

# Synthesis of Hierarchical Layered Quasi-Triangular $\text{Ce}(\text{OH})\text{CO}_3$ and Its Thermal Conversion to Ceria with High Polishing Performance

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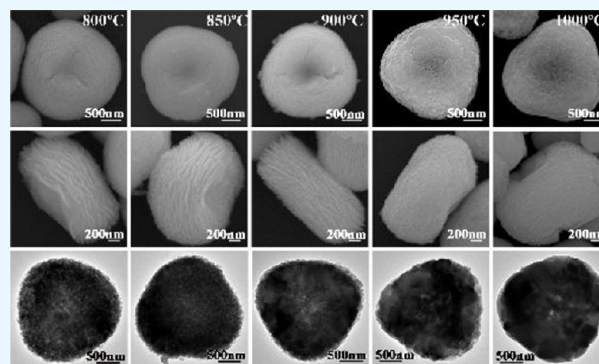


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**ABSTRACT:** Layered quasi-triangular  $\text{Ce}(\text{OH})\text{CO}_3$  assembled from primary nanoparticles was synthesized via a solvothermal method and converted into  $\text{CeO}_2$  abrasive particles by calcination at 800–1000 °C. With the increase of calcination temperature, the primary particle size increased and the microstructure, mechanical hardness, and chemical activity of the  $\text{CeO}_2$  particles changed, thus affecting the polishing performance. The calcined products obtained at 800, 850, and 900 °C maintained the layered edge structure of the  $\text{Ce}(\text{OH})\text{CO}_3$  precursor and had a relatively high specific surface area and surface  $\text{Ce}^{3+}$  concentration. The samples calcined at 950 and 1000 °C lost the layered structure due to the large-scale melting of the primary particles, and their surface chemical activity decreased. The polishing experiments on K9 glass showed that, with the calcination temperature rising from 800 to 1000 °C, the material removal rate (MRR) first increased and then decreased sharply. The initial increase of MRR was attributed to the increase of mechanical hardness of the layered quasi-triangular  $\text{CeO}_2$ , and the subsequent decrease of MRR was related to the decrease in surface chemical activity and disappearance of the layered edge structure. The product calcined at 900 °C had the highest MRR and best surface quality after polishing due to the layered edge structure and optimal match of chemical activity and mechanical hardness.



## 1. INTRODUCTION

The controlled synthesis of rare-earth architectures with different geometries has been of great importance because their optical, electric, magnetic, and catalytic properties are highly dependent on the size and shape of the particles.<sup>1–4</sup> Ceria, one of the promising rare-earth oxide functional materials, is of great interest due to its high mobility of oxygen vacancies, reversible redox transformation between  $\text{Ce}^{4+}$  and  $\text{Ce}^{3+}$ , and applications in catalysis,<sup>5–8</sup> polishing materials,<sup>9–11</sup> and electrolyte materials for solid oxide fuel cells (SOFCs).<sup>12–14</sup> Extensive studies have been carried out with respect to the size and shape control of cubic-fluorite-structured ceria. A number of  $\text{CeO}_2$  architectures with various morphologies have been successfully fabricated, including nanocubes with {100} faces,<sup>15–17</sup> nano-octahedra with {111} surfaces,<sup>18–20</sup> and nanorods with exposed {110} and {100} planes<sup>17,21–23</sup> as well as hierarchical organizations of octahedra,<sup>24,25</sup> spheres,<sup>26–28</sup> flowers,<sup>29–31</sup> and urchin-like structures.<sup>32</sup>

Ceria particles with different sizes/morphologies/structures usually exhibit different application properties. For example,  $\text{CeO}_2$  particles with a hierarchical structure showed enhanced catalytic activity due to their high surface area and unique microstructure. The catalytic activity of hierarchical  $\text{CeO}_2$  octahedra assembled from primary nanoparticles for CO oxidation was higher than that of single-crystal octahedra of

the same size.<sup>24</sup> Flowerlike hierarchical  $\text{CeO}_2$  spheres exhibited much higher catalytic activity than general  $\text{CeO}_2$  particles for the combustion of trichloroethylene.<sup>27</sup>

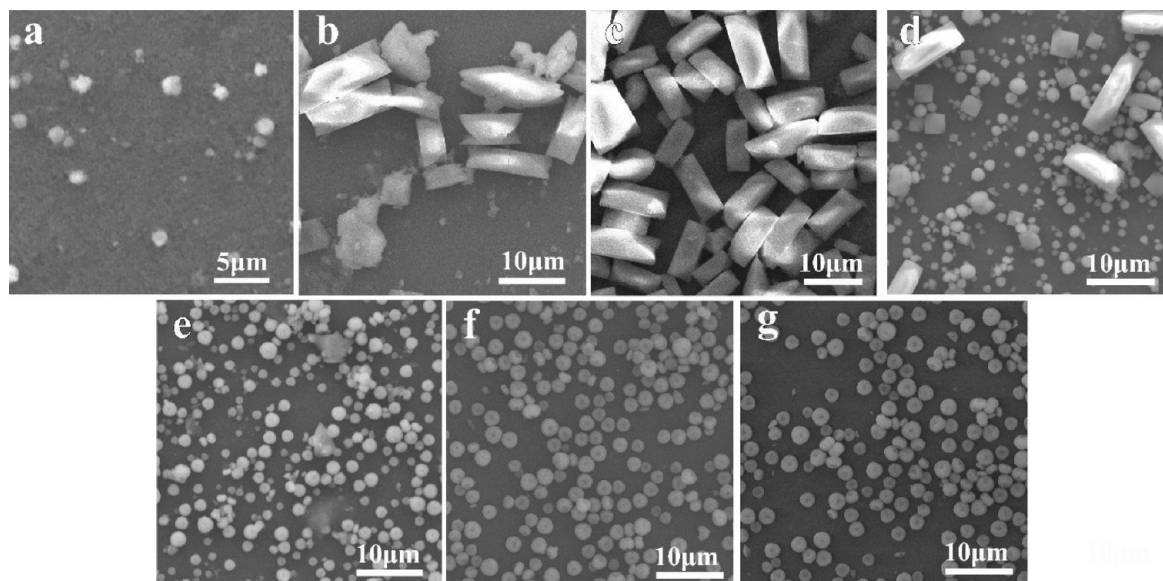
As a polishing material, ceria has also exhibited size-/morphology-/structure-dependent polishing properties. In glass polishing, nanosized ceria particles mainly achieved material removal through a chemical reaction, while micro-sized ceria abrasive underwent both a chemical reaction and mechanical friction.<sup>33</sup>  $\text{CeO}_2$  nanoparticles with a mixed morphology of rods and cubes exhibited a better surface finish and the highest material removal rate (MRR) in glass polishing compared with nanocubes and nanospheres.<sup>34</sup>  $\text{CeO}_2$  nano-octahedra with {111} facets had a higher MRR for single-crystal silicon than nanospheres because the abrasion mechanism of the silicon substrate polished by the nano-octahedra with sharp edges and corners was microploughing wear, while that polished by nanospheres was microscale abrasive wear.<sup>35</sup> Compared with single-crystal hexagonal

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**Figure 1.** SEM images of the samples obtained at 180 °C for solvothermal times of 4 h (a), 8 h (b), 12 h (c), 16 h (d), 20 h (e), 24 h (f), and 36 h (g).

particles, hierarchical nanospheres of CeO<sub>2</sub> exhibited a superior removal rate and scratch suppression ability in chemical–mechanical polishing (CMP) of a SiO<sub>2</sub> wafer due to their physical softness and high chemical activity.<sup>36</sup>

Although the effect of the ceria abrasive morphology on its mechanical and chemical polishing properties has been investigated, the studies were focused on simple-structured particles. Ceria particles with a hierarchical structure are fascinating because their complicated spatial arrangement may give rise to enhanced chemophysical properties and polishing performance. In this paper, a hierarchical layered quasi-triangular Ce(OH)CO<sub>3</sub> precursor was synthesized by a solvothermal reaction and then converted to hierarchical quasi-triangular CeO<sub>2</sub> particles with different microstructures by calcination at different temperatures. The formation mechanism of the precursor and the correlation between the microstructure of hierarchical quasi-triangular CeO<sub>2</sub> and its polishing performance are discussed.

