and 22.3  $\mu$ mol<sub>C3H8</sub>/g  $(2.56 \ \mu \text{mol}_{C3H8}/\text{m}^2)$  on Cat-12, while the irreversible  $C_3H_6$ adsorption heat and amount are respectively around 99.1 kJ/ mol and 1.8  $\mu$ mol<sub>C3H6</sub>/g (1.38  $\mu$ mol<sub>C3H6</sub>/m<sup>2</sup>) on Cat-0, 74.6 kJ/mol and 10.8  $\mu$ mol<sub>C3H6</sub>/g (4.32  $\mu$ mol<sub>C3H6</sub>/m<sup>2</sup>) on Cat-3, 59.6 kJ/mol and 20.4  $\mu$ mol<sub>C3H6</sub>/g (5.37  $\mu$ mol<sub>C3H6</sub>/m<sup>2</sup>) on Cat-6, and 46.4 kJ/mol and 31.1  $\mu$ mol<sub>C3H6</sub>/g (3.57  $\mu$ mol<sub>C3H6</sub>/m<sup>2</sup>) on Cat-12. The different adsorption heats of C<sub>3</sub>H<sub>8</sub> and C<sub>3</sub>H<sub>6</sub> on various catalysts directly prove that HCl treatment alters their surface structures, which could be correlated to the observed surface acidity changes. The mass-specific adsorption amounts of C<sub>3</sub>H<sub>8</sub> and C<sub>3</sub>H<sub>6</sub> keep increasing from Cat-0 to Cat-3, Cat-6, and Cat-12 due to the increased BET surface areas. However, the surface area-specific adsorption amounts of C<sub>3</sub>H<sub>8</sub> of Cat-3, Cat-6, and Cat-12 are smaller than that of Cat-0, whereas their surface area-specific adsorption amounts of C<sub>3</sub>H<sub>6</sub> are larger than that of Cat-0. These results support our previous results, which demonstrated that C<sub>3</sub>H<sub>8</sub> only adsorbed on the M1 phase of the mixed-phase MoVTeNbO, catalysts, while C<sub>3</sub>H<sub>6</sub> adsorbed on both the M1 phase and the M2 phase.<sup>33</sup> Meanwhile, they also indicate that the surface area increases of Cat-0 upon HCl treatment result from the surface area increases of both the M1 phase and the M2 phase and that the extent of the surface area increase of the M1 phase should be less than that of the M2 phase.

Although the adsorption heat of  $C_3H_8$  varies, the apparent activation energies of the  $C_3H_8$  conversion catalyzed by different mixed-phase catalysts are similar. This supports that the catalyzed selective oxidation of  $C_3H_8$  follows an Mvk mechanism,  $^{33}$  in which the reactivity of surface lattice oxygen

of a mixed-phase MoVTeNbOx catalyst determines the intrinsic catalytic activity. The mass-specific C<sub>3</sub>H<sub>8</sub> conversion rates at 340 °C were acquired under the kinetic-controlled regime (Figure S3) for the selective oxidation of C<sub>3</sub>H<sub>8</sub> catalyzed by various mixed-phase MoVTeNbO<sub>x</sub> catalysts. They were found to positively linearly correlate with both the surface V<sup>5+</sup> amount, represented by the surface V<sup>5+</sup> atomic percentage derived from XPS multiplied by the surface area, and the mass-specific adsorption amount of C<sub>3</sub>H<sub>8</sub> (Figure 5a,b). This demonstrates that the surface  $V^{5+}$  site on M1-phase MoVTeNbO<sub>x</sub> catalysts is the active site for C<sub>3</sub>H<sub>8</sub> adsorption and activation and further proves that the different apparent catalytic activity of various mix-phase MoVTeNbO, catalysts results from the different active site density, not from the active site activity. Taking the irreversible C<sub>3</sub>H<sub>8</sub> adsorption amount as the active site density, the TOF in the selective C<sub>3</sub>H<sub>8</sub> oxidation reaction at 340 °C was then calculated as  $3.48 \times 10^{-5}$ ,  $3.31 \times 10^{-5}$  $10^{-5}$ , 3.21 ×  $10^{-5}$ , and 3.25 ×  $10^{-5}$  s<sup>-1</sup> for Cat-0, Cat-3, Cat-6, and Cat-12, respectively, giving an average TOF of  $3.31 \times 10^{-5}$ s<sup>-1</sup>. Despite the very different C<sub>3</sub>H<sub>6</sub> irreversible adsorption heats, the mass-normalized C<sub>3</sub>H<sub>6</sub> irreversible C<sub>3</sub>H<sub>6</sub> adsorption amount on various catalysts was found to negatively linearly correlate with the selectivity of C<sub>3</sub>H<sub>6</sub> (Figure 5c). This suggests that the C<sub>3</sub>H<sub>6</sub> adsorption amount, rather than the C<sub>3</sub>H<sub>6</sub> adsorption heat (binding strength), is responsible for further conversions of adsorbed C<sub>3</sub>H<sub>6</sub> on the catalysts.

In summary, we have successfully developed an effective approach of HCl treatment to significantly enhance the catalytic performance of hydrothermally synthesized mixed-phase MoVTeNbO $_x$  catalysts in the selective oxidation of propane to acrylic acid. An optimal HCl treatment significantly increases the  $C_3H_8$  conversion from 38.9% to 58.2% without changes in the acrylic acid selectivity (around 71.0%) in the selective oxidation of propane to acrylic acid at 380 °C. HCl treatment preferentially dissolves the Te-containing amorphous phase in the mixed-phase MoVTeNbO $_x$  catalysts and increases the surface areas of both the M1 phase and the M2 phase, the surface  $V^{5+}/V^{4+}$  ratios, and the  $C_3H_8$  irreversible adsorption amounts. These lead to increased active site (surface  $V^{5+}$  sites on the M1 phase) densities on mixed-phase MoVTeNbO $_x$  catalysts for  $C_3H_8$  adsorption and

activation, resulting in significantly enhanced C<sub>3</sub>H<sub>8</sub> conversions.

## ASSOCIATED CONTENT

## Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/prechem.4c00089.

Experimental section, oxygen conversions of the catalytic reaction, stability test, summary of catalytic performance, reaction kinetic measurements and Arrhenius plots for propane reaction rate, mass loss and phase loss during HCl treatment, SEM images, length distributions of M1 particles, XPS spectra, and microcalorimetric measurements of  $C_3H_8$  and  $C_3H_6$  adsorptions (PDF)

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## **Author Contributions**

All authors have given approval to the final version of the manuscript.

## **Notes**

The authors declare no competing financial interest.

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