

## 3D-Printed Biomimetic Hierarchical Nacre Architecture: Fracture **Behavior and Analysis**

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(NS), and a pristine structure via fused deposition modeling (FDM) and explores their mechanically superior stacking structure, mechanism of failure, crack propagation, and energy dissipation. The examination reveals that the nacre structure has significant mechanical properties compared to a neat sample. Additionally, NS has 112.098 J/m impact resistance (9.37% improvement), 803.415 MPa elastic modulus (11.23% improvement), and 1563 MPa



flexural modulus (10.85% improvement), which are all higher than those of the NC arrangement.

## **1. INTRODUCTION**

Nacre, the iridescent hierarchy, yields superior mechanical performance, which is attributed to their toughening mechanisms at the micro level, such as the stacking arrangement of a tablet, the aspect ratio of a tablet, the volume fraction of hard and soft parts, and the interlocking angle, as well as at the nano level, such as nanoasperities, mineral bridges, organic interlamellar matrixes, and axial growth in the perpendicular direction.<sup>1</sup> Two diverse microarchitectures of nacre were found in nature known as bivalves and gastropods. The bivalve shell has a nacre sheet (NS), in which the platelets are arranged in a "brick wall" design where a mortar phase bridges the boundary among the respective underlying tiles. Columnar nacre (NC) is found in shells of gastropods, which have hexagonal platelets of almost equivalent size with matching centers that regulate the overlying tablets' nucleation.<sup>2,3</sup> The vigorous mechanical performance of nacre architecture relies on the accurate geometric sequencing of the tablet at the microscopic level.<sup>4</sup> The inner layer of mollusk shells comprises an iridescent nacre material, which has the most sought-after natural structure as it demonstrates unusual impact resistance and fracture toughness, although most of the material constitutes brittle ceramic.<sup>5</sup> It comprises 95 wt % brittle aragonite platelets, calcium carbonate (CaCO<sub>3</sub>) crystal form, and a 5 wt % soft phase of polysaccharides and protein, forming a nanostructure of brickand-mortar arrangement. The bricks are densely packed with polygonal aragonites of 5–8  $\mu$ m diameter and 20–90 Å thick platelets and welded by the mortar matrix of organic interlamellar of 1-5 Å thickness.<sup>6,7</sup> This distinctive hierarchical

building could be the basis of protective equipment and body armor with numerous functions, including high strength, lightweight, high energy absorbing capacity, and high stiffness due to its equally 3 times superior energy absorption associated with the fundamental composites.<sup>8</sup> Nacre columnar (NC) comprises almost uniform tablets which regulate the nucleation site of the overlying tablets as centers are overlapping, whereas in a NS, a "brick wall" pattern is followed for tablet stacking, and deposition starts over most of the inner surface of the shell.<sup>9</sup> The top view of the columnar nacre has revealed that the adjacent layers intersect and represent polygonal tablets in such a way that the lamellar interfaces are perpendicular to inter-platelet borders, which form tessellated bands on the other hand in NS geometry; the distributions of inter-tablet boundaries are random.<sup>10</sup> The overlap and core regions are significant in the NC because the stress experienced in both areas varies. In the NS, the core and overlap regions experience no distinction.<sup>11,12</sup> Nacre can achieve remarkable toughness and strength simultaneously, employed in diverse structural applications like aerospace and automotive, based on the loading direction and fracture mechanism. NC has well-defined deformation bands that are perpendicular to the loading

