



## Short Communication

## Hydrogen peroxide production in a pilot-scale microbial electrolysis cell

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## ABSTRACT

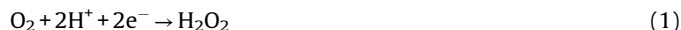
A pilot-scale dual-chamber microbial electrolysis cell (MEC) equipped with a carbon gas-diffusion cathode was evaluated for H<sub>2</sub>O<sub>2</sub> production using acetate medium as the electron donor. To assess the effect of cathodic pH on H<sub>2</sub>O<sub>2</sub> yield, the MEC was tested with an anion exchange membrane (AEM) and a cation exchange membrane (CEM), respectively. The maximum current density reached 0.94–0.96 A/m<sup>2</sup> in the MEC at applied voltage of 0.35–1.9 V, regardless of membranes. The highest H<sub>2</sub>O<sub>2</sub> conversion efficiency was only 7.2 ± 0.09% for the CEM-MEC. This low conversion would be due to further H<sub>2</sub>O<sub>2</sub> reduction to H<sub>2</sub>O on the cathode or H<sub>2</sub>O<sub>2</sub> decomposition in bulk liquid. This low H<sub>2</sub>O<sub>2</sub> conversion indicates that large-scale MECs are not ideal for production of concentrated H<sub>2</sub>O<sub>2</sub> but could be useful for a sustainable in-situ oxidation process in wastewater treatment.

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## 1. Introduction

Microbial electrochemical or electrolysis cells (MECs) are considered a potential sustainable platform for energy-efficient wastewater treatment, due to resource recovery and wastewater treatment. Because of the dual benefits, MECs have gained tremendous attention in the last decade [1,2]. Several studies have attempted pilot-scale MECs for either electricity or H<sub>2</sub> production [3–5] to deploy MECs in field. However, none of these studies provided significant benefits of the recovered resource against input energy and materials.

H<sub>2</sub>O<sub>2</sub>-producing MECs can give significant profits over other MECs due to high cost and demand of H<sub>2</sub>O<sub>2</sub> [6]. In addition, the recovered H<sub>2</sub>O<sub>2</sub> from organic waste or wastewater can be used as an in-situ oxidant in wastewater treatment, improving the sustainability of wastewater management. Similar to a conventional MEC system, H<sub>2</sub>O<sub>2</sub>-producing MECs comprise of two chambers separated by an ion exchange membrane. A solution containing dissolved organic matter is fed to the anode chamber where anode-respiring bacteria (ARB) such as *Geobacter* sp., *Pseudomonas* sp., *Shewanella* sp., etc. oxidize the organics and use the anode as the electron sink [7–10]. The electrons flow through an external circuit to the cathode where oxygen is electrochemically reduced to H<sub>2</sub>O<sub>2</sub> at the cathode surface by the two-electron pathway shown in Eq. (1) below [11]:



All studies to date have examined H<sub>2</sub>O<sub>2</sub>-MECs at the lab scale, investigating H<sub>2</sub>O<sub>2</sub> conversion efficiency, reactor design, electrode materials, and so on [11–14]. These lab-scale experiments have commonly showed high potential of H<sub>2</sub>O<sub>2</sub>-MECs, but scale-up tests are essential to demonstrate performance and benefits of the MECs; however, no large-scale MECs for H<sub>2</sub>O<sub>2</sub> generation have been conducted yet.

This study is the first pilot-scale MEC (110 L) experiment for H<sub>2</sub>O<sub>2</sub> production. The pilot MEC was featured with anode modulation for provision of high surface area for biofilm formation and passive oxygen diffusion to a non-Pt carbon cathode. To evaluate the effect of catholyte pH on H<sub>2</sub>O<sub>2</sub> yield, the pilot-scale MEC fed with acetate medium was run using an anion exchange membrane (AEM) and a cation exchange membrane (CEM), respectively, as electrode separator. Performance of the MEC was summarized, focusing on electrode potential, current density, pH, and H<sub>2</sub>O<sub>2</sub> yield.

