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## Article

Co-utilization of wastewater sludge and heavy metals for single-atom electrocatalytic reduction of gaseous CO<sub>2</sub>



Author(s). Published by Elsevier Inc. https://doi.org/10.1016/ j.isci.2024.109956

Zhou et al., iScience 27, 109956 June 21, 2024 © 2024 The

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### Article



## Co-utilization of wastewater sludge and heavy metals for single-atom electrocatalytic reduction of gaseous $CO_2$

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### **SUMMARY**

Synergetic management of waste activated sludge, heavy metals (HMs) and CO<sub>2</sub> for their valorization and cyclic utilization is rarely reported. Herein, we employed sludge-derived extracellular polymeric substances (EPS) and HMs in wastewater to fabricate a gas diffusion electrode (GDE) for electrochemical CO<sub>2</sub> reduction. This approach atomically dispersed Ni at each nanofiber of the GDE. Abundant N element in the EPS proved to play a key role in the formation of  $N_x$ -Ni (mixture of  $N_3$ -Ni and  $N_4$ -Ni) sites for highly efficient CO<sub>2</sub> to CO conversion. The atomical Ni<sup>3+</sup> shows high catalytic activity. Direct gaseous CO<sub>2</sub> reduction in a membrane electrode assembly generated a current density up to 50 mA  $\cdot$  cm<sup>-2</sup> with CO:H<sub>2</sub> ratio of  $\sim$ 100 and  $\sim$ 75% FE<sub>CO</sub> under 2.69 cell voltage. This strategy takes advantage of all waste streams generated on site and consolidates traditionally separated treatment processes to save costs, produces valueadded products and generates carbon benefits during wastewater treatment.

### INTRODUCTION

Current wastewater treatment leads to intensive energy consumption (~3% global electricity),<sup>1</sup> huge waste activated sludge (WAS) production (global 136 million tons)<sup>2</sup> and considerable greenhouse gas (GHG) emission (~1.6% global GHG emission) annually.<sup>1</sup> For achievement of sustainable development and "carbon neutral" pledge, therefore, more efforts should be made to synergize mitigation of both wastes and carbon emission during wastewater treatment. Renewable grids driven electrochemical CO<sub>2</sub> reduction reaction (ECO<sub>2</sub>RR) using single atoms catalysts (SACs), with the maximum catalytic sites and tunable electronic structures, holds a great potential for CO<sub>2</sub> mitigation and valorization (value-added chemicals production) in wastewater treatment industries, 3-5 such as converting abundant CO<sub>2</sub> (30-40% content) in biogas of WAS digestion to valuable products. Since the early reports on the introduction of SACs on ECO2RR,<sup>6-8</sup> great efforts have been made to advance the CO<sub>2</sub> turnover efficiency and duration of SACs. Yang et al.<sup>8</sup> first demonstrated the improvement of CO<sub>2</sub> to CO conversion by Ni SACs due to their specific electronic structure. The smallest catalytic sites in atomic level delivered the optimal CO<sub>2</sub> conversion, and the current news even reported that  $\sim$ 100% CO<sub>2</sub>-CO conversion at long-term operations.<sup>3</sup> However, large-scale application of SACs for ECO<sub>2</sub>RR is still challenged due to complicated and high-cost synthesis of materials, despite it has been extensively studied in the lab.<sup>9-11</sup> Recently, low-cost carbon matrices and earth-abundant metals show great potential for fabricating SACs.<sup>3,12,13</sup> Given WAS has served as a good organic adsorbent/carbon matrix for binding various heavy metals (HMs) in wastewater, 14-16 we suppose whether it is feasible to employ it to manufacture SACs for in situ ECO<sub>2</sub>RR and waste reclamation, achieving waste-to-wealth. So far, there have been few reports on this route.

Although SACs can be fabricated using low-cost carbon matrices, such as carbon black<sup>3</sup> and biochar<sup>12,13</sup> etc., the defined SACs need the coordination structure between HMs and the N-contained functional groups, which is crucial to the catalytic activity.<sup>3-5</sup> Thus, the SACs preparation by these low-cost materials requires introduction of quantitative N-contained chemicals, such as melamine<sup>13</sup> and urea.<sup>3</sup> As a natural polymer, extracellular polymeric substances (EPS) secreted by microorganisms is abundant in WAS<sup>14-16</sup> and has been shown to serve as an efficient bio-adsorbent for HMs adsorption with high adsorbing capacity.<sup>17,18</sup> The abundant C- and N-contained functional groups in EPS may serve as desirable sites for HMs anchoring inside the EPS cage, presenting a similar structure to the highly efficient SACs.<sup>5,17–19</sup> This may allow to center metals in the ligand with well-defined N coordination that will benefit adsorption or desorption of ECO<sub>2</sub>RR intermediates, and thus lowering the energy barriers. Recent studies show that SACs based on earth-abundant metals also lead to highly efficient ECO<sub>2</sub>RR.<sup>4,19</sup> For instance, Ni SACs with well-defined N coordination presents comparable selectivity (~95% Faradaic efficiency, FE) to the precious metals for  $CO_2$  to CO conversion,<sup>3,5,19,20</sup> where N<sub>x</sub>-Ni is the key site for  $CO_2$  reduction and exhibits weak CO binding energy to facilitate the

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https://doi.org/10.1016/j.isci.2024.109956





Figure 1. Schematic of co-utilization of wastewater sludge EPS and heavy metal to deliver electrochemical CO<sub>2</sub> conversion

desorption of CO (CO\*).<sup>20</sup> In contrast, the prevailing carbon matrices (e.g., CNTs, MOFs, COFs, and etc.) for N<sub>x</sub>-Ni formation are costly, developing the cheap and N-enriched alternatives are necessary. The WAS-derived EPS has plentiful N-contained functional groups, which can provide essential N element for N<sub>x</sub>-Ni formation during carbonization. So far, the use of N-rich wastes for SACs preparation is rarely reported.

