Research Article

Removal Dynamics of Nitric Oxide (NO) Pollutant Gas by Pulse-Discharged Plasma Technique

Lianshui Zhang, Xiaojun Wang, Weidong Lai, Xueliang Cheng, and Kuifang Zhao

College of Physics Science and Technology, Hebei University, Baoding, Hebei Province 071002, China

Correspondence should be addressed to Xiaojun Wang; xiaojunwang1978@163.com

Received 4 November 2013; Accepted 18 January 2014; Published 5 March 2014

Academic Editors: A. Hursthouse and G. Sen

Copyright © 2014 Lianshui Zhang et al. This is an open access article distributed under the Creative Commons Attribution License, which permits unrestricted use, distribution, and reproduction in any medium, provided the original work is properly cited.

Nonthermal plasma technique has drawn extensive attentions for removal of air pollutants such as NO_x and SO_2 . The NO removal mechanism in pulse discharged plasma is discussed in this paper. Emission spectra diagnosis indicates that the higher the discharge voltage is, the more the NO are removed and transformed into O, N, N₂, NO₂, and so forth. Plasma electron temperature T_e is ranged from 6400 K at 2.4 kV discharge voltage to 9500 K at 4.8 kV. After establishing a zero-dimensional chemical reaction kinetic model, the major reaction paths are clarified as the electron collision dissociation of NO into N and O during discharge and followed by single substitution of N on NO to form N₂ during and after discharge, compared with the small fraction of NO₂ formed by oxidizing NO. The reaction directions can be adjusted by N₂ additive, and the optimal N₂/NO mixing ratio is 2:1. Such a ratio not only compensates the disadvantage of electron competitive consumption by the mixed N₂, but also heightens the total NO removal extent through accelerating the NO oxidization process.

1. Introduction

Nitrogen Oxides (NO_x) , usually emitted through exhaust gas, have assumed the major responsibility with sulfur dioxide (SO_2) for acid rain formation, which is harmful to human health and to the environment through acid deposition [1-3]. High-efficient NO_x remediation or removal technologies has drawn extensive attentions for environmental protection from the viewpoint of fuel corporations, thermal power plants, explosive motor designers, and so on [4-7]. Catalysis reduction [8-11] or direct thermal decomposition [12, 13] approaches have been applied, but the reaction temperatures are usually high [14], which cannot directly be used for removing the 100-200°C diesel or power plant exhaust gas. One candidate way without high temperature control is the nonthermal plasma method at atmospheric pressure [15–17]. Such technique is typically consisting of an array of discharge filaments lasting for tens to hundreds of nanoseconds, in which high energy electrons are initiated by the high voltage and flowed into the exhaust gas. Electron collision can decompose the NO_x into other chemical species as atoms, ions, and molecules, restricted by the law of conservation of matter and the overall charge roughly of zero. Complicated

physical-chemical reactions have occurred between the electrons, by-products, and the pollutant NO_x [18, 19].

Various kinds of NO removal discharge techniques have been developed to date. One key factor that affects the removal efficiency is the appropriate gas components and discharge parameters. Leipold et al. plasma-treated exhaust gas by atmospheric pressure DBD (dielectric barrier discharges) and find that the N atoms have efficiently participated in the reaction of deoxidizing NO to N₂ and O [27]. Wang et al. regard the hydroxyl (OH), decomposed from H₂O, as the active radical to increase the oxidation efficiency of NO in $NO/O_2/N_2/C_2H_4$ system. When too more vapor is mixed, the quenching effect on NO removal appears through the consumption on other active species by H₂O [28]. Tsai et al. find that the elevated discharge power or decreased O_2 concentration can improve the NO removal efficiency for the NO/N₂/O₂ (2%)/H₂O (10%) mixtures [29]. To monitor the de-NO_x process, optical emission spectroscopy [30, 31] or laser induced fluorescence (LIF) [32] has been applied for contactless diagnosis of the radicals and by-products in plasma.

Another factor is the design of plasma reactor structure for improving energy consumption efficiency. Plasma



FIGURE 1: Schematic diagram of the pulse-discharged system for NO removal.

generated by radio-frequency (RF) electric field is reported to resonantly accumulate electromagnetic energy at low-voltage power supply, with NO efficiently oxidized to form NO₂ in the plasma at atmospheric pressure [33]. Multirod DBD reactor is introduced for NO removal based on both dielectric barrier discharges and sliding discharges, and higher NO removal rate is yielded by pulse discharge in comparison with AC discharge at same energy density [34]. The influence of surface plasma reactions on NO_x removal has been recognized; surface- and volume-plasma are compared [35]. In order to remove NO from exhaust gas, investigations are also focused on the conversion of NO into NO₂, which can be conveniently removed by chemical scrubbers such as sodium sulfite (Na₂SO₃) solution [36].

In order to further promote the NO_x removal, plasma technique can be combined with catalysts. Combined adsorption-discharge plasma technique has been proposed, as NO_x firstly adsorbed on H-ZSM-5c substrate and then reduced by CH₄ or NH₃ in plasma [37, 38]. Takahara et al. report that Pt catalyst can assist the discharged NO removal process with high activity under a humidified condition, in which N₂O formed as intermediate species for promoting N₂ formation [39]. Pulsed corona combined with CaOH₂ absorption technique presents that SO₂ and NO in the gas are oxidized into SO₃ and NO₂ by plasma and then absorbed by the CaOH₂ [40]. Such combined processes have the advantages of operating in a wide range of temperatures.

Most of the researches pay attentions to the topic about how to achieve higher NO_x removal efficiency with lower energy cost for practical demand. But the practicability has been restricted by the poor comprehensions of dynamic mechanism of NO removal due to the complicated reactions in plasma. Accurate measurements of the nitrogen oxides and other by-products under different conditions are usually difficult. It is necessary to clarify the NO removal process in order to optimize the operating conditions such as the applied voltage and the additive gas.

In this paper, the pulse discharged plasma for NO remediation has been experimentally achieved and theoretically simulated. Emission spectra are diagnosed to discriminate the category of by-products and supervise the NO removal process. The relationship between discharge voltage and plasma electron temperatures T_e is discussed to evaluate the chemical activity of NO removal reactions from macroscopic viewpoint. Since the microcosmic dynamic process is difficult to be experimentally obtained, a chemical kinetic model is developed in this paper. Generating and losing reactions of different main species in the plasma have been analyzed. The effects of pulse discharge duration width and additive gas on NO removal efficiency are focused on. It finds that pulse-discharged plasma technique assisted with N₂ additive can efficiently remove the gas pollutant of NO and has the potential utilization in power plants, automobiles, and so on.