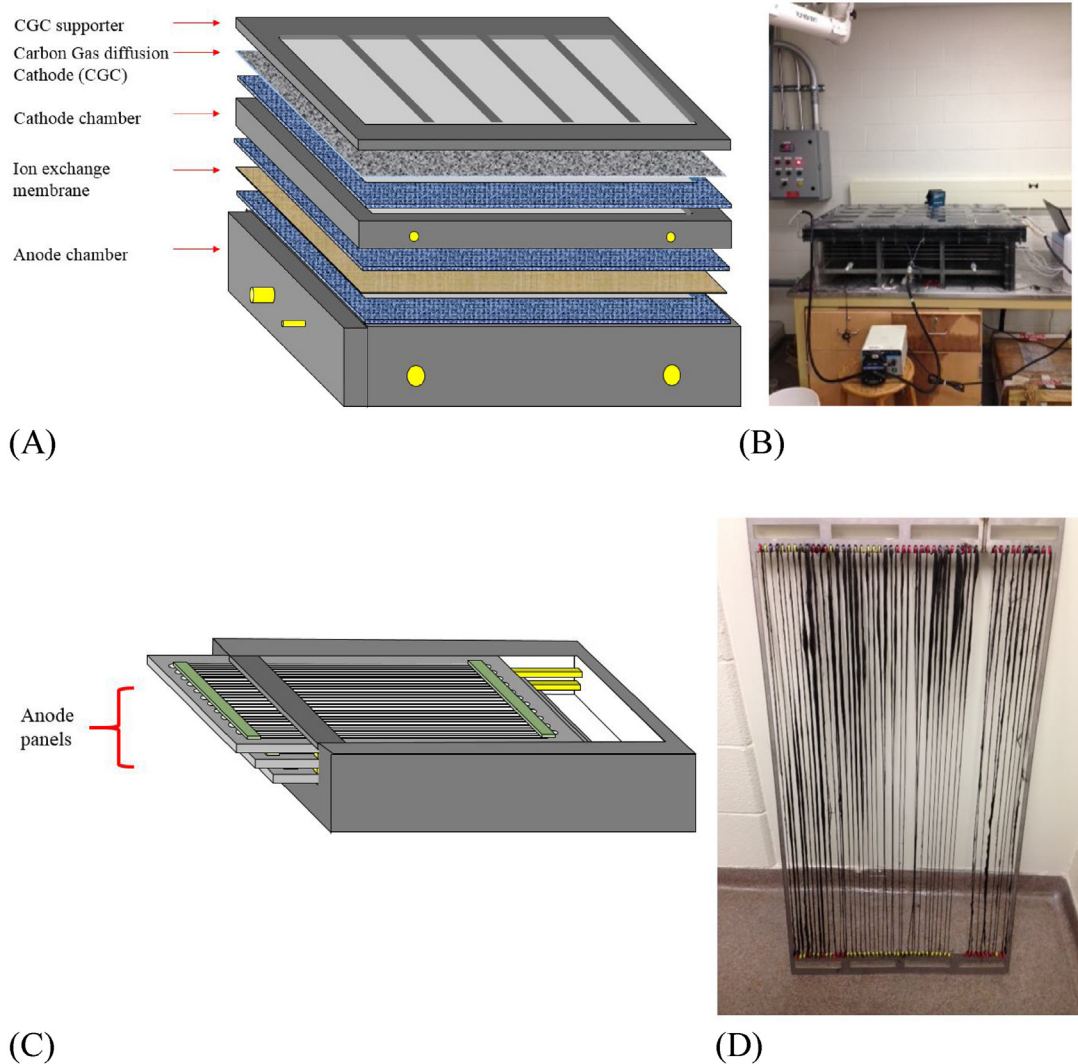
## 2. Materials and methods

## 2.1. Reactor configuration

Fig. 1 presents the schematic diagram and the picture of the pilot-scale MEC. The system has a dual-chamber configuration equipped with bioanode modules and a gas diffusion cathode (the anode chamber 1 m × 0.5 m × 0.2 m and the cathode chamber 1 m × 0.5 m × 0.02 m). The volumes of the anode and a cathode chamber were 100 L and 10 L, respectively. To provide the large