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direction of the columnar structure, and NS forms an unusual network of deformation bands at an angle to the main crack.<sup>1</sup> The research focuses on developing artificial nacre structures with strengthening mechanisms, such as crack blunt, deflection, stress delocalization, crack bridging, interfacial strengthening, topological interlocking, and aspect ratio<sup>14,15</sup> to accomplish the requirements of high structural applications. Researchers have studied the fracture modes and gained an understanding of the failure of the nacre using simulation and analytical modeling approaches; nevertheless, there have not been many experimental studies conducted to understand the observed behavior.<sup>16–18</sup> Modern manufacturing methods, such as 3D printing, open room to designing bio-inspired artificial nacre materials with systematic control over brick-and-mortar stacking, interlocking, toughening, and failure understanding.<sup>19,20</sup> Additive manufacturing (AM) enables on-demand customized construction of the object by virtue of 3D scan's digital slicing, CAD, or tomography data, where substances form layer-by-layer, devoid of the demand for machining and molds. AM techniques covered numerous categories per ISO/ ASTM 59200:2021 based on the feeding material type or curing mechanisms. Existing AM technologies include extrusion (Fused deposition modeling (FDM), 3D dispensing, direct ink writing (DIW), 3D plotting, and 3D fiber deposition), vat photopolymerization [stereolithography (SLA) and digital light processing (DLP)], powder bed fusion [selective laser sintering (SLS) and selective laser melting (SLM)], binder jetting (3D bioprinting, aerosol 3D printing, and inkjet), material jetting, sheet lamination (LOM), and direct energy deposition (DED).<sup>21</sup> The working principle, pertinent features, advantages, and limitations are covered in Table 1 and portrayed in Figure 1. FDM, fused filament fabrication (FFF), DIW, 3D dispensing, and 3D bio plotting fall into the material extrusion category where feedstock is particularly dispensed in an x-y plane through a heated nozzle with a predefined diameter, as described in Figure 1.<sup>22</sup> Extrusion-based AM involves printing of thin thread in a predefined first-layer pattern, followed by subsequent layer deposition (downward movement of platform in the z-axis) until the desired 3D piece is obtained  $^{23,24}$  (Figure 1a,b). Transformation of a liquid photopolymer to a solid object by application of a light source falls under the category of vat polymerization, where ultra-high molecular-weight monomer or oligomer material is reticulated using ultraviolet light. SLA and DLP are two sub-categories of vat polymerization (Figure 1c). First-layer adhesion with a platform or solidification of resin initiated at a specific depth with a precise geometrical pattern via a light beam from laser. After curing of the initial layer, the building stage is shifted downward for another liquid filling and second layer reticulation; subsequently, other layers are added until the defined height.<sup>25</sup> In the material jetting process (Figure 1d), the photopolymer droplets of specific shape are selectively deposited on a platform using one or more mobile printing heads. To facilitate a uniform and continuous flow of material during the injection process, the viscosity of material is reduced using heating and later deposited material is cured through a UV light beam. The drop deposition method permits accurate aligning of the material, providing high tolerance to the body under the building and reducing material waste. Powder-based AM begins by conveying a powder layer material from the materials feed platform to the printing stage using feeding rollers.<sup>20</sup> Fusion (in binder jetting, Figure 1e) or sintering (in SLS, SLM,

type of 3D printing	material used	solidification mechanism	feature resolution $(\mu m)$	pros	cons
vat polymerization	photosensitive resins, acrylates, epoxides	photopolymerization	25 - 100	high resolution, precision, and surface quality	photo processing is necessary; vulnerable to weak and heat
extrusion-based	soft polymers, thermoplastics, inks, PLA, ABS, PC, composites	sequencing layered cooling at moderate and room temperature	100-150	excellent strength component reduces the cost of production, versatility in material selection	a sluggish process, high rough processing temperature
powder-based fusion	PA12, PEEK, ceramics, metal, alloys	sintering, melting	50-100	a robust and complex part, less anisotropy	rough surfaces; poor Reusabili unsintered powder
material or binder jetting	dielectric starch, conductive inks, gels	crosslinking of polymers, room temperature cooling	10-25	multimaterial, fast printing, low-temperature process	low viscous ink needed, limited the part, low surface finish
sheet lamination	PVC, paper, plastic sheet	laser cutting and binder curing via laser	200-300	compact desktop printing	high anisotropy, low resolution materials
DED	metal powder pr wire	laser sintering or melting	150-200	more complex design printing, any shape building, low material waste	expensive, low resolution, surfa
3D bioprinting	thermoplastics, composites, photoresins, hydrogels, biomaterials	UV curing, crosslinking curing at an average temperature	10-100	a broad range of materials	narrow viscosity process windc
<sup>2</sup> Reused from r	efs 21 and 29 with permission. Copy	rright 2017 & 2021, ACS.			

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Table 1. Summary of Various Printing Technologies with Their Features, Merits, and Demerits<sup>a</sup>



**Figure 1.** Graphic representation of numerous 3D printing processes. (a) extrusion-based FDM with its features and proper extrusion, (b) extrusion-based DIW process, (c) SLA method of liquid resin, (d) photopolymerization in Polyjet, (e) 3D modeling via binder jetting, (f) sheet lamination process (LOM), and (g) method of SLM and SLS. Reused from refs 30 and 31 with permission: Copyright 2017, MDPI, and Copyright 2021, Springer Nature.

and EBM, Figure 1g) of the powder material to a desired shape is accomplished by a programed energy source or binder deposition to the platform surface. This step is repeated to obtain the final 3D geometry, and further post-processing is performed to eliminate the infiltrated or support material.<sup>27</sup> The sheet lamination printing technique can be employed to construct three-dimensional (3D) pieces from continuous cutting of 2D sections followed by lamination. This AM method can be classified into two, unrolled and rolled procedures linked by a sheet of material piloted by the revolving rollers. Deeding and storing of material are simultaneously performed in this system. In addition, sheet lamination has a printing stage (that can execute vertical changes), a roller, and a laser<sup>28</sup> (Figure 1f).

