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Review

The Resistance of SO₂ and H₂O of Mn-Based Catalysts for NO_x Selective Catalytic Reduction with Ammonia: Recent Advances and Perspectives

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Among numerous NO_x emission control technologies, the technology of selective catalytic reduction (SCR) using ammonia (NH₃) as the reducing agent (NH₃-SCR) is regarded as the most effective and promising technique. However, the development and application of high-efficiency catalysts is severely limited due to the poisoning and deactivation effect by SO₂ and H₂O vapor in the lowtemperature NH₃-SCR technology. In this review, recent advances in the catalytic effects from increasing the rate of the activity in low-temperature NH₃-SCR by manganese-based catalysts and the stability of resistance to H₂O and SO₂ during catalytic denitration are reviewed. In addition, the denitration reaction mechanism, metal modification, preparation methods, and structures of



the catalyst are highlighted, and the challenges and potential solutions for the design of a catalytic system for degenerating NO_x over Mn-based catalysts with high resistance of SO_2 and H_2O are discussed in detail.

1. INTRODUCTION

Among the denitrification technologies of flue gas, high selectivity, high denitration conversion, and low NH₃ leakage rate were contained by the selective catalytic reduction (SCR), and the core of the SCR was catalysts. $^{1-3}V_2O_5+WO_3(MoO_3)/$ TiO₂ was the most popular commercial SCR catalyst due to its excellent catalytic performance and strong stability. However, due to the limitation of the narrow temperature window (300-400 °C), the vanadium titanium catalyst must be arranged in front of the desulfurization and dedusting devices.⁴⁻⁹ This arrangement exposes the catalyst to an environment of high temperature, high dust, and high SO₂. Long-term operation is likely to lead to catalyst blockage and SO₂ poisoning and deactivation, and the active component V has strong biological toxicity, which may cause secondary pollution. The toxicity of vanadium also causes difficulties for the disposal of the waste catalysts, which hinders further applications of V-based oxide catalysts.^{10,11} For this reason, a plethora of efforts have been made on developing low-temperature catalysts. The transition metals and their oxides have demonstrated considerable potential in replacing V-based catalysts. As a transition metal element, Mn has rich variable valence states, high electron mobility, and high redox performance at low temperature.^{12–15} However, the stability of Mn-based catalysts is poor, which limits practical application of the catalyst especially the resistance to SO2 and H2O. Focus has centered on the research progress on water and sulfur resistance of Mn-based

catalysts. Be that as it may, Mn-based catalysts are easily deactivated by SO_2 at low temperature, since SO_2 can be oxidized in the presence of Mn to form metal sulfate and ammonium sulfate species. Hence, an urgent need exists for the preparation of Mn-based catalysts that have significant SCR activity, sulfur and water resistance characteristics, and wide working temperature windows.

Nowadays, optimizing the performance of Mn-based catalysts with doped active metal is a research hotspot. Zhang et al.¹⁶ prepared a series of MnM/palygorskite (PG) (M = La, W, Mo, Sb, Mg) for low-temperature NH₃-SCR denitration. The MnSb_{0.156}/PG possessed high NO_x conversion in the presence of SO₂ at low temperature, indicating that the SO₂ tolerance of the catalyst was effectively improved with addition of Sb. Shi et al.¹⁷ prepared a series of Ce-modified La–Mn catalysts. Ce–La–Mn catalysts possessed 95% NO_x conversion in the presence of SO₂ and H₂O at 200 °C. In addition to doping active metals, scholars have studied other ways to improve the catalyst resistance, including renewing the support, manufacturing special structures, and

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(6)

$$[\mathrm{NH}_2]_{(\mathrm{ad})} + \mathrm{NO}_{(\mathrm{g})} \to \mathrm{NH}_2\mathrm{NO} \to \mathrm{N}_2 + \mathrm{H}_2\mathrm{O} \tag{7}$$

 $\mathrm{NH}_{3(\mathrm{ad})} + \mathrm{Me}^{n+} = \mathrm{O} \rightarrow [\mathrm{NH}_2]_{(\mathrm{ad})} + \mathrm{Me}^{(n-1)+} - \mathrm{OH}$

$$Me^{(n-1)+} - OH + 1/4O_2 \rightarrow Me^{n+} = O + 1/2H_2O$$
 (8)

2.2. The Deactivation Mechanism of SO₂ and H₂O. Nowadays, high sulfur content is contained in the coal used in China. In low-temperature NH₃-SCR system, a denitrification device is usually placed behind the desulfurization device. However, a small amount of SO2 could cause the lowtemperature denitration performance of the catalyst to be reduced or even deactivated.⁵⁰ Therefore, a catalyst with high sulfur resistance and achieving commercial application for environmental treatment needs to be developed in China. The SO₂ inactivation mechanism of four types may be contained. First, denitration efficiency is reduced with the ammonium sulfate generated by the reaction between SO₂ and NH₃. Second, SO₂ forms a competitive adsorption with NO. Third, metal sulfate is formed. Fourth, gaseous SO₂ is easily oxidized to SO₃ on the catalyst surface, which forms polysulfuric acid. Kwon et al.⁵¹ explored the resistance to SO₂ of the NH₃-SCR catalyst and found that SO₂ and NH₃ generated (NH₄)₂SO₄ and NH₄HSO₄ on the V/Sb/Ti catalysts. Additionally, ammonium salts were difficult to decompose at low temperature and blocked the SCR reaction active sites. Sheng et al.⁵² studied the low-temperature NH3-SCR resistance of Mn-Ce/ TiO₂ catalyst to SO₂ and found that the Mn/TiO₂ catalyst could be sulfated by SO₂ to form stable $Mn(SO_4)_{xy}$ which led to the deactivation of the catalyst. Zhang et al.⁵³ proposed that SO_2 was easily oxidized to SO_3 on the $MnO_x/palygorskite$ (PG) catalyst surface, resulting in the formation of polysulfuric acid, the encapsulation of active components, and the blockage of micropores. Jiang et al.⁵⁴ studied the influence of SO₂ on Fe-Mn/TiO₂ low-temperature SCR catalyst, which showed that the adsorption capacity of SO₂ surpassed that of NO, thus occupying the adsorption site of NO. Yu et al.⁵⁵ investigated the deactivation mechanism of MnO₂-Fe₂O₃-CeO₂-TiO₂ catalyst in the presence of SO₂. The results demonstrated that SO₂ did not form MnSO₄ directly with MnO_x. MnSO₄ was formed by the combination of SO₃ with MnO. SO₃ in this reaction was derived from the decomposition of $(NH_4)_2SO_4$. The SO₂ deactivation mechanisms may have cross-linkages, and the toxicants also may have a certain connection, from which the degree of catalyst poisoning was likely to be strengthened. Each deactivation mechanism refused to intersect, so the resistance to SO₂ was likely to be improved. Thus, the mechanism of SO₂ deactivation may require further research.