2. Experimental Methods

The experimental instrument is schematically present in Figure 1. Two tungsten pointing electrodes of 1 mm in diameter are oppositely placed to act as discharge system, with the separation distance of 3 mm. The two electrodes are powered by high voltage pulse source, which can be adjusted in the range from 1 to 15 kV. The pulse duration is 24.5 ns, with discharge frequency of 50 Hz. Discharge process between the electrodes is operated in a glass reactor with diameter of 25 mm and volumetric capacity of 40 mL. Gases with purity of 99.99% are delivered into the discharge zone after flowing through the connected pipes. The air pressure in the reactor is manipulated by vacuum pump and gas flowmeter and controlled at 0.2 atm.

Emission spectra are collected through a quartz window, with diameter of 18 mm on the glass reactor wall corresponding to the discharge zone. The spectra are then detected by OMA (Optical Multichannel Analyzer, ACTON, SP-2300) with the spectra detecting resolution of 0.1 nm.

3. Results and Discussion

There are two critical factors in practical application for discharge removing pollutant gas: (1) electrical energy consumption and (2) by-product identification. Here, the former is evaluated as plasma electron temperature T_e based on *Boltzmann* distribution theory; the latter is obtained based on the emission spectra diagnostic technique.

3.1. Emission Spectra Diagnostics of NO. The NO emission spectra have been detected and shown in Figure 2(a). A notable sequence of UV radiation has been produced, which



FIGURE 2: (a) Emission spectra detected from the pulse discharged instrument; (b) *Lorentz* fitting for the emission spectra of O atoms at 777.0 nm.

belongs to NO and new species of N_2 molecules as well as N_2^+ ion. From 493 nm, spectra of another new species NO_2 appear. In the wavelength range from 656 nm to 867 nm, the atom or ion species of N, O, N⁺ have played the essential roles. The atom spectra of N and O have only instrument broadening and can be well fitted by *Lorentz* function, which has been shown in Figure 2(b) with O atom at 777.0 nm as an example.

Apart from those lines of the NO, the most important feature of the emission diagnostics is that new species of N, N_2 , N^+ , N_2^+ , and O as well as NO_2 appeared. O_2 molecules are also formed, though no distinct emission lines detected, due to its very low transition probability for radiation. It implies that some extent of NO has been transformed into new species, including harmless species such as N, O, N_2 , O_2 , N^+ , and N_2^+ , or can be further removed by other methods such as NO_2 .

The emission spectra and their transition channels are evaluated [41] and outlined in Table 1.

Based on the species diagnostic details in Table I, the main reaction paths and chemical species with comparatively large reaction magnitude order are estimated as follows (Figure 3). During discharge between the two electrodes, elastic collision and inelastic collision between the injected electrons and NO molecules have initiated the electron-impact dissociation of NO, followed by other subsequent reactions to form NO⁺, N, N₂, N₂⁺, N⁺, O, and O₂ as well as NO₂.

Though NO₂ is generated as another kind of nitrogen oxides which is also harmful, the NO₂ can be conveniently reduced using sulfite solution based on the reaction as $2NO_2 + 4SO_3^{-2} \rightarrow 4SO_4^{-2} + N_2$ [42]. NO₂ generation is usually accepted to be effective for NO removal.

TABLE 1: Emission spectra and transition channel diagnosed from the NO emission lines.

λ /nm	Transition channel	Species
236.1	$A^2 \sum \rightarrow X^2 \prod (0-1)$	NO
247.3	$A^2 \sum \rightarrow X^2 \prod (0-2)$	NO
258.9	$A^2 \sum \rightarrow X^2 \prod (0-3)$	NO
271.4	$A^2 \sum \rightarrow X^2 \prod (0-4)$	NO
280.0	$A^2 \sum \rightarrow X^2 \prod (1-6)$	NO
295.2	$A^2 \sum \rightarrow X^2 \prod (1-7)$	NO
315.8	$C^{3}\prod_{u} \rightarrow B^{3}\prod_{g} (1-0)$	N_2
337.2	$C^3 \prod_u \rightarrow B^3 \prod_g (0-0)$	N_2
357.3	$C^{3}\prod_{u} \rightarrow B^{3}\prod_{g} (0-1)$	N_2
375.1	$C^{3}\prod_{u} \rightarrow B^{3}\prod_{g} (1-3)$	N_2
380.0	$C^{3}\prod_{u} \rightarrow B^{3}\prod_{g} (0-2)$	N_2
391.2	$\mathrm{B}^{2}\Sigma_{u}^{+} \rightarrow \mathrm{X}^{2}\Sigma_{g}^{+} (0-0)$	N_2^+
399.5	$C^3 \prod_u \rightarrow B^3 \prod_g (1-4)$	N_2
405.6	$C^{3}\prod_{u} \rightarrow B^{3}\prod_{g} (0-3)$	N_2
426.5	$B^2 \sum_{u}^{+} \rightarrow X^2 \sum_{g}^{+} (0-1)$	N_2^+
434.0	$C^{3}\prod_{u} \rightarrow B^{3}\prod_{g} (0-4)$	N_2
441.4	$C^{3}\prod_{u} \rightarrow B^{3}\prod_{g} (3-8)$	N_2
464.5	$B^2 \Sigma_u^+ \rightarrow X^2 \Sigma_g^+ (1-3)$	N_2^+
470.7	$B^2 \Sigma_u^{+} \rightarrow X^2 \Sigma_g^{+} (0-2)$	N_2^+
493.4	$A^{2}B_{1} \rightarrow X^{2}A_{1}(1, 5, 0-0, 0, 0)$	NO_2
516.8	$A^{2}B_{1} \rightarrow X^{2}A_{1}(1, 4, 0-0, 0, 0)$	NO_2
540.4	$A^{2}B_{1} \rightarrow X^{2}A_{1}(1, 3, 0-0, 0, 0)$	NO_2
552.3	$A^{2}B_{1} \rightarrow X^{2}A_{1}(3, 0, 0-0, 0, 0)$	NO_2
568.0	$A^{2}B_{1} \rightarrow X^{2}A_{1}(1, 2, 0-0, 0, 0)$	NO_2
5884	$A^{2}B_{1} \rightarrow X^{2}A_{1}(2, 0, 0-0, 0, 0)$	NO_2
597.3	$A^2B_1 \rightarrow X^2A_1(1, 1, 0-0, 0, 0)$	NO_2
602.2	$A^{2}B_{1} \rightarrow X^{2}A_{1}(0, 0, 1-0, 0, 0)$	NO_2
656.4	$2s2p^2(^4P)3s \rightarrow 2s^22p4s$	N^+
674.6	$2s^2 2p^2({}^{3}\mathrm{P})4d \rightarrow 2s^2 2p^2({}^{3}\mathrm{P})3p$	Ν
715.5	$2s2p^2(^4P)3s \rightarrow 2s^22p4s$	N^+
746.8	$2s^2 2p^2({}^{3}\mathrm{P})3p \rightarrow 2s^2 2p^2({}^{3}\mathrm{P})3s$	Ν
777.0	$2s^2 2p^3 ({}^4S^{\circ}) 3p \rightarrow 2s^2 2p^3 ({}^4S^{\circ}) 3s$	0
821.5	$2s^2 2p^2({}^{3}\mathrm{P})3p \rightarrow 2s^2 2p^2({}^{3}\mathrm{P})3s$	Ν
844.2	$2s^2 2p^3 ({}^4S^{\circ}) 3p \rightarrow 2s^2 2p^3 ({}^4S^{\circ}) 3s$	О
867.6	$2s^22p5s \rightarrow 2s^22p4p$	N^+