In this study, we originally used WAS-derived EPS to capture Ni in the real wastewater and directly converted the EPS-Ni ligands into a Ni-SAs distributed gas diffusion electrode (GDE) through electrospinning coupled with carbonization (Figure 1). This novel strategy integrates both catalyst synthesis and electrode fabrication, thus simplifying the GDE manufacture process for cost reduction. Currently matured electrospinning technique allows to fabricate large-scale GDE with increased exposure of catalytic sites on the GDE nanofibers. The as-prepared GDE with hydrophobic treatment could be applied in the membrane electrode assembly (MEA) for direct gaseous CO<sub>2</sub> reduction into CO (Figures 1 and S1). This configuration significantly suppresses the preferred H<sub>2</sub> evolution in contentional liquid-phase CO<sub>2</sub> reduction, and demonstrates the enhanced ECO<sub>2</sub>RR kinetics due to a higher CO<sub>2</sub> diffusion coefficient (16 mm<sup>2</sup>·s<sup>-1</sup>) in gaseous-phase (vs. 0.0016 mm<sup>2</sup>·s<sup>-1</sup> in liquid-phase)<sup>21,22</sup> and the low electrochemical resistance resulted from the sandwiched configuration of MEA (Figure S1). The roles of individual EPS compositions (protein, polysaccharide, and humic acid) in the SACs formation and the corresponding ECO<sub>2</sub>RR performance and catalytic mechanisms were investigated. The results show the excellent CO selectivity (~75% FE<sub>CO</sub> and CO:H<sub>2</sub> ratio of ~100) with large current density of 50 mA·cm<sup>-1</sup> and the great potential for win-win on both resource recovery and environment remediation in large-scale.

### RESULTS

### Characterization of gas diffusion configuration of GDE<sub>EPS</sub>

The as-formed gas diffusion configuration of GDE<sub>EPS</sub> allows gaseous CO<sub>2</sub> to diffuse into the electrode inside for direct electrochemical reduction between the liquid and the gaseous phase. This conjunction of solid/liquid/gas interface enables to suppress competitive H<sub>2</sub> evolution reaction at a conventional solid/liquid interface.<sup>21–24</sup> Electrospinning method employed here is able to fabricate large-size GDE<sub>EPS</sub> with ~200 cm<sup>2</sup> (Figure S3), and its size can be further enlarged by using industrial-scale instrument. For the microscopic structure, electrospinning enables disordered stack of numerous fibers with diameter of ~300 nm (Figures 2A, 2B, and S4). Millimetric fractures spreading on the hydrophobic PTFE layer provides ample region for gas crossing since the dynamic diameter of CO<sub>2</sub> is merely 3.4 Å (Figures 2C and 2D).<sup>20</sup> The ~300-µm thick GDE<sub>EPS</sub> is full of cavities with various dimensions below the PTFE layer, capable of gas and liquid diffusion (Figures 2E and 2F). Exposure of ample Ni catalysts on the nanofibers' surface facilitates more contact between catalytic sites and CO<sub>2</sub> molecules (Figure 2G). BET result shows that GDE<sub>EPS</sub> is capable of CO<sub>2</sub> storage with ~8 cm<sup>3</sup>-CO<sub>2</sub> · g<sup>-1</sup>-GDE<sub>EPS</sub> under atmospheric pressure (Figure 2H). Type IV N<sub>2</sub> ad-desorption isotherm with meso-macropores distribution demonstrates well developed channels for gas diffusion.<sup>17</sup> The incremental pore volume mainly located between 50 and 250 nm further proves this opinion (Figures 2H–2J and S5). One side of GDE<sub>EPS</sub> was coated by one layer of PTFE with a contact angle of 112.19° (Figures 2K and S6). In an electrolyte penetration test using fluorescent dye, confocal laser scanning microscope detects a penetration depth of only a few micrometers for GDE<sub>EPS</sub> with PTFE layer, in contrast, the counterpart without





### Figure 2. Gas diffusional configuration of GDE<sub>EPS</sub>

Photographs and SEM images of GDE<sub>EPS</sub> surface without PTFE layer (A and B) and with PTFE layer (C and D). (E and F) SEM images of cross section of GDE<sub>EPS</sub>.

(G) Elemental mapping of GDE<sub>EPS</sub> surface.

(H–J) BET analysis.

(K) Contact angle of GDE<sub>EPS</sub> at PTFE layer.

(L and M) Confocal laser scanning microscope images of overlapped plane and cross section of GED<sub>EPS</sub> wetted by dye (1 M KOH/NaOH solution containing Rhodamine B) to show the penetration level on GED<sub>EPS</sub> surface by water. The color represents the different penetration depth in I, and the thickness of green stripe indicates the penetration depth in m.

PTFE layer was penetrated considerably with more than 50 µm depth (Figures 2L, 2M, and S7). These results indicate that the well hydrophobicity was provided by a PTFE layer.

The distribution of catalytic sites onto  $GDE_{EPS}$  (poised at -0.6 V vs. RHE) surface was detected by a scanning electrochemical microscopy equipped with a Pt ultramicroelectrode tip (poised at 0.84 V vs. RHE) that move across  $GDE_{EPS}$  surface to oxidizes the  $ECO_2RR$  products of CO







### Figure 3. Characterization of Ni SACs dispersed on the nanofibers of GDE<sub>EPS</sub>

Current signal images collected by a scanning electrochemical microscopy for (A and B) the microscopic structure of GDE<sub>EPS</sub> (plane or 3D contour charts) and (C) a whole GDE<sub>EPS</sub> (bright part) fixed by epoxy resin (dark part) with scanning step length of  $50 \sim 100 \text{ nm} \cdot \text{s}^{-1}$ .

(D–F) TEM and HAADF-STEM images of a single nanofiber of  $\mathsf{GDE}_{\mathsf{EPS}}.$ 

(G) Marginal TEM image of nanofiber with clear graphene-liked lattice.

(H) Aberration-corrected HAADF-STEM image of Ni single atoms that are highlighted by red cycles.

or H<sub>2</sub> to generate the current, which allows to image electrochemical activity (Figures 3A–3C and S8). The overall current distribution just like a wave with the waviness width of 200–300 nm (Figures 3A and 3B), consistent with the diameter of GDE<sub>EPS</sub> nanofibers, indicating that efficient catalytic sites are well located at each fiber's surface. As a comparison, the surface of epoxy resin used to fix GDE<sub>EPS</sub> presents ~0 current signals and a clear boundary formed between GDE<sub>EPS</sub> and epoxy resin (Figure 3C). Upon the nanometer and even atomic view, Ni SAs

**iScience** Article в ■GDE<sub>EPS</sub>-CO ØDE<sub>EPS</sub>-H₂ 0 GDE<sub>PR</sub>-CO <mark>⊘</mark>GDE<sub>PR</sub>-H<sub>2</sub> 100 -10 75