The remarkable deactivation of the catalyst results from the high content of the water vapor in flue gas. There were two types of inactivation mechanisms of H₂O. First, H₂O competed with NH₃ and NO for adsorption, occupying the active sites on the catalyst surface and blocking the catalyst pores. Second, SO₂ poisoning was aggravated by H₂O. Xiong et al.⁵⁶ comparatively studied the adsorption performance of Mn–Fe spinel catalysts for NH₃ and NO_x in the presence or absence of H₂O. The results showed that the adsorption performance of the catalysts for NH₃ and NO_x decreased in the presence of H₂O. Phil et al.⁵⁷ investigated the resistance to SO₂ of low-temperature V₂O₅/TiO₂ catalysts for NH₃-SCR and found that the number of Bronsted sizes was increased with the increase

selecting suitable preparation methods. Raja et al.¹⁸ improved the denitrification stability of Mn/TiO2, and Mn-Cu5/Ti-CNT had excellent SO₂ and H₂O resistance. One of the reasons was that the doping of Cu promoted the production of Mn⁴⁺. In addition, the addition of carbon nanotubes increased the specific surface area and total pore volume and reduced the average pore size of the catalyst. Wang et al.¹⁹ prepared a series of 3DOM (three-dimensionally ordered macroporous)-Mn_xCe_yTi_z catalysts. Both the 3DOM-Mn₃Ce₁ and 3DOM-Mn₃Ce₁Ti₁ catalysts had excellent water resistance. Chen et al.²⁰ prepared Ce-Mn/TiO₂ catalysts using reverse coprecipitation, conventional coprecipitation, and impregnation methods. The Ce-Mn/TiO₂ catalysts prepared by the reverse precipitation method had the best SO₂ resistance. The possible reason is that the catalysts prepared by this method have high dispersion, large specific surface area, excellent redox properties, and numerous acid sites. In this paper, these methods will be introduced in detail. Moreover, the advantages and limitations over different catalysts are pointed out and future development direction is proposed. The Mn based SCR catalysts with excellent resistance to SO_2 and H_2O is summarized in Table 1. The table is introduced in the order of no-load, load, and special structure. Each part is introduced according to the number of active metal doping from simple to complex. The information in the table and the content in the text complement each other.

2. THE MECHANISM OF SCR AND DEACTIVATION MECHANISM ABOUT SO₂ AND H₂O

2.1. The Mechanism of SCR. In ammonia selective catalytic reduction technology, the main reaction of low-temperature SCR reaction refers to the reaction in which NH₃ reduces NO to N₂ and generates H₂O. Moreover, two reaction pathways are constituted with the differences in intermediate reactions, namely, L-H mechanism and E-R mechanism. The L-H mechanism is a double adsorption mechanism. NH₃ and NO are adsorbed on the catalyst surface, as shown in eqs 1 and 2. The adsorbed NO is oxidized to nitrous acid by Me^{*n*+}, as shown in eq 3. In addition, adsorbed ammonia reacts with these species to form ammonium nitrite, which is then decomposed into nitrogen, as shown in eq 4. The E-R mechanism is a single adsorption mechanism. The adsorbed ammonia reacts with gaseous NO, and the detailed process is shown in formulas 5-8.

The L-H mechanism is shown below:

$$NH_{3(g)} \rightarrow NH_{3(ad)}$$
 (1)

$$NO_{(g)} \rightarrow NO_{(ad)}$$
 (2)

$$Me^{n+} = O + NO_{(ad)} \rightarrow Me^{(n-1)+} - O - NO$$
(3)

$$NH_{3(ad)} + Me^{(n-1)+} - O - NO \rightarrow Me^{(n-1)+} - O - NO - NH_{3}$$
$$\rightarrow Me^{(n-1)+} - OH + N_{2} + H_{2}O$$
(4)

Me represents active center of metal atom in the reaction equation.

The E-R mechanism is shown below:

$$NH_{3(g)} \rightarrow NH_{3(ad)}$$
 (5)

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ref	21	22	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
X _{NO} -A- SO ₂ +H ₂ O	92%		94%	97%				91%	100%	6%		89%	95%					100%	66%	86%			81%			67%	
X _{NO} -U- SO ₂ +H ₂ O	91%		89%	76%	94%		63%	77%	84%	83%		68%	85%					%06	79%	83%			81%			91%	
X _{N0} -A- H ₂ O	94%	100%		%66			6%	91%	100%		100%	93%				91%		100%	96%			91%		100%			
X _{NO} -U- H ₂ O	87%	%50		92%	95%		88%	80%	%06	96%	100%	82%				91%		%06	88%			76%		100%			
X _{NO} -A- SO ₂	97%	%96		%66				88%	100%	67%	20%	%96	95%	75%		89%	84%		96%		95%		88%		78%	95%	98%
X _{NO} -U- SO ₂	%06	83%		96%	%66	%26	92%	78%	96%	87%	20%	82%	88%	20%	84%	80%	84%		%06		66%		88%		75%	94%	95%
<i>t</i> (h)	4, 4, 4	3, /, / 10, 8, /	/, /, 2	4, 4, 4	10, 15, 15	25, /, /	5, 50, 30	4, 6, 6	7, 7, 7	24, 12, 19	30, 30, /	4, 4, 4	3, /, 3	25, /, /	6.5, /, /	2, 2, /	10, /, /	/, 5, 5	3, 3, 4	/, /, 6	4, /, /	/, 5.5, /	8, /, 8	/, 5, /	6, /, /	4, /, 4	4.5, /, /
X _{NO}	%66	98% 100%	100%	%66	%66	%66	%26	91%	100%	100%	100%	100%	67%	85%	100%	91%	98%	100%	96%	95%	100%	91%	%66	100%	100%	67%	98%
() (C) T	120	120	350	120	240	200	230	175	240	200	200	150	220	150	150	200	180	150	250	180	160		200	225	220	240	300
reaction conditions	1000 ppm of NH ₃ , 1000 ppm of NO, 3% O ₃ , 5% H ₂ O, 100 ppm of SO ₂ , 5% H ₂ O+100 ppm of SO ₃ GHSV at 30,000 h ⁻¹	1000 ppm of NH ₃ , 1000 ppm of NO, 3% O ₂ , 100 ppm of SO ₂ GHSV at 30,000 h ⁻¹ 500 mm of NH. 500 mm of NO 5% O. 5% H.O. 50 mm of SO. GHSV at 80 000 h ⁻¹	500 ppm of M_{3} , 600 ppm of NO, $5\% O_2$, $5\% H_2O+100 \text{ ppm}$ of SO_2 , $GHSV$ at 108,000 h^{-1}	1000 ppm of NH ₃ , 1000 ppm of NO, 3% O ₂ 5% H ₂ O, 100 ppm of SO ₂ , 10% H ₂ O+100 ppm of SO ₂ GHSV at 30,000 h ⁻¹	1000 ppm of NH ₃ , 1000 ppm of NO, 3% O ₂ , 15% H ₂ O, 100 ppm of SO ₂ , 15% H ₂ O+100 ppm of SO ₂ GHSV at 40,000 h ⁻¹	500 ppm of NH ₃ , 500 ppm of NO, 4% O_2 , 100 ppm of SO ₂ GHSV at 35,000 h ⁻¹	500 ppm of NH ₃ , 500 ppm of NO, 5% O ₂ , 15% H ₂ O, 50 ppm of SO ₂ 15% H ₂ O+50 ppm of SO ₂ GHSV at 75,000 h ⁻¹	500 ppm of NH ₃ , 500 ppm of NO, 5% O ₂ , 10% H ₂ O, 150 ppm of SO ₂ , 5% H ₂ O+100 ppm of SO ₂ GHSV at 48,000 h ⁻¹	1000 ppm of NH ₃ , 1000 ppm of NO, 3% O ₂ , 5% H ₂ O, 100 ppm of SO ₂ , 5% H ₂ O+100 ppm of SO ₂ GHSV at 40,000 h ⁻¹	500 ppm of NH ₃ , 500 ppm of NO ₁ 5% O ₂ , 2.5% H ₂ O, 100 ppm of SO ₂ , 2.5% H ₂ O+100 ppm of SO ₂ GHSV at 30,000 h ⁻¹	500 ppm of NH ₃ , 500 ppm of NO, 4% O ₂ , 5% or 10% H ₂ O, 200 ppm of SO ₂ GHSV at 35,000 h ⁻¹	500 ppm of NH ₃ , 500 ppm of NO ₁ 5% O ₂ 10% H ₂ O, 100 ppm of SO ₂ , 10% H ₂ O+100 ppm of SO ₂ GHSV at 40,000 h ⁻¹	1000 ppm of NH ₃ , 1000 ppm of NO, 2% O ₂ 100 ppm of SO ₂ , 5% H ₂ O+100 ppm of SO ₂ GHSV at 40,000 h ⁻¹	600 ppm of NH ₃ , 600 ppm of NO, 5% O ₂ , 100 ppm of SO ₂	1000 ppm of NH ₃ , 1000 ppm of NO, 3% O_{2} 100 ppm of SO ₂ GHSV at 40,000 h ⁻¹	500 ppm of NH ₃ , 500 ppm of NO, 5% O ₂ , 5% H ₂ O, 100 ppm of SO ₂ 5% H ₂ O+100 ppm of SO ₂ GHSV at 80,000 h ⁻¹	800 ppm of NH ₃ , 720 ppm of NO, 3% O ₂ , 100 ppm of SO ₂ GHSV at 30,000 h^{-1}	1000 ppm of NH ₃ , 1000 ppm of NO, 2% O ₂ 2.5% H ₂ O, 2.5% H ₂ O+100 ppm of SO ₂ GHSV at 30,000 h ⁻¹	700 ppm of NH ₃ , 700 ppm of NO ₁ 3% O ₂ , 10% H ₂ O, 350 ppm of SO ₂ , 10% H ₂ O+350 ppm of SO ₂ GHSV at 10,000 h ⁻¹	600 ppm of NH ₃ , 600 ppm of NO, 3% O ₂ , 3% H ₂ O+100 ppm of SO ₂ GHSV at 50,000 $\rm h^{-1}$	500 ppm of NH ₃ , 500 ppm of NO, 5% O_2 , 200 ppm of SO ₂ GHSV at 24,000 h ⁻¹	500 ppm of NH ₃ , 500 ppm of NO, 5% O ₂ , 10% H ₂ OGHSV at 20,000 h ⁻¹	500 ppm of NH ₃ , 500 ppm of NO, 5% O ₂ , 100 ppm of SO ₂ , 10% H ₂ O+100 ppm of SO ₂ GHSV at 18,000 h ⁻¹	500 ppm of NH ₃ , 500 ppm of NO, 3% O ₂ , 4% H ₂ OGHSV at 48,000 h ⁻¹	800 ppm of NH ₃ , 800 ppm of NO, 5% O_2 , 100 ppm of SO ₂ GHSV at 40,000 h ⁻¹	550 ppm of NH ₃ , 550 ppm of NO, 5% O ₂ , 100 ppm of SO ₂ , 10% H ₂ O+100 ppm of SO ₂ GHSV at 20,000 h ⁻¹	500 ppm of NH ₃ , 500 ppm of NO, 3% O ₂ , 200 ppm of SO ₂ GHSV at 10,000 h ⁻¹
catalyst	Fe-MnO _x	Cr-MnO _x CoMnO	MnEuO _x	Ce-FeMnO _x	Ni-Mn-Ti	FeMnZr	Mn-Eu-Fe	$Co-Mn-CeO_x$	$SmMnNiTiO_x$	$MnSmZrTiO_x$	$MnO_x/ZrTiO_2$	Mn/TiO_2	Mn-MOF-74	MnEu/TiO ₂	$Mn-Ce/TiO_2$	$Mn-Sm/TiO_2$	$Cu-Mn/TiO_2$	Fe-Mn/TiO ₂	FeMnCe/ γ -Al ₂ O ₃	Fe-Mn-Ce/TiO ₂	Mn-Ce-Pd/GR	$\rm Fe-Ce-Mn/ACF_N$	Mn-Ce-V/AC	$nf-MnO_x @CNTs$	CeO_2 -MnO ₂	Fe@Mn@CNTs	meso- TiO ₂ @MnCe/ CNTs