The electrical energy consumption for achieving desirable NO removal efficiency is of critical importance in practice. Under different discharge voltage from 2.4 to 4.8 kV, the emission spectra are shown in Figure 4.

By high voltage loaded, the emission spectra lines are located at the almost unchanged wavelength. Differently, the emission intensity has varied.

In order to clarify the influence of discharge energy, the characteristic spectra are selected at 337.2, 516.8, 777.0, and

 E_k/eV λ_k/nm $A_k \times g_k/s^{-1}$

 10.740931
 777.0
 2.58 × 10⁸

 10.988861
 844.2
 1.61 × 10⁸

TABLE 2: Spectra constants of O atoms at 777.0 and 844.2 nm [20].



FIGURE 3: Diagram of main reaction paths and species during discharge.

844.2 nm for N_2 , NO_2 , and O, respectively. Figure 5 shows the emission intensity variance under different inputting voltages. With input energy increasing, the emission intensity of the new species N_2 , NO_2 , and O all have increased.

According to *Einstein* spontaneous emission law in (1) [43], the species concentration $n_{k,Z}$ is proportional to the emission intensity $I_{ki,Z}$ as follows:

$$I_{ki,Z} = \frac{1}{4\pi} \frac{hc}{\lambda_{ki,Z}} n_{k,Z} A_{ki,Z} l.$$
(1)

In (1), A_{ki} is the transition probability from energy level k to level i and λ_{ki} is the corresponding emission wavelength. l is the total plasma thickness. h is the *Planck*'s constant and c is the light velocity in vacuum. $n_{k,Z}$ is the population in energy level k of the species.

Based on (1) and Figure 5, a qualitative conclusion can be made that the higher input energy has heightened NO removal efficiency to generate more new species of N_2 , NO_2 , O, and so forth.

In order to evaluate the plasma variance at different inputting energy, the plasma electron temperature T_e is analyzed according to the *Boltzmann* distribution law [44] under Local Thermodynamic Equilibrium (LTE) approximation as follows:

$$\frac{n_{k,Z}}{n_Z} = \frac{g_{k,Z}}{P_Z} \exp\left[-\frac{E_{k,Z}}{k_B T_e}\right].$$
 (2)

In (2), k_B is the *Boltzmann's* constant. P_Z is related to the neutral or singly ionized atom state. n_Z is the total population density. $g_{k,Z}$ and $E_{k,Z}$ are the degeneracy and energy of the level k.

Since the emission intensity is detected with arbitrary unit, the electron temperature T_e is impossible to be directly calculated. In order to obtain the T_e , it is deduced from the



FIGURE 4: Emission spectra under different pulse voltage inputted from 2.4 to 4.8 kV.

ratio of two emission lines of the same atoms with same ionization stage Z, which is applied based on (1) and (2) as

$$\frac{I_{1}}{I_{2}} = \frac{A_{1}g_{1}/\lambda_{1}}{A_{2}g_{2}/\lambda_{2}} \exp\left(-\frac{E_{1}-E_{2}}{k_{B}T_{e}}\right)$$
or
$$T_{e} = -\frac{E_{1}-E_{2}}{k_{B}\left(\ln\left(I_{1}A_{2}g_{2}\lambda_{1}\right) - \ln\left(I_{2}A_{1}g_{1}\lambda_{2}\right)\right)}.$$
(3)

Such procedure has eliminated the disturbance of arbitrary unit. The characteristic emission has been selected as the two O atom lines at 777.0 and 844.2 nm, due to their high signal-to-noise ratio. The emission constants are shown in Table 2.

Plot of T_e versus the inputted voltage yields Figure 6. The obtained plasma electron temperature T_e is increasing with the voltage heightened. The 4.8 kV discharge has achieved higher T_e of about 9500 K, compared with that of 6403 K at 2.4 kV. Such T_e implies that the chemical reaction activation of the species in plasma is heightening for the NO removal.

It also should be noticed that NO transforming and removing process is difficult to be thoroughly detected by experimental methods, due to the complicated reactions in the plasma as shown in Figure 3. There has been a necessity to establish simulation model for analyzing the reaction dynamic.

3.2. Dynamic Simulation of NO Removal Process. To investigate the NO removal dynamic during and after discharge, the concentration variance of the *i*th species is modeled as a time varying differential equation [45], which includes the generating and losing reaction paths of this given *i*th species as in

$$\frac{dn_i}{dt} = -\sum_{i,j} k_{ij} n_i n_j + \sum_{p,q} k_{pq} n_p n_q, \qquad (4)$$

where, n_i , n_j , n_p and n_q are concentrations of the respective species and k_{ij} and k_{pq} are reaction rate coefficients of the losing and generating routines. Concentration loss of the *i*th specie has occurred in the reaction between species *i* and *j*, while specie *i* generation is determined by the reaction between species *p* and *q*.



FIGURE 5: The characteristic spectra under different pulse voltage, identified at (a) 337.2 nm of N₂ molecule, (b) 516.8 nm of NO₂ molecule, and (c) 777.0 nm and 844.2 nm of O atom.

With spatial homogeneity hypothesis of the discharge, the plasma is simulated in zero-dimensional scale. Space diffusion of electrons, NO, and other by-products has been neglected, and the concentration of electrons and gas molecules in the whole volume of the plasma are assumed to be uniform. The reaction paths and corresponding kinetic rate coefficients k are outlined in Table 3. For the electron-excited dissociation process, the rate constant k can be calculated by

$$k = \left(\frac{2}{m_{\rm e}}\right)^{1/2} \int_0^\infty E^{1/2} \sigma\left(E_{\rm e}\right) f\left(E_{\rm e}\right) dE_{\rm e}.$$
 (5)

In which, E_e and m_e are the electron energy and mass. $f(E_e)$ is the electron distribution function, and $\sigma(E_e)$ is the corresponding collision cross section [46].