## 2. EXPERIMENTAL SECTION

**2.1. Preparation.** All chemicals were of analytical grade and were used without further purification. The water used in the experiments was deionized (DI) water. Typically, 6.52 g of Ce(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O and 12.0 g of polyvinylpyrrolidone (PVP, K30) were dissolved in 250 mL of ethylene glycol (EG). Then, 50 mL of 0.3 M ammonia aqueous solution was added dropwise into the above mixture with stirring. After further stirring for 30 min, the resulting solution (pH ≈ 7.3) was transferred into a Teflon-lined stainless steel autoclave (capacity 500 mL) and heated at 180 °C for 4, 8, 12, 16, 20, 24, or 36 h. After the autoclave cooled to room temperature, the precipitate was separated by centrifugation, washed with DI water and ethanol, and dried at 50 °C for 12 h. The precursor synthesized with a reaction time of 24 h was put into an alumina crucible and calcined in a muffle furnace under an air atmosphere at various temperatures from 800 to 1000 °C for 3 h at a heating rate of 10 °C/min. After calcining, the samples were cooled to room temperature in the furnace.

**2.2. Characterization.** The composition and phase of the samples were characterized using X-ray powder diffraction (XRD) on a Bruker axS D8 Advance X-ray diffractometer with Cu K $\alpha$  radiation ( $\lambda = 0.15406$  nm). The morphology and crystal structure were examined using scanning electron microscopy (SEM) with a FEI Quanta-200F microscope operated at an acceleration voltage of 20 kV and transmission electron microscopy (TEM) on a JEOL JEM-2100 microscope operated at 200 kV. Thermogravimetric (TG) analysis was performed on a PerkinElmer TGA 4000 instrument to monitor the mass loss of the sample as a function of temperature from room temperature to 800 °C at a heating rate of 10 °C/min under an air atmosphere. The specific surface area of the calcined samples was measured using the BET method (N<sub>2</sub> adsorption) with a Quantachrome Autosorb-iQ gas adsorption analyzer. The surface  $\zeta$  potential measurement of ceria abrasive was performed using an Agilent Zetaprobe 7020 instrument. The surface cerium valence states of the calcined products were detected using X-ray photoelectron spectroscopy (XPS) on a Thermo Scientific Escalab 250Xi with Al K $\alpha$  radiation ( $h\nu = 1486.6$  eV).

**2.3. Polishing Tests.** The slurry was prepared by dispersing ceria abrasive obtained at different calcination temperatures in DI water with stirring and then treated by ultrasound for 15 min. The concentration of ceria abrasive was 5.0 wt %. The pH value of the slurry was about 6.6. CMP tests were performed at K9 optical glass wafers with a diameter of 6.0 cm and a thickness of 2.0 mm with a UNIPOL-802 polishing machine (Shenyang Kejing Co. Ltd.) equipped with a slurry circulation system. The polishing process parameters were set as follows: use of a synthetic leather polishing pad, pad rotation speed 200 rpm, down pressure 6.6 kPa, feed rate of the slurry 2 L/min, polishing temperature 25 ± 2 °C, and polishing time 1 h. After polishing, the wafers were rinsed with absolute ethyl alcohol and DI water and then dried naturally in a superclean room. The material removal rate (MRR) was calculated by  $MRR = (m_0 - m)/\rho tS$ , where  $\rho$  is the density of K9 glass (2.51 g/cm<sup>3</sup>),  $S$  is the area of the wafer,  $t$  is the polishing time,  $m_0$  is the original mass of the wafer, and  $m$  is

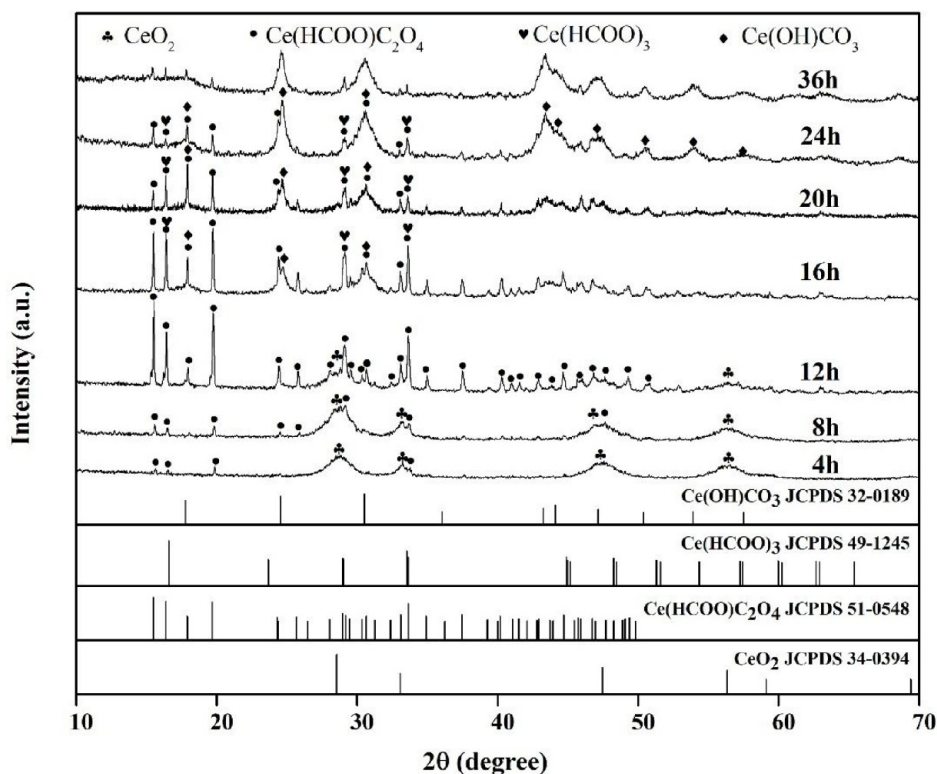


Figure 2. XRD patterns of the samples obtained at 180 °C for solvothermal times of 4, 8, 12, 16, 20, 24, and 36 h.

