



Effect of dentin surface roughness on the shear bond strength of resin bonded restorations

Roodabeh Koodaryan¹, Ali Hafezeqoran^{1*}, Sajjad Poursoltan²

¹Dental and Periodontal Research Center, Faculty of Dentistry, Tabriz University of Medical Sciences, Tabriz, Iran

²Dentist, Private Practice, Tabriz, Iran

PURPOSE. This study aimed to investigate whether dentin surface preparation with diamond rotary instruments of different grit sizes affects the shear bond strength of resin-bonded restorations. **MATERIALS AND METHODS.** The buccal enamel of 60 maxillary central incisors was removed with a low speed diamond saw and wet ground with silicon carbide papers. The polished surfaces of the teeth were prepared with four groups of rotary diamond burs with super-coarse (SC), coarse (C), medium (M), and fine (F) grit sizes. Following surface preparation, 60 restorations were casted with nickel-chromium alloy and bonded with Panavia cement. To assess the shear bond strength, the samples were mounted on a universal testing machine and an axial load was applied along the cement-restoration interface at the crosshead speed of 0.5 mm/min. The acquired data was analyzed with one way ANOVA and Tukey post hoc test ($\alpha=.05$). **RESULTS.** The mean \pm SD shear bond strengths (in MPa) of the study groups were 17.75 ± 1.41 for SC, 13.82 ± 1.13 for C, 10.40 ± 1.45 for M, and 7.13 ± 1.18 for F. Statistical analysis revealed the significant difference among the study groups such that the value for group SC was significantly higher than that for group F ($P<.001$). **CONCLUSION.** Dentin surface roughness created by diamond burs of different grit sizes considerably influences the shear bond strength of resin bonded restorations.

[J Adv Prosthodont 2016;8:224-8]

KEY WORDS: Dentin; Resin-bonded bridge; Bonding; Shear strength; Dental instruments

INTRODUCTION

Since the introduction of resin bonded restorations by Rochette, these prostheses have been notably enhanced and changed. Despite successful clinical treatments, debonding of these restorations is regarded as the main problem of this treatment.¹⁻⁴ In early resin-bonded prostheses, the weak bond of cement to metal was the main cause of debonding.

This deficiency was improved through several techniques, such as electrolytic or chemical etching of the casting surface, incorporation of macromechanical retention, applying silicoater, and air abrasion with aluminum oxide particles. The current resin cements are chemically active and capable of creating strong bond with base metal alloys.⁵ Although adhesion to metal has been enhanced, the retention rate of resin bonded restorations is not satisfactory yet. Debonding still occurs commonly at the cement-dentin interface.¹⁻³ Several studies have evaluated the effects of biomechanical properties and preparation design on the success of resin-bonded prostheses. They have consequently emphasized the resistance and retention forms as the determining factors of better clinical retention of resin-bonded restorations.⁴⁻⁹ Therefore, the design of these prostheses has changed from minimum or no preparation to extensive preparations with additional features such as boxes and grooves or occlusal rest seats. Unfortunately, extensive preparations increase the potential loss of enamel, which is highly crucial for bonding and adversely affects the retention.^{6,7,9,10}

Corresponding author:

Ali Hafezeqoran
Dental and Periodontal Research Center, Faculty of Dentistry, Tabriz University of Medical Sciences, Golgasht St., Azadi Ave, Tabriz 51664, Iran
Tel. 98 41 33355965; e-mail, Hafezeqoran@gmail.com
Received January 2, 2016 / Last Revision March 30, 2016 / Accepted March 31, 2016

© 2016 The Korean Academy of Prosthodontics
This is an Open Access article distributed under the terms of the Creative Commons Attribution Non-Commercial License (<http://creativecommons.org/licenses/by-nc/3.0>) which permits unrestricted non-commercial use, distribution, and reproduction in any medium, provided the original work is properly cited.

Increasing the adhesive-tooth contact surface through managing the surface roughness is a technique to improve the retention. However, there are limited studies evaluating the effect of roughness created by different rotary instruments on the success of full coverage restorations. Ayad *et al.* studied the surface roughness produced by diamond, tungsten carbide, and tungsten carbide finishing burs and found that diamond burs increased the surface area by a larger degree when compared with carbide burs.¹¹ In another study, Ayad *et al.* detected that crosscut carbide burs raised the retention of full coverage restoration cemented with zinc polycarboxylate by 46-55%. The study suggested considering retentive measures in preparation design when smooth surface is preferred. Roughening the preparation surface with rotary instruments increases the cement-tooth interlocking mechanism and improves the retention; consequently, the need for extra retentive measures declines.¹²

Due to the inconclusive literature about the effect of dentin roughness on the retention of crowns and also the lack of similar studies on resin-bonded restorations, it seems essential to determine the influence of dentin roughening by diamond rotary instruments on the retention of these restorations. Therefore, the present study aims to compare the effects of diamond rotary burs with different grit sizes on retention of resin-bonded restorations. The null hypothesis of this study is that different grit sizes of diamond rotary instruments do not affect the shear bond strength of resin-bonded restorations.