The species' reactions are modeled as discrete timevarying stiff differential equation system and have been solved by *Runge-Kutta* algorithm [47].

NO concentration variance is shown in Figure 7, in which the concentration variance of electrons is also present. During pulse discharge, the concentration of NO is monotonically decreased. There was obvious NO removal effect, and about 5.5289% NO has been transformed into other species during discharge that lasted for 24.5 ns. After discharge, the electron concentration was assumed to be zero, whereas the NO



FIGURE 6: Plasma electron temperature $T_{\rm e}$ variance versus inputted voltage.



FIGURE 7: Concentration variance of NO molecules and electrons versus time. The concentration of NO is 5.37×10^{18} /cm³ at 0 ns, 5.0731×10^{18} /cm³ at 24.5 ns, 5.0046×10^{18} /cm³ at 60 ns, and 4.9999 $\times 10^{18}$ /cm³ at 120 ns.

concentration is also decreasing, and achieving 6.8045% NO removal efficiency after 60 ns as well as 6.8920% after 120 ns.

From the viewpoint of main reaction paths for NO removal, the collision dissociation reaction by electrons on NO molecules during discharge is occupied the major position, and determined the most part of the NO removal percentage. On the contrary, the by-product species and radicals are playing important role after discharge and contribute to a small part of the NO removal percentage.

In order to clarify the effect of by-products on NO removal efficiency after discharge, the generating and losing dynamic process of $O({}^{3}P)$, N_{2} , NO_{2} , O_{2} , N, $N({}^{2}D)$, N_{2}^{+} , N^{+} , and $O({}^{1}D)$ are shown in Figure 8. During discharge, concentrations of all the by-product species are increasing. When discharge is completed, some species such as N, $N({}^{2}D)$, N_{2}^{+} , N^{+} , and $O({}^{1}D)$ are consumed as shown in

TABLE 3: Reaction paths and the corresponding reaction rate coefficients [21–26].

Reaction path	$k/\mathrm{cm}^3\mathrm{s}^{-1}$
$e^* + N_2 \rightarrow N_2^+ + 2e$	2.4×10^{-12}
$e^* + N_2 \rightarrow N + N + e$	2.0×10^{-11}
$e^* + NO \rightarrow N + O(^{3}P) + e$	$8.5 imes 10^{-10}$
$e^* + NO \rightarrow NO^+ + 2e$	$1.1 imes 10^{-10}$
$e^* + NO^+ \rightarrow N + O(^3P)$	8.2×10^{-9}
$e^* + N_2^+ \rightarrow N_2$	4.0×10^{-12}
$e^* + NO^+ \rightarrow O(^{3}P) + N(^{2}D)$	4.3×10^{-7}
$N^+ + NO \rightarrow N_2^+ + O(^{3}P)$	5.0×10^{-11}
$N^+ + O_2 \rightarrow NO^+ + O(^{3}P)$	2.6×10^{-10}
$N_2^+ + N \rightarrow N^+ + N_2$	$1.0 imes 10^{-11}$
$N_2^+ + O(^3P) \rightarrow NO^+ + N$	$1.4 imes 10^{-10}$
$N + NO_2 \rightarrow N_2 + O(^3P) + O(^3P)$	9.1×10^{-13} *
$O(^{3}P) + NO + N_{2} \rightarrow NO_{2} + N_{2}$	1.0×10^{-31}
$N_2(A) + O_2 \rightarrow N_2 + O(^{3}P) + O(^{3}P)$	2.54×10^{-12}
$N_2(A) + NO \rightarrow NO + N_2$	$7.0 imes 10^{-11}$
$N_2(A) + N_2 \rightarrow N_2 + N_2$	3.0×10^{-18}
$N_2(A) + NO_2 \rightarrow NO + O(^3P) + N_2$	$1.0 imes 10^{-12}$
$NO_2 + O(^{3}P) \rightarrow NO + O_2$	9.1×10^{-12}
$O(^{3}P) + O(^{3}P) + O_{2} \rightarrow O_{2} + O_{2}$	6.7×10^{-33} *
$N_2(B) + O_2 \rightarrow N_2(A) + O_2$	3.0×10^{-10}
$N(^{2}D) + O_{2} \rightarrow NO + O(^{1}D)$	$6.0 imes 10^{-12}$
$N(^{2}D) + NO \rightarrow N_{2} + O(^{3}P)$	$4.5 imes 10^{-11}$
$O(^{1}D) + NO \rightarrow N + O_{2}$	$8.5 imes 10^{-11}$
$e^* + N_2 \rightarrow N^+ + N + 2e$	$2.4 imes 10^{-17}$
$e^* + N_2 \rightarrow N_2(A) + e$	$1.1 imes 10^{-10}$
$e^* + N \rightarrow N^+ + 2e$	$1.1 imes 10^{-10}$
$e^*+N^+\rightarrowN$	$3.5 imes 10^{-12}$
$e^* + NO^+ \rightarrow NO$	4.0×10^{-12}
$N^+ + NO \rightarrow NO^+ + N$	$5.1 imes 10^{-10}$
$N^+ + NO_2 \rightarrow NO^+ + NO$	5.0×10^{-10}
$N_2^+ + O_2 \rightarrow NO^+ + NO$	$1.0 imes 10^{-17}$
$N_2^+ + NO \rightarrow NO^+ + N_2$	3.3×10^{-10}
$N + NO \rightarrow N_2 + O(^3P)$	3.0×10^{-11}
$N + NO_2 \rightarrow 2NO$	$6.0 imes 10^{-13}$
$N + O_2 \rightarrow NO + O(^{3}P)$	8.9×10^{-17}
$N_2(A) + O(^3P) \rightarrow NO + N(^2D)$	7.0×10^{-12}
$\mathrm{N_2(A)} + \mathrm{N_2(A)} \rightarrow \mathrm{N_2} + \mathrm{N_2(C)}$	1.6×10^{-10}
$N_2(A) + O(^3P) \rightarrow N_2 + O(^1D)$	$2.1 imes 10^{-11}$
$O(^{1}D) + O_{2} \rightarrow O(^{3}P) + O_{2}$	$8.0 imes 10^{-12}$
$O(^{3}P) + O(^{3}P) + N_{2} \rightarrow O_{2} + N_{2}$	$3.0 \times 10^{-33*}$
$\mathrm{N_2(B)} + \mathrm{N_2} \ \rightarrow \ \mathrm{N_2(A)} + \mathrm{N_2}$	3.0×10^{-11}
$N_2(B) + NO \rightarrow N_2(A) + NO$	$2.4 imes 10^{-10}$
$\mathrm{N_2(C)} + \mathrm{N_2} \ \rightarrow \ \mathrm{N_2(B)} + \mathrm{N_2}$	$1.0 imes 10^{-11}$
$N(^{2}D) + O_{2} \rightarrow NO + O(^{3}P)$	$1.5 imes 10^{-12}$
$N(^{2}D) + N_{2} \rightarrow N + N_{2}$	$6.0 imes 10^{-15}$
$O(^{1}D) + N_{2} \rightarrow O(^{3}P) + N_{2}$	2.6×10^{-11}
*Its unit is cm ⁶ s ⁻¹	