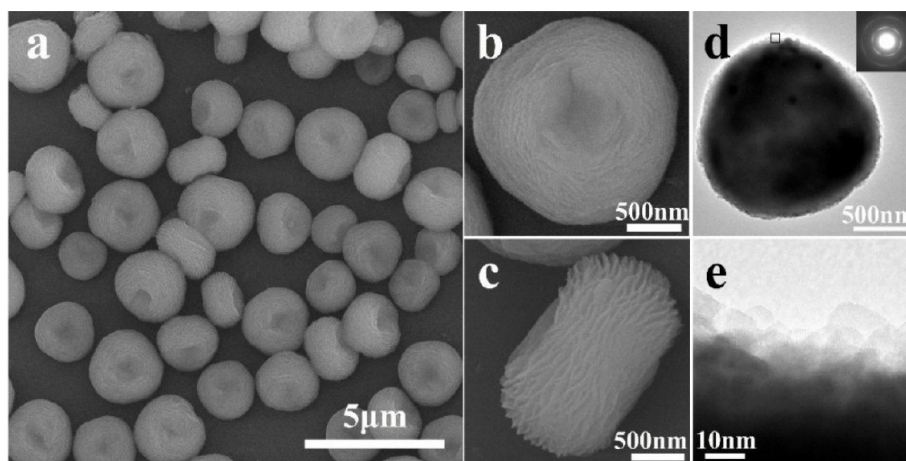


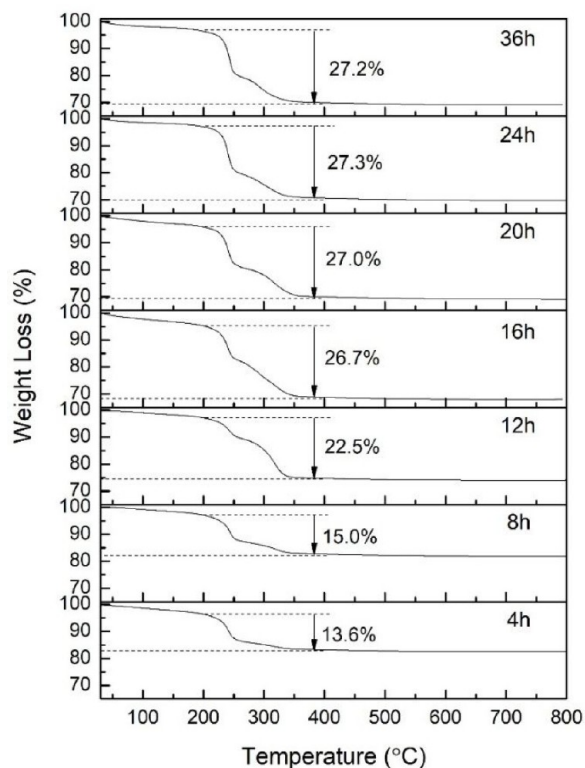
Figure 3. (a–c) High-magnification SEM images of the sample synthesized at 180 °C for a solvothermal time of 24 h, showing its concave layered quasi-triangular structure. (d) TEM image of a single particle and corresponding SAED pattern (inset). (e) HRTEM image recorded from the black-box region marked in d.

the mass of the wafer after polishing. A Sartorius precision electron balance was used to measure the mass of K9 glass (before and after polishing), and all the MRR values were the average of three measurements. The topography of the K9 surface was measured with a SuperView W1 surface profilometer (Chotest Technology Inc.).

### 3. RESULTS AND DISCUSSION

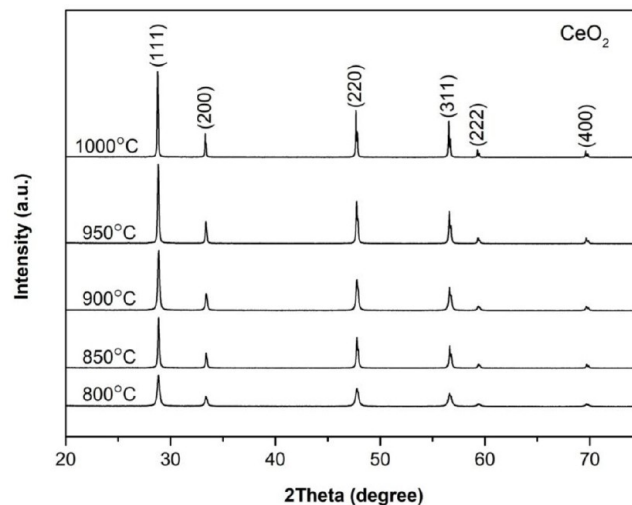
**3.1. Hierarchical Layered Quasi-Triangular Precursor and Its Formation Mechanism.** The solvothermal reaction time has a significant influence on the morphology and phase of the precursors. As shown in Figures 1 and 2, when the reaction time was 4 h, the main product was nanosized small particles accompanied by some large particles. The corre-

sponding XRD pattern showed that the phase composition of the sample was cubic fluorite  $\text{CeO}_2$  (JCPDS 34-0394) along with a trace amount of orthorhombic  $\text{Ce}(\text{HCOO})\text{C}_2\text{O}_4$  (JCPDS 51-0548). As the solvothermal time was extended to 8 h, micrometer-sized rods were formed and they became the main product at the solvothermal time of 12 h. Correspondingly, the intensity of the characteristic diffraction peaks of orthorhombic  $\text{Ce}(\text{HCOO})\text{C}_2\text{O}_4$  increased significantly. The position and intensity of the main diffraction peaks of the sample after a solvothermal reaction for 12 h were in good agreement with the standard data of JCPDS 51-0548, indicating that the rod-shaped particles were the  $\text{Ce}(\text{HCOO})\text{C}_2\text{O}_4$  phase. But there were still two weak diffraction peaks at  $2\theta = 28.5$  and  $56.3^\circ$ , which belong to  $\text{CeO}_2$  phase diffraction.



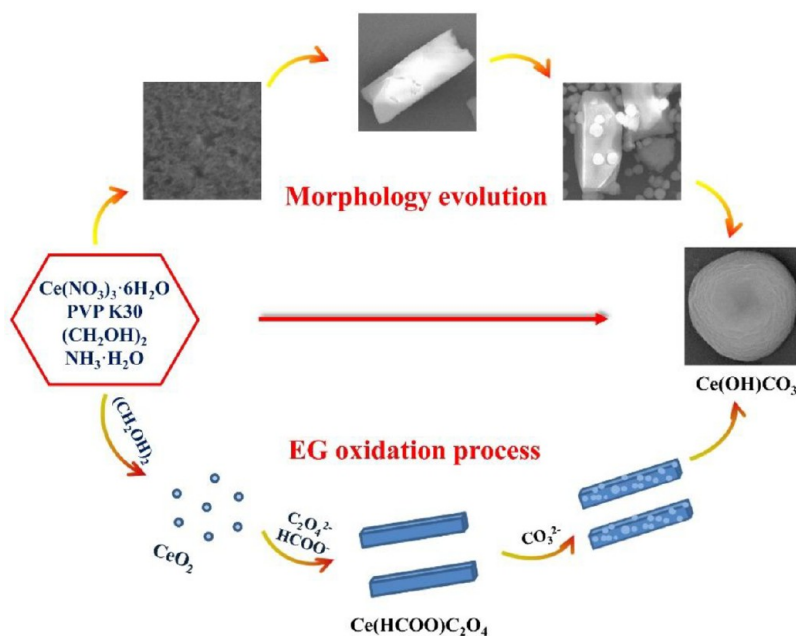
**Figure 4.** TG curves of the samples obtained at 180 °C for solvothermal times of 4, 8, 12, 16, 20, 24, and 36 h.