### Figure 4. Performance of GDE<sub>EPS</sub> for ECO<sub>2</sub>RR

(A) Faradic efficiency (FE) for CO and H2 production, (B) corresponding current density and (C) Tafel plots under different potentials as well as (D) long-term stability of GDE<sub>EPS</sub> (-0.8 V vs. RHE) that were tested in bulk solution using a single-chamber three-electrode electrochemical cell. The GDE<sub>EPS</sub> was also tested in a (E) MEA for examining (F) CO and H<sub>2</sub> selectivity, (G) cell voltage of MEA, (H) a molar ratio of CO to H<sub>2</sub> produced and the energy efficiency under different current densities as well as (I) long-term stability of GDE<sub>EPS</sub> under 40 mA·cm<sup>-2</sup> operation. A GDE<sub>PR</sub> fabricated by using pure protein as matrix is served as a control. Data are reported as average  $\pm$  SD.

are well dispersed onto the surface of nanofibers and surrounded by quantitative N element (Figure 3D-3H). No Ni nanoparticles are detected, indicating protein-rich EPS may prevent the Ni agglomeration. In contrast, we found that the Ni nanoparticles formed on the GDEs that were made by using polysaccharide and humic acid as matrix. Because the powders obtained by milling these GDEs were attracted by a neodymium magnet (Figure S9), which is an indicator of metal particles formed. This observation indicates the incapability of N-poor matrix to disperse or anchor Ni SAs. Interestingly, a GDE without matrix (manufacture by only N-contained supporting material of PAN) shows formation of both abundant Ni SAs and a few of Ni nanoparticles on the fibers (Figures S9-S12). This further approves the importance of N-doping for forming Ni SAs, and the introduction of N-poor matrixes may be detrimental to this process.

### Performance of GDE<sub>EPS</sub> for ECO<sub>2</sub>RR

The performance of GDE<sub>FPS</sub> for ECO<sub>2</sub>RR was tested in both bulk solution and a MEA (Figure 4). GC results reveal that H<sub>2</sub> and CO are only gaseous products, while H<sup>1</sup> NMR spectra does not identify the production of organic compounds in liquid (Figure S13). In the bulk solution,



the Faradic efficiency of CO production (FE<sub>CO</sub>) by GDE<sub>EPS</sub> reaches a maximum of 64.3% (-0.8 V vs. RHE, 9.96 mA·cm<sup>-2</sup>), which is comparable with ~71.8% of GDE<sub>PR</sub> (2.82 mA·cm<sup>-2</sup>) fabricated by using pure protein, the main composition in EPS, as matrix (Figures 4A and 4B). The higher current obtained by GDE<sub>EPS</sub> can be attributed to its larger conductivity. The fundamental single-electron transfer dominates the rate-limiting step with a Tafel slope of 192.2 mV·dec<sup>-1</sup> (Figure 4C). Applying GDE<sub>EPS</sub> as the cathode in the MEA (Figure 4E), the CO selectivity is remained even under the higher current density (~50 mA·cm<sup>-2</sup>). H<sub>2</sub> evolution is significantly suppressed (FE<sub>H2</sub> ~5%) due to the lack of H<sub>2</sub>O surrounding the cathode (Figure 4F). A molar ratio of CO to H<sub>2</sub> in MEA (~100) is far higher than that obtained in bulk solution using a singlechamber cell (~2.5) (Figures 4H and S14). However, the total Faradic efficiency of MEA (~75%) is lower than that in bulk solution (~95%), which could be attributed to the redox reaction occurred on the GDE material to consume the electron. The energy efficiency of MEA for CO production is around 50%–60% with a cell voltage between 2 V and 3 V (Figures 4G and 4H). Long-term operation under high current density of ~40 mA·cm<sup>-2</sup> demonstrates the durability of GDE<sub>EPS</sub> (Figures 4D and 4I). The GDE<sub>PR</sub> fabricated by the pure protein shows the similar performance as the GDE<sub>EPS</sub> in MEA (Figures 4 and S15). The thickness of the GDE plate on the electrocatalytic performance was also tested using 2 plates in 1 mm and 0.5 mm thickness, respectively. The 1 mm-thick plate was the employed GDE in this study, while the 0.5 mm-thick plate was sliced from the 1 mm-thick plate. However, the thickness seemed to show limited effect on CO evolution at the same potential window (Figure S16). Furthermore, the carbonization temperature of 800°C–1000°C also exerted limited effect on CO evolution (Figure S17), demonstrating that lower energy input can also prepare GDE with similar elect

### The role of different organic compositions of EPS in CO<sub>2</sub> reduction

The role of different organic compositions of EPS in ECO<sub>2</sub>RR was further investigated by using these compositions as matrixes to fabricate the ECO<sub>2</sub>RR catalysts (Figure 5). The onset potential of CO production by EPS-based catalyst is -0.4 V (vs. RHE), indicating that the overpotential is at least smaller than 0.29 V since the theoretical potential of CO<sub>2</sub> to CO conversion is -0.11 V (Figure 5A). The CO selectivity (FE<sub>CO</sub>) reaches the maximum of 50.2% at the potential between -0.7 V and -0.8 V, further applying the more negative potential will decrease the FE<sub>CO</sub>. Protein-based catalyst presents the highest FE<sub>CO</sub> of  $\sim$ 92.0% at -0.8 V vs. RHE (Figures 5A and S18). The polysaccharide and humic acid-based catalysts as well as the supporting material of PAN are more liable to produce H<sub>2</sub> over CO. Protein has abundant N-contained functional groups existed in the polysaccharide and humic acid.<sup>14,16</sup> Our results and many previous studies show that the N-doping is crucial in CO<sub>2</sub> reduction to CO,<sup>3,5,19,25</sup> since N-doping favors the formation of Ni SAs (Figure 2D–2H) and N<sub>x</sub>-Ni coordination that presents relatively weak binding energy for CO\*, an important intermediate during ECO<sub>2</sub>RR, and thus facilitates CO evolution.<sup>8,19</sup> In contrast, polysaccharide and humic acid-based catalysts as well as PAN with a little N-doping tend to form Ni particles (Figure S9), which are regarded as desirable catalysts for H<sub>2</sub> evolution. This was also supported by an observation that FE<sub>CO</sub> obviously increased after acid soaking of these catalysts to exclude Ni particles (Figure S10). Moreover, the control of catalyst fabricated by polysaccharide + PVA with no N-doping shows the lowest CO selectivity regardless of whether acid soaking, indicating the importance of N-doping. The difference in matrix also affects the current density of the catalysts (Figure SB), which is consistent with GDE performance (Figure 4B).

