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# rac-(Z)-Methyl 1-benzyl-3-[(3-hydroxyquinuclidin-2-ylidene)methyl]-1H-indole-6-carboxylate

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Key indicators: single-crystal X-ray study; T = 90 K; mean  $\sigma$ (C–C) = 0.002 Å; disorder in main residue; R factor = 0.039; wR factor = 0.102; data-to-parameter ratio = 14.7.

In the title compound, C25H26N2O3, the double bond connecting the aza-bicyclic and indole units has Z geometry. The compound was obtained as a racemate, and since the crystal is centrosymmetric it contains equal amounts of the S and R enantiomers. However, the structure is disordered such that the asymmetric unit contains both enantiomers in unequal amounts [refined occupancies 0.904 (2) and 0.096 (2)]. The dihedral angle between the benzene ring of the benzyl group and the mean plane of the indole ring is 76.07 (3) °. In the crystal, molecules are linked by O- $H \cdots O_{carbonvl}$  hydrogen bonds into chains propagating in [110].

#### **Related literature**

For background literature, see: Sekhar et al., (2003), Amudhan et al., (2010). For the biological activity of N-benzyl indole quinuclidinone, see: Sonar et al. (2007). For a similar crystal structure, see: Sonar et al., (2004).



3831 reflections with  $I > 2\sigma(I)$ 

 $R_{\rm int} = 0.024$ 

# **Experimental**

#### Crystal data

$C_{25}H_{26}N_2O_3$	$\gamma = 85.9410 \ (7)^{\circ}$
$M_r = 402.48$	V = 1006.04 (3) Å <sup>3</sup>
Triclinic, P1	Z = 2
a = 6.1619 (1)  Å	Mo $K\alpha$ radiation
b = 10.3119 (2) Å	$\mu = 0.09 \text{ mm}^{-1}$
c = 16.5959 (3) Å	T = 90  K
$\alpha = 75.6705 \ (7)^{\circ}$	$0.28 \times 0.22 \times 0.12 \text{ mm}$
$\beta = 80.0939 \ (7)^{\circ}$	

#### Data collection

Nonius KappaCCD diffractometer 9126 measured reflections 4597 independent reflections

#### Refinement

$R[F^2 > 2\sigma(F^2)] = 0.039$	64 restraints
$wR(F^2) = 0.102$	H-atom parameters constrained
S = 1.04	$\Delta \rho_{\rm max} = 0.27 \ {\rm e} \ {\rm \AA}^{-3}$
4597 reflections	$\Delta \rho_{\rm min} = -0.20 \text{ e } \text{\AA}^{-3}$
312 parameters	

#### Table 1

Hydrogen-bond geometry (Å, °).	
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 $D - H \cdot \cdot \cdot A$ D-H $H \cdot \cdot \cdot A$  $D \cdot \cdot \cdot A$  $D - H \cdot \cdot \cdot A$  $O1 - H1A \cdots O2^{i}$ 0.84 1 97 2.7989 (13) 169

Symmetry code: (i) x - 1, y - 1, z.

Data collection: COLLECT (Nonius, 1998); cell refinement: SCALEPACK (Otwinowski & Minor, 1997); data reduction: DENZO-SMN (Otwinowski & Minor, 1997); program(s) used to solve structure: SHELXS97 (Sheldrick, 2008); program(s) used to refine structure: SHELXL97 (Sheldrick, 2008); molecular graphics: XP in SHELXTL (Sheldrick, 2008); software used to prepare material for publication: SHELXL97 and local procedures.

This investigation was supported by NIH/National Cancer Institute grant PO1 CA140409.

Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: HG5242).

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# supplementary materials

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# *rac-(Z)-*Methyl 1-benzyl-3-[(3-hydroxyquinuclidin-2-ylidene)methyl]-1*H*-indole-6-carboxylate

# Narsimha Reddy Penthala, Purushotham Rao Ponugoti, Sean Parkin and Peter A. Crooks

# Comment

The *N*-benzyl indole quinuclidin-3-one moiety has been found to possess interesting biological properties which range from NADPH oxidase activity (Sekhar *et al.*, 2003), thermal sensitizing activity to radiation treatment (Sonar *et al.*, 2007), and also exhibit antiangiogenic properties (Amudhan *et al.*, 2010). Previously, we reported the crystal structure of *Z*-(*S*)-2-(1- phenylsulfonyl-1*H*-indol-3-ylmethylene)-1-azabicyclo[2.2.2]octan-3-ol (Sonar *et al.*, 2004) and in continuation of our research work on the *N*-benzyl indole quinuclidin-3-one scaffold (Sonar *et al.*, 2007) we designed and synthesized a novel series of carboxymethyl *N*-benzyl indole quinuclidin-3-ones as potent anticancer agents. The title compound was prepared by the reduction of *Z*-methyl 1-benzyl-3-[(3-oxoquinuclidin-2-ylidene)methyl]-1*H*-indole-6- carboxylate with NaBH<sub>4</sub> in methanol at room temperature (Sonar *et al.*, 2004). Recrystallization of the title compound from methanol afforded colorless needles that were suitable for X-ray analysis.