When the reaction time reached 16 h, quasi-triangular particles emerged in the product. Accordingly, the intensity of diffraction peaks at  $2\theta = 15.5$  and  $19.7^\circ$  ascribed to  $\text{Ce}(\text{HCOO})\text{C}_2\text{O}_4$  decreased. At the same time, the relative intensity of diffraction peaks at  $2\theta = 16.5$ ,  $17.9$ , and  $30.6^\circ$  increased and a new peak appeared at  $2\theta = 24.6^\circ$ . The increase in the relative intensity of the diffraction peak at  $2\theta = 16.5^\circ$  was attributed to the newly formed hexagonal phase of

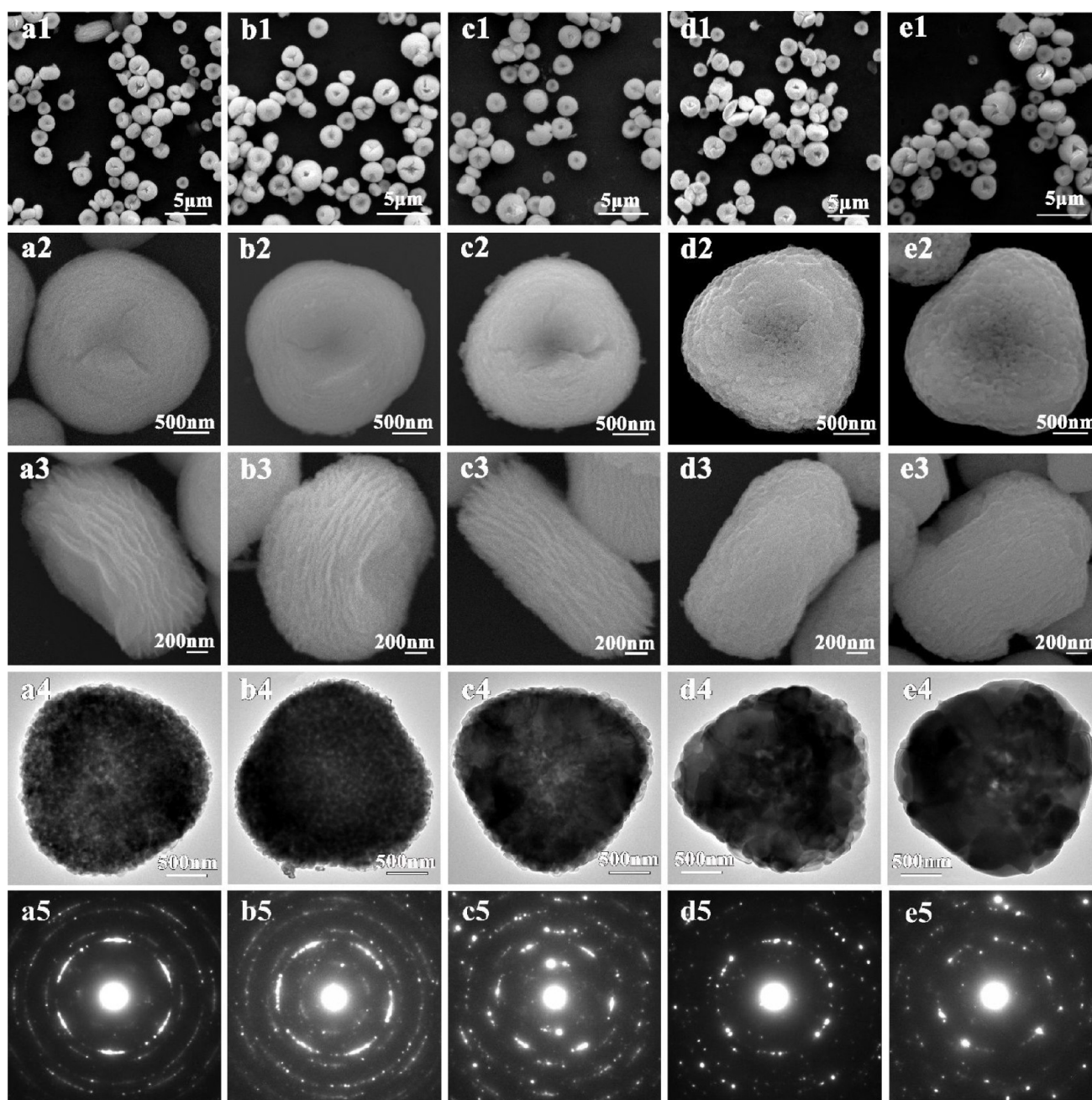


**Figure 6.** XRD patterns of the products obtained by calcining the layered quasi-triangular precursor in air at 800, 850, 900, 950, and 1000 °C for 3 h.

$\text{Ce}(\text{HCOO})_3$  (JCPDS 49-1245), whose characteristic diffraction peaks at  $2\theta = 16.5$ ,  $29.1$ , and  $33.6^\circ$  overlapped with those of the previously formed  $\text{Ce}(\text{HCOO})\text{C}_2\text{O}_4$ . Simultaneously, the newly formed hexagonal phase of  $\text{Ce}(\text{OH})\text{CO}_3$  (JCPDS 32-0189) led to an increment of diffraction peak intensity at  $2\theta = 17.9$  and  $30.6^\circ$  as well as a new peak at  $2\theta = 24.6^\circ$ . No obvious  $\text{CeO}_2$  diffraction peak was observed in the XRD pattern of this sample. After 20 h of solvothermal reaction, quasi-triangular particles were dominant in the product, but there were still a certain number of residual fragments of the previously formed rods. The XRD characterization indicated that the sample was composed of  $\text{Ce}(\text{OH})\text{CO}_3$ ,  $\text{Ce}(\text{HCOO})_3$ , and  $\text{Ce}(\text{HCOO})\text{C}_2\text{O}_4$  phases. Compared with the product reacted for 16 h, the characteristic diffraction peak intensity of  $\text{Ce}(\text{HCOO})\text{C}_2\text{O}_4$  and  $\text{Ce}(\text{HCOO})_3$  decreased while that of  $\text{Ce}(\text{OH})\text{CO}_3$  increased. When the solvothermal time was



**Figure 5.** Schematic illustration of the mechanism responsible for the formation of the hierarchical layered quasi-triangular precursor.



**Figure 7.** SEM images of the products obtained by calcining the layered quasi-triangular precursor in air at 800 (a1), 850 (b1), 900 (c1), 950 (d1), and 1000 °C (e1) for 3 h. High-magnification SEM images of a single particle with different orientations obtained at calcination temperatures of 800 (a2, a3), 850 (b2, b3), 900 (c2, c3), 950 (d2, d3), and 1000 °C (e2, e3). TEM images of a single calcined particle and corresponding SAED patterns: (a4, a5) 800 °C; (b4, b5) 850 °C; (c4, c5) 900 °C; (d4, d5) 950 °C; (e4, e5) 1000 °C.