Tafel slopes partly explain reasons for the difference of CO selectivity. EPS, protein and PAN-based catalysts show the slopes of 187–198 mV·dec<sup>-1</sup> under the low overpotential window, indicating the capability to conduct CO<sub>2</sub> reduction in this range (Figures 5C and S19).<sup>8</sup> Humic acid and polysaccharide-based catalysts demonstrate the ultrahigh or even negative slope at the whole overpotential window, suggesting inactivity of catalytic sites for ECO<sub>2</sub>RR. Therefore, extremely low turnover frequencies (TOF) (<10 h<sup>-1</sup>, calculations were provided in SI) were observed for the polysaccharide and humic acid-based catalysts. Electrochemical double layer capacity, an indicator of the electrochemical structure, was used to calculate the TOF. However, no correlation between electrochemical double layer capacity and CO TOFs was observed (Figures 5D and 5E), indicating that other factors (e.g., the number of efficient catalytic sites, specific areas etc.) rather than electrochemical structure have more influence on CO<sub>2</sub> to CO conversion. The presence of small amounts of polysaccharide and humic acid (~10 wt %) in EPS-based catalyst (~90 wt % protein) (Table S2) is also detrimental to the CO evolution compared to the protein-based catalyst (Figure 5A) despite few Ni nanoparticles were detected in both catalysts, suggesting that these impurities (polysaccharide and humic acid) may impair the formation of efficient catalytic sites.

### The significance of N<sub>x</sub>-Ni formation on CO<sub>2</sub> reduction

The mass loading of Ni was below 1 at% in all catalysts (Figure S20). There is no obvious Ni crystal peak observed in the X-ray photoelectron spectroscopy (XPS) with no obvious peak of zero-valent Ni (852.6 eV) detected (Figure 6A), indicating these catalysts are capable of well dispersing Ni SAs. A peak between the 852.6 eV (zero-valent Ni) and 855.8 eV (entirely oxidized Ni) is observed, which represents partially oxidized Ni for Ni SAs.<sup>5,8,20</sup> For catalyst without any N-doping (polysaccharide + PVA), the visible peak of zero-valent Ni shows it is much more liable to form Ni particles (Figures 6A, S20, and S21). N<sub>x</sub>-Ni structure has been proved to be crucial for CO<sub>2</sub> to CO conversion.<sup>16,17,25</sup> The higher proportion of N<sub>x</sub>-Ni in the N 1s spectra was observed in EPS, protein and PAN-based catalysts, indicating numerous catalytic sites for CO<sub>2</sub> to CO conversion in these catalysts (Figure 6B). The N-contained functional groups in these catalysts may provide N element for the formation of N<sub>x</sub>-Ni. The obvious change in the N 1s spectra after Ni loading was observed for protein (3.49 at% N element) (Table S4; Figure S22), indicating that N-contained functional groups in protein participate in Ni anchoring. Interestingly, there is a negligible change in the N 1s spectra after Ni loading by EPS (14.26 at% N element), suggesting the C- and O-contained functional groups in EPS are more competitive than N-contained functional groups in seizing Ni. The Ni species in EPS- and protein-based catalysts show the higher valence than Ni<sup>2+</sup> (NiO and NiPc) and Ni<sup>0</sup> (Ni foil) due to their higher energy location than Ni<sup>2+</sup> and Ni<sup>0</sup> in X-ray absorption near-edge spectroscopy (XANES) and 1<sup>st</sup> derivation XANES spectra (Figures 6C and 6D). EPR results present



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(A) CO and H<sub>2</sub> selectivity, (B) current density, (C) Tafel plots, (D) electrochemical double layer capacitance, and (E) turnover frequency (TOF) of different ECO<sub>2</sub>RR catalysts fabricated by using different compositions of EPS as matrixes. The catalytic experiments were conduct in bulk solution using a single-chamber three-electrochemical cell. Data are reported as average ±SD.

a signal at 150–450 mT for both EPS- and protein-based catalysts, which also indicates the existence of high-valence Ni species in these catalysts (Figure 6E), and it was like +3 valent compared with studies of Zhecheva et al.<sup>26</sup> However, EPS-based catalyst displays a slight shift toward lower energy, indicating its Ni species have a lower valence than protein-based catalyst.<sup>24,25</sup>

Fourier transformed (FT)  $k^2$ -weighted extended X-ray absorption fine structure (FT-EXAFS) spectra (Figure 6F, 6G, and S23) and wavelet transform (WT) of  $\chi$ (k) spectra (Figure 6H) clearly demonstrate N-Ni coordination over Ni-O or Ni-Ni coordination in EPS- and protein-based catalysts. A coordination number of 3.6  $\pm$  0.3 suggests the presence of both N<sub>3</sub>-Ni and N<sub>4</sub>-Ni in EPS-based catalyst while the N<sub>4</sub>-Ni is dominant in protein-based catalyst with a coordination number of 4.1  $\pm$  0.2 (Table S6). Because the both pyridinic N and pyrrolic N were found in XPS splitting spectra, we propose the existence of 4 kinds of N<sub>x</sub>-Ni structures, namely pyrrolic N<sub>3</sub>-Ni and N<sub>4</sub>-Ni as well as pyridinic N<sub>3</sub>-Ni and N<sub>4</sub>-Ni, based on the results of XPS and EXFAS (Figure 6I). The results show that pyrrolic N<sub>4</sub>-Ni must exist in a coordination with some vacancies, which is different from pyrrolic N<sub>3</sub>-Ni and pyridinic N<sub>3</sub>-Ni/N<sub>4</sub>-Ni where vacancy is not necessary in the coordination. This is consistent with the previous finding that Ni is distinct than Fe, Co, Cu, Mn and etc. whose pyrrolic N<sub>4</sub>-metal coordination could exist without any









Figure 6. Characterizations of chemical bonds in different ECO<sub>2</sub>RR catalysts fabricated by using different compositions of EPS as matrixes (A) XPS spectra of Ni 2p, (B) XPS spectra of N 1s splitting peaks, (C) XANES spectra at the Ni K-edge, (D) the first derivate of XANES spectra, (E) EPR results, (F and G) the Fourier transform of EXAFS, (H) Wavelet transform (WT) of  $\chi$ (k) spectrum, and (I and J) proposed 4 N<sub>x</sub>-Ni structures and corresponding Gibbs free energy change during CO<sub>2</sub> to CO conversion.

vacancy.<sup>27,28</sup> Generally, the  $N_4$ -Ni coordination requires relatively lower energy for ECO<sub>2</sub>RR than  $N_3$ -Ni regardless of pyridinic or pyrrolic N coordination (Figures 6K and S24). This explains that why protein-based catalyst ( $N_4$ -Ni coordination) presents better ECO<sub>2</sub>RR performance than EPS-based catalyst (mixture of  $N_4$ -Ni and  $N_3$ -Ni coordination). In other hand, the existence of polysaccharide and humic acid will prevent the formation of  $N_4$ -Ni to lead to the poor ECO<sub>2</sub>RR performance.