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**Fig. 1.** Schematic diagram of a large-scale microbial electrochemical cell (MEC). (A) MEC components, (B) photo of the MEC, (C) anode modulation, and (D) photo of an anode module.

surface area for biofilm formation without increasing footprint of the MEC, the anode was fabricated by connecting carbon fibers (2293-A, 24A Carbon Fiber, Fibre Glast Development Corp., Ohio, USA) to a stainless current collector, as shown in Fig. 1B. The MEC was equipped with five anode modules (Fig. 1C), providing a specific surface area of  $1.27 \text{ m}^2/\text{m}^3$  anode. The carbon fibers were pretreated with nitric acid (1 N), acetone (1 N), and ethanol (1 N), and finally washed with tap water before use [15]. Peristaltic pumps (Masterflex L/S Economy Drive 7554-90, Cole-Parmer, USA) were used to circulate both anolyte and catholyte at a flow rate of 2 L/min for mixing.

Cathode catalyst selection is one of the critical parameters in  $\text{H}_2\text{O}_2$  producing MECs. Precious-metal-free carbon cathodes are preferred for  $\text{H}_2\text{O}_2$  production [16,17]. When using precious metal-based catalysts like platinum, the four-electron oxygen reduction to water (Eq. (2)) many outcompete the two-electron reduction to  $\text{H}_2\text{O}_2$  (as shown in Eq. (1)).



Due to advantages of high conductivity, low cost, long-term stability and low catalytic activity of  $\text{H}_2\text{O}_2$  decomposition to water, carbon-gas diffusion electrode (GD2230, Fuel Cell Earth, USA) was used as the cathode (called, carbon gas-diffusion cathode (CGC) in

this study. Passive diffusion of  $\text{O}_2$  from atmosphere through the CGC, means no energy requirement for oxygen supply to the cathode in the MEC. An anion exchange membrane (AEM) (AMI-7001, Membranes International Inc., USA) having a surface area of  $0.5 \text{ m}^2$  was used for the MEC, which was later replaced with a cation exchange membrane (CEM) (CMI-7000, Membranes International Inc., USA) for comparison.

## 2.2. Inoculation and operation

The pilot MEC equipped with AEM was inoculated with effluent from lab-scale MECs (3.5 L of anolyte) operated with acetate medium, and was fed with 20 mM acetate medium [15]. The medium was sparged with ultra-pure nitrogen (99.999%) for 30 min. Then,  $\text{FeCl}_2 \cdot 2\text{H}_2\text{O}$  (20 mM) and  $\text{Na}_2\text{S} \cdot 9\text{H}_2\text{O}$  (77 mM) were added to acetate medium (1 mL per L). The pH in acetate medium was constant at  $7.3 \pm 0.1$ . The cathode chamber was filled with tap water. The AEM-MEC had been run in batch mode ( $\sim 4$  months) until a peak current density of  $\sim 0.9 \text{ A}/\text{m}^2$  ( $\sim 0.45 \text{ A}$ ) was repeatedly observed in the MEC. Then, experimental data was collected in the batch pilot MEC. AEM was replaced with CEM later, and the CEM-MEC was operated for comparison experiments.

To monitor voltage and electrode potentials, a saturated calomel electrode (SCE) (MF-2052, Bioanalytical System Inc. (BASI), USA) was used as the reference electrode placed in the anode chamber; here, electrode potentials were reported against SCE reference electrode. The anode modules and the cathode were connected to a data logging system (Keithly 2700, Keithly Instruments, Inc. USA) with copper wires [18]. The power supply (Array 3654A, Array Electronic co., LTD, China) was utilized as an external voltage supplier, and applied voltage was adjusted manually daily to maintain anode potential between  $-0.3$  and  $-0.5$  V vs SCE in which kinetically efficient ARB can be enriched well [15,19,20]. A pH probe (RK-27003-12, Cole-Parmer, USA) was installed in the anode chamber and connected to a meter (ECPHCP0550, Eutech Instruments, USA) to continuously monitor anolyte pH. For measuring catholyte pH,  $H_2O_2$  concentration, and anolyte COD concentration, approximately 10 mL of liquid samples were taken.