FDM demonstrates an encouraging route among all 3Dprinting manufacturing techniques to facilitate direct incorporation of the intricate, micro-level, multi-material, and porous geometries within the final 3D object.<sup>32</sup> FFF and FDM are widely utilized techniques among other 3D printing techniques that permit the adequate printing of intricate constructions guided by XYZ movement according to CAD models. Over traditional manufacturing, the key advantages of the FDM technique are that it enables rapid prototyping and on-demand

fabrications. Moreover, FDM is at the lead of facilitating restructured production, which is crucial to diminishing the carbon footprint and empowering smart production approaches in the upcoming market.<sup>23</sup> Though effective in building satisfactory erections, compared with FDM, the existing volumetric AM technologies, SLA, and DLP printing have a low utilization efficiency of wet material (the weight proportion of the final fabricated architecture to the original quantity of liquid resin in a bath). Other than this, they have less utilization efficiency of the remaining material (the weight proportion of the attained dry printed geometry to the initial quantity of liquid resin).<sup>33</sup> Aspects of FDM printing and processing parameters such as building speed and improving the accuracy, functionality, mechanical properties, porosity, surface finish, and stability are addressed.<sup>34</sup> Versatile applications establish how FDM-based AM has been developed for energy technology, lightweight engineering, optics, architecture, food processing, drug delivery, dentistry, and personalized medicine.<sup>35</sup> The collection of polymeric materials used in FDM encompasses materials like polymer blends, thermoplastics, functional polymers, elastomers, hydrogels, biological systems, and composites. FDM uses most thermoplastic materials, such as polylactic acid (PLA),



**Figure 2.** (a) Difference between the 3D and 4D printing processes and output. Reused from  $ref^{22}$  with permission. Copyright 2021, Taylor & Francis, (b) General advantages and disadvantages achieved by 3D and 4D printing technology. Reprinted from  $ref^{48}$  with permission. Copyright 2022, Elsevier. (c) SWOT analysis for both techniques. Adapted from  $ref^{46}$  with permission. Copyright 2023, Elsevier.

acrylonitrile butadiene styrene (ABS), nylon, polyethylene terephthalate glycol, and their blends like polycarbonate–ABS (PC-ABS), nylon carbon fibers in the form of the continuous diameter filament.<sup>20,36</sup> Apart from conventional materials,

filaments are produced with reinforced composites to enhance thr mechanical properties, non-flammability, chemical stability, and high abrasion. Wang et al. evaluated a high-performance PEEK composite reinforced with the carbon fiber (CF) and

	3D printing	4D printing		
materials	thermoplastics, metals, ceramics, biomaterials, or nanomaterials	self-assembled materials, multi-materials designed materials examples: shape memory alloy/polymer/hybrids, self-degradation/deformation materials, temperature/UV-driven materials		
design	3D digital information	3D digital information for change		
printer	3D printer examples: SLA, material extrusion, and SLS	smart 3D printer examples: modified nozzle, binder, and laser multimaterial 3D printer examples: solid/liquid, solid/solid, gradient materials, and nanocomposites		
static or astatic	as printed/static	After printing changes in shape, color functions over time		
applications	jewelery, toys, fashion, entertainment, automobiles, aerospace, defense, and bio/ medical devices	applications involved a dynamic change in configurations		
<sup>a</sup> Reused from <sup>47</sup> with permission. Copyright 2020, Elsevier.				

# Table 2. Comparison of 3D and 4D Printing with Different Materials, Designs, Changes Undergone (if Any), and Applications<sup>a</sup>

glass fiber (GF). The investigation indicated that incorporation of CF and GF from 5 to 15 wt % improved the thermal properties, mechanical characteristics (flexural properties are 5 wt % GF/PEEK (165 MPa) and 5 wt % CF/PEEK (94 MPa), with the improvement of 17% and 19% over that of produced pure PEEK, respectively), and surface porosity.<sup>37</sup> A mechanical attribute of an object significantly differs from bulk material or input material properties, in which adhesive bonding creates each layer from the extruded fiber's connection. Layered fabrication depends on various property-controllable characteristics like direction of the printing layer, raster angle, infill pattern, and infill direction, which untimely result in either being brittle or ductile depending on the combination of printing parameters.<sup>38</sup> Josef Kiendl investigated that incorporating a brittle PLA material in FDM-printed objects renders brittle behavior in the parallel printing direction to the loading direction, while the inclined direction of printing to loading results in ductile behaviour.<sup>39</sup> Consequently, many of the researchers have established numerous nature-inspired hierarchies, including a mollusk shell layer of nacreous material, utilizing filament-based AM and verifying the modification in structural characteristics. Peng and co-workers designed fused deposition-modeled biomimetic architecture to mimic Elytrigia repens and examined the resilience and stiffness through mechanical analysis and multiscale finite element analysis (FEA).<sup>40</sup> Jia et al. created numerous nature-inspired constructions, through multi-material FDM printing for the compact tension (CT) fracture test. They estimated the toughness for fracture employing a nonlinear elastic J-integral approach and evaluated the mechanisms of toughening using fracture theories.<sup>41</sup> Padole et al. fabricated a range of biomimetic structures, including NC and NS, prismatic, complex cross lamellar, and foliated structures using FDMbased 3D printing. The result of their study shows that, owing to the well-defined hierarchical architecture, superior toughness and extraordinary impact strength were observed in the nacreous structure among the produced architectures.<sup>3</sup> Yadav et al., developed nature-inspired materials by mimicking the architecture of molluscan shells, such as complex cross lamellae, foliated, cross-lamellae, and nacre, using a layer-bylayer FDM printing technique. They concluded each constituent affected the mechanical and surface frictional properties according to structural manipulation.<sup>42</sup> Ko et al. designed the nacre-mimicked architecture to fabricate an optimum impact resistance under three various impact conditions through an integrative utilization of bi-material 3D printing, drop-weight impact test, parametric study, and FEA.43