Table 1. Summary of the Current Status of the Resistance to SO, and H_2O on Mn-Based Catalysts in the Literature^a

tef 49

50,+H,O

, conversion of conventional SCR reaction, the NO_x conversion under

100%

X_{NO}-A-SO2

X_{NO}-U-SO,

> t (h) 6, /

X_{NO}

() (C)

of water vapor concentration at low temperature. NH_3 combined with the Bronsted sites formed NH_4^+ , while SO_2 and SO_3 combined with the NH_4^+ to form ammonium salts, which enhanced the toxic effect of SO_2 . In general, the effect of H_2O on the catalyst is generally reversible, while the inhibitory effect of SO_2 on the catalyst is remarkable and irreversible, as shown in Figure 1.



Figure 1. Mechanism of the NH_3 -SCR reaction and the influence of SO_2 and H_2O on the reaction pathway. Reprinted with permission from 58. Copyright 2010 Elsevier.

3. THE OPTIMIZATION OF Mn-BASED CATALYST

The Mn-based catalyst has multiple valence states such as Mn^{2+} , Mn^{3+} , and Mn^{4+} , due to the orbital arrangement of Mn element $3d_54s_2$, which ensures high redox performance of Mn-based catalyst and the high activity of single MnO_x catalyst at low temperature. However, the SO₂ and H₂O tolerance of the catalyst is poor. In order to improve the sulfur resistance of the catalyst, four strategies have been presented by researchers. First, during the process of sulfate formation, the adsorption and oxidation of SO₂ on the catalyst surface play an important role. Second, changing or enhancing the active interlocutor species makes the effect of SO₂ on the SCR reaction weaker. Third, the main active sites are protected with the construction of sacrificial sites. Fourth, the purpose of improving the sulfur resistance of the catalyst can also be achieved by promoting the decomposition of sulfate species. As shown in Figure 2, metal



Figure 2. Diagram for the suppressed oxidation of SO_2 to SO_3 . Reprinted with permission from ref 31. Copyright 2018 Elsevier.

sulfates are formed with electron transfer between SO_2 and Mn^{4+} . The addition of Sm results in the transfer of electrons

Table 1. continued

catalyst

 ^{a}t (h), X_{NO} , X_{NO} -U, and X_{NO} -A represent the time of the resistance tests on different poisons (SO₂, H₂O, and SO₂+H₂O), the NO_x 100%210 500 ppm of NH₃, 500 ppm of NO, 5% O₂, 5% H₂O, 50 ppm of SO₂GHSV at 36,000 h^{-1} test, respectively resistance test and after resistance Mn/CeO₂-MSs

reaction conditions



Figure 3. Scheme of V as trapper. Reprinted with permission from ref 44. Copyright 2019 Elsevier.



Figure 4. Effect of cavity size for ABS decomposition. Reprinted with permission from ref 59. Copyright 2019 Elsevier.



Figure 5. Influences of SO₂ on SCR mechanism over $Mn_4Ce_6O_{xy}$ $Ni_1Mn_4Ce_5O_{xy}$ and $Co_1Mn_4Ce_5O_x$ catalysts. Reprinted with permission from ref 29. Copyright 2017 Elsevier.

from Sm^{2+} to Mn^{4+} instead of SO_2 , which prevents the oxidation of SO_2 and eventually reduced the metal sulfate. As displayed in Figure 3, SO_2 forms SO_4^{2-} on the catalyst surface and combines with NH₃ to form ammonium salts. After V₂O₅ modification, V₂O₅ traps SO₂ and prevents the formation of ammonium salt. As shown in Figure 4, In a large cavity, the rate of the decomposition on ammonium salts is more rapid. As shown in Figure 5, The monodentate nitrite species on the surface of MnO_x-CeO₂ are inhibited by SO₂. The NO_x species adsorbed on the surface of catalyst Co(Ni)-MnO_x-CeO₂ is generally a bidentate nitrate without influences by SO₂. The catalyst can still react along the L-H mechanism. In addition, researchers have made some progress in the H₂O tolerance of catalysts. As shown in Figure 6, The NO desorption amount of



Figure 6. TPD of NO on (a) Mn-Eu-550 and (b) Mn-Eu-Fe-500 catalysts. Reprinted with permission from ref 28. Copyright 2019 Wiley.