### 2.3. Analytical method and computation

$H_2O_2$  concentration was determined spectrophotometrically with vanadate, according to the literature [21] and the  $H_2O_2$  conversion efficiency was calculated using Eq. (3);

$$\text{Conversion efficiency} = \frac{n \cdot F \cdot V \cdot C}{Q} \quad (3)$$

where  $n$  is the number of electrons transferred per mole  $H_2O_2$  generated ( $2 \text{ mol } e^-/\text{mol } H_2O_2$ )  $F$  is Faraday's number ( $96,485 \text{ C/mol } e^-$ ),  $V$  is the catholyte volume (10 L),  $C$  is the concentration of  $H_2O_2$  measured, and  $Q$  is the cumulative coulombs during operation (C).

COD measurement was carried out spectrophotometrically using the dichromate method [22]. Chemical analyses were carried out in triplicate and standard deviations were reported with average values.

## 3. Results and discussion

### 3.1. Voltage, electrode potential, current density, and COD removal

The peak current density was  $0.94\text{--}0.96 \text{ A/m}^2$  ( $0.47\text{--}0.48 \text{ A}$ ) during the experiments. This current density is much lower than  $\sim 10 \text{ A/m}^2$  in MECs fed with acetate medium, although the enrichment procedure and inoculum used in this pilot was the same to our lab scale MECs showing  $\sim 10 \text{ A/m}^2$  [23]. The significant difference in this work is the size of the MEC is several orders of magnitude larger than lab scale MECs, which suggests the importance of ARB enrichment in full scale MECs. To enrich *Geobacter* in the biofilm anode of the pilot MEC, we only used the effluent from lab-scale MECs, instead of recycle activated sludge or anaerobic digestion sludge. Despite long acclimation for  $\sim 4$  months, the maximum current density was less than  $1 \text{ A/m}^2$ . This result means that biomass density would be very small in the biofilm anode, although five anode modules were installed to provide large surface area to ARB's biofilm formation. This suggests the significance of inoculation or bio-augmentation in large-scale MECs.

The anode potential ( $E_{\text{anode}}$ ) in the AEM-MEC and the CEM-MEC was kept relatively stable at  $-0.3$  and  $-0.5$  V (vs SCE) during operation. In comparison, significant polarization was observed for the cathode potential ( $E_{\text{cathode}}$ ), ranging from  $-2.0$  to  $-2.4$  V (applied voltage  $1.6\text{--}2.0$  V) and from  $-1.4$  to  $-2.0$  V (applied voltage  $1.0\text{--}1.6$  V) in the AEM-MEC and the CEM-MEC, respectively (see Supporting information). The applied voltage is relatively higher than literature values from  $0.2$  to  $1.3$  V [11,24]. The abrupt declines in the  $E_{\text{cathode}}$  (on Day 1, 2, 3, 4, 5, 10, 12, 13, 14, 15, and 17