### DISCUSSION

We extracted EPS from wastewater sludge to adsorb the Ni in electroplating wastewater, and the EPS-Ni mixture was then electrospun into an integrated GDE for the electro-conversion of CO<sub>2</sub> to CO. This strategy enabled the Ni dispersed onto the nanofiber's surface of the GDE in an atomic form, which delivered the desirable CO<sub>2</sub> conversion with >60% FE<sub>CO</sub>. The protein over polysaccharide and humic acid in the EPS was found as the foremost matrix to synthesize efficient catalyzing sites, as the N-enriched functional groups in protein provided quantitative N element for the formation of N<sub>X</sub>-Ni. The further analysis pointed that the mixture of N<sub>3</sub>-Ni/N<sub>4</sub>-Ni played the big role in CO<sub>2</sub> conversion, and the pyridinic N<sub>4</sub>-Ni portfolio was more preferable. Scaling up the current density and directly inserted the GDE into a MEA, the swift conversion of CO<sub>2</sub> to CO was also delivered with ~75% FE<sub>CO</sub> under 2.69 V cell voltage.

Annually, a huge amount of WAS is produced globally, leading to the great environmental risk and GHG emission. For example, around  $\sim$  30.8 million tons of sludge (dry weight) is produced in major economies, meaning that  $\sim$ 15.4 million tons of EPS could be reclaimed given  $\sim$ 50 wt % recovery ratio.<sup>2,29–31</sup> The medium C and N content in dry biomass are estimated to 31.39 wt % and 3.97 wt %, <sup>30</sup> equaling to 4.83 million tons C and 0.61 million tons N. The scenario of *in situ* CO<sub>2</sub> reduction in wastewater treatment plant can be divided into 4 steps, including the CO<sub>2</sub> feed, electrocatalytic process (both GDE manufacture and electrocatalysis), electrical energy input, and product separation (Figure S25). Herein, we assume that a direct feed of anaerobic digestion biogas (30–40% CO<sub>2</sub>) to the electrocatalytic process, without CO<sub>2</sub> capture procedure, will be conducted as well as a high Faradic efficiency (FE) for CO and H<sub>2</sub> production will be obtained (experiment shows an approximate 100% FE), thus the associated carbon-foot and cost derived from steps of CO<sub>2</sub> feed and product separation are excluded from the calculation. The analysis shows that a total of 0.67-ton CO<sub>2</sub> will be mitigated by generating one ton CO, with the consideration of CO<sub>2</sub> fixation in the GDE manufacture, CO<sub>2</sub> to CO conversion by electrocatalysis, and indirect CO<sub>2</sub> emission due to electricity consumption. A net profit of US\$1809 per ton CO-produced will be obtained by including the CO global market, CO production cost and the revenues due to wastes recovery and H<sub>2</sub> production (Detailed calculation was provided in Text S3).

Given that protein plays an important role in CO selectivity, other protein-rich wastes, such as soybean peptide and albumen wastes generated from food industry, have also been investigated for synthesizing the corresponding GDEs (labeled as  $GDE_{SP}$  and  $GDE_{AL}$ ), presenting similar CO selectivity as  $GDE_{EPS}$  (Figures S26 and S27). This shows a great potential for more CO<sub>2</sub>-CO conversion by using various N-rich wastes. This route can also be directly integrated with an anaerobic fermentation, where the target products of CO<sub>2</sub> reduction will be switched to 1C organics (e.g., formate and methanol) that subsequently return to the fermenter for *in situ* improving methanogenesis.

### Limitations of the study

Although the GDE<sub>EPS</sub> fabricated here shows characteristics of low-cost, sustainability, and the efficient CO<sub>2</sub> to CO conversion, two major challenges need to be resolved in future. The first is the inferior conductivity of GDE<sub>EPS</sub> compared with traditional CNTs, MOFs, and etc., which limits the current density in the MEA configuration. High current density (>200 mA · cm<sup>-2</sup>) is the threshold for the profit competing with other CO<sub>2</sub> conversion technologies. The second is the durability needed to be further extended. Despite the GDE<sub>EPS</sub> is relatively stable under high current density operation, there is still a gap between the performance and the practical scenario. Further surface modification of GDE<sub>EPS</sub> to simultaneously improve the conductivity and stability is the key to promote the application of GDE<sub>EPS</sub> for CO<sub>2</sub>-CO conversion.

### **STAR\*METHODS**

Detailed methods are provided in the online version of this paper and include the following:

- KEY RESOURCES TABLE
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### SUPPLEMENTAL INFORMATION

Supplemental information can be found online at https://doi.org/10.1016/j.isci.2024.109956.

### ACKNOWLEDGMENTS

This work was financially supported by the National Natural Science Foundation of China (22176046), Science Fund for Creative Research Groups of the National Natural Science Foundation of China (52321005), Shenzhen Science and Technology Program (KQTD20190929172630447, JCYJ20210324124209025 and GXWD20220811173949005), and Natural Science Foundation of Guangdong Province (2022A1515012016).

### **AUTHOR CONTRIBUTIONS**

B.Z. and L.L. conceived the experiments and wrote the manuscript. B.Z. did the material fabrication and characterizations as well as electrochemical measurement. Z.L., X.H., and C.Z. did material and electrochemical characterizations. S.P., M.Y., G.L., and Z.Z. prepared matrix for GDE synthesis. W.Z. provided insightful clues in designing the MEA. There is no competing interest within the authors.

### **DECLARATION OF INTERESTS**

L.L., B.Z., Z.L., and C.Z. are co-inventors on filed China patent ZL202210841460.1 related to a method for GDE fabrication based on electrospinning technology that incorporate discoveries included in this manuscript.

Received: March 7, 2024 Revised: April 9, 2024 Accepted: May 8, 2024 Published: May 10, 2024

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### **STAR\*METHODS**

### **KEY RESOURCES TABLE**

REAGENT or RESOURCE	SOURCE	IDENTIFIER
Chemicals, peptides, and recombinant proteins		
Wastewater sludge	Luofang wastewater treatment plant of Shenzhen, China	N/A
$H_2 IrCI_6 \cdot xH_2O$	Sigma-Aladdin	N/A
BCA kit	Thermo Scientific	N/A
Ni electroplating wastewater	Zhongchuang electroplating Co. Ltd. of Huizhou, China	N/A
GDE <sub>EPS</sub>	This paper	GDE <sub>EPS</sub>

### **RESOURCE AVAILABILITY**

### Lead contact

Further information and requests can be directed to the lead contact, Lu Lu (lulu@hit.edu.cn).

