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Alison Grazioli,¹ Sanjeev R Shah,² Joseph Rabin,³ Rashmikant Shah,⁴ Ronson J Madathil,⁵ Joshua D King,⁶ Laura DiChiacchio,⁷ Raymond P Rector,⁸ Kristopher B Deatrick,⁵ Zhongjun J Wu⁷ and Daniel L Herr⁹

High-efficiency, high-flux in-line

flow extracorporeal circuit

hemofiltration using a high blood

Abstract

The ability of current renal replacement therapy modalities to achieve rapid solute removal is limited by membrane surface area and blood flow rate. Extracorporeal membrane oxygenation offers high blood flow and hemodynamic support that may be harnessed to overcome limitations in traditional renal replacement therapy. Using an extracorporeal membrane oxygenation circuit, we describe a high blood flow, high-efficiency hemofiltration technique using in-line hemofilters (hemoconcentrators) and standard replacement fluid to enhance solute clearance. Using this approach and a total of 5L of replacement volume per treatment, creatinine (Cr) clearances of 8.3L/hour and 11.2L/hour using one and two hemoconcentrators, respectively, were achieved. With use of a high blood flow rate of up to 5L/min, this hemofiltration technique can potentially offer clearance of 30 times that of continuous renal replacement therapy and of 6 times that of hemodialysis which may expand the ability to remove substances traditionally not considered removable via existing extracorporeal therapies.

Keywords

extracorporeal therapy; convective clearance; hemofiltration; high-flux dialysis; renal replacement therapy

Case

A 62-year-old 62 kg man with a history of hypertension, diabetes, coronary artery disease, and chronic kidney disease presented to an outside hospital with dyspnea. Left heart catheterization (LHC) was performed showing 99% occlusion of right coronary artery. The patient was later transferred to our institution for additional percutaneous coronary intervention. Renal replacement therapy (RRT) was initiated at the outside hospital for non-oliguric acute kidney injury (AKI). During LHC on day of arrival, the patient suffered cardiac arrest and was placed on veno-arterial extracorporeal membrane oxygenation (ECMO) peri-arrest. The patient's AKI worsened and he developed oliguria within 24 hours.

After emergent initiation of ECMO, consent was obtained for continuation and for initiation of RRT (convective clearance for solute removal). Initially, fluid overload was managed using an in-line hemofilter as is already the standard of care in most ECMO units in the United States.¹ The hemofilter, an in-line Sorin-14 (polyethersulfone membrane) hemoconcentrator (LivaNova USA, Inc., ¹Division of Pulmonary and Critical Care Medicine, Department of Medicine, University of Maryland School of Medicine, Baltimore, MD, USA

²Division of Renal-Electrolyte and Hypertension, Department of Medicine, Perelman School of Medicine, University of Pennsylvania, Philadelphia, PA, USA

³R Adams Cowley Shock Trauma Center and Department of Surgery, University of Maryland School of Medicine, Baltimore, MD, USA ⁴Retired Mechanical Engineer, Farmington Hills, MI, USA

⁵Division of Cardiac Surgery, Department of Surgery, University of Maryland School of Medicine, Baltimore, MD, USA

⁶Department of Medicine, School of Pharmacy and Maryland Poison Center, University of Maryland School of Medicine, Baltimore, MD, USA

⁷Department of Surgery, University of Maryland School of Medicine, Baltimore, MD, USA

⁸Univeristy of Maryland Medical Center, Baltimore, MD, USA ⁹Department of Medicine and Program in Trauma, R Adams Cowley Shock Trauma Center, University of Maryland School of Medicine, Baltimore, MD, USA

Corresponding author:

Alison Grazioli, Division of Pulmonary and Critical Care Medicine, Department of Medicine, University of Maryland School of Medicine, 2nd Floor, 110 South Paca Street, Baltimore, MD 21201, USA. Email: Alison.grazioli@gmail.com



Figure 1. (a) Two Sorin-14 hemofilters (blue arrows) placed in parallel in-line with ECMO circuit with effluent tubing to allow for gravity drainage. Black arrows indicate gravity drainage tubing. (b) Theoretical use of high-flux hemofilters arranged in parallel within a high blood flow circuit (for example, an ECMO circuit). (c) A theoretical large area hemofilter able to accommodate high blood flow throughput (~5-7L/minute) in series within a high blood flow circuit. Effluent removal is supported by an effluent pump and collects in a waste container. Replacement fluid is delivered via use of replacement fluid pump and is delivered to circuit post-filter (though pre-filter delivery is also possible).