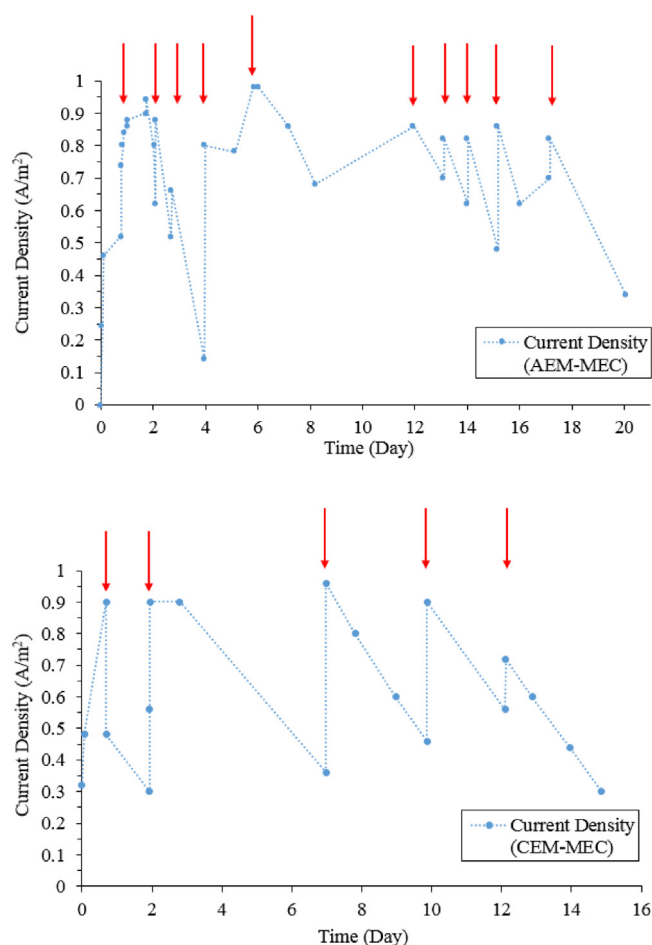


Fig. 2. The evolution of current density in the MEC. Red arrows indicate addition of tap water into the cathode due to catholyte evaporation.

for the AEM-MEC, and Day 1, 2, 7, 10 and 12 for the CEM-MEC) were found, probably due to water evaporation in the cathode chamber, leading to poor contact with the cathode and consequently substantial cathodic polarization in the MEC. To overcome this operational challenge, fresh tap water was manually added to the cathode chamber. Fig. 2 demonstrates the sharp increase of current density after refilling catholyte with tap water. The CGC was installed on an exterior side of the reactor for passive air diffusion, but this study showed that in practice this cathode design can cause water evaporation in the cathode chamber and significant cathode overpotential, requiring a regular makeup of catholyte (tap water in this work). Initial COD concentration of  $\sim 1000 \text{ mg/L}$  was gradually decreased with time due to metabolism of ARB (Supporting information). The final COD concentration was  $229 \pm 1.0 \text{ mg/L}$  and  $504 \pm 32 \text{ mg/L}$ , respectively, for the AEM-MEC and the CEM-MEC at the end of batch operation (20 d for the AEM-MEC and 16 d for the CEM-MEC). Although fresh tap water was added to the anode at the end of operation (20 d and 16 d), current density was not recovered, implying anodic limitation. Accumulated acetate indicates that substrate would not account for abrupt reduction of current density in the MEC, implying other influential parameters, such as acidic pH in anolyte.

### 3.2. pH changes in anolytes and catholytes

In both AEM-MEC and CEM-MEC, the anolyte pH was gradually decreased with time; the final pH was  $\sim 6.5$  after 15–20 d of batch operation (Supporting information). This acidic pH can significantly

inhibit ARB's metabolism and decrease current density [19], which is able to account for abrupt decline of current density even in the presence of acetate at the end of batch operation ( $503.76 \pm 32.30$  mg COD/L for the AEM-MEC and  $229 \pm 1.0$  mg COD/L for the CEM-MEC). Proton accumulation in the anode was not expected for the AEM-MEC because  $\text{OH}^-$  accumulated in  $\text{O}_2$  reduction to  $\text{H}_2\text{O}_2$  can transfer from the cathode to the anode for charge neutrality in dual chamber AEM-MECs where neutral pH was kept well in the anode [11,15,25]; moles of  $\text{OH}^-$  accumulated in the  $\text{O}_2$  reduction in the cathode are equivalent to moles of protons generated from ARB's acetate oxidation in the anode. Cathodic pH in the CEM-MEC was increased by 11.4 much higher than cathodic pH 9.7 in the AEM-MEC, which supports  $\text{OH}^-$  transfer from the cathode to the anode in the AEM-MEC. The acidic anolyte in the AEM-MEC implies that the  $\text{OH}^-$  did not neutralize all protons generated in the anode, and additional protons would be produced in the anode. The anode chamber placed on the bottom of the AEM-MEC did not have a separate gas outlet, leading to proton production from the dissolution of  $\text{CO}_2$  generated from ARB's acetate oxidation ( $\text{CO}_2 + \text{H}_2\text{O} \rightarrow \text{H}^+ + \text{HCO}_3^-$ ). As shown in Fig. 1, the cathode chamber was designed on the top of the MEC, forcing the anode chamber at the bottom of the MEC without gas outlets. It was challenging to design gas outlets in the anode because we could not create headspace in the anode chamber of the horizontally stacked MEC. This result indicates that MECs should be vertically stacked to have headspace in the anode chamber to mitigate anolyte acidification due to  $\text{CO}_2$  dissolution. In addition, ion exchange membranes can be swallowed during operation of MECs, providing small headspace in the anode. Then, biogas in the anode might be built up, accelerating membrane expansion and possibly deteriorating ion transport due to a gap between membrane and anolyte (increase of ohmic resistance). Alternatively, partial circulation of alkaline catholyte to the anode can readily neutralize acidic anolyte, but it will decrease  $\text{H}_2\text{O}_2$  recovery. Catholyte circulation can be an effective solution to neutralize acidic anolyte if produced  $\text{H}_2\text{O}_2$  is directly utilized to oxidize reduced forms of contaminants (e.g., BOD) in the anode chamber.