Mn-Eu-Fe-500 is higher than that of Mn-Eu-550 before and after the modification, which may be an essential reason for the excellent H_2O resistance of Mn-Eu-Fe-500. Within a short time, the SO₂ poisoning can effectively be weakened with the reduction of SO₂ adsorption and oxidation, the construction of the sacrificial sites to the protecting active site, and promoting the decomposition rate of the sulfate species. Combining these strategies, the consumption of the constructed sacrificial sites may be decreased with reduced adsorption and oxidation of SO₂ and increased decomposition rate of the sulfate species. Accordingly, an effective long-term application catalyst may be obtained. Metal doping type, supported type, special structure type, and optimized preparation method type are contained in specific methods.

3.1. Metal Doping. A Mn-based catalyst has high denitration activity. However, the stability of the catalyst is poor. Denitration performance and stability can be improved with the catalyst-doped active metals. From the view of physicochemical properties, the morphology and structure of the material can be changed, the dispersion of active sites can be increased, grain size can be reduced, and redox performance and surface acidity can be improved by doping active metals. From the catalytic point of view, catalytic activity, selectivity, and the poison resistance can be improved by doping active metals. Suitable calcination temperature, high redox performance, excellent acidity, and low surface area loss are beneficial to improve the SO₂ and H_2O resistance of the catalyst.^{25,28} The resistance of the catalyst to SO2 and H2O could be improved by doping MnO_x with other oxides.⁵ The Mn-based SCR catalyst with doped active metals has been extensively studied. As shown in Figure 7, in the presence of SO_2 , the



Figure 7. Resistance to SO₂ over MnCeO_x, CuMnCeO_x, CoMnCeO_x, CrMnCeO_x, NiMnCeO_x, FeMnCeO_x, SnMnCeO_x, and MgMnCeO_x at 175 °C. Reaction conditions: [NO] = [NH₃] = 500 ppm, [O₂] = 5 vol %, [SO₂] = 150 ppm, [H₂O] = 10 vol %, N₂ to balance, total flow rate = 200 mL/min, GHSV = 48000 h⁻¹. Reprinted with permission from ref 29. Copyright 2017 Elsevier.

resistance of the catalyst to SO_2 can be improved with various doped active metals on the basis of Mn–Ce catalyst. After stabilization, the order of the NO_x conversion from high to low is Ni, Co, Mg, Sn, Cr, Fe, and Cu. CeO₂ is frequently used as a MnO_x dopant. France et al.²⁵ optimized FeMnO_x and found the decomposition of ammonium salts might be accelerated by doped Ce. Besides, the loss of the intermediate active species

can be reduced, and the main active metal components can be protected by doped Ce. A fast SCR reaction could not only improve NO_x removal efficiency but also inhibit SO_2 adsorption.⁶⁰ The formation of oxygen vacancies on the surface of the catalyst was promoted with the redox cycle between Ce⁴⁺ and Ce³⁺, which could effectively promote the oxidation of NO to NO₂ at low temperature,^{61,62} thus increasing the fast SCR reaction. A high denitrification performance Mn-Ce catalyst was obtained by Chen et al.⁶³ The NO_x conversion was increased from 92.6 to 97.8% at 150 °C with 200 ppm of SO₂. Superior SO₂ resistance might be attributed to the porous structure formed by the Mn-Ce oxide. In addition to Ce, Fe was also considered as an ideal additive to improve the denitration performance of Mn-based SCR catalysts.⁶⁴ Doped Fe is beneficial for improving the resistance to SO₂ and H₂O. After doping Fe, NO oxidation is greatly enhanced with the presence of a high redox potential pair of Fe and Mn.²¹ Guo et al.²⁸ found the Mn-Eu-Fe catalyst doped with Fe had a high surface Fe³⁺ concentration, a low binding energy of Fe³⁺ and Fe²⁺, a high O_{α} quantity, a high redox performance, and more acid content, which were beneficial for improving the resistance to H₂O. Besides, Mn-Eu-Fe had the best H₂O resistance when then calcination temperature was 500 °C. Doping of Sm has been widely used and studied because the redox ability, specific surface area, and sulfur resistance of the catalyst can be greatly improved. Pure SmO_x has almost no effect on the lowtemperature NH₃-SCR reaction. However, the resistance to H₂O and SO₂ is significantly improved when Sm is doped into Sm-Mn mixed oxide catalysts.⁶⁵ The $Sm_aMnNi_2Ti_7O_x$ catalysts (a = 0.1, 0.2, 0.3, 0.4) were prepared by Tong et al.³⁰ The oxidation of SO_2 to SO_3 can be restrained by the doped Sm. This is possibly due to the suppressed electron transfer from SO₂ to Mn⁴⁺. Qin et al.⁶⁶ compared the SO₂ resistance of MnTiSnO_x and SmMnTiSnO_x catalysts and obtained similar results. In addition to Ce, Fe, and Sm doping, doping with other elements has also been studied. Chen et al.² prepared Mn-Cr mixed oxides by the citric acid method and found that CrMn_{1.5}O₄ was formed with the introduction of Cr, which significantly improved the SO₂ tolerance of the catalyst. The Mn catalyst doped with Co exhibited excellent water resistance due to a relatively large specific surface area and orderly pore structure inside the catalyst.^{36,67} Additionally, the Co-doped catalyst has a remarkable resistance to SO₂. The $Co_1Mn_4Ce_5O_x$ and $Ni_1Mn_4Ce_5O_x$ catalysts prepared by Gao et al.²⁹ could maintain a NO_x conversion of 78% at 175 °C in an atmosphere of 150 ppm of SO2. The main reactants of the $Co_1Mn_4Ce_5O_x$ and $Ni_1Mn_4Ce_5O_x$ catalysts were not inhibited by SO2. The Cu-modified Mn-based catalyst appears to not only have high activity but also maintain stable resistance to SO_2 and H_2O , which is a potential doped active metal. Wang et al.⁶⁸ prepared a series of AMn_2O_4 (A = Cu, Co) catalysts and found that catalytic activity of CuMn₂O₄ was higher than that of CoMn₂O₄, while the tolerance of CuMn₂O₄ was excellent at 100 ppm of SO₂ and 10 vol % H₂O. Chen et al.²⁶ prepared $Ni_xMn_{1-x}Ti_{10}$ catalysts. The oxidation of SO₂ to SO₃ was restrained with doped Ni. Chang et al.⁶⁹ found that the resistance to H₂O and SO₂ was significantly improved with doped Sn. The thermogravimetric analysis (TGA) showed that the main peaks of the Sn-Mn-Ce-O catalysts shifted to lower temperature. Guo et al.²⁷ found that the interaction of Fe, Mn, and Zr on the Fe_{0.3}Mn_{0.5}Zr_{0.2} catalyst protected the active ingredients from vulcanization. The catalyst-doped Eu



Figure 8. Influence of SO₂ and H₂O or combined H₂O and SO₂ on NO_x conversion of FeMnO_x and FeMnCeO_x. Reaction conditions: $[NO] = [NH_3] = 0.1\%$, $[H_2O] = 5$ or 10%, $[SO_2] = 100$ ppm, $[O_2] = 3\%$, N₂ to balance, GHSV = 30,000 h⁻¹; reaction temperature = 120 °C. Reprinted with permission from ref 25. Copyright 2017 Elsevier.

also had excellent resistance to H₂O and SO₂.²⁴ To sum up, the adsorption and oxidation of SO₂ can be inhibited by the Mn-based catalyst-doped Fe, Sm, and Ni, the active ingredients can be protected by the doped Zr, the sulfate decomposition can be accelerated by the doped Sn, and the intermediate adsorbed species can be protected by the doped Co. The Ce can accelerate the decomposition of sulfate, enhance the adsorption of intermediate species, and build sacrifice points. Besides, the adsorption and oxidation of SO₂ can be reduced by the doped Ce. This comprehensive influence appears to be the reason why the SO₂ resistance can be greatly improved by Ce as an additive. Additionally, the Ce and Fe are often used as the first doped active metals of Mn-based catalysts. The composite Mn-based catalysts with more excellent sulfur resistance can often be obtained by doping appropriate second active metals. However, only the excellent sulfur resistance can be determined within a short time, and the sulfur resistance evaluation is also mostly at 200 °C or above, as shown in Table 1. The multicomponent Mn-based catalysts suitable for different industrial requirements are likely to be obtained by doping more kinds of active metals and adjusting appropriate proportion.