### **Materials** availability

There are restrictions to the availability of the prepared GDE<sub>EPS</sub> used in this study due to the claimed filed China patent ZL202210841460.1.

### Data and code availability

- Collected data on the figure and table, and detailed data of the prepared GDEs reported in this paper will be shared by the lead contact upon request.
- The article does not report any new code.
- Any additional information required to reanalyze the data reported in this paper is available from the lead contact upon request.

### **EXPERIMENTAL MODEL AND STUDY PARTICIPANT DETAILS**

This study does not use any experimental model.

### **METHOD DETAILS**

### **EPS** extraction from sludge

WAS with ~98% moisture content was obtained from a wastewater treatment plant in Shenzhen. EPS was extracted using modified alkalialdehyde extraction method.<sup>20</sup> Briefly, 6 mL acetaldehyde (35 wt%) were added into 300 mL sludge under icy bath and stir for 1 h, followed by adding 120 mL NaOH solution (1 M) for another 12 h reaction, finally, the dialysis of supernatant for 100 h to obtain solution containing EPS (~3 g·L<sup>-1</sup>) with molecular weight more than 1000 Dalton. The frozen-dried EPS was in faint-yellow (Figure S2).

### Treatment of the Ni-contained electroplating wastewater

Ni-contained electroplating wastewater was a combined wastewater obtained from a factory in Meizhou, Guangdong Province. Content and concentration of the main heavy metals in the electroplating wastewater were presented in Table S1. The raw 1 L wastewater was added with concentrated HNO<sub>3</sub> to adjust solution pH below 1. The acidified wastewater was followed by heated at 85°C for 1 h and then added with 50 mL 30% H<sub>2</sub>O<sub>2</sub>. This process was used to dissolve metal particles in the flocs in the wastewater. Then the wastewater filtered by a qualitative filter paper to exclude other particles or flocs. And the solution pH was then adjusted to 6-8 by 3 M NaOH addition.

### **GDE** fabrication based on electrospinning

One electrospinning solution containing EPS-Ni ligands was prepared by mixing Ni-contained electroplating wastewater (Table S1) with EPS solution, followed by ultrasonication (details in Supporting Information, SI). The mass ratio of EPS : Ni is around 50 : 1. Another electrospinning solution is 12 wt% polyacrylonitrile (PAN) served as a supporting material of membrane in N'N-Dimethylformamide (DMF). Two spinning solutions were separately injected into an electrospinning machine (TL-Pro-BM2020, Tongli Tech, China) with a roller collector of 10 cm in diameter and 15 cm in length by using a voltage of  $16\sim22$  kV at the two syringes and  $\sim$  -4 kV at the roller collector. The mass ratio of EPS to PAN is 1:1. The pristine GDE (Figure S3) was fabricated by  $40\sim50$  h electrospinning, which was then pre-oxidized at  $260^{\circ}$ C in a muffle furnace, followed by carbonization at 1000°C in a tube furnace under argon atmosphere protection. Finally, carbonized GDE<sub>EPS</sub> was coated by a layer of





polytetrafluoroethylene (PTFE) as the hydrophobic layer. Since protein is the dominant content of EPS (Table S2), pure protein of bovine serum albumin (BSA) was employed as a control of matrix to combine Ni for manufacturing GDE named GDE<sub>PR</sub>.

EPS as a very complex organic mainly consists of protein, polysaccharide and humic acid (Table S2). In order to investigate their roles on the coordination of SACs and the corresponding ECO<sub>2</sub>RR performance, we individually employed EPS, protein, polysaccharide and humic acid as matrixes to anchor Ni to produce the ECO<sub>2</sub>RR catalysts by using the similar process as manufacture of carbonized GDE without PTFE layer, but the GDEs were milled to powdery catalysts that are convenient for electrochemical tests. A blank of catalyst containing supporting material of PAN only (without any matrix) was prepared. To exclude the impact of N-doping, we also prepared another control of catalyst without N element by using N-free polyvinyl alcohol (PVA), another supporting material as PAN, to mix with N-free polysaccharide for production of Polysaccharide+PVA catalyst.

### **PTFE** layer preparation

60% polytetrafluoroethylene concentrated dispersions were brushed onto one surface of the GDE<sub>EPS</sub> and dried out naturally. The GDE<sub>EPS</sub> was heated in a furnace at 320°C for 10 minutes to allow the formation of PTFE layer.

### ECO<sub>2</sub>RR experiment

The ECO<sub>2</sub>RR performance of GDE<sub>EPS</sub> and GDE<sub>PR</sub> served as cathodes was tested in a customized membrane electrode assembly (MEA) with an IrO<sub>2</sub>-coated titanium mesh anode and a Fumasep-FAA-30 anion exchange membrane separator (Figure 3). The CO<sub>2</sub> gas was injected into the cathode with a flow of 20~50 standard cubic centimeter per minute (sccm). The anolyte is the 0.5 M KHCO<sub>3</sub> solution that was circulated by a peristaltic pump. The performance of catalysts derived from different composition of EPS was tested in a traditional single-chamber three-electrode electrochemical cell with a platinum counter electrode, an Ag/AgCl reference electrode and a carbon paper (Tory TGP-H-060) working electrode with normalized 2 mg  $\cdot$  cm<sup>-2</sup> catalyst powder loading. All electrochemical experiments were carried out using a potentiostat (1010E, Gamry, USA).