3D printed materials are not limited to static nature but can be reformed by shifting distinct characteristics, such as shape, hardness, color, functions, and transparency, when subjected to heat, magnetic or electrical source, water, pH, and light, which is an advance form of 3D printing known as 4D printing<sup>44,45</sup> (Figure 2a). 3D- and 4D-printed composites cover vital applications in mechanical constructions, in aeronautical, automotive, consumer goods, and aviation industries, and in sports or safety equipment. The prime benefits of 3D and 4D printing technologies are that they have fewer waste materials, require less energy during manufacturing, and have extreme flexibility in the fabrication related to conventional techniques; therefore, both the printing techniques have tremendous potential for innovation, design, and development in various sectors<sup>46,47</sup> (Figure 2b,c). A recapitulation of 3D/4D printing based on innovation, materials employed, and changes in printed objects, printers, and applications is presented in Table 2.

The present investigation focuses on an experimental comparison of FDM-printed artificial nacre structures concerning different stacking arrangements, columnar nacre, and sheet nacre. The monolithic Polycarbonate-Acrylonitrile Butadiene Styrene (PC-ABS) was chosen for the experiment because it provides excellent processibility and heat distortion resistance and exhibits good impact resistance, improved shrinkage, and dimensional stability. The mechanical response via the Izod impact test, tensile test, and flexural bending testing elucidated NS's superior stress-distributing capability compared to NC erection. Therefore, our report comparing the performance of different nacreous structures shows the experimental validation and potentially broadens the feasible fabrication route of NS and NC architectures.

## 2. MECHANISM OF NACRE FRACTURE

The natural organic region in the hierarchy behaves as a multidomain structure of adhesion binding in-between aragonite ceramic platelets, which provides good energy dissipation in every ceramic platelet delamination. It has been contemplated that the aragonite plates exhibit ductile attributes when perpendicular to the direction of applied strain renders. Additionally, Gries and co-workers revealed the existence of holes with the width of 2.5 and 38.4 nm in the aragonite region and considered that the presence of voids diminishes the propagation of the crack, thus enhancing the fracture toughness of shells.<sup>49</sup> Besides that, Xia and the team established that controlled sliding of nanoasperities renders an unusual mechanical behavior to strain hardening.<sup>50</sup> Chen and

colleagues presented five mechanisms for nacre toughening: (1) weak organic interface, (2) interlocking of nanoasperities, (4) inter-lamellar mineral bridges, (4) plastic deformation of individual tiles, (5) numerous cracks, and enormous-scale crack bridging<sup>51</sup> (Figure 3). Nacre fracture is further reduced



Figure 3. Illustration of various fracture mechanisms in the nacreous mollusk shell, the mother-of-pearl.

by adding nanoasperities, voids, pre-strain, cracks, mineral bridges, and soft materials with long polymeric chains.<sup>52</sup> The composite of nacre hierarchy can be directly applied in materials currently employed in structural components due to they demonstrate length scales and polymer chemistry analogous to those of traditional fiber-reinforced polymers. The high stiffness, toughness, and strength of these natureinspired materials could be readily applied, such as in the leading edge of aircraft foils, or protective layers in turbine blades, to locally diminish abrasion, damage by impact, and surface wear in these vital structural applications. On the other hand, the chemistry between organic and inorganic region could be altered to generate resorbable and osteoinductive hierarchical materials for application in regeneration of bone.<sup>53,54</sup> This experiment focused on ballistic performance to characterize nacre composite using the following parameters crucial in determining the impact energy absorption.<sup>43</sup> Consequently, the absorbed impact energy by the fabricated Nacre-like structure "e" can be mathematically formulated by a function of the dimensional parameters as,<sup>4</sup>

$$e = f(A_{\rm M}, A_{\rm B}, v_i, D_i, m_i, \rho_c, E_c, \sigma_{yc}, I_c)$$
(1)

where  $A_{\rm M}$  and  $A_{\rm B}$  represent the areas of mortar and brick, respectively,  $\rho_{\rm c}$  Is the density of the composite,  $E_{\rm c}$  and  $\sigma_{\rm yc}$  are the composite's elastic modulus and yield strength, and  $I_{\rm c}$ describes the Izod strength of the composite. A nacre-like composite comprised an equal number of fundamental dimensions and repeating variables, with three essential dimensions and ten repeating variables. Therefore, seven pi equations were possible as the impact velocity  $v_{ij}$  the diameter of the impactor  $D_{ij}$  and the impactor's mass  $m_i$  have all dimensional components.