FIGURE 8: Concentration variance of by-product species and electrons versus time. (a) N^+ , N_2^+ , $O(^1D)$, $N(^2D)$, N, and electron; (b) $O(^3P)$, N_2 , O_2 , NO_2 , and electron.

Figure 8(a), while other species including $O({}^{3}P)$, N_{2} , and O_{2} as well as NO₂ show an increasing trend of concentration in Figure 8(b). According to the law of conservation of matter, the generation of $O({}^{3}P)$, N_{2} , O_{2} , and NO₂ should be derived from the consumption of N, N({}^{2}D), N_{2}^{+}, N⁺, and $O({}^{1}D)$. Also, it should take the different concentration magnitude order of all the species into consideration.

(1) Role of $O({}^{3}P)$ for NO Removal. During discharge, large amount of $O({}^{3}P)$ atoms have been accumulated. At 24.5 ns, the atom $O({}^{3}P)$ concentration of 2.9648 × 10¹⁷/cm³ is higher than $O({}^{1}D)$ of 3.0111 × 10¹¹/cm³ with 10⁶ magnitude order. $O({}^{3}P)$ has obviously played the major role in oxidizing NO to higher oxides. As consequence, the concentration increase of NO₂ from 1.1101 × 10¹⁴/cm³ at 24.5 ns to final 2.6668 × 10¹⁵/cm³ has been mainly ascribed to the oxidation reaction between $O({}^{3}P)$ and NO. Such oxidation reaction is ruled by

$$O({}^{3}P) + NO + N_{2} \longrightarrow NO_{2} + N_{2};$$

 $k = 1.0 \times 10^{-31} \text{ cm}^{6} \text{ s}^{-1}.$ (6)

But when it comes to the low magnitude order 10^{15} /cm³ of NO₂ produced after discharge, it can be deduced that there is a relatively small contribution of the oxidation reaction for the total 10^{16} /cm³ NO removal after discharge from 5.0731 $\times 10^{18}$ /cm³ at 24.5 ns to final 4.9999 $\times 10^{18}$ /cm³ as shown in Figure 7.

There also has been O_2 of 4.4522×10^{14} /cm³ generated at 120 ns, which is obviously generated by bimolecular reactions between $O(^{3}P)$ atoms. But its concentration is relatively low and can be considered as neglectable reaction routine for NO removal.

(2) Role of N Atoms for NO Removal. Main part consumption of NO after discharge should be ascribed to generation of N₂.



FIGURE 9: Diagram of main reaction paths for NO removal after discharge, including NO substituted by N as major reaction path (solid line) and NO oxidized by $O(^{3}P)$ as minor reaction path (dotted line).

For NO, the concentration decrease is in 10^{16} /cm³ magnitude order. For N₂, the concentration increase is also in the same 10^{16} /cm³ orders from 1.1301×10^{17} /cm³ at 24.5 ns to 1.8356×10^{17} /cm³. In Figure 8(a), it can also be observed that the N atom of 7.0503×10^{16} /cm³ at 24.5 ns which decreased to final 1.3421×10^{13} /cm³ has shared the key reaction routine with NO to generate N₂ after discharge. The N atoms have chemically substituted NO to produce N₂ and O(³P) through the following reaction:

N + NO
$$\longrightarrow$$
 N₂ + O(³P); $k = 3.0 \times 10^{-11} \text{ cm}^3 \text{ s}^{-1}$. (7)

From the viewpoint of concentration magnitude, other species such as $N(^{2}D)$, N_{2}^{+} , and N^{+} have little effect on NO removal after discharge.

Based on the above NO removal simulation after discharge, the N atoms in Reaction (7) are very effective in substituting NO, while the Reaction (6) of $O({}^{3}P)$ atoms make a relatively small contribution by oxidizing NO. The main reaction paths and chemical species for NO removal after discharge are concluded in Figure 9.



FIGURE 10: (a) NO concentration and (b) NO removal percentage achieved by adjusting pulse discharge duration width.

3.3. Approaches for Improving the NO Removal Efficiency

(1) Effect of Discharge Pulse Duration Width on NO Removal Efficiency. Since the species of N and $O(^{3}P)$ atoms are both produced by electron impact dissociation of NO, the electron concentration has decided the dissociation rate of NO during discharge and has also affected the subsequent reactions between NO and the by-products during and after discharge.

Adjustment of pulse discharge width can influence the electron accumulated concentration. In Figure 10(a), the pulse duration width is varied from 10 to 110 ns. The final NO concentrations are monotonically decreased with pulse width increasing.

Quantitatively, NO removal extent is calculated as

$$\eta = \frac{n[\text{NO}]_{t=0 \text{ ns}} - n[\text{NO}]_{t=120 \text{ ns}}}{n[\text{NO}]_{t=0 \text{ ns}}} \times 100\%.$$
 (8)

Linear increasing trend of NO removal extent has been presented in Figure 10(b); even 32% removal percentage is achieved at pulse duration of 110 ns. It is obvious that the electron concentration during discharge is accumulated with such a principle that its concentration is proportional to pulse duration width; the linear trend means that the NO removal efficiency is proportionally decided by the electron concentration in this simulation model. It also implies that the mechanism of NO removal during and after discharge is unchanged, though the inputted electron concentrations are different when pulse duration width varied.

(2) Effect of N_2 Additive on NO Removal Efficiency. Based on the above analysis, the cost of NO removal is the discharge energy consumption with direct proportion principle. Then a question is brought out to find methods for more efficiently removing NO with less consumed discharge energy. Since the by-product species of N and O have played important roles on NO removal as shown in Figure 9, one practicable way is proposed to adjust gas ingredient in order to modify the reaction directions during and after discharge.