The X-ray studies revealed that the title compound is the Z isomer having the C2—C18 bond in a *trans* position with respect to the C19—C20 bond. The double bond (C18=C19) has a nearly planar atomic arrangement, since the r.m.s. deviation from the best plane passing through atoms N2, C19, C20, C18 and C2 is 0.265 (1) Å. In this molecule, the azabicyclic system presents very small distortions around atoms N2, C24, C21, C22, C23 and C20. The value of the C1—C2 —C18—C19 torsion angle [-5.1 (2)°] indicates the deviation of the indole ring from the plane of the double bond connected to the azabicyclic ring. The dihedral angle between the benzene ring of the benzyl group and with the mean plane of the indole ring is 76.07 (3) Å. The crystal of the title compound is a racemic equimolar mixture of *R* and *S* configurations. However, the structure is disordered such that the asymmetric unit contains both enantiomers, but in unequal amounts [refined occupancies 0.904 (2) and 0.096 (2)]. The hydrogen atom of the disordered OH group is involved in an intermolecular hydrogen bond with the carbonyl oxygen O2 on an adjacent molecule, thus forming an infinite chain-like structure along the (110) direction.

# Experimental

The compound *Z*-methyl 1-benzyl-3-[(3-oxoquinuclidin-2-ylidene)methyl] -1*H*-indole-6-carboxylate was prepared by the available literature procedure (Sonar *et al.*, 2004). To a stirred solution of *Z*-methyl 1-benzyl-3-((3-oxoquinuclidin-2-yl-idene)methyl)-1*H*-indole-6-carboxylate (0.40 g, 1 mmol) in methanol (15 ml) at 273 K was added NaBH<sub>4</sub> (0.38 g, 10 mmol) over a period of 15 min and stirring was continued for 2 h at room temperature. Water (50 ml) was added and the mixture was extracted with CHCl<sub>3</sub> (3 times 10 ml). The combined organic layers were dried over Na<sub>2</sub>SO<sub>4</sub> and evaporated to give the title compound as a white solid. Recrystallization from methanol afforded colorless needles suitable for X-ray analysis.

# Refinement

H atoms were found in difference Fourier maps and subsequently placed in idealized positions with constrained distances of 0.98 Å (RCH<sub>3</sub>), 0.99 Å ( $R_2$ CH<sub>2</sub>), 1.00 Å ( $R_3$ CH), 0.95 Å ( $C_{sp2}$ H), 0.84 Å (O—H), and with  $U_{iso}$ (H) values set to either 1.2 $U_{eq}$  or 1.5 $U_{eq}$  (RCH<sub>3</sub>, OH) of the attached atom.

To ensure satisfactory refinement of the disordered parts of the structure, restraints were needed. The restraints (*SHELXL97* commands SAME, DELU, SAME) were used to ensure similar geometries and displacement parameters of closely proximate, chemically similar groups.

# **Computing details**

Data collection: *COLLECT* (Nonius, 1998); cell refinement: *SCALEPACK* (Otwinowski & Minor, 1997); data reduction: *DENZO-SMN* (Otwinowski & Minor, 1997); program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *XP* in *SHELXTL* (Sheldrick, 2008); software used to prepare material for publication: *SHELXL97* (Sheldrick, 2008) and local procedures.



# Figure 1

A view of the molecule with displacement ellipsoids drawn at the 50% probability level.