MATERIALS AND METHODS

In this experimental study, 60 maxillary central incisors of the same size were collected and stored in 1% chloramine-T solution (Solarbio Bioscience & Technology Co., Ltd., Shanghai, China) at 4°C for one month after extraction. The teeth were intact and extracted because of periodontal diseases.

By using a dental surveyor, each tooth was embedded in a polymeric tube filled with auto-polymerizing acrylic resin (Unifast II, GC Corp., Tokyo, Japan) and was aligned parallel with the tube wall. The teeth were prepared for resin bonded restoration by cutting the incisal enamel. Then the proximal and buccal enamel surfaces of the teeth were cut with a low speed diamond saw (Diamant, GmbH, D&Z, Berlin, Germany) and the buccal dentin was prepared as a rectangle (4 × 4 mm). A caliper with an accuracy of 0.1 mm (Mitutoya, Tokyo, Japan) was used to measure and control the dimensions of all specimens. Once the samples were ready, their buccal dentin was ground with wet silicon carbide paper (Shanghai Hangli Co., Ltd., Shanghai, China). Different grit sizes of silicon carbide papers were used in a sequence of 420, 600, 1000, and 1200 for 20 seconds.

After standardization of the dentin roughness, samples were randomly classified into four groups and polished surface of each group was prepared by using diamond rotary burs (NTI-Kahla GmbH; Kahla, Germany) of different grit sizes. Diamond rotary instruments used to prepare den-

Table 1. Diamond rotary instruments used to prepare the samples

Color code	Description	Grit size (µm)	ISO
Black	Super coarse	181	544
Green	Coarse	151	534
Without ring	Medium	107 - 126	524
Red	Fine	40	514

tin surfaces are listed in Table 1.

Based on the grit size of the diamond bur used, each group was named as SC (super-coarse with surface roughness of 181 µm), C (coarse: 151 µm), M (medium: 107-126 µm), and F (fine: 40 µm). The samples in group SC were prepared merely by very coarse diamond bur with surface roughness of 181 microns and a high-speed air turbine. The samples in group C were prepared with super-coarse grit size diamond bur followed by a coarse grit bur (151 µm). The surfaces of samples in group M were prepared with super-coarse, coarse, and a medium grit size (107-126 µm) diamond burs sequentially. Group F was prepared with the same method of the previous group (M) and then treated with a fine bur (40 µm).¹³

Having prepared the dentin surface, a custom acrylic resin tray (Unifast II: GC Corp., Tokyo, Japan) was constructed for each sample, and the final impression was made with polyether impression material (Impregum; 3M ESPE AG, Seefeld, Germany). Employing lost-wax casting technique, 60 metal castings (4 × 4 mm, 1 mm thick) were made of nickel-chromium alloy (Verabond II: AalbaDent, Cordelia, CA, USA). After finishing and polishing of the castings, their internal surfaces were air-abraded with 50 µm aluminum oxide particles for 10 seconds. According to the manufacturer's instruction, ED primer liquids A and B were mixed equally, applied on dentin surface, and air dried gently. Then, equal amounts of Panavia cement pastes (Panavia F2; Kuraray, Osaka, Japan) were mixed for 20 seconds and applied on the surface of the casting and bonded to the prepared dentin surfaces. Each sample was loaded in the universal testing machine (Hounsfield; Model H5-KS, Surray, UK) for 5 minutes with a load of 10 N. Cement excess was removed and, after 5 minutes, samples were cured for 40 seconds by light curing unit (Astralis 7; Ivoclar Vivadent AG, Lichtenstein, Germany). All samples were thermocycled in 5°C to 55°C water baths for a total of 1000 cycles with dwell and transfer times of 15 seconds.

In order to determine the shear bond strength, samples were mounted on the universal testing machine and an axial load was applied with a chisel-shaped rod at a crosshead speed of 0.5 mm/min along the casting-cement interface until failure occurred. The maximum load that caused debonding was recorded in MPa for each sample.