$$\pi_{1} = [m_{i}]^{\alpha} [D_{i}]^{\beta} [V_{i}]^{\gamma} [e]$$
(2)

$$\pi_2 = [m_i]^{\alpha} [D_i]^{\beta} [V_i]^{\gamma} [A_{\text{TPU}}]$$
(3)

$$\pi_3 = [m_i]^{\alpha} [D_i]^{\beta} [V_i]^{\gamma} [A_{\text{PLA}}]$$
(4)

$$\pi_4 = [m_i]^{\alpha} [D_i]^{\beta} [V_i]^{\gamma} [\rho_c]$$
(5)

$$\pi_{5} = [m_{i}]^{\alpha} [D_{i}]^{\beta} [V_{i}]^{\gamma} [E_{c}]$$
(6)

$$\pi_{6} = [m_{i}]^{\alpha} [D_{i}]^{\beta} [V_{i}]^{\gamma} [\sigma_{\rm yc}]$$
<sup>(7)</sup>

$$\pi_7 = [m_i]^{\alpha} [D_i]^{\beta} [V_i]^{\gamma} [I_c]$$
(8)

The exponents are independent variables described by  $\alpha$ ,  $\beta$ , and  $\gamma$  and from eq 1 dimensional parameters can be written in terms of fundamental physical units mass M, length L, and time T,  $[e] = ML^2 T^{-2}$ ,  $[A_{TPU}] = [A_{PLA}] = L^2$ ,  $[\nu_i] = LT^{-1}$ ,  $[D_i] = L$ ,  $[m_i] = M$ ,  $[\rho_c] = ML^{-3}$ ,  $[E_c] = [\sigma_{yc}] = ML^{-1} T^{-2}$ , and  $[I_c] = MT^{-2}$ . Solving all the nondimensional pi equations from (2) to (8) derivation gives

$$\pi_{1}, \ \left[m_{i}\right]^{\alpha+1} \left[D_{i}\right]^{\beta+2+\gamma} \left[V_{i}\right]^{-2-\gamma} = 0 \tag{9}$$

$$\pi_{2}, \ [m_{i}]^{\alpha} [D_{i}]^{2+\beta+\gamma} [V_{i}]^{-\gamma} = 0$$
(10)

$$\pi_{3}, \ [m_i]^{\alpha} [D_i]^{2+\beta+\gamma} [V_i]^{-\gamma} = 0 \tag{11}$$

$$\pi_{4}, \ [m_{i}]^{1+\alpha}[D_{i}]^{-3+\beta+\gamma}[V_{i}]^{-\gamma} = 0$$
(12)

$$\pi_5, \ [m_i]^{1+\alpha} [D_i]^{-1+\beta+\gamma} [V_i]^{-2-\gamma} = 0$$
(13)

$$\pi_6, \ [m_i]^{1+\alpha} [D_i]^{-1+\beta+\gamma} [V_i]^{-2-\gamma} = 0$$
(14)

$$\pi_7, \ [m_i]^{1+\alpha} [D_i]^{\beta+\gamma} [V_i]^{-2-\gamma} = 0 \tag{15}$$

Nondimensional variables can be derived as follows because the dimensions in eqs 9-15 are zero

$$\pi_1 = \frac{e}{m_i v_i^2} \tag{16}$$

$$\pi_2 = \frac{A_{\rm TPU}}{D_i^2} \tag{17}$$

$$\pi_3 = \frac{A_{\rm PLA}}{D_i^2} \tag{18}$$

$$\pi_4 = \frac{\rho_c D_i^3}{m_i} \tag{19}$$

$$\pi_5 = \frac{E_c D_i^3}{m_i v_i^2} \tag{20}$$

$$\pi_6 = \frac{\sigma_{\rm yc} D_i^3}{m_i v_i^2} \tag{21}$$

$$\pi_7 = \frac{I_c D_i^3}{m_i v_i^2}$$
(22)

where  $\pi_1$  represents the ratio of energy absorbed to the kinetic energy of the projectile,  $\pi_2$  represents the zone ratio of the soft matrix and the zone of the impactor,  $\pi_3$  is the contact area ratio of the complex phase and impactor area,  $\pi_4$  indicates the percentage mass per volume of composites to the impactor



Figure 4. Mechanical testing results of (a) Izod impact test, (b) tensile test, and (c) flexural bending test.

density,  $\pi_5$  represent elastic modulus vs dynamic energy per volume,  $\pi_6$  is a ratio of strength at a yield to vibrant energy per volume,  $\pi_7$  indicates the ratio of Izod impact strength vs kinetic energy per volume.