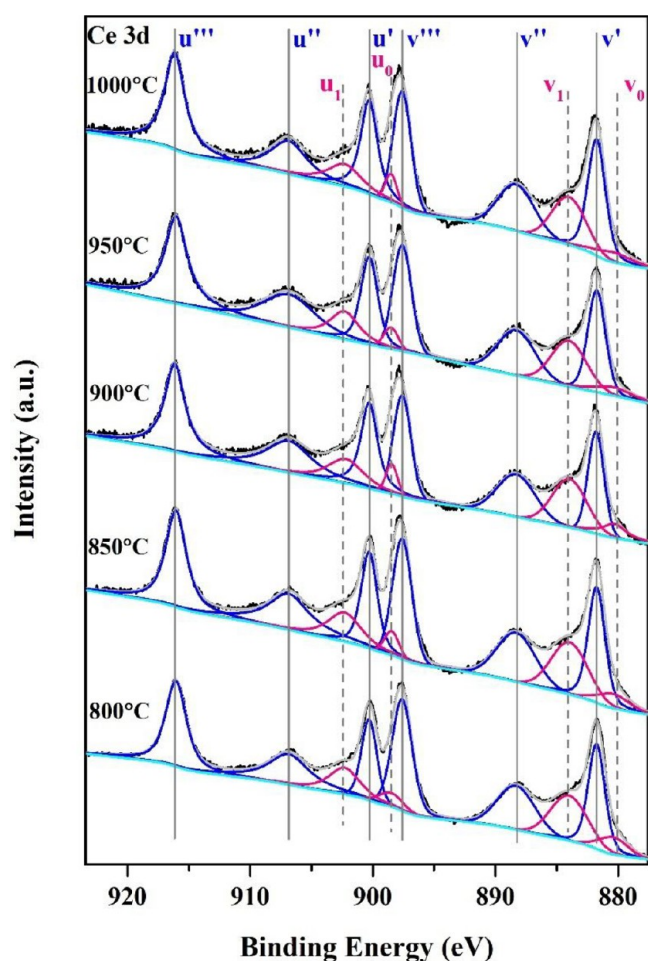
**Table 1. Specific Surface Area,  $\zeta$  Potential, and Surface  $\text{Ce}^{3+}$  Concentration of the Calcined Products**

calcination temp (°C)	specific surface area ( $\text{m}^2/\text{g}$ )	$\zeta$ potential (mV)	surface $\text{Ce}^{3+}$ concn (%)
800	13.30	36.7	23.65
850	10.55	38.0	23.17
900	10.45	39.4	23.67
950	6.93	34.2	21.60
1000	4.07	15.3	21.49

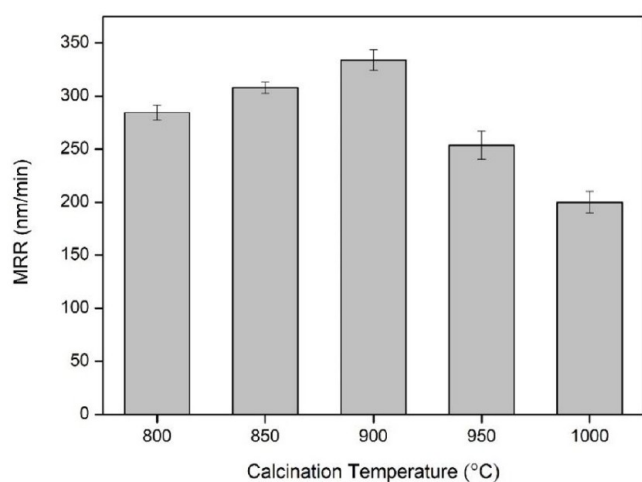
extended to 24 h, quasi-triangular particles with a uniform size became the main product and further extension of the reaction time to 36 h had little effect on the morphology of the product.

An XRD analysis demonstrated that the samples reacted for 24 and 36 h were mainly the  $\text{Ce}(\text{OH})\text{CO}_3$  phase with a small amount of  $\text{Ce}(\text{HCOO})\text{C}_2\text{O}_4$  and  $\text{Ce}(\text{HCOO})_3$  phases.

High-magnification SEM images of the quasi-triangular particles synthesized at 180 °C for a solvothermal time of 24 h revealed that they had a concave center and layered edges (Figure 3a–c). The particle size ranged from 1.2 to 2.8  $\mu\text{m}$ . The structure was further studied using TEM, selected area electron diffraction (SAED), and high-resolution TEM (HRTEM). As shown in Figure 3d,e, the concave layered quasi-triangular particle possessed a hierarchical structure which was formed through the aggregation of small primary nanoparticles. SAED showed a symmetrical arc-like pattern,



**Figure 8.** Ce 3d XPS spectra for the products calcined at different temperatures.

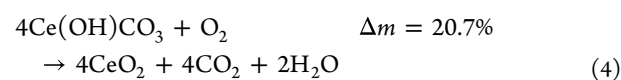
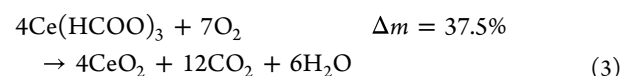
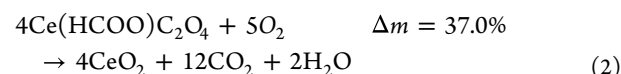
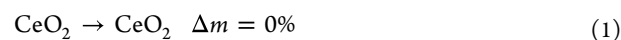


**Figure 9.** MRR of K9 glass by the products calcined at different temperatures.

indicating that the primary nanoparticles were aggregated with large-angle misorientation.<sup>37,38</sup>

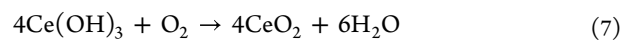
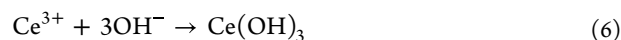
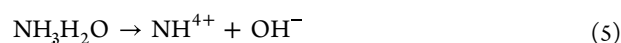
The thermal behavior of the samples for different solvothermal reaction time was investigated with TG. As shown in Figure 4, the weight loss before 200 °C was attributed to the removal of free water or adsorbed water, while the significant weight loss from 200 to 400 °C was attributed