Arvada, CO, USA), had a blood flow throughput of $\sim 1 L/$ minute per flow meter measurement and was paced before the oxygenator, with proper technique and with close monitoring for safety purpose. The Sorin-14 hemofilter has characteristics that, at minimum, match high-flux hemodialyzers with a sieving cut-off of 65,000 Da and is well suited for high-pressure convective solute clearance.^{1,2} To establish the validity of baseline convective qualities, effluent electrolyte concentrations from both the Sorin-14 and the PRISMAFLEX M-150 set AN 69 (Baxter International, Deerfeild, IL, USA) conventional continuous renal replacement therapy (CRRT) membrane were concurrently compared in another patient and were nearly identical (data not shown). During patient's first solute clearance treatment period (treatment one), 5L of PrismaSATE replacement fluid (Baxter International) was administered and 5L of hemofiltration was performed using the hemofilter. This was achieved by first delivering 500 cc increments of replacement fluid via the ECMO

circuit followed by the exact physician-matched removal of the same effluent volume (500 cc) via the hemofilter using gravity drainage. This process was repeated over the span of 50 minutes until the total effluent removed and replacement fluid volume administered each totaled 5 L. Risk of volume depletion was minimized by exactly matching the amount of replacement fluid given to the amount of effluent removed. Hemodynamics remained stable with mean arterial pressure (MAP) range of 80-90.

For the subsequent treatment (Treatment 2), a second Sorin-14 hemofilter was placed in-line (Figure 1(a)). Both hemofilters, now in parallel with one another, maintained blood flow throughput of \sim 1 L/minute each as measured by flow meters. A similar procedure was followed to administer 5L of replacement fluid along with matched effluent volume removal of 5L via gravity drainage. However, during Treatment 2, effluent was removed simultaneously from both hemofilters via gravity drainage, which doubled the effluent removal rate. This process of replacing and removing 5L of fluid was completed in 25 minutes, around 10% of time required to achieve standard CRRT clearance goals of 20 cc/kg/hour.³ The patient remained hemodynamically stable (MAP 70-90) without any adverse effects and there was no net fluid removal. Traditional CRRT was subsequently initiated for further convective clearance and volume management. Basic metabolic panels were obtained pre and post both treatment sessions (Supplemental Table 1a). Effluent fluid was collected and sodium, potassium, and creatinine values were measured from both sessions (Supplemental Table 1b).

Traditional calculations for clearance in CRRT using post-filter replacement fluid utilize the concept that K $(clearance) = hemofiltration rate \times S$ (the ratio of effluent solute concentration/blood solute concentration).4 Theoretically, S = 1 for most small solutes like Cr given that they freely pass through membrane pores during convection. In our patient, as anticipated, the S value for Cr was nearly one. The above replacement rates (5 L/time of treatment) normalized to 1 hour yielded a theoretical K (clearance) value of 6 L/hour in Treatment 1. In Treatment 2, the K value was twice the value of Treatment 1 (12 L/hour) as expected given that filter area doubled during the second treatment. Clearance can also be calculated as measured mass flux across the membrane (J)/average blood solute concentration (Table 1). With this approach, the Cr clearance for Treatment one was 8.3 L/hour, whereas in Treatment 2, it was 11.2 L/hour. Differences between the theoretical and calculated values may represent inherent lab variability when measuring small concentrations of Cr in effluent samples or drug interference with the Cr assay.5 The overall trend of both calculations, however, shows near doubling of clearance when two filters were used in parallel approximating the upper limit of what conventional CRRT is currently able to achieve. This was using only 1 L/minute of blood flow per hemofilter, whereas the ECMO circuit can actually flow ~5-7 L/minute. This high blood flow could theoretically allow for even greater convective clearance (Table 1).