Under a stereomicroscope (Nikon; Tokyo, Japan) at 40 × magnification, the types of failure were evaluated and classified into three categories as the following: (i) adhesive failure with the cement remnant on the prepared dentin surfaces, (ii) adhesive failure with the cement remnant on the casting surface, and (iii) mixed failure with cement remnants on both prepared dentin and casting surfaces.

SPSS software (IBM SPSS version 17, Chicago, IL, USA) was used for data analysis. One-way ANOVA was performed to determine the effect of dentin roughness on shear bond strength, and Tukey's post-hoc test was used to compare the differences among the study groups. The level of statistical significance was set at 5%.

RESULTS

The mean ± SD shear bond strength (in MPa) of the groups are summarized in Table 2. The shear bond strength of the samples prepared with super coarse grit diamond burs (group SC) was significantly higher than that with fine grit rotary instruments (group F) ($P < .001$).

Table 3 illustrates the failure mode distribution. Regardless of the surface treatment, the most frequent failure type was adhesive failure with the resin cement remnants remained on the castings. Mixed failure mode was detected in all groups; however, it was most seen in group SC (33%) followed by group C (20%).

DISCUSSION

The results of the present study showed that the bond strength of Panavia cement to dentin surfaces treated with super coarse grit diamond bur was higher than that with the fine grit diamond bur, and the difference was statistically significant. Thus, the null hypothesis of the study that dentin roughness would not affect the retention of the resin-bonded restorations was rejected. Although there is no similar previous study about the bond strength of resin-bonded restorations, the result of this study supports several reported studies that have emphasized the important effect of dentin roughness on crown retention.

Ayad *et al.*¹¹ demonstrated that dentin surface treatment affects the adhesive bond strength through changing the surface structure. In a similar study, Ayad *et al.* showed that higher dentin roughness increased the retention of the crowns cemented with zinc phosphate cements while the smooth surfaces of teeth created by finishing burs provided less retention. The study also reported that, regardless of the type of instrumentation, Panavia exhibited more retentive strength than zinc phosphate cement. Ayad concluded that the retention of casting restorations depended on both the type of cement and the bur used in dentin surface finishing.¹² Likewise, the study by Mowery *et al.* revealed that the rough surface of prepared dentin provided a higher bond strength, which might be attributed to the increased total surface area involved in the bond.¹⁴

Table 2. Mean shear bond strength values (in MPa) and standard deviations calculated for different surface instrumentation of the groups

Study group	N	Mean ± SD	Minimum	Maximum
Super Coarse (SC)	15	17.75 ± (1.41) ^a	15.41	20.73
Coarse (C)	15	13.82 ± (1.13) ^b	11.08	15.61
Moderate (M)	15	10.40 ± (1.45) ^c	6.31	12.83
Fine (F)	15	7.13 ± (1.18) ^d	4.68	8.53
Total	60			

Values followed by distinct lowercase letters represent statistical differences between groups.

Table 3. Failure mode distributions of study groups after debonding

Study group	N	Cement remnants on dentin	Mixed (Cement remnants on dentin and casting)	Cement remnants on casting
Super Coarse (SC)	15	2 (13.3%)	5 (33.3%)	8 (53.3%)
Coarse (C)	15	1 (6.6%)	3 (20%)	11 (73.3%)
Moderate (M)	15	0 (0%)	2 (13.3%)	13 (86.6%)
Fine (F)	15	0 (0%)	1 (6.6%)	14 (93.3%)

Intimate contact of two opposing surfaces is necessary to establish a stable bond between dentin and the resin cement. The degree to which the adhesive moistens the dentin surface depends on the cement viscosity, contact angle between the two surfaces, topography of dentin surface, and the grit size of the cutting instrument.¹⁵⁻²⁰ When the dentin is cut, a smear layer of different thickness and density is formed on it, whose morphology and characteristics depend on the grit size of burs or abrasive instruments. Accordingly, the greater the grit size of the abrasive rotary instrument, the thicker the smear layer.^{18,19,21,22} Debris and smear layer reduce the surface energy, which may lead to poor adhesion; for that reason, some investigations have recommended removing the smear layer to improve the bond strength.²³⁻²⁵

To interpret the results of this study, it should be considered that the condition of the dentin surface after preparation (including the roughness and smear layer characteristics) has antagonistic effects on bonding of resin cements.²⁶⁻²⁸ Increasing the roughness of dentin surface provides a larger surface area for physical interaction with resin cement, resulting in stronger chemical bond with the dentin. On the other hand, thicker smear layer formed by diamond burs may prevent proper interaction between high-viscosity resin cement and the underlying dentin.^{18,19,22,29-31} The negative effect of smear layer thickness on the bond strength was not observed in the present study. The ED primer in Panavia cement kit had the ability to etch through the smear layer and leave the underlying dentin partially demineralized, increasing dentin permeability to the functional monomer of resin cement.^{32,33} Moreover, bonding to the prepared surface of dentin might also have been influenced by other factors.