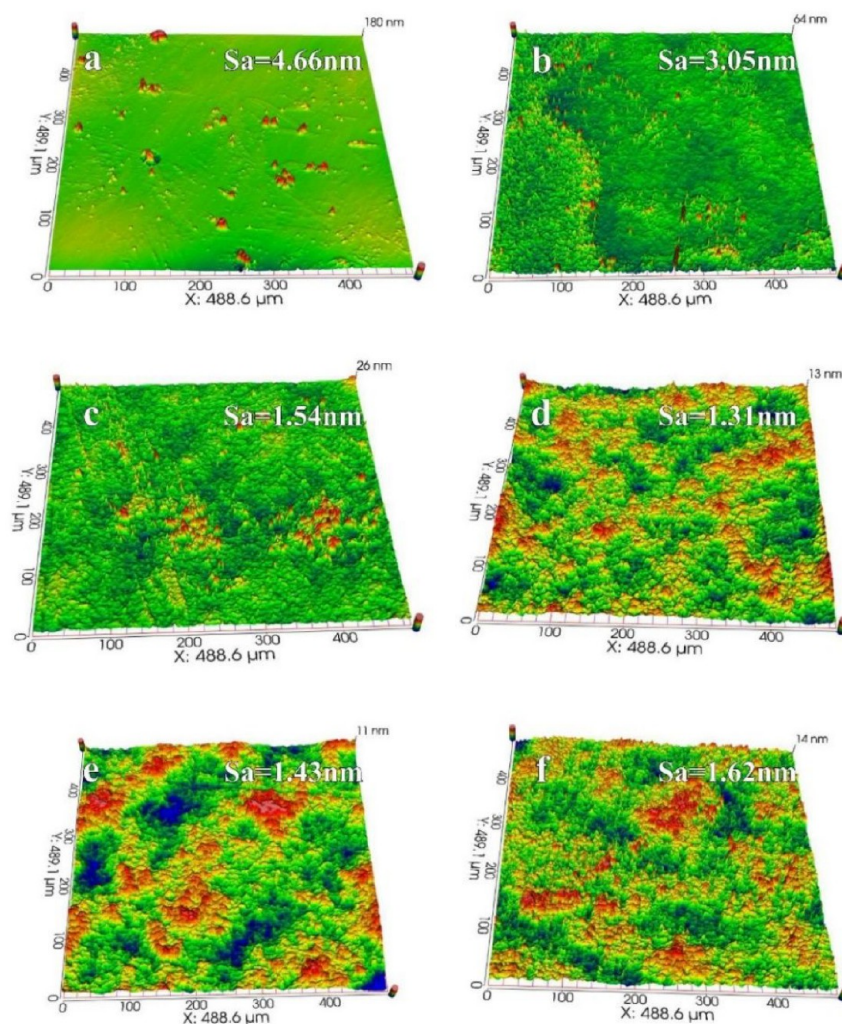
to the decomposition of the mixed-phase cerium compound samples.<sup>39,40</sup> The total weight loss between 200 and 400 °C first increased and then remained basically unchanged with an extension of the reaction time, corresponding to the transformation of the dominant phase of the product from CeO<sub>2</sub> to Ce(HCOO)C<sub>2</sub>O<sub>4</sub>, Ce(HCOO)<sub>3</sub>, and Ce(OH)CO<sub>3</sub>. The theoretical weight loss values of CeO<sub>2</sub>, Ce(HCOO)C<sub>2</sub>O<sub>4</sub>, Ce(HCOO)<sub>3</sub> and Ce(OH)CO<sub>3</sub> can be calculated from the following reactions:<sup>41</sup>



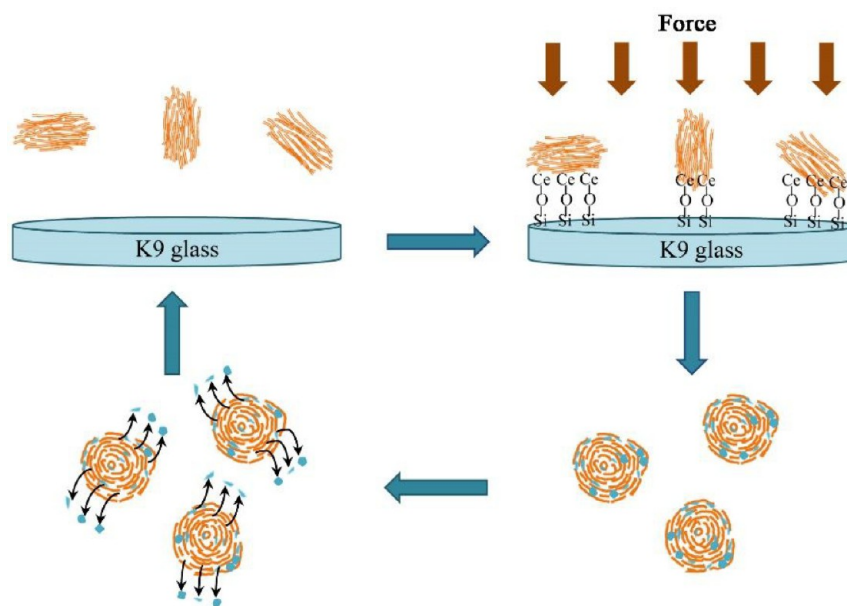
During the solvothermal reaction time of 4–12 h, with the increase of the Ce(HCOO)C<sub>2</sub>O<sub>4</sub> phase and the decrease of the CeO<sub>2</sub> phase in the product, the total weight loss between 200 and 400 °C increased from ~13.6% to ~22.5%. A mixed-phase product of Ce(HCOO)C<sub>2</sub>O<sub>4</sub>, Ce(HCOO)<sub>3</sub>, and Ce(OH)CO<sub>3</sub> with a total weight loss of ~26.7% was obtained at a reaction time of 16 h. As the reaction time was extended from 16 to 24 h, the Ce(OH)CO<sub>3</sub> phase in the mixed-phase product increased, which should lead to a decrease in total weight loss, since Ce(OH)CO<sub>3</sub> has a lower theoretical weight loss value compared to Ce(HCOO)C<sub>2</sub>O<sub>4</sub> and Ce(HCOO)<sub>3</sub>. However, the weight loss of the sample reacted for 24 h was slightly greater than that of the sample reacted for 16 h. This may be due to the conversion of CeO<sub>2</sub> to Ce(HCOO)C<sub>2</sub>O<sub>4</sub> or Ce(HCOO)<sub>3</sub> during the solvothermal time of 16–24 h, although no obvious CeO<sub>2</sub> phase was observed in the XRD pattern of these samples. When the reaction time increased from 24 to 36 h, the composition of the product remained basically unchanged, that is, a mixed-phase product dominated by the Ce(OH)CO<sub>3</sub> phase; thus, the total weight loss changed little.

The possible mechanism for the formation of the hierarchical layered quasi-triangular precursor is presented in Figure 5. The initial feeding included Ce(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O, PVP K30, EG, and ammonia aqueous solution, and the pH value of this mixed solution was ~7.3. With an increase in the solvothermal time, the morphology of the product evolved from fine nanoparticles to micrometer-sized rods and finally to the layered quasi-triangular structure and the corresponding main phase changed from CeO<sub>2</sub> to Ce(HCOO)C<sub>2</sub>O<sub>4</sub> and finally to Ce(OH)CO<sub>3</sub>. The evolution of the product morphology and the main phase was related to the oxidation process of the solvent EG. The chemical reactions involved were as follows:<sup>42–44</sup>

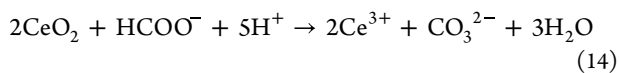
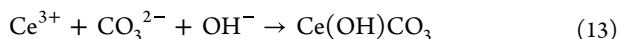
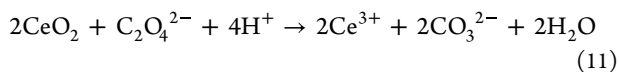
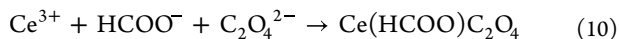
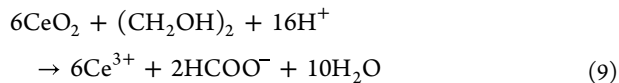
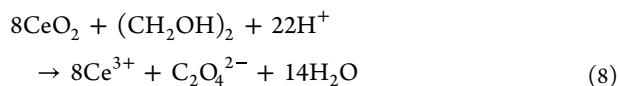




**Figure 10.** Surface topography of K9 glass before (a) and after polishing using the products calcined at 800 (b), 850 (c), 900 (d), 950 (e), and 1000 °C (f) as abrasive particles.