In Figure 11(a), the N₂ gas is mixed with NO. With N₂ initial concentration increased, the NO concentration at 24.5 ns is heightened. It implies that the electron-collision dissociation reaction of NO has been weakened by increasing the N₂ concentration. But the final NO removal percentage at 120 ns shows a trend as increasing first and then decreasing in Figure 11(b). The removal efficiency has been improved with mixed relatively low concentration of N₂ and deteriorated by high concentration of N₂ mixed.

In Figure 11(b), the highest removal extent is 7.52% at N_2/NO ratio of 2:1, compared with 7.11% of no N_2 mixed. When more N_2 inputted, the removal extent is monotone decreased and even occurred as 5.44% at N_2/NO ratio of 15:1. Such result shows that the by-products have affected or even improved the reaction dynamic after discharge, though electron collision dissociation of NO during discharge have been weakened when N_2 mixed.

In order to clarify the improving mechanism by mixed N_2 , the final concentration variance Δ of the main species under different N_2/NO ratio is shown in Figure 12. By defining n^i as the concentration of *i*th species, the Δ_i is defined as

$$\Delta_i = n_{t=0\,\mathrm{ns}}^i - n_{t=120\,\mathrm{ns}}^i. \tag{9}$$

In Figure 12, the removal variance of NO is accompanied with the generation variance of N_2 and NO_2 as well as $O(^{3}P)$ and varied in same magnitude order. With N_2/NO ratio increased, the final generation concentrations of N_2 and $O(^{3}P)$ are monotonically decreased, while that of NO_2 is first increasing and then decreasing. Variance of other species such as NO^+ , O_2 , and N can be neglected.



FIGURE 11: (a) The time evolution of NO concentration under different NO/N2 ratio; (b) NO removal percentage under different NO/N2 ratio.

It is obvious that the higher the N_2/NO concentration ratio is, the less the electrons are consumed by NO due to the decreased collision probability. Consequently, the concentration of N and O(³P) atoms dissociated from NO as ruled in Reaction (10) would be decreased. Consider

$$e^* + NO \longrightarrow N + O({}^{3}P) + e; \quad k = 8.5 \times 10^{-10} \text{ cm}^3 \text{ s}^{-1}.$$
(10)

But there is also a compensative path for N atom loss according to Reaction (11) by electron collision on the N_2 molecules:

$$e^* + N_2 \longrightarrow N + N + e; \quad k = 2.0 \times 10^{-11} \text{ cm}^3 \text{s}^{-1}.$$
 (11)

The two reactions are competitive with each other for consuming electrons, during which the dissociation energy of NO is found to be smaller than that of N₂. For the former, the dissociation energy of N–O bond is 6.496 eV. For the latter, the N–N bond is dissociated at 9.76 eV [48]. As a result, the reaction rate coefficients are different, and the N₂ dissociation rate coefficient of 2.0×10^{-11} cm³ s⁻¹ is lower at the magnitude order of 10^{-1} than 8.5×10^{-10} cm³ s⁻¹ of NO. The N and O(³P) atom concentrations are predicted to present a decreasing trend though more N₂ mixed at higher N₂/NO ratio.

This phenomenon is verified based on the time-evolution of main species' concentrations in Figure 13. With more N_2 mixed, the N concentration at 24.5 ns is monotonically decreased in Figure 13(a). For the O(³P) atoms, its concentration is also decreased in Figure 13(b).

Also in Figure 13(b), $O({}^{3}P)$ accumulating process has presented longer time than the discharge width of 24.5 ns. With N₂/NO ratio increased, the accumulating process has been shortened. The reason is that the $O({}^{3}P)$ is not only derived from the electron collision dissociation in Reaction



FIGURE 12: The final concentration variance Δ of the main species under different N₂/NO ratio.

(10) during discharge, but can also be generated from Reaction (12) as

N + NO
$$\longrightarrow$$
 N₂ + O (³P); $k = 3.0 \times 10^{-11} \text{ cm}^3 \text{ s}^{-1}$. (12)

Since the N atom concentration generated during discharge has been weakened by increasing N_2/NO ratio, the Reaction (12) for further generating $O(^3P)$ between N and NO has sequently been weakened. Reaction (10) during discharge has played more and more important roles for $O(^3P)$ generation; therefore, the accumulating process presents a shorter time at higher N_2/NO ratio in Figure 13(b). As another result, the generated N_2 concentration, which operated according



FIGURE 13: Concentration evolution versus time of (a) N atoms, (b) $O(^{3}P)$ atoms, and (c) NO₂ molecules under different N₂/NO mixing ratio. The arrow direction represents the N₂/NO mixing ratio increase.

to the Reaction (12), has also been attenuated. Consequently, concentrations of the generated N_2 and $O(^{3}P)$ both have shown monotonically decreasing trends in Figure 12.

When it comes to NO_2 , the NO_2 yielded from Reaction (13) is determined by $O({}^{3}P)$ and N_2 :

$$O(^{3}P) + NO + N_{2} \longrightarrow NO_{2} + N_{2};$$

$$k = 1.0 \times 10^{-31} \text{ cm}^{3} \text{ s}^{-1}.$$
(13)

Raising reactant concentrations usually makes the reaction operates at a higher rate by increasing collision probability per unit time. More N_2 additive has accelerated Reaction (13) for oxidizing NO into more NO₂. With N₂/NO mixing ratio increased, the formation of NO₂ is achieved to be maximal at N₂/NO of 8:1. When too more N₂ molecules are inputted, the O(³P) atom concentration is remarkably decreased according to the above analysis; then the Reaction (13) becomes slow. As shown in Figure 13(c), NO₂ concentration is decreased when too more N₂ are inputted at the N₂/NO ratio of 10:1 and 15:1.

Overall, the NO removal is decided by the electron collision dissociation during discharge and the substitution reaction or oxidation process during and after discharge. The optimal N_2/NO mixing ratio is 2:1. In such a ratio, the total generated $O/N_2/NO_2$ concentration is maximum, which can not only compensate the disadvantage of competitive electron consumption by the added N_2 during discharge as shown in Figure 11(a) but also heighten the total removal percentage in Figure 11(b). By mixing N_2 gas at appropriate concentration ratio, the NO removal process has been more efficiently achieved, without depositing additional discharge energy.

The optimal condition of pulsed-discharged plasma technique for NO pollutant gas removal has been quantitatively obtained in this paper through the numerical simulation method. Such results can be applied for NO gas remediation in power plants, automobile exhaust treatment, and so on.