It seems that the pressure imposed on indirect restorations during cementation plays an important role in resin bonding and determines the efficacy of reaction between adhesive cement and dentin surface covered with smear layer. Some studies agree that the seating pressure applied on luting agents during cementation of indirect restoration improves their adaptation and bond strength to dentin.^{16,26,34} According to De Munck *et al.*, viscosity of the material decreases under continuous shear rate.³⁵ Besides, higher seating pressure reduces the number of pores left on the bond interface or inside the adhesive cement. Furthermore, intimate contact between the adhesive cement and the underlying dentin improves the physical interaction between the surfaces through affecting the factors involved in bond strength, including Van der Waals force, hydrogen bridges, and charge-transfers.^{16,29,35}

In addition to the positive effect of the seating pressure on the bond strength, Chieffi *et al.* and other researchers have evaluated the effect of applying a constant pressure during the cement setting and concluded that it prevented water absorption and globule formation; therefore, a better adhesive surface would be achieved.^{34,36} As a result, decreasing infiltration of water from the underlying dentin into the primer-cement system might lead to better coupling of the

resin to dentin and improve bond strength. Thus, selecting the appropriate cement in combination with pressure application duration affected the bond strength significantly.³⁶

With respect to the findings of this study, dentin surface roughness has the potential to improve the bond strength of resin bonded restoration. However, long-term *in vitro* and *in vivo* studies should be conducted to support clinical cases. Additionally, new miscellaneous adhesive cements with high variety must be evaluated of their specific performance.

CONCLUSION

According to findings of the current study, preparing tooth surface by using coarse diamond burs enhances the bond strength of resin-bonded restorations.

ORCID

Ali Hafezeqoran <http://orcid.org/0000-0002-7756-3616>

REFERENCES

1. Goodacre CJ, Bernal G, Rungharassaeng K, Kan JY. Clinical complications in fixed prosthodontics. *J Prosthet Dent* 2003; 90:31-41.
2. Pjetursson BE, Tan WC, Tan K, Bragger U, Zwahlen M, Lang NP. A systematic review of the survival and complication rates of resin-bonded bridges after an observation period of at least 5 years. *Clin Oral Implants Res* 2008;19:131-41.
3. Priest G. An 11-year reevaluation of resin-bonded fixed partial dentures. *Int J Periodontics Restorative Dent* 1995;15: 238-47.
4. Wyatt CC. Resin-bonded fixed partial dentures: what's new? *J Can Dent Assoc* 2007;73:933-8.
5. Doh RM, Lee KW. Dislodgement resistance of modified resin-bonded fixed partial dentures utilizing tooth undercuts: an *in vitro* study. *J Adv Prosthodont* 2009;1:85-90.
6. Chow TW, Chung RW, Chu FC, Newsome PR. Tooth preparations designed for posterior resin-bonded fixed partial dentures: a clinical report. *J Prosthet Dent* 2002;88:561-4.
7. el-Mowafy O, Rubo MH. Retention of a posterior resin-bonded fixed partial denture with a modified design: an *in vitro* study. *Int J Prosthodont* 2000;13:425-31.
8. Keulemans F, Shinya A, Lassila LV, Vallittu PK, Kleverlaan CJ, Feilzer AJ, De Moor RJ. Three-dimensional finite element analysis of anterior two-unit cantilever resin-bonded fixed dental prostheses. *ScientificWorldJournal* 2015;2015:864389.
9. Shimizu H, Takahashi Y. Retainer design for posterior resin-bonded fixed partial dentures: a technical report. *Quintessence Int* 2004;35:653-4.
10. el-Mowafy O, Rubo MH. Resin-bonded fixed partial dentures-a literature review with presentation of a novel approach. *Int J Prosthodont* 2000;13:460-7.
11. Ayad MF, Rosenstiel SF, Hassan MM. Surface roughness of dentin after tooth preparation with different rotary instrumentation. *J Prosthet Dent* 1996;75:122-8.