**Figure 11.** Schematics illustrating the polishing mechanism of the hierarchical layered quasi-triangular  $\text{CeO}_2$ .



In the initial stage of solvothermal treatment, the main reaction was the oxidation of  $\text{Ce}^{3+}$  in the presence of  $\text{OH}^-$  to form  $\text{CeO}_2$ , as illustrated in reactions 5–7. Due to the insufficient amount of ammonia as precipitant (the molar ratio of  $\text{Ce}^{3+}$  to ammonia is 1:1 at the initial feeding), there was still a large amount of free  $\text{Ce}^{3+}$  in the reaction system. Under the solvothermal conditions of high temperature and high pressure,  $\text{CeO}_2$  generated in reaction 7 oxidized the solvent EG to  $\text{C}_2\text{O}_4^{2-}$  and  $\text{HCOO}^-$ , while itself was reduced to  $\text{Ce}^{3+}$ , as shown in reactions 8 and 9. The resulting  $\text{C}_2\text{O}_4^{2-}$  and  $\text{HCOO}^-$  ions then underwent precipitation (reaction 10) to form  $\text{Ce}(\text{HCOO})\text{C}_2\text{O}_4$ . The continuous progress of reactions 6–10 made  $\text{Ce}(\text{HCOO})\text{C}_2\text{O}_4$  the main phase of the product reacted for 12 h. With an extension of the solvothermal time,  $\text{CeO}_2$  generated in reaction 7 further oxidized  $\text{C}_2\text{O}_4^{2-}$  to  $\text{CO}_3^{2-}$ , as shown in reaction 11. The oxidation of  $\text{C}_2\text{O}_4^{2-}$  resulted in the dissolution of  $\text{Ce}(\text{HCOO})\text{C}_2\text{O}_4$ , and the released  $\text{HCOO}^-$  ions combined with  $\text{Ce}^{3+}$  to produce  $\text{Ce}(\text{HCOO})_3$ , as illustrated in reaction 12. Meanwhile,  $\text{CO}_3^{2-}$  ions, the oxidation product of  $\text{C}_2\text{O}_4^{2-}$ , reacted with  $\text{Ce}^{3+}$  and  $\text{OH}^-$  to form  $\text{Ce}(\text{OH})\text{CO}_3$ , as shown in reaction 13. Thus, a mixed-phase product of  $\text{Ce}(\text{HCOO})\text{C}_2\text{O}_4$ ,  $\text{Ce}(\text{HCOO})_3$ , and  $\text{Ce}(\text{OH})\text{CO}_3$  was obtained at a reaction time of 16 h. Further prolongation of solvothermal time also led to the oxidation of  $\text{HCOO}^-$  to  $\text{CO}_3^{2-}$  by  $\text{CeO}_2$ , as illustrated in reaction 14. The continuation of reactions 6, 7, 11, 14, and 13 made  $\text{Ce}(\text{OH})\text{CO}_3$  the dominant phase of the sample after 24 h of reaction. Owing to the continuous consumption of  $\text{OH}^-$  in reaction 13 to generate  $\text{Ce}(\text{OH})\text{CO}_3$ , the acidity of the reaction system increased, which hindered the formation of  $\text{CeO}_2$  in reactions 6 and 7. Therefore, the conversion of  $\text{Ce}(\text{HCOO})\text{C}_2\text{O}_4$  and  $\text{Ce}(\text{HCOO})_3$  to  $\text{Ce}(\text{OH})\text{CO}_3$  was incomplete, and the product reacted for 36 h was still a mixture with  $\text{Ce}(\text{OH})\text{CO}_3$  as the main phase. A decrease in pH of the reaction system was observed with prolonged reaction time, and the pH value of the supernatant after 24 h of reaction was  $\sim 4.6$ . At this time,  $\text{Ce}^{3+}$  in the reaction system was basically precipitated completely. Calculated according to the weight of  $\text{CeO}_2$  obtained by calcining the hierarchical layered quasi-triangular precursor, the yield was over 95%.

**3.2. Hierarchical Quasi-Triangular  $\text{CeO}_2$  and the CMP Performance.** The hierarchical layered quasi-triangular precursor with a reaction time of 24 h was then calcinated at

800–1000 °C to obtain the ceria abrasives. The XRD patterns of the calcined products are displayed in Figure 6. All of the diffraction peaks were in good agreement with JCPDS No. 34-0394, which was cubic-fluorite-structured  $\text{CeO}_2$  with the lattice constant  $a = 5.41 \text{ \AA}$ . The diffraction peaks became higher and sharper with the increment of calcination temperature, indicating an improvement in crystallinity and an increase in the grain size.

The morphology and structure of the calcined products were characterized by SEM and TEM. As shown in Figure 7a1–e1, the samples calcined at different temperatures maintained a concave quasi-triangular shape. High-magnification SEM images of a single particle with different orientations showed that the samples calcined at temperatures of 800, 850, and 900 °C had layered edges similar to those of the precursor (Figure 7a2–c2, a3–c3), while for the products obtained at calcination temperatures of 950 and 1000 °C, the layered structure disappeared and the melting of the particle surface could be observed (Figure 7d2, e2, d3, e3). Further TEM characterization revealed the microstructure of the calcined products. As shown in Figure 7a4–e4, the calcined products were aggregated from primary particles. The size of the primary particles increased with the increase in calcination temperature, and the melting zone could be clearly seen for the samples calcined at 950 and 1000 °C (Figure S1). The corresponding SAED patterns are displayed in Figure 7a5–e5. The samples calcined at 800 and 850 °C showed symmetrical arc-like diffraction spots. The elongation of diffraction spots indicated that the products were aggregated from many primary particles with large-angle orientation deviations.<sup>37,38</sup> For the samples calcined at 900, 950, and 1000 °C, the arc-like diffraction spots gradually disappeared and individual circular diffraction spots appeared, corresponding to the melting-induced increase in primary particle size as well as a large-scale melting zone in the samples.

Table 1 shows the specific surface area,  $\zeta$  potential, and surface  $\text{Ce}^{3+}$  concentration of the calcined products. As the calcination temperature increased from 800 to 900 °C, the specific surface area gradually decreased from 13.30 to 10.45  $\text{m}^2/\text{g}$ , corresponding to the increase in primary particle size caused by the increase in calcination temperature. A further increase of calcination temperature to 950 and 1000 °C resulted in a large melting zone and disappearance of the layered structure; thus, the specific surface area dropped sharply to 6.93 and 4.07  $\text{m}^2/\text{g}$ . The products obtained at calcination temperatures of 800–950 °C possessed  $\zeta$  potential values of more than 30 mV, suggesting their good dispersion stability,<sup>45,46</sup> while for the product calcined at 1000 °C, its  $\zeta$  potential value was 15.3 mV and the dispersion stability was poor. This may be related to the fact that the particles calcined at 1000 °C are denser due to large-area melting and the disappearance of layered edges; thus, the gravity effect is greater than that of the samples calcined at 800–950 °C. The surface  $\text{Ce}^{3+}$  concentration of the calcined products was determined from the Ce 3d XPS spectra. As shown in Figure 8, the peaks between 876.8 and 923.3 eV could be deconvoluted into ten bands, which can be divided into two multiplets, labeled as v and u, corresponding to the spin-orbit coupling of  $3d_{5/2}$  and  $3d_{3/2}$ .<sup>47–49</sup> The bands denoted as v' (u'), v'' (u''), and v''' (u''') can be assigned to the photoemissions from different final states of the  $3d^{10}4f^0$  of  $\text{Ce}^{4+}$  ions. Meanwhile, the signals  $v_0$  ( $u_0$ ) and  $v_1$  ( $u_1$ ) are ascribed to photoemissions from different final states of  $3d^{10}4f^1$  of  $\text{Ce}^{3+}$  ions. The concentration of  $\text{Ce}^{3+}$  ions in the calcined products