The fracture of nacre materials relies on a stiff and stacking arrangement, the shape and size of a tablet, volume fraction of tablet (hard) material and organic (soft) material, the interlocking angle, aspect ratio, and mineral bridges. However, numerous analytical and simulation studies were conducted to examine failure behavior and superior mechanical structure concerning stacking arrangements in NC and NS. The crack propagation, crack hindering, and braking of these significant uniform and nonuniform placements in NC and NS were represented by various models like (i) discrete element method (DEM),<sup>18</sup> (ii) representative volume element (RVE),<sup>17</sup> and (iii) trans-scale shear-lag model.<sup>16</sup> The study showed using DEM (eqs 23-25) that the propagation of a crack in NC is through the tablet boundary, which can be hindered and pinned; nevertheless, a slight amount increases in toughness; as a result, it will reduce the cohesive length of pinning compared to the coherent size of the crack. On the other hand, NS structure crack propagation was uneven, and pinning at many stages improved the mechanical strength and toughness.

Moreover, the developed NC model shows all junctions open, conveying linear deformation and sliding of the tablet during RVE analysis. In contrast, the NS model exhibits a stair pattern where a large number of intersections remain closed or partially open.<sup>17</sup> More explanation regarding analytical and simulation models for the fracture of different stackings in nacre will be found in Supporting Information file S1.

bridging model toughness,  $J_{\rm B}$ 

$$= k \rho J_{i_{i}} \text{ normalised toughness}$$
$$= \frac{J}{J_{B}}$$
(23)

tablet aspect ratio,  $\rho = L/t$ , specific aspect ratio  $= \overline{\rho}$ 

crack extension = 
$$\Delta \alpha / t$$
 (25)

## 3. METHODOLOGY

Artificial nacre is manufactured via PC-ABS owing to an appropriate impact strength of 25.5 kJ/m<sup>2</sup>, tensile strength of 37 MPa, low density of 1.1 g/cm<sup>3</sup>, high flow, and Vicat softening temperature 108 °C. FDM (Method X, MakerBot) was used to fabricate a shell architecture with 100% infill density and a 0.1 mm layer height. Characterizing intricate nacre geometry analyzed using an Izod impact tester (Tinius Olsen Impact 503) as per ASTM D256, tensile testing, and 3-point flexural bending test (UTM. Instron) performed according to ASTM D638 and ASTM D790 accordingly. The microstructure examination of fractured hierarchical and cryogenic fractures was analyzed using FESEM (Zeiss, Germany). The surface roughness of FDM-printed components was quantified using RUGOSURF 90G surface rough-

(24)



Figure 5. Representation of surface roughness evolution results, (a) surface roughness,  $R_A$  value of three different arrangements, (b) maximum height of top layer profile,  $R_z$  value, and (c) surface waviness graphs of pristine, NC, and NS geometry.

ness testers (TESA SWISS MAKE) for pure and nacre parts to estimate the surface imperfection considering different designs. The mean surface roughness (Ra) and the mean maximum height of the profile (Rz) are quantified for the upper surface layer of the FDM-printed neat PCABS, columnar, and sheet samples. Three different regions on a sample were assessed for roughness of the surface in each arrangement.

## 4. RESULTS AND DISCUSSION

The impact resistance was performed as per ASTM D256, where the specimen was designed via Solid Works, followed by fused deposition 3D printing of PC-ABS. According to the NS and NC, the prepared specimens had different stacking arrangements, tablet interfaces, and tablet locking from each other. Therefore, each sample noticeably comprises a varied capacity for absorbing impact energy.<sup>43</sup> Figure 3a delineates identical features of the printed nacre composite, where the impact resistance (IR) and absorb energy (AE) of the NS system (AE = 0.7323 J) was thought to be uppermost in addition to the supreme energy absorption of the NC skeleton (AE = 0.6106 J) compared to the monolithic PC-ABS sample (AE = 0.5457 J). The toughness of mollusk shells is attributed (deformation and fracture) to various mechanisms comprising void formation, nanoasperities, and their controlled sliding, interlocking of a tablet, and interlayer mineral bridges.