 H_2O and SO_2 usually work together to aggravate the poisoning effect of the catalyst. However, researchers have found some different phenomena. As shown in Figure 8, at 120 °C, the conversion is close to full recovery after stopping the introduction when SO₂ and H₂O are introduced at the same time. However, the recovery of NO_x conversion for FeMnO_x catalyst is not prominent when SO₂ is introduced alone. Other researchers have found some similar phenomena. As shown in Figure 9, at 110 °C, the NO_x conversion is higher when SO₂ and H_2O are simultaneously introduced. At 220 °C, the NO_x conversion is higher when SO₂ is introduced alone. Different reaction temperatures may have a different influence on the catalyst resistance. At lower temperature, H₂O may have a certain positive effect on the catalyst. The former experimental conditions are 120 °C, 10% H₂O, and 100 ppm of SO₂, and the latter are 110 $^\circ\text{C}$, 9% H_2O, and 100 ppm of SO_2, which proves that H₂O may improve the SO₂ resistance of Mn-based composite catalysts under certain conditions. Studying the positive temperature range of H₂O and the dosage range of poisons is likely to promote the development of Mn-based catalysts for low-temperature NH₃-SCR of NO₂. In addition, calcination temperature, space velocity, and the proportion of active components of composite Mn-based catalysts appear to have an impact on the resistance of the catalyst.



Figure 9. Resistance to SO_2 and combined H_2O and SO_2 over different catalysts (reaction temperature = 110 or 220 °C). Reprinted from ref 69. Copyright 2013 American Chemical Society.

3.2. Carrier. The carrier plays an important role in the catalyst. High redox performance, excellent acidity, and low surface area loss can be obtained with selecting a suitable carrier, thus improving the SO₂ and H₂O resistance of the catalyst.^{70,71} The resistance of the Mn-based low-temperature SCR catalysts to H₂O and SO₂ is closely related to the catalyst support. The tolerance of the catalysts can be significantly improved by selecting suitable the metal oxides as supports, as shown in Figure 10. Among them, the Al₂O₃ has hightemperature resistance, excellent mechanical properties, large specific surface area and simple shape control. Obrist et al." studied the NH₃-SCR activity of MnO_x/ γ -Al₂O₃ catalysts and the catalysts had high catalytic activity. However, the SO₂ resistance of the Al₂O₃ is poor. For Mn-based low-temperature SCR catalysts, the TiO₂ was proven to be an ideal support.^{73,74} Compared with Al₂O₃, TiO₂ has less acidic and more stable physicochemical properties. The findings of Kang et al.³³ confirm that the TiO_2 -supported catalyst has higher NO_x conversion compared with the γ -Al₂O₃-supported catalyst when SO₂ is introduced. Active components can be effectively dispersed by the TiO₂ support, and sulfates are easily decomposed on the surface of the TiO₂. Additionally, Smirniotis et al.⁷⁵ found that the MnO_x/TiO_2 catalyst had high water resistance. The resistance of the catalyst to SO₂ and H₂O can be significantly improved with the composite metal as a carrier. Xiong et al.⁷⁰ found that the doping of Ti increased Ce³⁺ concentration relatively, which inhibited the loss of Mn species on the surface of Mn/CeTi catalysts. Jiang et al.



Figure 10. Influence of combined H₂O and SO₂ on NO_x conversion of the catalyst using different carriers(Reaction conditions: [NO] = [NH₃] = 0.06%, [H₂O] = 3%, [SO₂] = 100 ppm, [O₂] = 3%, N₂ to balance, GHSV = 30,000 h⁻¹; reaction temperature = 180 °C. Reprinted with permission from ref 76. Copyright 2014 Elsevier.

found that Zr modification on the Fe-Mn/Ti-Zr_{0.03} catalyst weakened the effect of SO_2 on NO_2 and nitric acid. Jia et al.³² prepared a series of MnO_x/ZryTi_{1-y}O₂ catalysts with different Zr/Ti ratios. The catalysts exhibited excellent water resistance and sulfur resistance at 200 °C. Shen et al.⁷⁶ found that the NO conversion of $MnO_{x(0.6)}/Ce_{0.5}Zr_{0.5}O_2$ catalysts remained above 90% after 5 h of reaction at 180 °C in an atmosphere of 3 vol % H₂O and 100 ppm of SO₂. The combination of the advantages of ZrO₂ and CeO₂ carrier was an important reason to improve the resistance to SO_2 and H_2O of the catalysts. Catalyst stability is likely to be further improved by selecting a suitable support combined with a variety of doped active metals. The performance of CeO_x -based capturing SO_x is excellent.⁷⁷ Sulfate stability can be reduced with the TiO_{2} which is consistent with the previous section on accelerating sulfate decomposition by the Ce and Sn. The stability of sulfate is likely to be further reduced by using TiO₂ as a carrier and the catalyst may decompose at lower temperature to meet industrial low-temperature demand. The number of species for intermediate adsorption can be increased with the composite metal carriers. The species of intermediate adsorption can be also increased with the doped additives. Combining these strategies, the demand of the intermediate adsorbed species in the SCR reaction after poisoning may be still met.

Moreover, the catalyst using other carrier also has excellent tolerance. Pourkhalil et al.⁷⁸ found the $MnO_x/functionalized$ multiwalled carbon nanotube (FMWNT) catalyst had

excellent resistance to H2O and SO2. At 200 °C and 30,000 h^{-1} space velocity, NO_x conversion only decreased by 5% when 2.5 vol % H₂O and 100 ppm of SO₂ were introduced for 6 h. Molecular sieves have a unique mesoporous structure and large specific surface area. Nowadays, the field of molecular sieves involves research of NO and SO₂ gases. Molecular sieves are used to simultaneously adsorb NO and SO₂ to removing the two pollutants. Deng et al.⁷⁹ prepared a variety of ionexchanged molecular sieves and found that K-NaX molecular sieves had the best effect on simultaneously adsorbing NO and SO₂. Yi et al.⁸⁰ studied the coadsorption of SO₂ and NO by NaY, NaX, and CaA molecular sieves and found that the stronger the polarity, the better the adsorption capacity of molecular sieves. The molecular sieve has a regular pore structure and molecular sieve screening characteristics. The NO, NH₃, and SO₂ are likely to be separated due to the screening characteristics. The contact between SO2 and lowtemperature SCR catalyst is likely to be reduced thus fundamentally reducing the toxic effect of SO₂ on lowtemperature SCR catalyst.