Discussion

Volume management for patients supported with extracorporeal circulation is often through hemoconcentration via a hemofilter placed in-line with the circuit.¹ However, the use of an in-line hemofilter for solute management has not been studied to our knowledge. Here, we report the novel utilization of in-line hemofiltration with commercial hemofilters and replacement solutions to achieve high-efficiency, high-flux convective solute clearance.

Currently, solute clearance is most often achieved through use of a CRRT circuit placed at a dedicated access site or in-line with an ECMO apparatus. Using CRRT to achieve convective clearance has two significant limitations. Convective clearance is determined by the volume of hemofiltration/time which is limited by the system's blood flow.⁶ Blood flow rates in CRRT circuits do not typically exceed 300 mL/minute due to smaller diameter access catheters and tubing.⁴ Currently, achievable hemofiltration rates are also restricted by filtration fraction (hemofiltration rate/blood flow in the circuit) with filtration fractions >20% leading to excessive hemoconcentration and clotting. Both the impediments of filtration fraction ceiling and lower blood flow can be addressed with the use of systemic anticoagulation and large-diameter catheters, respectively.

The second limitation of conventional RRT (continuous and intermittent modalities) is the use of a single standardsize hemofilter or hemodialyzer. These membranes are designed to accommodate blood flow ranges attainable through dialysis catheters (up to 400 mL/minute) or via cannulation of peripheral arteriovenous access sites (up to ~ 600 mL/minute). Since the efficiency of convective solute removal is dependent on both the hemofilter surface area and rate of hemofiltration, proportionally increasing the hemofilter capacity to accommodate higher blood flows of 5-7L/minute achieved by an extracorporeal circuit, like ECMO, could dramatically enhance the efficiency of solute clearance to 30 times that of CRRT and 6 times that of hemodialysis (Table 1). This could be theoretically accomplished by placing standard high-flux hemofilters in parallel with one another as reported in this case (Table 1, Figure 1(b)). Alternatively, this could be achieved via development of a single larger hemofilter placed in series within a high-flow extracorporeal circuit engineered to maintain the ratios of blood flow to surface area achieved with traditional RRT (Figure 1(c)). Maintenance of these ratios would be essential to preserve the transmembrane pressures and solute sieving properties that standard hemofilter membranes are designed to sustain. In addition, this would prevent complications of hemolysis secondary to increased shear forces created by blood membrane interactions at higher pressures.⁷ Finally, to ensure ease and accuracy of replacement fluid delivery, an additional pump could theoretically be incorporated to deliver replacement fluid to the extracorporeal circuit (preor post-filter) at a desired rate (Figure 1(b) and (c)). This rate would match the hemofiltration rate unless additional fluid removal was desired.

Here, we demonstrate that use of hemofilters incorporated into a high-flow circuit and in parallel with each other can achieve solute clearance rates that exceed current RRT capabilities. Using this novel method, Cr clearance between 11 and 12 L/hour using two in-line hemofilters was achieved. While traditional RRT provides adequate support for renal failure, its limited efficiency can prevent its application to other critical clinical scenarios. Patients suffering from toxin ingestion, such as drug overdose, endogenous toxic molecule production such as myoglobin in rhabdomyolysis, or cytokine release as occurs in sepsis, may require higher