4. Conclusion

This paper discusses the NO removal mechanism in pulsedischarged plasma. Emission spectra diagnosis indicates that the NO has transformed into O, N, N₂, NO₂, and other by-products, and the higher the discharge voltage is, the more the NO removed is. The plasma electron temperature T_e is deduced as 9500 K at voltage of 4.8 kV inputted. The chemical reaction activation of the species has been heightened in such high $T_{\rm e}$. In order to clarify the complicated NO removal dynamic process, zero-dimensional numerical simulation indicates that the main reaction paths during pulsed discharge are the electron collision dissociation of NO into N and O atoms, and followed single substitution of N on NO to form N₂. After discharge, the single substitution between N and NO to form N₂ also plays the major role, compared with the NO₂ formation by oxidizing NO. This model also implies that the NO removal mechanism is almost the same when pulse discharge with different duration width is operated.

Furthermore, the dynamic model gives particular notice on the N₂ additive for improving NO removal efficiency. With the N₂/NO ratio increased, the maximum concentration of NO₂ is achieved at ratio of 8:1, but the N₂ and O(³P) concentrations are decreasing remarkably due to the modified reaction directions. There has an optimal N₂/NO concentration ratio as 2:1 to achieve the maximal NO removal efficiency. At such a ratio, the total generated O/N₂/NO₂ concentration is maximum, which cannot only compensate the competitive electron consumption by N₂ additive during discharge but also heighten the total removal percentage than that without N₂ mixed.

Such preliminary results indicate that the nonthermal pulse-discharged plasma technique for NO pollutant gas control must necessarily include adequate additive gas, such as the N₂, for low-costly improving the removal efficiency.

Conflict of Interests

The authors declare that there is no conflict of interests regarding the publication of this paper.

Acknowledgments

This work was financially supported by the National Nature Science Foundation of China no. 10875036 and the Nature Science Foundation of Hebei Province nos. A2007000131, A2010000177.

References

- J. A. van Aardenne, G. R. Carmichael, H. Levy, D. Streets, and L. Hordijk, "Anthropogenic NO_x emissions in Asia in the period 1990–2020," *Atmospheric Environment*, vol. 33, no. 4, pp. 633– 646, 1999.
- [2] M. Iwamoto and H. Hamada, "Removal of nitrogen monoxide from exhaust gases through novel catalytic processes," *Catalysis Today*, vol. 10, no. 1, pp. 57–71, 1991.
- [3] D. I. Stern, "Global sulfur emissions from 1850 to 2000," Chemosphere, vol. 58, no. 2, pp. 163–175, 2005.
- [4] M. V. Twigg, "Progress and future challenges in controlling automotive exhaust gas emissions," *Applied Catalysis B*, vol. 70, no. 1–4, SI, pp. 2–15, 2007.
- [5] G. J. Frost, S. A. McKeen, M. Trainer et al., "Effects of changing power plant NO_x emissions on ozone in the eastern United States: proof of concept," *Journal of Geophysical Research D*, vol. 111, no. D12, Article ID D12306, 2006.
- [6] S. Kim, A. Heckel, S. A. McKeen et al., "Satellite-observed U.S. power plant NO_x emission reductions and their impact on air quality," *Geophysical Research Letters*, vol. 33, no. 22, Article ID L22812, 2006.
- [7] F. Normann, K. Andersson, B. Leckner, and F. Johnsson, "Emission control of nitrogen oxides in the oxy-fuel process," *Progress in Energy and Combustion Science*, vol. 35, no. 5, pp. 385–397, 2009.
- [8] L. Chen, J. Li, and M. Ge, "Promotional effect of ce-doped V₂O₅-WO₃/TiO₂ with low vanadium loadings for selective catalytic reduction of NO_x by NH₃," *Journal of Physical Chemistry C*, vol. 113, no. 50, pp. 21177–21184, 2009.
- [9] M. Takeuchi and S. Matsumoto, "NO_x storage-reduction catalysts for gasoline engines," *Topics in Catalysis*, vol. 28, no. 1–4, pp. 151–156, 2004.
- [10] A. Keskin and A. Emiroglu, "Catalytic reduction techniques for post-combustion diesel engine exhaust emissions," *Energy Education Science and Technology A*, vol. 25, no. 1-2, pp. 87–103, 2010.
- [11] X. Tang, X. Xu, H. Yi, C. Chen, and C. Wang, "Recent developments of electrochemical promotion of catalysis in the techniques of DeNO_x," *Scientific World Journal*, vol. 2013, Article ID 463160, 13 pages, 2013.

- [12] F. Normann, K. Andersson, B. Leckner, and F. Johnsson, "High-temperature reduction of nitrogen oxides in oxy-fuel combustion," *Fuel*, vol. 87, no. 17-18, pp. 3579–3585, 2008.
- [13] D. Kühnemuth, F. Normann, K. Andersson, F. Johnsson, and B. Leckner, "Reburning of nitric oxide in oxy-fuel firing-the influence of combustion conditions," *Energy & Fuels*, vol. 25, no. 2, pp. 624–631, 2011.
- [14] Z. Liu and S. Woo, "Recent advances in catalytic DeNO_x science and technology," *Catalysis Reviews*, vol. 48, no. 1, pp. 43–89, 2006.
- [15] A. Mizuno, "Industrial applications of atmospheric nonthermal plasma in environmental remediation," *Plasma Physics and Controlled Fusion*, vol. 49, no. 5 A, SI, pp. A1–A15, 2007.
- [16] J. S. Chang, "Physics and chemistry of plasma pollution control technology," *Plasma Sources Science and Technology*, vol. 17, no. 4, Article ID 045004, 2008.
- [17] R. Hackam and H. Akiyama, "Air pollution control by electrical discharges," *IEEE Transactions on Dielectrics and Electrical Insulation*, vol. 7, no. 5, pp. 654–683, 2000.
- [18] T. Namihira, S. Tsukamoto, D. Wang et al., "Improvement of NO_x removal efficiency using short-width pulsed power," *IEEE Transactions on Plasma Science*, vol. 28, no. 2, pp. 434–442, 2000.
- [19] Y. Lee, W. Jung, Y. Choi et al., "Application of pulsed corona induced plasma chemical process to an industrial incinerator," *Environmental Science and Technology*, vol. 37, no. 11, pp. 2563– 2567, 2003.
- [20] NIST Atomic Spectra Database Lines Form, http://physics.nist .gov/PhysRefData/ASD/lines_form.html.
- [21] O. Eichwald, M. Yousfi, A. Hennad, and M. D. Benabdessadok, "Coupling of chemical kinetics, gas dynamics, and charged particle kinetics models for the analysis of NO reduction from flue gases," *Journal of Applied Physics*, vol. 82, no. 10, pp. 4781– 4794, 1997.
- [22] M. Uddi, N. Jiang, I. V. Adamovich, and W. R. Lempert, "Nitric oxide density measurements in air and air/fuel nanosecond pulse discharges by laser induced fluorescence," *Journal of Physics D*, vol. 42, no. 7, Article ID 075205, 2009.
- [23] F. J. Gordillo-Vázquez, "Air plasma kinetics under the influence of sprites," *Journal of Physics D*, vol. 41, no. 23, Article ID 234016, 2008.
- [24] J. T. Herron and D. S. Green, "Chemical kinetics database and predictive schemes for nonthermal humid air plasma chemistry, part II: neutral species reactions," *Plasma Chemistry and Plasma Processing*, vol. 21, no. 3, pp. 459–481, 2001.
- [25] T. Arcos, C. Domingo, V. J. Herrero, M. M. Sanz, and I. Tanarro, "Diagnostics and kinetic modeling of the ignition and the extinction transients of a hollow cathode N₂O discharge," *Journal of Physical Chemistry A*, vol. 104, no. 17, pp. 3974–3983, 2000.
- [26] M. Castillo, I. Méndez, A. M. Islyaikin, V. J. Herrero, and I. Tanarro, "Low-pressure DC air plasmas. Investigation of neutral and ion chemistry," *Journal of Physical Chemistry A*, vol. 109, no. 28, pp. 6255–6263, 2005.
- [27] F. Leipold, A. Fateev, Y. Kusano, B. Stenum, and H. Bindslev, "Reduction of NO in the exhaust gas by reaction with N radicals," *Fuel*, vol. 85, no. 10-11, pp. 1383–1388, 2006.
- [28] T. Wang, B. Sun, H. Xiao, D. Wang, X. Zhu, and Y. Zhong, "Effect of water vapor on NO removal in a DBD reactor at different temperatures," *Plasma Chemistry and Plasma Processing*, vol. 33, no. 4, pp. 681–690, 2013.