### **GDE** characterizations

Scanning electron microscopy (SEM) (TESCAN MIRA4), transmission electron microscopy (TEM) (FEI Talos F200X), and X-ray diffraction (XRD) (RIGAKU Ultima IV) were used to characterize the morphology and structure of GDE. Aberration-corrected scanning transmission electron microscopy (AC-STEM) (Titan Cubed Themis G2300) was used to identify Ni SAs. Porous structure was analyzed by a BET analyzer (Micrometrics ASAP 2460) using N<sub>2</sub>, and CO<sub>2</sub> gas was also applied to examine material's CO<sub>2</sub> storage ability. The hydrophilic or hydrophobic nature of GDE's surface was characterized by contact angle (KRUSS DSA25; Dingsheng JY-82) and the aqueous penetration that was probed by a confocal laser scanning microscope (Nikon AX-SHR). Heavy metals species and content were identified by an inductively coupled plasma mass spectrometry (NexION 1000, PerkinElmer). Chemical bonds and compositions were analyzed by an X-ray photoelectron spectroscopy (XPS) (Scientific K-Alpha). Gas products were identified and quantified by a gas chromatography equipped with a thermal conductivity detector (TRACE 1310, Thermo, USA). The liquid products were identified by a proton nuclear magnetic resonance (NMR) at 400 MHz (Bruker Avance NEO). The X-ray absorption near-edge spectroscopy (XANES) and extended x-ray absorption fine structure spectroscopy (EXAFS) were collected at a beamline BL44B2 by the SPring-8 synchrotron in Japan. The storage rings of SPring-8 were operated at 8.0 GeV with a maximum current of 250 mA. Using Si (111) double-crystal monochromator, the data collection was carried out in transmission mode using ionization chamber. The k<sup>3</sup>-weighted EXAFS spectra were obtained by subtracting the post-edge background from the overall absorption and then normalizing with respect to the edge-jump step. Subsequently,  $k^3$ -weighted  $\chi(k)$  data of Ni K-edge were Fourier transformed to real (R) space using a Hanning window (dk=1.0 Å<sup>-1</sup>) to separate the EXAFS contributions from different coordination shells. All spectra were collected in ambient conditions. The chemical valent of Ni SAs was detected by electron paramagnetic resonance (EPR) (EMXnano, Bruker, Germany) with magnetic field between 100-600 mT. The surface electro-activity of GDE<sub>EPS</sub> was characterized by a scanning electrochemical microscopy (SCEM) (Versascan, Ametek) equipped with a position system, two potentiostats (VersaSTAT 3/3F) and a microprobe (\$25 \mu Pt microprobe) using substrate generation/tip collection (SG/TC) model. All details in material characterization were provided in SI.

### Measurement of protein, polysaccharide and humic acid content in EPS

Protein was colored by standard BCA kit (Pierce™ BCA Protein Assay Kit, Thermo Scientific, USA), and an enzyme-labeled instrument (Synergy H1, Biotek, USA) was employed to detect protein content at 562 nm. Phenol-sulfuric acid method was applied to detect the content of poly-saccharide by an UV-Vis spectrophotometer (GENESYS 150, Thermo Scientific, USA) at 485 nm. Folin-Lowry method detected humic acid content by an UV-Vis spectrophotometer at 735 nm.

### Calculations

Potentials reported in this study versus reversible hydrogen electrode (RHE) were derived from converting detected values according to Nernst equation:

 $E vs RHE = E vs Ag/AgCl + 0.197 + 0.059 \times pH$ 





Partial current density for given gas products was calculated by the following formula:

$$j_i = x_i \times v \times z_i \times F \times P_0 \times electrode area / (RT)$$

Where,  $j_i$  (mA·cm<sup>-2</sup>) is the partial current density;  $x_i$  (ppm) is the volume fraction of given gas product *i*; v (sccm) is the flow rate;  $z_i$  is the number of transferred electrons;  $F(C \cdot mol^{-1})$  is the Faraday constant;  $P_0$  equals to 101.325 kPa;  $R(J \cdot mol^{-1} \cdot K^{-1})$  is the gas constant; and T(K) is the temperature. The corresponding Faradic Efficiency (FE, %) was deduced as the follow:

$$FE = j_i / j_{total} \times 100\%$$

Where,  $j_{total}$  (mA·cm<sup>-2</sup>) is the total current density. Energy efficiency (%) can be calculated as the follows:

Energy efficiency = 
$$(E^0 \times FE_{CO})/E_{cell} \times 100\%$$

$$E^0 = E_{O2} - E_{CO} = 1.23 V - (-0.11 V) = 1.34 V$$

Where, E<sub>O2</sub> (V) and E<sub>CO</sub> (V) are O<sub>2</sub>/H<sub>2</sub>O and CO<sub>2</sub>/CO equilibrium potential, respectively; E<sub>cell</sub> is a voltage applied to the MEA.

### **Evaluation of turnover frequency (TOF)**

TOFs(h<sup>-1</sup>) for ECO<sub>2</sub>RR products were evaluated based on the electrochemical active surface area (ECSA) normalization proposed by Jiang et al.<sup>5</sup> and Chen et al.<sup>32</sup> The ECSA results were presented in Table S3, which were calculated according to 21  $\mu$ F·cm<sup>-2</sup> of reported electrochemical double layer capacity (EDLC) of graphene. Then the moles of C atoms were estimated by the formula: ESCA/(specific surface area)×12 (Table S3). And considering the Ni atomic content in the membrane electrode (XPS result, Table S3). Then TOFs based on ESCA normalization was calculated by ( $j_{total} \times t \times FE_{CO}$ )/(2F×the number of Ni sites).

#### Calculation of potential carbon-foot and economic benefits in practice

The calculations of potential carbon-foot and economic benefits are based on following 4 steps (Figure S23) including the CO<sub>2</sub> feed (Step 1), the preparation of GDE<sub>EPS</sub> and the conversion of CO<sub>2</sub> (Step 2), electricity input (Step 3) and product separation (Step 4). We consider the emission and fixation of CO<sub>2</sub> during GDE manufacture and electrocatalysis, CO<sub>2</sub> emission associated with electrical energy consumption, the cost of GDE manufacture, and the economic benefits derived from sludge treatment, heavy metal recovery and H<sub>2</sub> production. The energy consumption and cost for the CO<sub>2</sub> capture and CO separation as well as transportation of the raw materials and products were not considered. The detailed calculations were provided as follows:

### Carbon footprint

Step 1: In this study, we assumed that a direct feed of anaerobic digestion biogas (30-40% CO<sub>2</sub>) to the electrocatalytic process. We did not consider the cost of the purification of CO<sub>2</sub>, and thus no emission or conversion or fixation of CO<sub>2</sub> occurred in the Step 1. The CO<sub>2</sub> emission was 0 ton-CO<sub>2</sub>-eq/ton-CO-produced.

Step 2: This step calculated the fixed CO<sub>2</sub> in GDE<sub>EPS</sub> and converted CO<sub>2</sub>. Globally, annual ~30.79 million tons sludge (dry weight) were produced in major economies, meaning that ~15.4 million tons EPS could be reclaimed given ~50 wt% biomass ratio in the sludge.<sup>29,30</sup> The medium C and N content in dry biomass are estimated to 31.39 wt% and 3.97 wt%,<sup>30</sup> equaling to 4.83 million tons C-eq/year or 17.72 million tons CO<sub>2</sub>-eq/year 0.61 million tons N-eq/year. The CO<sub>2</sub> fixed amount is 0.70 ton-CO<sub>2</sub>-eq/ton-CO-produced.