Table 1. Comparison of theoretical an is made between CVVH, conventional h fractions.	id achieved Cr cle emodialysis, and i	arance using o extracorporea	one and two Sc I circuit hemof	rrin-14 hem Iltration loc	ofilter in-line witl king at small-mol	1 a high blood fle ecule clearance	ow extracorporeal ci at various blood flow	rcuit. Theoreti 's and different	al comparison filtration
Comparison of creatinine clearance ach	ieved with one ve	rsus two Sori	n-14 hemofilter	S.					
	Time of treatment	Hemo- filtration amount (L)	Theoretical Cr clearance (K) L/hour ^a	Filtration fraction*	Serum Cr be- fore treatment (mg/dL)	Serum Cr af- ter treatment (mg/dL)	Average serum Cr over treatment time (mg/dL)	Effluent Cr (mg/dL)	Calculated clearance (K킨) L/hour ^b
Treatment 1—one hemoconcentrator Treatment 2—two hemoconcentrators	50 minutes 25 minutes	5L 5L	6 L/hour 12 L/hour	13% 13%	3.62 4.26	3.07 3.86	3.3 4.06	4.6 3.8	8.3 L/hour 11.2 L/hour
Comparison of clearance capabilities be	tween renal repla	cement moda	lities						
Modality	СЛИН	Standard her using one filt of 800 ^c	nodialysis er with K0A	Extracorpo hemofiltra in-line Sor concentra	oreal circuit tion with two in-14 hemo- tors	Extracorporeal tion using multi trators (>2) to to trators (>2) to total circuit blo	circuit hemofiltra- iple hemoconcen- a accommodate od flow	Extracorpore mofiltration u hemofilters to modate total flow	al circuit he- sing multiple accom- circuit blood
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Average blood flow rate Filtration fraction*	250 cc/minute	Not andirah		2 L/MINUTE		5 L/minute 76%		3-/ L/Minute	
Replacement rate	50 cc/minute	Not applicab	<u>e</u>	400 cc/mir	iute	L/minute		L.5 L/minute	
Theoretical clearance	3 L/hour	14.4L/hour		24 L/hour		60 L/hour		90 L/hour	
Kt/V in I hour in 70kg male assuming 60% volume of distribution ^e	0.07	0.34		0.57		I.42 ^f		2.1	
CVVH: continuous veno-venous hemofiltrati High-efficiency hemofiltration is easily able to clotting, traditional filtration fraction limits of a Theoretical clearance (K) = (hemofiltration a able to be filtered at the membrane. Post-filt bCalculated clearance is $K \square =$ (hemofiltration $K \square$ may be different from K due to higher effi reflect other compounds hemofiltered along %OA refers to the efficiency of a given dialyz blood flow provided in standard tables. Filtration fraction of higher than 20% is rarel used in high blood flow extracorporeral circui %TTV is a unitles number that compares the feven with convention filtration fraction value ECMO-based therapy. It would take $20 \times$ as "Based on patient hemoglobin of 8 g/dL (hem	on: RRT: renal repla orival hemodialysis of 20% can be exceed mount/treatment ti er administration of amount/treatment luent Cr in relation with Cr (e.g. antibio with Cr (e.g. antibio of the extinitie blood i by applied with conv its like ECMO). e amount of clearan its like ECMO). e amount of clearan its like achieve equ atocrit 24%).	cement therapy with two filterapy and two filterapy me) × S, where ine) × S, where ine) × effluent to average seru- to average seru- seru	r, ECMO: extract in parallel and clac is the sieving co sis the sieving co raid is assumed. Cr/average seru im Cr. This may im Cr. This may im Cr. This may im Cr. This may im cr. This may if for the values ir te flow, with high ven risk of filter ven risk of filter ven risk of the value of d i the volume of d	arporeal mer farance mark oefficient of (m Cr ⁴ . Telate to inhe r the Cr assa ier values sug ier values sug ier values of th varison to th istribution of th	nbrane oxygenation tedy increases at m the medy increases at m the membrane. For the membrane. For setting a bigger sur gesting a bigger sur vever, filtration frac vever, filtration frac de total volume of d a small molecular olumn 5).	n. aximal blood flow small molecules, t Cr measurements : face area. Clearar face area. Clearar face area. clearar substance can be e	s. If systemic anticoagula his is assumed to be 1. ⁻ at very low effluent con- ice K is calculated from sed when using systemic stance in the body.	ation is used to p That is, all of the centrations. In ac nomograms base anticoagulation y with high blood	revent filter compounds are dition, this may d on actual (as is routinely flow

levels of solute clearance for potential therapeutic benefit.⁸ Thus, the high-efficiency, high-flux clearance that can be achieved by this approach may broaden the utilization of convective solute removal as a possible therapeutic tool for a variety of disease states mediated by endogenous or exogenous toxins.