### 3.3. $\text{H}_2\text{O}_2$ concentration and conversion efficiency

The MEC designed for passive air diffusion to the non-Pt carbon cathode successfully produced  $\text{H}_2\text{O}_2$ , but  $\text{H}_2\text{O}_2$  production (Fig. 3) was very low as compared to literature showing high conversion of 80–90% in small-scale (<0.6 L)  $\text{H}_2\text{O}_2$  MECs [12,13]. In the AEM-MEC, the cumulative  $\text{H}_2\text{O}_2$  concentration was only  $9.0 \pm 0.38$  mg/L ( $p = 0.007$ ) in 20d operation, and  $\text{H}_2\text{O}_2$  conversion efficiency was extremely low at  $0.35 \pm 0.05\%$  ( $p = 0.050$ ). For the CEM-MEC in 15d operation, the cumulative  $\text{H}_2\text{O}_2$  concentration was  $98.48 \pm 1.6$  mg/L ( $p = 0.007$ ) with  $\text{H}_2\text{O}_2$  conversion efficiency of  $7.2 \pm 0.09\%$  ( $p = 0.006$ ).

An abiotic test using a small electrolysis cell showed that  $\text{H}_2\text{O}_2$  conversion efficiency approached to 100% in a catholyte continuous flow electrolysis cell as hydraulic retention time in a cathode chamber was changed from 10 to 0.6 min (Fig. 4). This supplementary test suggests that  $\text{H}_2\text{O}_2$  would be formed at the cathode first and then either lost by further reduction to  $\text{H}_2\text{O}$  at the cathode or by  $\text{H}_2\text{O}_2$  decomposition in the bulk liquid. This study did not investigate which mechanism mainly account for  $\text{H}_2\text{O}_2$  loss, but clearly presents that MECs are poor for recovery of concentrated  $\text{H}_2\text{O}_2$ . Preventing significant, spontaneous  $\text{H}_2\text{O}_2$  loss seems very challenging in large MECs, and hence it is efficient to utilize the  $\text{H}_2\text{O}_2$  generated from the cathode immediately, such as in-situ oxidation. The higher pH 11.4 in the CEM-MEC mitigated  $\text{H}_2\text{O}_2$  losses, probably because of  $\text{H}_2\text{O}_2$  ionization to  $\text{HO}_2^-$  ( $\text{pK}_a = 11.65$ ); the electrostatic repulsion between the peroxide species and the cathode can attenuate the  $\text{H}_2\text{O}_2$  loss on the cathode [26].