For the converted  $CO_2$ , the durability of each GDE<sub>EPS</sub> is set at 4 h and 70% FE<sub>CO</sub> and 30% FE<sub>H2</sub> are considered as the average value when current operation is under 40 mA/cm<sup>2</sup>. Therefore, one ton EPS annually capturing  $CO_2$  amount can be calculated as the following equation:

 $CO_2$  capture amount =  $x_{CO} \times v \times 60 \times 24 \times 365 / [EPS amounts in per cm<sup>2</sup> \times (365 \times 24 / 4)]$ 

Where,  $x_{CO}$  is the volume fraction of CO; v (sccm) is the CO<sub>2</sub> flow rate; EPS amount in one cm<sup>2</sup> is as follows:

EPS amount in per cm<sup>2</sup> = EPS addition during electrospinning / (pristine GDE<sub>EPS</sub> area × contraction factor)

Where, the pristine GDE<sub>EPS</sub> is  $\sim$ 450 cm<sup>2</sup> (the GDE collector was a roller in diameter of 10 cm and in width of 15 cm) with 10 g EPS as the matrix. After preoxidation and carbonization, the final GDE<sub>EPS</sub> shrinks to around 30% in size of the pristine one, thus the contraction factor is 0.7.

The optimal C capture can come to 40.02 million tons  $CO_2$ -eq/year or 1.57 ton- $CO_2$ -eq/ton-CO-produced. 0.03 ton- $H_2$ -eq/ton-CO-produced can be harvested at the same time.

**Step 3**: This step calculated the energy-related CO<sub>2</sub> emission which was used for the manufacture of GDE<sub>EPS</sub> and CO<sub>2</sub>-CO conversion. And the energy was derived from the combustion of fossil fuels. According to the energy limitation to produce common graphene (6440 kW·h/ton), carbonizing annual EPS yield into GDE<sub>EPS</sub> (mass ratio of EPS : PAN is 1:1) consumed 15.4 million tons  $\times 2 \times 6440$  kW·h/t = 198.36 billion kW·h, relative to 24.38 million tons standard coal combustion and 65.58 million tons CO<sub>2</sub> emission or 2.58 ton-CO<sub>2</sub>-eq/ton-CO-produced (1 kW·h electricity generation needs 0.1229 kg standard coal combustion, and the combustion of 1-ton standard coal equaled 2.69 tons CO<sub>2</sub> emission based on the proposed value of 2.66-2.72 tons CO<sub>2</sub> emission from the combustion of 1-ton standard coal, this data was suggested by Nation Development and Reform Commission of China and National Bureau of Statistics). However, this





data can be further decreased to 1.52 ton-CO<sub>2</sub>-eq/ton-CO-produced considering that only 58.9% energy was from the combustion of fossil fuels in the electricity grid.

The energy input for converting  $CO_2$  to CO was based on the energy efficiency (EF, 52.34%) and the relationship between the change of Gibbs free energy and electromotive force:

$$\Delta G = - n \cdot F \cdot E$$

$$N = \Delta G / EF \times converted CO_2$$

Where,  $\Delta G$  (J) is the change of Gibbs free energy; *n* is the number of transferred electrons (2); *F* is Faradic constant (96485 C/mol) *E* is the electromotive force between CO and CO<sub>2</sub> (-0.11 V); W is the real energy for CO<sub>2</sub> to CO (10.25 billion kW·h). The corresponding CO<sub>2</sub> emission was 3.39 million tons CO<sub>2</sub>-eq/year or 0.13 ton-CO<sub>2</sub>-eq/ton-CO-produced. And it can be decreased to 0.08 ton-CO<sub>2</sub>-eq/ton-CO-produced given the current electricity mix.

Step 4: This study did not consider the cost and energy for the separation/purification of the produced CO and  $H_2$ , and thus the emission or fixation/conversion of CO<sub>2</sub> was 0 ton-CO<sub>2</sub>-eq/ton-CO-produced in the Step 4.

Total CO<sub>2</sub> fixation or conversion: Step 1 + Step 2 - Step 3 + Step 4 = 0 + 0.7 + 1.57 - 1.52 - 0.08 + 0 = 0.67 ton-CO<sub>2</sub>-eq/ton-CO-produced.

### Economic benefits

Step 1: In this study,  $CO_2$  was from the fermenters of sludge or wastewater. We did not consider the cost of the purification of  $CO_2$ , no cost or economic yield was generated.

**Step 2**: The cost of manufacture of GDE<sub>EPS</sub> and electrolysis includes the expenditure for PAN and the energy. The cost of PAN is 1234 US\$/ ton, equaling to  $\sim$ 752 US\$/ton-CO-produced (mass ratio of PAN : EPS is 1 : 1). Total energy input is 208.61 billion kW·h (198.36 billion kW·h for GDE<sub>EPS</sub> manufacture and 10.25 billion kW·h for CO<sub>2</sub>-CO conversion) means 37.34 billion US\$ for electricity considering the average price of electricity of 0.179 US\$/kW·h globally. The corresponding energy cost of one ton produced CO is  $\sim$ 1466 US\$/ton-CO-produced.

Step 3: Some revenues can also be generated from the alternatives from sludge treatment, Ni recovery and byproducts H<sub>2</sub>. The average cost of sludge treatment is ~205 US\$/ton,<sup>33</sup> which equals to ~248 US\$/ton-CO-produced. Based on the mass ratio of 1 : 1of EPS : Ni, around 0.31 million tons Ni can be recovered annually, which equals ~243 US\$/ton-CO-produced considering the cost of Ni is 20000 US\$/ton-Ni.<sup>34</sup> The average price of H<sub>2</sub> is 6500 US\$/ton-H<sub>2</sub>.<sup>35</sup> which equals to revenue of ~199 US\$/ton-CO-produced.

Step 4: This study did not consider the cost and energy for the separation/purification of the produced CO and H<sub>2</sub>, and thus no cost or economic yield was generated in the Step 4.

The cost for producing one ton CO in this study was estimated to be: 752 + 1466 = 2218 US\$/ton-CO-produced. The potential economic from the waste recovery (sludge and heavy metals) and H<sub>2</sub> generation was estimated to be: 248 + 243 + 199 = 690 US\$/ton-CO-produced. The global price of CO is 3337 US\$/ton-CO. Thus, the total economic benefits for producing ton CO were to be estimated: 3337 + 690 - 2218 = 1809 US\$/ton-CO-produced.

### QUANTIFICATION AND STATISTICAL ANALYSIS

The presented data in this paper are in average value  $\pm$  SD with triplication.