Potential limitations of highly efficient solute clearance include two major considerations: first, potential removal of beneficial drugs, electrolytes (e.g. phosphate), and important molecules such as micronutrients (e.g. B-6, B-12, ascorbic acid, etc.)^{9,10} This would need to be further studied along with consideration of drug dosing modification and development of replacement fluid to include physiologic concentrations of important molecules at risk for depletion. Abrupt change in serum osmolality due to highly efficient solute clearance is another potential risk. This could likely be managed with the addition of urea or an alternative osmole to the replacement fluid to avoid development of hemodynamic instability, cerebral edema, and dialysis disequilibrium. Second, there is risk of poor volumetric control that could lead to hemodynamic instability.1 This was addressed by first giving volume and then removing it as opposed to the converse, obviating the potential for becoming volume contracted from the beginning of therapy. Strict perfusionist monitoring of hemofiltration via gravity-based drainage (i.e. exactly matching input replacement volume with effluent output volume) further prevented risk of inaccuracy in volume removed. Obviously, for routine practical patient care, this would require an alternative, automated, and accurate means of effluent measurement beyond gravity drainage that is not currently available. Finally, cost and invasiveness of this robust hemofiltration system would need to be weighed against benefit.

Conclusion

Hemofiltration at high blood flow rates with high-flux membranes offers highly efficient solute clearance well beyond current RRT capabilities. Traditional RRT limitations of blood flow dependency and filtration fraction can be overcome to offer rapid clearance of toxins, including those not currently dialyzable (e.g. those with high volumes of distribution).⁸ Further study of this high-efficiency, high-flux hemofiltration circuit may maximize the potential utility of this novel form of convective clearance.

Author's Note

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Informed Consent

Written informed consent was obtained for publication of patient's clinical details and clinical images from the patient. A copy of the consent form is available for review by the Editor of this journal. IRB oversight was also obtained (IRB number HP-00086910).

ORCID iDs

Alison Grazioli D https://orcid.org/0000-0003-4455-3371 Ronson J Madathil https://orcid.org/0000-0002-0855-3270 Laura DiChiacchio https://orcid.org/0000-0002-0854-7241

Supplemental Material

Supplemental material for this article is available online.

References

- 1. Askenazi DJ, Selewski DT, Paden ML, et al. Renal replacement therapy in critically ill patients receiving extracorporeal membrane oxygenation. *Clin J Am Soc Nephrol* 2012; 7: 1328–1336.
- Sorin Hemoconcentrators. Palex medical, http://www. palexmedical.com/file_download.cfm?ftid=1&fid=292 (accessed 14 January 2019).
- Palevsky PM, Zhang JH, O'Connor TZ, et al. Intensity of renal support in critically ill patients with acute kidney injury. N Engl J Med 2008; 359: 7–20.
- Macedo E, Mehta RL. Continuous dialysis therapies: core curriculum 2016. Am J Kidney Dis 2016; 68: 645–657.
- Syal K, Banerjee D, Srinivasan A. Creatinine estimation and interference. *Indian J Clin Biochem* 2013; 28: 210–211.
- Sigler M, Teehan B, Daugirdas J, et al. Slow continuous therapies. In: Daugirdas J, Blake P, Ing T (eds) *Handbook* of dialysis. Philadelphia, PA: Lippincott Williams & Wilkins, 2001, pp. 169–197.
- Fasano A, Farina A. Modeling high flux hollow fibers dialyzers. *Disc Cont Dyn Syst B* 2012; 17: 1903–1937.
- Winchester J, Kitiyakara C. Use of dialysis and hemoperfusion in treatment of poisoning. In: Daugirdas J, Blake P, Ing T (eds) *Handbook of dialysis*. Philadelphia, PA: Lippincott Williams & Wilkins, 2001, pp. 300–320.
- Kasama R, Koch T, Canals-Navas C, et al. Vitamin B6 and hemodialysis: the impact of high-flux/high-efficiency dialysis and review of the literature. *Am J Kidney Dis* 1996; 27: 680–686.
- Rocco M, Blumenkrantz M. Nutrition. In: Daugirdas J, Blake P, Ing T (eds) *Handbook of dialysis*. Philadelphia, PA: Lippincott Williams and Wilkins, 2001, pp. 420–445.