Meanwhile, the developed nacre architecture does not encompass either interlocking, mineral bridges, or nanohierarchy; consequently, the impact performance could be a function of the tablet's center direction and its configurations.<sup>55</sup> Figure 4a delineated the average value of five sequential experiments for impact resistance and absorb energy. Furthermore, tensile testing was conducted as per the ASTM D638 type IV standards for PC-ABS printed samples, which boosted the experimental and analytical study on NC and NS. It was evident from the survey that crack propagation, while fracture in mollusk shell follows numerous methodologies; however, the phenomenon of stress whitening or process zone was observed in the energy dissipation mechanism of nacre, which is equivalent to the polymeric systems crazing.<sup>56</sup> Following that, Figure 4b deduces the tensile characteristics of advanced composites, where the initial stress–strain curve indicates an almost equivalent nature to yielding or low-strain applications.

Additionally, promoting further load on structures, NS manifests a noteworthy enhancement in force dissipation up to 33.3897 MPa of ultimate stress, although NC ends at 31.5986 MPa and the clean sample reached 27.9189 MPa. In contrast, Young's modulus (E) of the NS (803.42 MPa) describes a superior value to the NC (746.55 MPa) sequentially compared to the pristine structure (623.33). As per the RVE model, a similar behavior shows that under the action of uniaxial force, cracks propagate in the direction that grips low energy; hence, a NC skeleton made of uniform stacking yields a crack deflection path, while at the same point, breaks encounters with hard bricks in an asymmetrical network, which urges for surpassing energy in NS.

Additionally, Figure 4c also provides the load-displacement curve of dynamic mechanical flexural bending flexural results of monolithic, NC, and sheet architecture.<sup>57</sup> As per Figure 4c, from the initial loading until the fracture, the NC structure deforming slightly subordinately corresponds to a non-uniformed nacre array, whereas the pristine geometry trails

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Figure 6. Design of NC and NS architectures. (a) design of the single tablet, a 2D sheet of brick-and-mortar phase, CAD model of NC and sheet, and 3D printed view (expanded top view); (b) fracture surface morphology of pristine, columnar, and sheet structure analysis using an optical microscope and SEM images with a specific region of hard (brick) and soft (mortar) segments.

an identical path. For columnar stacking, the crack propagates at the interface of brick, which can be separated quickly, leading to crazing in the zone, while the sheet also has an equivalent tendency to a generation of crack, yet the propagation hinders subsequent bricks in layered position. The bending strengths of 3D-printed immaculate geometry and gastropod architecture achieved the maximum levels of 32.05 and 33.79 MPa, respectively, whereas bivalve shell geometry reached the ultimate power of 43.75 MPa. However, it has been noticed that total energy absorbance capacity was superior for the NC, attributed to minor interlayer deviation and interface tablet cohesion against bending load conditions.<sup>58</sup>

**PC-ABS** 

The surface unevenness value of the upper layer of PCABS objects is calculated, and the mean average of surface roughness (Ra) and the mean maximum profile height (Rz) for each bio-inspired skeleton are provided in Figure 5a,b. As per shown in Figure 5c for the 2D roughness profiles, it is observed that the roughness profile is higher if the peak-tovalley difference is height, which is described by the nacreous sheet; however, it progressively declines for columnar nacre and a neat sample.<sup>59</sup> The new PCABS component comprises an  $R_A$  value (arithmetic average) of 2.02  $\mu$ m and an  $R_Z$  value of 14.336  $\mu$ m; nonetheless, for the NC structure, a maximum  $R_A$ reaches 11.038  $\mu$ m, and a value of  $R_Z$  observed as 49.408  $\mu$ m and the highest surface roughness  $R_A$  of 20.842  $\mu$ m, and  $R_Z$  of 103.959  $\mu$ m are obtained for densely packed NC tablets. Printing top layer patterns such as 0/90, -45/+45, hexagonal, and concentric have voids and porosity, which act as unevenness in the outermost layers, increasing roughness.

Chemical treatments in 3D printing modify the top surface due to dissolving surface material and filling the voids between rasters, resulting in a smoother and more uniform surface. Surface texture is a surface roughness component that plays a crucial role in defining the composite interaction with other environments such as temperature, water, coatings, and adhesives. Roughness is an excellent gauge of the prospective functioning of a mechanical component owing to irregularities on the plane that could form a nucleation site for corrosion or cracks.<sup>60,61</sup>

Combining the high toughness and strength of nacre-like 2D sheets can be achieved by blocking crack propagation along the platelet side and the interface in their nanostructure of brickand-mortar. Although the variation of cracks in the microstructure of brick-and-mortar is well detailed, numerous other mechanisms for energy absorption in bio-inspired materials can exist.<sup>62</sup> Numerical connections between bulk, micro-, and nanostructures revealed the microscopic effect on mechanical performance. While a crack propagates in locally disordered zones, the crack is pinned and generates stress concentration around that zone. These hurdles to crack propagation are either bunches of platelet unevenness or greater-than-mean platelets concerning most of the platelets. Such microstructural divergencies are, therefore, crucial to inhibiting crack propagation in nacre-like geometries.63,64 There are various computation models to predict fracture behavior, toughening mechanisms, and microstructural change during loadings like the cohesive finite-element method, MD simulation, Monte Carlo simulation, DEM, representative volume element, FEA, and trans-scale shear-lag model.<sup>65–67</sup> The nacre hierarchy was