was calculated by dividing the area corresponding to  $\text{Ce}^{3+}$  by the total integrated area of Ce 3d (Table S1). As shown in Table 1, the surface  $\text{Ce}^{3+}$  concentrations of the products calcined at 800–1000 °C were 23.65, 23.17, 23.67, 21.60, and 21.49%, respectively. The products calcined at 800, 850, and 900 °C had a higher concentration of  $\text{Ce}^{3+}$  ions than those calcined at 900 and 1000 °C, indicating their higher surface chemical activity.<sup>50–53</sup> Studies on the mechanism of polishing of glass and  $\text{SiO}_2$  by  $\text{CeO}_2$  particles have proved that ceria not only relies on mechanical friction but also reacts with the workpiece surface to achieve material removal.<sup>54–56</sup> In an aqueous medium, ceria and glass react with water molecules and form Ce–OH and Si–OH on the surface. During CMP, the OH groups on the ceria surface form strong Ce–O–Si bonds with Si–OH groups on the glass surface. The Ce–O–Si bonds are much stronger than Si–O–Si bonds, leading to the removal of  $\text{SiO}_2$ .<sup>57,58</sup>  $\text{Ce}^{3+}$  sites help the formation of Ce–OH groups at the  $\text{CeO}_2$  surface through  $\text{H}_2\text{O}$  dissociation and facilitate the breaking up of Si–O bonds during polishing.<sup>54–56,59,60</sup> From the perspective of the chemical effect of CMP, the surface  $\text{Ce}^{3+}$  concentration of the products calcined at 800–900 °C is high and they should have better polishing performance.

The CMP behavior of the calcined products on K9 glass was tested. As shown in Figure 9, with the calcination temperature increasing from 800 to 1000 °C, the MRR increased first and then decreased sharply, which reflected the chemical and mechanical effects as well as microstructure factors in CMP. The samples calcined at 800–900 °C maintained the layered structure of the precursor and had similar surface  $\text{Ce}^{3+}$  concentrations. Therefore, the initial increase of MRR was attributed to the increase in mechanical hardness of the hierarchical layered quasi-triangular  $\text{CeO}_2$  particles with an increment of calcination temperature. The products calcined at 900 °C had the highest MRR (about 333.9 nm  $\text{min}^{-1}$ ). The subsequent sharp drop in MRR was ascribed to the decrease in the surface chemical activity as well as the disappearance of layered edges. The quasi-triangular  $\text{CeO}_2$  abrasive with a layered structure has a larger specific surface area, which can provide more contact sites for a chemical reaction and mechanical friction during CMP. Moreover, the removed substances can be entrained in the layered structure and leave the workpiece surface along with the particles. Compared with the sample calcined at 950 °C, the MRR of the product calcined at 1000 °C was further reduced to about 200.0 nm  $\text{min}^{-1}$  due to its poor dispersion stability.

Figure 10 shows the surface topography of K9 glass before and after polishing with the calcined products. The roughness was measured for each sample in a 488.6  $\mu\text{m} \times 489.1 \mu\text{m}$  region. The surface roughnesses ( $S_a$ ) of K9 glass after CMP with quasi-triangular  $\text{CeO}_2$  abrasives calcined at 800, 850, 900, 950, and 1000 °C were  $3.05 \pm 0.13$ ,  $1.54 \pm 0.09$ ,  $1.31 \pm 0.06$ ,  $1.43 \pm 0.07$  and  $1.62 \pm 0.08$  nm, respectively. The sample calcined at 900 °C exhibited the best surface quality after polishing. Compared with the products calcined at 850–1000 °C, the roughness of K9 glass polished by the product calcined at 800 °C was higher, which was related to the insufficient hardness of particles calcined at 800 °C. SEM characterization showed that the abrasive particles calcined at 800 °C were partially broken after polishing, while the samples calcined at 850–1000 °C had no obvious morphology change after polishing (Figure S2). For the sample calcined at 800 °C, the fragments generated in CMP caused surface damage, resulting

in high surface roughness. The product calcined at 900 °C had a layered structure, and its chemical activity and mechanical hardness were matched the best; thus, it had the best polishing performance for K9.

The polishing mechanism of the hierarchical layered quasi-triangular  $\text{CeO}_2$  is shown in Figure 11. The abrasive particles approach the workpiece surface and chemically and mechanically interact with the K9 surface under pressure. The substances removed from the workpiece surface are entrained in the layered structure of quasi-triangular  $\text{CeO}_2$  and leave the K9 surface along with the particles. The abrasive particles shake off the substances entrained in the layer, exposing a fresh surface. The fresh particles approach the K9 surface, and the above process is repeated.

## 4. CONCLUSIONS

Layered quasi-triangular  $\text{Ce}(\text{OH})\text{CO}_3$  assembled from primary nanoparticles was synthesized by a solvothermal method, and its formation mechanism was related to the continuous oxidation of EG by  $\text{CeO}_2$  generated in the reaction system at high temperature and high pressure. The as-prepared  $\text{Ce}(\text{OH})\text{CO}_3$  was transformed to  $\text{CeO}_2$  abrasives by calcination at 800–1000 °C. The microstructure, mechanical hardness, and chemical activity of the obtained  $\text{CeO}_2$  abrasives changed with the calcination temperature, thus affecting the polishing performance. With an increase in calcination temperature, the size of the primary particles increased. The products calcined at 800–900 °C kept the layered edge structure of  $\text{Ce}(\text{OH})\text{CO}_3$  precursor, while the layered edges disappeared in the samples calcined at 950 and 1000 °C due to the large-scale melting of primary particles. The polishing tests on K9 glass showed that, in the calcination temperature range of 800–900 °C, the increase in hardness of the hierarchical layered quasi-triangular  $\text{CeO}_2$  resulted in an increase in MRR. The decrease in surface chemical activity of quasi-triangular  $\text{CeO}_2$  and disappearance of layered edges led to a sharp decrease of MRR in the calcination temperature range of 950–1000 °C. The product calcined at 900 °C maintained a layered edge structure, and its chemical activity and mechanical hardness were optimally matched and thus had the highest MRR for K9 glass and best surface quality after polishing.

## ■ ASSOCIATED CONTENT

### Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/acsomega.2c07682>.

HRTEM images of the calcined products, peak areas of individual peaks of Ce 3d for calcined products, and SEM images of the calcined products after polishing (PDF)

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## Author Contributions

The manuscript was written through contributions of all authors. All authors have given approval to the final version of the manuscript.

## Notes

The authors declare no competing financial interest.

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