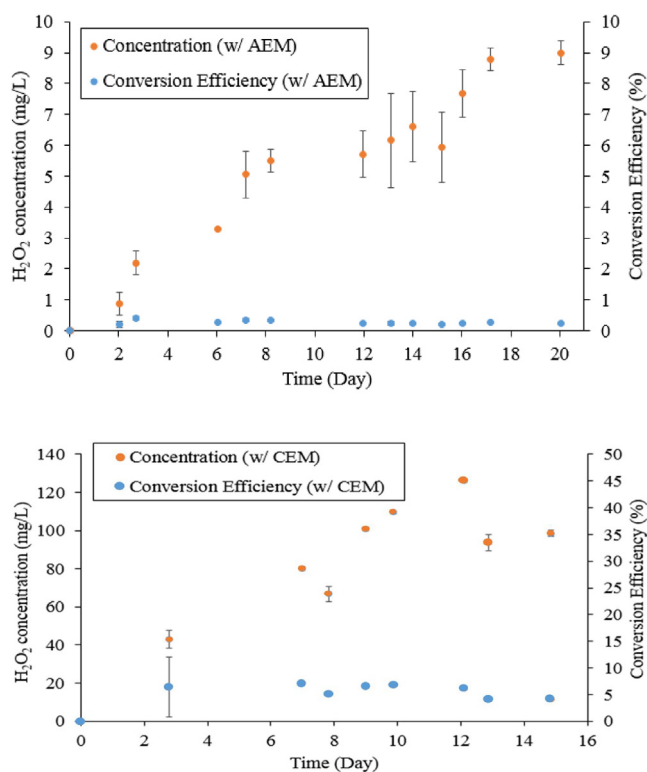


Fig. 3.  $\text{H}_2\text{O}_2$  concentration and  $\text{H}_2\text{O}_2$  conversion efficiency in the MEC.

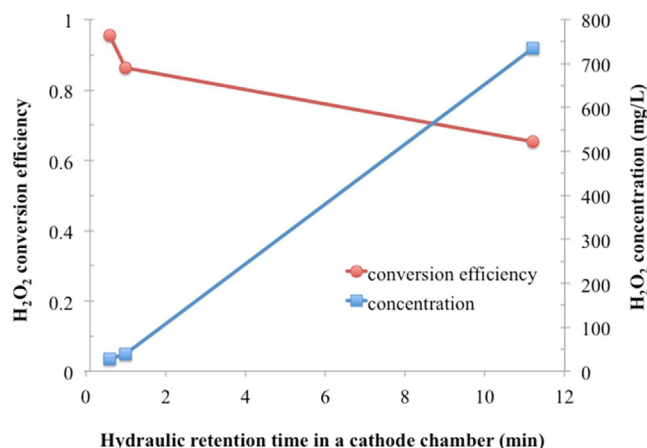


Fig. 4. Small-scale  $\text{H}_2\text{O}_2$  electrolysis cell performance. Tests were performed in a dual chamber reactor with 10 mL cathode chamber volume using 0.1 M NaCl as electrolyte and the same GDE and AEM as used in the pilot MEC. Cathode potential was fixed at  $-1.25$  V vs SCE. Hydraulic retention time was 0.6, 1.0, and 11.2 min, respectively. The same trends were observed for the cathode potential at  $-1.5$  to  $-2$  V vs SCE (data not shown).

## 4. Conclusions

This study first assessed  $\text{H}_2\text{O}_2$  production in the pilot MEC equipped with the non-Pt cathode for passive air diffusion. The non-Pt carbon cathode successfully produced  $\text{H}_2\text{O}_2$  without intensive air supply, but the maximum cumulative  $\text{H}_2\text{O}_2$  concentration was only 98 mg/L in 20d of operation with 7.2% of conversion efficiency, indicating significant losses of  $\text{H}_2\text{O}_2$  in either further reduction on the cathode or decomposition in bulk liquid. It is challenging to stop spontaneous, substantial  $\text{H}_2\text{O}_2$  losses in the pilot MEC, and hence using  $\text{H}_2\text{O}_2$ -MECs as in-situ oxidation will be more practical than  $\text{H}_2\text{O}_2$  synthesis.



## Conflict of interest

None.

## Acknowledgement

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## Appendix A. Supplementary data

Supplementary material related to this article can be found, in the online version, at doi:<https://doi.org/10.1016/j.btre.2018.e00276>.

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