Figure 7. FESEM images of NS and NC for (a,b) Izod and (c,d) cryogenic fracture.

produced as a 3D brick and mortar model for both sheet and columnar and fractured evolute using the optical microscopic image and SEM to study the surface morphology of fabricated samples, as illustrated in Figure 6. It has been expansively studied that the glassy polymers' failure process largely relies on shear banding or crazing (microscopic) or necking (macroscopic) flow, and it scatters the constrained stress via cavitation, bond rupture, viscoelastic deformation, crack growth, and crazing before catastrophic material failure. The SEM analysis of ruptured PCABS parts has proved their distinctive fracture mechanics, that is, the interlayer raster delamination, multiple crazing, and shear deformation mechanism.<sup>68,69</sup> The FDM-printed nacre design revealed the nonregular contiguity formation between the layers of PCABS samples; however, such structural local imperfection does not relinquish any compromise in the impact resistance compared to the neat PCABS sample. As mentioned above, mollusk structure follows various methodologies for dissipating energy during cracking. Nevertheless, Barthelat illuminated that the "process zone" known as "stress whitening" was exhibited in nacreous architectures during the fracture process. Such an exterior surface fracture is equivalent to crazing in polymeric systems.42,56

Moreover, FESEM micrographs of microstructure observations concerning Izod and cryogenic fracture surfaces are elucidated in Figure 7. Impact fracture of NS and NC articulated architecture is coined as a non-brittle failure phenomenon that exhibits a tearing surface that involves crazing and cavitation phenomena of plastic deformation. Additionally, liquid nitrogen-dipped fracture of NS and NC, evident interlayer crack propagation, and cracked delocalization result in energy dissipation, presumably without interfacial debonding.<sup>42</sup>

PC/ABS composites are known for their excellent mechanical properties, thermal stability, extrudability, and poor biodegradation due to inadequate PC and ABS links. The structural properties of PC/ABS cannot be altered using mechanical or chemical separation, so the utilization of this composite is highly beneficial for structural applications. On the other hand, the decomposition of the PCABS composite was conducted using pyrolysis, where heating in the presence of various catalysts and bromine was generally combined with solid residues or pyrolysis oil. It is essential to utilize feasible methods to decompose PCABS components to obtain dibrominated products without catalysts or additives.<sup>35,70,71</sup> Li and Xu applied a supercritical water oxidation process for environmentally friendly and efficient decomposition where depolymerization, conjugation of free radicals, carbonization, and generation of free radicals could be the mechanism.<sup>72</sup>

## 5. CONCLUSIONS

Nacre has remarkable resistance to impact load due to the distinctive hierarchy created by the two diverse contrasting arrangements: the unidirectional tablet stacking columnar and an angular tablet organized sheet. By controlling the proportions of the intermediate component (soft phase), the augmented resistance of impact, elastic and flexural modulus, and strength of the unique nacre-like compounds could be attained. The aragonite phase is surrounded by biopolymeric materials and entails a brick-and-mortar microarchitecture in a lamellar manner with tremendous energy dissipation during rupture. The biomineralization process of nacre occurs in a bottom-up approach, which can be mimicked using a similar bottom-up fabrication tool, such as FDM, a 3D printing technique. Organic-inorganic bonding, tablet size, interlocking, tablet distribution, volumetric percentage of soft and hard phases, and intra-layer adhesion are crucial to strengthening fracture resistance in an artificial nacre. This study demonstrates a unified approach to identifying and validating numerous analytic and simulation models of NC and NS. We first utilized dimensionless parameters and analytical models to illustrate the stacking of geometry, characteristics of the material, and mechanical response of the nacre-like composites for 3D design. The designed models were fabricated via FDM printing with the PC-ABS filament in a brick-and-mortar manner. We envisioned that the NS structure with the same other parameters, excluding stacking, was superior in impact, tensile, and bending properties. The

mechanical behavior of NS structures showed improvement of 9.37% in impact resistance, 11.23% in elastic modulus, and 10.85% in flexural modulus as compared to NC, while 36, 29, and 37% improvements in impact, elastic modulus, and flexural modulus, respectively, were noticed in contrast to pure geometry. Nacre design structures can be applied as bulk implants, coatings, inflammable films, structural components, or composite components when merged with ceramics and other polymeric materials.

#### ASSOCIATED CONTENT

#### Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acsomega.2c08076.

Brief description of analytical, numerical, and simulation models such as DEM, RVE, and Monte Carlo for determining the fracture, crack propagation, and toughening mechanism of mollusk seashell nacreous hierarchy (PDF)

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## Notes

The authors declare no competing financial interest.

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