3.3. Load Type. Mn-based supported catalysts have made some progress. High redox performance, low surface area loss, and excellent acidity can be obtained with the combination of metal modification and support, thus improving the SO₂ and H₂O resistance of the catalyst.^{35,38,44,81,82} The metal oxide, the molecular sieve supports, and the carbon-based supports summarized in the previous section are mainly contained in the carrier. Among metal oxide supports, the TiO₂ is widely used, while the molecular sieve and carbon-based ones have a wide variety and flexible choices. Doping active metals and selecting suitable carriers are beneficial for improving sulfur resistance and water resistance of the catalyst. Among them, the most doped elements are Ce and Fe. The catalysts doped with Ce had excellent sulfur resistance and water resistance.^{83,84} Jin et al.⁸¹ found that doped Ce was beneficial for reducing thermal stability of NH4HSO4 on the catalyst surface, as shown in Figure 11. This is also confirmed by Liu et al.,⁸² who prepared a Ce-Cu-Mn/SAPO-34 catalyst. Moreover, the Ce protects the main active components from being sulfurized, as shown in Figure 12. The supported catalyst-doped Ce not only has excellent sulfur resistance but also achieves remarkable regeneration. As shown in Figure 11, the activity of the Cemodified catalyst is mostly restored after washing and regeneration. Fe is a promising Mn-based catalyst dopant. Qi et al.³⁹ prepared Fe-Mn/TiO₂ and found the formation rate of sulfate species on the catalyst surface could be reduced with doped Fe. Li et al.³⁸ confirmed that the generation of Mn sulfate and ammonium sulfate can be significantly alleviated with doped Fe, thus improving the sulfur resistance of Mn/



Figure 11. TG and DSC curves of NH_4HSO_4 deposited on $Mn/TiO_2(A)$ and $Mn-Ce/TiO_2(B)$ catalysts and The resistance to SO_2 over Mn/TiO_2 and $Mn-Ce/TiO_2$ at 150 °C ($[NH_3] = [NO] = 800$ ppm, $[O_2] = 3\%$, $[SO_2] = 100$ ppm, $[H_2O] = 3$ vol %, N_2 to balance, GHSV = 40,000 h⁻¹). Reprinted with permission from ref 81. Copyright 2014 Elsevier.



Figure 12. XRD pattern of 2% Ce-modified catalyst after SO_2 poisoning. Reprinted with permission from ref 82. Copyright 2019 MDPI.

 $\rm TiO_2$ catalysts. Wang et al. 85 prepared a series of Fe-Mn/Al_2O_3 catalysts and found that the catalysts also had a certain tolerance to water and sulfur dioxide after doping Fe. Ce and Fe are commonly used as Mn-based catalyst dopants. Ce, Fe, and Mn ternary composite metal Mn-based catalysts have been widely studied. Cao et al.⁴⁰ doped Fe into Mn-Ce/ γ -Al₂O₃ to prepare Fe-Mn-Ce/ γ -Al₂O₃ catalysts. The FeMnCe/ γ -Al₂O₃ catalysts had the excellent resistance to H₂O and SO₂. Shen et al.⁴¹ doped Fe into Mn-Ce/TiO₂ catalysts and obtained a series of Fe-Mn-Ce/TiO₂ catalysts. The FeMnCe/TiO₂ catalysts had excellent resistance to H2O and SO2. Shen et al.⁸⁶ compared the sulfur resistance of the (Fe,Cu,V)-MnO_x- $CeO_x/ACF(activated carbon fiber)$ catalyst under the atmosphere of 100 ppm of SO₂. The FeMnCe/ACF material had remarkable SO₂ resistance. Gu et al.⁴³ successfully prepared MnO_x/ACF_N (the rayon-based ACF pretreated with 40 wt % HNO₃ solution), Ce-MnO_x/ACF_N, and Fe-Ce-MnO_x/ACF_N catalysts by ultrasonic impregnation method. The interaction between Mn, Ce, and Fe made the catalysts have excellent water resistance. As shown in Figure 13, the change in the 1199 cm^{-1} band before and after the introduction of H2O confirms that there was competitive adsorption of NH₃ and H₂O on L acid. The change in the 1400 cm⁻¹ band confirmed that the interaction between H₂O and B acid was weaken with Fe-Ce-MnO_x/ACF_N. Mn/TiO₂ and Mn-Nb/TiO₂ catalysts were prepared by Sun et al.⁸⁷ The Mn-Nb/TiO₂ catalysts showed outstanding SO₂ resistance. The possible reason was that more NO₂ was formed on the surface of the Mn-Nb/TiO₂ catalyst. Li et al.⁸⁸ doped Ho into Mn-Ce-O/TiO₂ catalysts by impregnation method and found that the excellent sulfur resistance and water resistance of the Ho-Mn-Ce-O/TiO₂ catalysts were attributed to the increase of specific surface area, surface O_{α} and Mn^{4+}/Mn^{3+} . Jiang et al.⁴⁴ modified Mn-Ce-O/AC (activated carbon) catalyst with V2O5. Doped V effectively inhibits the formation of ammonium salt and protects main active components, as shown in Figure 14. Chen et al.⁸⁹ doped Zr, Co, or Ni into Mn/BC (biochar) catalysts by the impregnation method. The materials doped with Zr had the best sulfur and water resistance. Liu et al.³⁵ prepared MnO_x/TiO₂ catalysts modified by Eu, and TGA showed sulfate deposition was decreased with doped Eu. The



Figure 13. Fourier transform infrared spectra of the fresh and H₂Oresisted $Fe_{(1)}$ -Ce₍₃₎-MnO_{x(7)}/ACFN catalyst. Reprinted with permission from ref 43. Copyright 2019 Springer Nature.

adsorption peak of NO₂ and NH₄⁺ is retained with doped Eu and the intensity of sulfate on the surface of MnEu/TiO₂ is lower than that of Mn/TiO_2 , as shown in Figure 15. Liu et al.³⁷ prepared a series of Mn-Sm/TiO₂ catalysts by adding different amounts of Sm elements. The catalyst-doped Sm can inhibit the formation of metal sulfate and the oxidation of SO_2 to SO_3 , as shown in Figure 16. Wu et al.⁹⁰ doped respectively Fe, W, and Mo into MnOx/TiO2 catalyst. The W had better sulfur tolerance. Yang et al.⁴² prepared the MnO_x-CeO₂/graphene catalyst doped with noble metals by hydrothermal method. Specific surface area, Mn⁴⁺, chemically adsorbed oxygen, and acid sites were increased with the catalyst-doped Pd, thus enhancing SO₂ poisoning resistance. Song et al.⁹¹ synthesized a series of Cu-Mn-SSZ-13 catalysts by exchanging manganese and copper. The catalysts doped with Cu had excellent hydrothermal stability. Zhang et al.⁹² prepared Co-Mn-ZSM-5 catalyst by Co and Mn coimpregnating ZSM-5. Under the condition of 100 ppm of SO_2 , the NO_x conversion only decreased by 20% at 150 °C. To sum up, the activity, sulfur resistance, and water resistance of supported catalysts are frequently higher than the unsupported catalysts. The Fe, Ce, Eu, Co, Sm, and Cu have excellent sulfur resistance or water resistance in both unsupported and supported catalysts. Both unsupported and supported catalysts appear to have the similar strategies of sulfur resistance. The Eu can enhance the adsorption of intermediate species, and the oxidation of SO₂ to SO₃ can be inhibited with the Sm-modified catalyst. The Ce and V can be used as sacrificial agents to protect the main active components. Moreover, the stability of the ammonium salt can be reduced with doped Ce. The interaction among Mn, Ce, and Fe can makes catalyst keep excellent sulfur resistance or water resistance under different supports, which proves that Fe, Mn, and Ce composite metal catalysts may have the excellent performance independent of supports. And the performance of unloaded FeMnCe catalysts is excellent. Additionally, the Mn-Ce/TiO₂ catalyst-doped Ce has excellent regeneration. The research on catalyst regeneration and recycling is likely to improve catalyst life and reduce industrial cost.