12. Ayad MF, Rosenstiel SF, Salama M. Influence of tooth surface roughness and type of cement on retention of complete cast crowns. *J Prosthet Dent* 1997;77:116-21.
13. Li YQ, Wang H, Wang YJ, Chen JH. Effect of different grit sizes of diamond rotary instruments for tooth preparation on the retention and adaptation of complete coverage restorations. *J Prosthet Dent* 2012;107:86-93.
14. Mowery AS Jr, Parker M, Davis EL. Dentin bonding: the effect of surface roughness on shear bond strength. *Oper Dent* 1987;12:91-4.
15. Al-Omari WM, Mitchell CA, Cunningham JL. Surface roughness and wettability of enamel and dentine surfaces prepared with different dental burs. *J Oral Rehabil* 2001;28:645-50.
16. Goracci C, Cury AH, Cantoro A, Papacchini F, Tay FR, Ferrari M. Microtensile bond strength and interfacial properties of self-etching and self-adhesive resin cements used to lute composite onlays under different seating forces. *J Adhes Dent* 2006;8:327-35.
17. Hipilito V, Azevedo LC, Piveta FC, Filho WSV, Netto CA, Alonso RCB, Alpino PHP. Effect of dentinal surface preparation on the bonding of self-adhesive luting cements. *J Adhes Sci Technol* 2014;28:1907-24.
18. Hosoya Y, Shinkawa H, Suefiji C, Nozaka K, García-Godoy F. Effects of diamond bur particle size on dentin bond strength. *Am J Dent* 2004;17:359-64.
19. Peerzada F, Yiu CK, Hiraishi N, Tay FR, King NM. Effect of surface preparation on bond strength of resin luting cements to dentin. *Oper Dent* 2010;35:624-33.
20. Reifeis PE, Cochran MA, Moore BK. An in vitro shear bond strength study of enamel/dentin bonding systems on enamel. *Oper Dent* 1995;20:174-9.
21. Ayad MF, Johnston WM, Rosenstiel SF. Influence of dental rotary instruments on the roughness and wettability of human dentin surfaces. *J Prosthet Dent* 2009;102:81-8.
22. Barros JA, Myaki SI, Nör JE, Peters MC. Effect of bur type and conditioning on the surface and interface of dentine. *J Oral Rehabil* 2005;32:849-56.
23. Brännström M, Glantz PO, Nordenvall KJ. The effect of some cleaning solutions on the morphology of dentin prepared in different ways: an in-vivo study. *ASDC J Dent Child* 1979;46:291-5.
24. Pashley DH, Tao L, Boyd L, King GE, Horner JA. Scanning electron microscopy of the substructure of smear layers in human dentine. *Arch Oral Biol* 1988;33:265-70.
25. Tagami J, Tao L, Pashley DH, Hosoda H, Sano H. Effects of high-speed cutting on dentin permeability and bonding. *Dent Mater* 1991;7:234-9.
26. Escribano N, de la Macorra JC. Microtensile bond strength of self-adhesive luting cements to ceramic. *J Adhes Dent* 2006;8:337-41.
27. Marshall GW Jr, Marshall SJ, Kinney JH, Balooch M. The dentin substrate: structure and properties related to bonding. *J Dent* 1997;25:441-58.
28. Perdigão J. Dentin bonding-variables related to the clinical situation and the substrate treatment. *Dent Mater* 2010;26:e24-37.
29. Burgess JO, Ghuman T, Cakir D. Self-adhesive resin cements. *J Esthet Restor Dent* 2010;22:412-9.
30. McInnes PM, Wendt SL Jr, Retief DH, Weinberg R. Effect of dentin surface roughness on shear bond strength. *Dent Mater* 1990;6:204-7.
31. Wahle JJ, Wendt SL Jr. Dentinal surface roughness: a comparison of tooth preparation techniques. *J Prosthet Dent* 1993;69:160-4.
32. Van Meerbeek B, Yoshihara K, Yoshida Y, Mine A, De Munck J, Van Landuyt KL. State of the art of self-etch adhesives. *Dent Mater* 2011;27:17-28.
33. Yang B, Ludwig K, Adelung R, Kern M. Micro-tensile bond strength of three luting resins to human regional dentin. *Dent Mater* 2006;22:45-56.
34. Chieffi N, Chersoni S, Papacchini F, Vano M, Goracci C, Davidson CL, Tay FR, Ferrari M. Effect of the seating pressure on the adhesive bonding of indirect restorations. *Am J Dent* 2006;19:333-6.
35. De Munck J, Vargas M, Van Landuyt K, Hikita K, Lambrechts P, Van Meerbeek B. Bonding of an auto-adhesive luting material to enamel and dentin. *Dent Mater* 2004;20:963-71.
36. Chieffi N, Chersoni S, Papacchini F, Vano M, Goracci C, Davidson CL, Tay FR, Ferrari M. The effect of application sustained seating pressure on adhesive luting procedure. *Dent Mater* 2007;23:159-64.