- [29] C. Tsai, H. Yang, C. G. Jou, and H. M. Lee, "Reducing nitric oxide into nitrogen via a radio-frequency discharge," *Journal of Hazardous Materials*, vol. 143, no. 1-2, pp. 409–414, 2007.
- [30] J. L. Hueso, A. R. González-Elipe, J. Cotrino, and A. Caballero, "Plasma chemistry of NO in complex gas mixtures excited with a surfatron launcher," *Journal of Physical Chemistry A*, vol. 109, no. 22, pp. 4930–4938, 2005.
- [31] G. Yu, Q. Yu, Y. Jiang, K. Zeng, and F. Gu, "Mechanism of NO reduction with non-thermal plasma," *Journal of Environmental Sciences*, vol. 17, no. 3, pp. 445–447, 2005.
- [32] G. Zhang, W. Jin, and H. Zheng, "Dynamic mechanism about the fluorescence emission of NO dielectric barrier discharge plasma," *Journal of Quantitative Spectroscopy and Radiative Transfer*, vol. 127, pp. 90–95, 2013.
- [33] T. Yumii, T. Yoshida, K. Doi, N. Kimura, and S. Hamaguchi, "Oxidation of nitric oxide by atmospheric pressure plasma in a resonant plasma reactor," *Journal of Physics D*, vol. 46, no. 13, Article ID 135202, 2013.
- [34] H. Wedaa, M. Abdel-Salam, A. Ahmed, and A. Mizuno, "NO removal using dielectric barrier discharges in a multirod reactor stressed by AC and pulsed high voltages," *IEEE Transactions on Dielectrics and Electrical Insulation*, vol. 18, no. 5, pp. 1743–1751, 2011.
- [35] M. A. Malik, J. F. Kolb, Y. Sun, and K. H. Schoenbach, "Comparative study of NO removal in surface-plasma and volume-plasma reactors based on pulsed corona discharges," *Journal of Hazardous Materials*, vol. 197, pp. 220–228, 2011.
- [36] E. Böös and W. Wang, "Apparatus and method for the removal of nitrogen dioxide from a flue gas stream," US Patent, US20130259786 A1, 2012.
- [37] H. Wang, X. Li, P. Chen, M. Chen, and X. Zheng, "An enhanced plasma-catalytic method for DeNO_x in simulated flue gas at room temperature," *Chemical Communications*, vol. 49, no. 81, pp. 9353–9355, 2013.
- [38] H. Wang, Q. Yu, T. Liu, L. Xiao, and X. Zheng, "NO_x storage and reduction with methane by plasma at ambient temperature," *RSC Advances*, vol. 2, no. 12, pp. 5094–5097, 2012.
- [39] Y. Takahara, A. Ikeda, M. Nagata, and Y. Sekine, "Lowtemperature NO decomposition in humidified condition using plasma-catalyst system," *Catalysis Today*, vol. 211, pp. 44–52, 2013.
- [40] L. Huang and Y. Dang, "Removal of SO₂ and NO_x by pulsed corona combined with in situ Ca(OH)₂ absorption," *Chinese Journal of Chemical Engineering*, vol. 19, no. 3, pp. 518–522, 2011.
- [41] NIST Atomic Spectra Database Lines Form, http://physics.nist .gov/PhysRefData/ASD/lines_form.html.
- [42] Z. Wang, X. Zhang, Z. Zhou, W. Chen, J. Zhou, and K. Cen, "Effect of additive agents on the simultaneous absorption of NO₂ and SO₂ in the Calcium Sulfite slurry," *Energy & Fuels*, vol. 26, no. 9, pp. 5583–5589, 2012.
- [43] H. Griem, Principles of Plasma Spectroscopy (Cambridge Monographs on Plasma Physics), Cambridge University Press, 2005.
- [44] J. Cooper, "Plasma spectroscopy," *Reports on Progress in Physics*, vol. 29, part I, pp. 35–130, 1966.
- [45] G. Froment, K. Bischoff, and J. Wilde, *Chemical Reactor Analysis and Design*, John Wiley & Sons, New York, NY, USA, 2011.
- [46] K. Behringer and U. Fantz, "Spectroscopic diagnostics of glow discharge plasmas with non-Maxwellian electron energy distributions," *Journal of Physics D*, vol. 27, no. 10, pp. 2128–2135, 1994.
- [47] J. Butcher, Numerical Methods for Ordinary Differential Equations, John Wiley & Sons, New York, NY, USA, 2003.
- [48] M. Brook and J. Kaplan, "Dissociation energy of NO and N₂," *Physical Review*, vol. 96, no. 6, pp. 1540–1542, 1954.