Figure 14. XRD patterns of different catalysts: (a) AC, (b) Mn/AC, (c) Mn-Ce_(0.4)/AC, (d) Mn-Ce_(0.4)-V/AC, (e) Mn-Ce_(0.4)/AC-S, and (f) Mn-Ce_(0.4)-V/AC-S. The right corresponding to the higher resolution diffraction peaks in 20–40°. Reprinted with permission from ref 44. Copyright 2019 Elsevier.



Figure 15. SO₂ adsorption DRIFT spectra for (A) Mn/TiO₂ and (B) MnEu/TiO₂ catalysts under the SCR reactions (500 ppm of NH₃ + 500 ppm of NO + 5% O₂, balance to N₂, 100 ppm of SO₂ (when used)) at 150 °C. Reprinted with permission from ref 35. Copyright 2018 Elsevier.



Figure 16. TG-DSC-MS curves of $20Mn/TiO_2$ (a) and $20Mn-10Sm/TiO_2$ (b) catalysts pretreated by H₂O and SO₂ during SCR reaction. Reprinted with permission from ref 37. Copyright 2020 Elsevier.

3.4. Special Structure Type. *3.4.1. Core–Shell Structure Type.* Core–shell structure combines inner and outer layers to achieve desired effect. The outer layer is mainly used as a sacrificial layer, inhibits SO_2 adsorption, slows down the formation of sulfate substances and protects main active components of the inner layer. The CeO₂ shells of high redox performance were beneficial for capturing SO_2 .⁴⁶ Fe₂O₃ shell was beneficial for enhancing the alkalinity of the catalyst surface.⁴⁷ CNT-supported core–shell structure was widely

studied. Zhang et al.⁴⁸ prepared a core–shell SCR catalyst mesoTiO₂@MnCe/CNTs with mesoporous TiO₂ as the shell and CNT-loaded MnO_x -CeO_x nanoparticles as the core. The adsorption of SO₂ and the generation of sulfate could be inhibited with the mesoporous TiO₂ shell of the catalyst. The research of Zhang et al.⁹³ also confirmed this point. Mesoporous TiO₂ layer was coated on MnO_x and CeO_x nanoparticles supported by carbon nanotubes, thus improving the SO₂ poisoning resistance of the catalyst. Cai et al.⁴⁷ got a

similar conclusion. The formation of sulfate on the surface of catalysts could also be effectively inhibited with Fe₂O₃ shell. Fang et al.⁴⁵ prepared nf-MnO_x@CNT catalysts with coreshell structure by chemical deposition. Compared with MnO_x/ CNT and MnOx/TiO2 catalysts, nf-MnOx@CNT catalyst showed excellent H₂O resistance. Additionally, Liu et al.⁹⁴ prepared MnO₂@NiCO₂O₄ core-shell nanorods with nickel foam as carrier. The Ni-Co nanorods had high specific surface area and there was an excellent synergy among Ni, Co, and Mn oxides, thus promoting the excellent low-temperature activity and H₂O resistance of the catalyst. Li et al.⁴⁶ prepared coreshell CeO_2 -MnO_x bimetallic oxide. The catalysts had relatively excellent SO2 resistance. In the presence of SO2, the high activity of the catalyst can be only maintained with the method doping metal for a limited time. The sulfur resistance time of the catalyst can be relatively prolonged with the protective shell method. However, the activation temperature is relatively high. In order to find a catalyst with excellent denitration activity and excellent sulfur resistance at low temperature, the fresh strategy based on the two methods is necessary to further research. In the core-shell structure, SO₂ adsorption can be inhibited with the mesoporous TiO₂ layer, sulfate formation can be inhibited with the Fe₂O₃ shell, and the shell layer plays an important role in improving SO₂ resistance. Combined with the research of the catalyst-doped metal, other metal oxides or composite metal oxides can be considered as shell layers to further improving the performance of Mn-based catalysts.

 MnO_x nanoparticles are surrounded by a layer of crystalline CeO_2 shell, as shown in Figure 17. It can be found from Figure



Figure 17. High-resolution transmission electron microscopy image of the CeO_2 -MnO_x. Reprinted from ref 95. Copyright 2017 American Chemical Society.

18 that the TiO_2 layer is wrapped with Mn Ce/CNTs. Fe, Mn and C are listed from outside to inside (Figure 19). The coreshell structure had distinct layers, and the outer layer was designed to protect the inner layer. On account of the layering, each layer can be independently designed. The inner and outer layers were designed combined with the metal doping modification. The overall stability of the catalyst can be mainly improved with the outer layer. And the catalyst activity was mainly increased with the inner layer, which can improve the catalyst performance to the greatest extent. If the catalyst activity was satisfied, metal doping in the inner layer was conducive to improving the tolerance of the catalyst, which may improve the tolerance of the catalyst to meet the requirements of industrial application.



Figure 18. Transmission electron microscopy image of meso-TiO₂@ MnCe/CNTs. Reprinted with permission from ref 48. Copyright 2013 Royal Society of Chemistry.

3.4.2. Other Special Structure Types. The hollow structure improves the resistance to SO₂ and H₂O. The probable reason is that the active ingredients are uniformly dispersed in the nanotubes (Figure 20). Li et al.⁹⁶ obtained a composite MnO_{x} -CeO₂ nano-oxide with a hollow tubular structure by an interfacial redox reaction. Excellent sulfur resistance and water resistance were obtained, which might be related to the unique hollow tubular structure. Jiang et al.³⁴ prepared the Mn-MOF-74 catalyst with a hollow spherical structure and found that the NO conversion efficiency of Mn-MOF-74 could be kept at 85% in the presence of 5% H_2O and 100 ppm of SO_2 . Moreover, other special structures also have certain sulfur resistance and water resistance. Gao et al.⁹⁷ obtained highly sulfur-resistant spinel nanosheet-structured Mn-Ni catalysts. The high sulfur resistance of the catalysts was attributed to the external tetrahedral configuration protecting the internal Mn active site. Meng et al.²³ prepared a series of $Co_a Mn_b O_x$ catalysts. The $Co_7Mn_3O_r$ catalysts with the spinel structure promoted the resistance to SO_2 and H_2O . Gao et al.⁴⁹ successfully prepared two Mn/CeO₂ catalysts by impregnating CeO₂ microspheres and CeO₂ micron rods with Mn. The Mn/ CeO₂-MSs catalyst had excellent SO₂ and H₂O resistance. Zhang et al.⁹⁸ found that the $Mn_xCo_{1-x}O_4$ catalysts with nanocages had better SO₂ and H₂O resistance than the $Mn_xCo_{1-x}O_4$ catalysts with nanoparticles. The probable reason is that nanocages of the $Mn_xCo_{1-x}O_4$ catalysts enhanced the interaction between MnO_x and CoO_x. Additionally, adjusting the pore structure of catalysts can achieve a dynamic balance between the formation and decomposition of ammonium sulfate on the catalyst's surface. Then, the catalysts can reduce the degree of ammonium sulfate deposition on the surface. Yu et al.55 found that Mn-based catalysts showed excellent sulfur resistance when pore size was 2-50 nm. The $(NH_4)_2SO_4$ specie achieved the balance of formation and decomposition in mesoporous channels. The larger pore structure was beneficial for the decomposition of the ammonium salts on the catalyst's surface,^{59,99,100} as shown in Figure 21.

3.5. Preparation Method. The preparation method has a significant effect on the structure of the catalyst, and the physical form structure of the catalyst is closely related to its physicochemical properties. Moreover, the preparation method is critical in determining the excellent dispersion of active components and particle size. Accordingly, the preparation method can be optimized for the catalyst's performance. Different preparation methods obtain different tolerance of the catalysts, as shown in Figure 22. Sol–gel and surfactant template methods play a more significant role than the



Figure 19. Elemental mapping images of Fe@Mn@CNTs. Reprinted with permission from ref 47. Copyright 2016 Royal Society of Chemistry.



Figure 20. Scanning transmission electron microscopy (a) image of MnO_x -CeO₂ nano-oxide and energy-dispersive X-ray spectroscopy of Mn (b), Ce (c), and O (d). Reprinted with permission from ref 96. Copyright 2018 Elsevier.

coprecipitation and impregnation methods in resisting SO₂ and H₂O. The MnO_x/TiO₂ catalyst was prepared by Jiang et al.¹⁰¹ using the sol-gel way. The way showed better SO₂ tolerance than the MnO_x/TiO₂ catalyst prepared by the impregnation and coprecipitation methods. Liu et al.⁶² compared the performance of the MnO_x-CeO₂ catalyst prepared by surfactant template and conventional coprecipitation method. At a space velocity ratio of 64,000 h⁻¹ and 150–200 °C, the MnO_x-CeO₂ catalyst prepared by the surfactant template

method could keep the NO_x conversion above 90% in the atmosphere of 5 vol % H₂O and 50 ppm of SO₂. Yu et al.⁵⁵ reported a mesoporous MnO₂-Fe₂O₃-CeO₂-TiO₂ catalyst prepared by the sol-gel method, which had higher resistance to SO₂ and H₂O than the conventional impregnation method. The improvement of traditional preparation methods has achieved some progress. Yao et al.¹⁰² prepared MnO_x/CeO₂ nanomaterials by adjusting the solvent. The catalyst prepared by (HCOOH)₂ solution as solvent showed excellent sulfur and water resistance. Zhang et al.¹⁰³ loaded MnO_x and CeO_2 on the CNTs using an auxiliary reflux route. Compared with the traditional preparation process, the method had certain advantages in sulfur and water resistance. Sheng et al.¹⁰⁴ used a novel coprecipitation method to synthesize the Mn-Ce/ TiO_2 catalyst. The catalyst had stable SO_2 resistance. Shi et al.¹⁰⁵ systematically compared the SO_2 tolerance of Mn/TiO₂ prepared by the conventional sol-gel method and layered mesoporous Mn/TiO₂ catalysts prepared by the Planck F127 assisted sol-gel method. After adding 30 ppm of SO₂ to inlet flue gas at 120 °C, the NO conversion rate of ordinary Mn/ TiO₂ drops sharply from 57 to 15% within 6 h, while the NO conversion rate of HM Mn/TiO₂ remains above 84%. Zou et al.¹⁰⁶ prepared Mn-Fe/ZSM-5 catalysts by coprecipitation and precipitation-chemical vapor deposition methods. The Mn-Fe/ZSM-5 catalyst obtained by method B had higher SO₂ resistance. The possible reason was that the decomposition of sulfate was faster for the Mn-Fe/ZSM-5 catalyst prepared by this method. The unique preparation methods can obtain the catalysts with the better effect of treating H₂O alone to meet some industrial scenes. Huang et al.¹⁰⁷ found that the SCR activity of the MnO₂-Co₃O₄/TiO₂ catalyst was hardly affected by H₂O. The probable reason was that the MnO₂-Co₃O₄/TiO₂ catalyst obtained nanorod heterostructure using the photocatalyst method.



Figure 21. Decomposition of ammonium salts on the catalyst with different pore sizes. Reprinted from ref 100. Copyright 2019 American Chemical Society.



Figure 22. Influence of H_2O and SO_2 on NO_x conversion of the catalyst using different preparation methods: (A) the conventional coprecipitation method and (B) the surfactant-template method (reaction conditions: $[NO] = [NH_3] = 0.05\%$, $[H_2O] = 5\%$, $[SO_2] = 50$ ppm, $[O_2] = 5\%$, N_2 to balance, GHSV = 64,000 h⁻¹). Reprinted with permission from ref 62. Copyright 2013 Elsevier.

4. CONCLUSIONS AND PROSPECTS

For low-temperature denitration catalyst, the strong inactivation effect of H₂O and SO₂ on the active metal of catalyst is the main reason for the NH₃-SCR, which severely reduces the catalytic efficiency and performance in many fields. Thus, an ideal catalyst is required to possess not only a strong adsorption for NO_x but also the ability to propel denitration conversion efficient, which is expected as the ultimate remedy for suppressing the catalyst poisoning from the deactivation with H₂O and SO₂. Most of Mn-based catalytic materials have been widely used and investigated in the de-NO_x industry, the catalysts promoting denitration based compound conversion in traditional chemical reactions may provide a new way to highefficiency catalytically promote conversion in the comprehensive denitration industry. At the current stage, identifying the catalytic mechanism is expected to provide a design principle for the catalytic denitration conversion. Thus, the mechanisms of H₂O and SO₂ poisoning on NH₃-SCR catalysts and performance of Mn-based low-temperature denitration catalysts are greatly needed to help understand the conversion process from NO_x to N_2 .

In this review, some key points for high-efficiency catalyst design for the reaction of denitration conversion are summarized:

(1) Mn-based catalytic materials have a potential application value in large-scale industrial application, which consist of cement, glass, metallurgy, petrochemical catalytic cracking, chemical industry, waste incineration and other fields, attributing to the superior low-temperature catalytic activity, nontoxicity and low cost. To achieve industrial expectations, Mn based low-temperature SCR catalyst not only needs to have high denitration efficiency, thermal stability and good N₂ selectivity, but also have strong anti-H₂O and SO₂ performance. Therefore, it is very important to carry out research to improve its relevant performance and clarify its relevant mechanism, especially the Manganese–Cerium catalyst for sulfur and water resistance at low temperature.

(2) The deactivation mechanism of Mn-based denitration catalyst under SO_2 was systematically identified. The passivated contact reaction focuses on the formation of ammonium sulfate and metal sulfate on the surface of the catalyst in NH₃-SCR, which will block the active sites and causes deactivation, which generating the competitive adsorption SO_2 , reducing the formation of active intermediates and causing deactivation. Intrinsically, part of SO_2 was catalytically oxidized into SO_3 by the active components in

denitration catalyst, and then the continuous reaction was triggered between SO₃ with escaping NH₃ and H₂O to producing fine particles of ammonium sulfate, and also the coterminous reaction with metal oxides in fly ash was formed to producing sulfate particles, all of that will cover the active sites of the catalyst resulting in blockage and deactivation of the catalyst eventually; SO₂ can also react with metal oxides on the catalyst surface to generate metal sulfate, which will adsorb on the surface of catalyst and hinder the subsequent denitration reaction. According to the deactivation mechanism of catalyst, it is found that the sulfur resistance of catalyst at low temperature can be improved by reducing SO₂ oxidation and protecting active sites. There are mature methods including metal modification, construction of special coreshell structure, selection of better supports and acidification catalysts.

(3) Although the reported methods have been proved to be helpful to improve the anti-SO₂ poisoning performance of denitration catalyst, the mechanism of anti-SO₂ poisoning under complex working conditions is still unclear. It is necessary to further study the anti-SO₂ poisoning mechanism of NH₃-SCR denitration catalyst, especially in the following aspects: (1) properly adjust the acidity and introduce a protective layer to inhibiting SO₂ adsorption; (2) properly reduce the oxidation of active sites to suppression the oxidation of SO₂; (3) realize the dynamic balance between the formation and decomposition of ammonium sulfate, inhibit its deposition of generated sulfate.

In summary, the low-temperature denitration activity and stability of denitration catalyst with the impact of SO_2 is still the focus of future research. It is necessary to develop novel and efficient modification strategy on anti- SO_2 poisoning catalyst to further improve the catalytic performance of NH₃-SCR denitration in low-temperature. It is the future research orientation of low-temperature denitration catalyst regeneration to match the online thermal regeneration and thermal analysis device in the low-temperature denitration to realize online regeneration catalyst.

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Notes

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