## rac-(Z)-Methyl 1-benzyl-3-[(3-hydroxyguinuclidin-2-ylidene)methyl]-1H-indole-6- carboxylate

#### Crystal data

C25H26N2O3  $M_r = 402.48$ Triclinic,  $P\overline{1}$ Hall symbol: -P 1 a = 6.1619(1) Å b = 10.3119(2) Å c = 16.5959 (3) Å  $\alpha = 75.6705 (7)^{\circ}$  $\beta = 80.0939 (7)^{\circ}$  $\gamma = 85.9410 (7)^{\circ}$ V = 1006.04 (3) Å<sup>3</sup>

#### Data collection

Nonius KappaCCD diffractometer Radiation source: fine-focus sealed tube Graphite monochromator Detector resolution: 9.1 pixels mm<sup>-1</sup>  $\omega$  scans at fixed  $\chi = 55^{\circ}$ 9126 measured reflections

#### Refinement

Refinement on  $F^2$ Least-squares matrix: full neighbouring sites  $R[F^2 > 2\sigma(F^2)] = 0.039$  $wR(F^2) = 0.102$ S = 1.044597 reflections  $(\Delta/\sigma)_{\rm max} = 0.001$  $\Delta \rho_{\text{max}} = 0.27 \text{ e} \text{ Å}^{-3}$ 312 parameters  $\Delta \rho_{\rm min} = -0.20 \ {\rm e} \ {\rm \AA}^{-3}$ 64 restraints Primary atom site location: structure-invariant direct methods Secondary atom site location: difference Fourier Extinction coefficient: 0.023 (4) map

## Special details

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

**Refinement**. Refinement of  $F^2$  against all reflections. The weighted *R*-value w*R* and goodness of fit *S* are based on  $F^2$ . Conventional *R*-values *R* are based on *F*, with *F* set to zero for negative  $F^2$ . The threshold expression of  $F^2 > 2\sigma(F^2)$  is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-values based on  $F^2$  are statistically about twice as large as those based on F, and R-values based on ALL data will be even larger.

Z = 2F(000) = 428 $D_{\rm x} = 1.329 {\rm Mg m^{-3}}$ Mo *K* $\alpha$  radiation,  $\lambda = 0.71073$  Å Cell parameters from 4571 reflections  $\theta = 1.0-27.5^{\circ}$  $\mu = 0.09 \text{ mm}^{-1}$ T = 90 KBlock, yellow  $0.28 \times 0.22 \times 0.12 \text{ mm}$ 

4597 independent reflections 3831 reflections with  $I > 2\sigma(I)$  $R_{\rm int} = 0.024$  $\theta_{\max} = 27.5^{\circ}, \ \theta_{\min} = 2.0^{\circ}$  $h = -8 \rightarrow 8$  $k = -13 \rightarrow 13$  $l = -21 \rightarrow 21$ 

Hydrogen site location: inferred from H-atom parameters constrained  $w = 1/[\sigma^2(F_o^2) + (0.0442P)^2 + 0.3522P]$ where  $P = (F_0^2 + 2F_c^2)/3$ Extinction correction: SHELXL,  $Fc^* = kFc[1+0.001xFc^2\lambda^3/sin(2\theta)]^{-1/4}$ 

	x	v	Z	$U_{\rm iso}^*/U_{\rm eq}$	Occ. (<1)
 N1	0 31767 (16)	0 66937 (10)	0 24130 (6)	0.0190(2)	
02	1.05912(15)	0.00557 (10)	0.09629 (6)	0.0190(2) 0.0280(2)	
03	1.05912(13) 1.17472(13)	0.78520(8)	0.09029(0)	0.0200(2) 0.0213(2)	
C1	1.17472(13) 0.1010(2)	0.76520(0) 0.56130(12)	0.00000(3) 0.24673(7)	0.0215(2)	
U1 Н1	0.1919 (2)	0.5379	0.24075(7)	0.0190(2) 0.024*	
$C^2$	0.0015 0.28163 (10)	0.3379 0.40210(11)	0.2801 0.18710 (7)	0.024	
C2 C3	0.28103(19) 0.47803(10)	0.49219(11) 0.56152(11)	0.18719(7) 0.14224(7)	0.0181(2)	
C3	0.47803(19) 0.64453(10)	0.30135(11) 0.52027(11)	0.14234(7) 0.07740(7)	0.0172(2)	
U4	0.04433 (19)	0.33937 (11)	0.07749(7)	0.0180(2) 0.022*	
П <del>4</del> С5	0.0330	0.4077	0.0317	$0.022^{\circ}$	
	0.82107 (19)	0.02300 (11)	0.03107(7)	0.0182 (2)	
	0.9329	0.0092	0.0072	$0.022^{+}$	
C0 C7	0.83809(19)	0.72871(11) 0.75246(11)	0.08999(7)	0.0171(2)	
U7	0.67658 (19)	0.75340 (11)	0.15415 (7)	0.0181(2)	
П/ С9	0.0879	0.8245	0.1802	$0.022^{+}$	
	0.49701 (19)	0.6/018 (11)	0.1/8/5(7)	0.01/1(2)	
C9	1.03202 (19)	0.81587 (11)	0.06408 (7)	0.0184(2)	
	1.3663 (2)	0.86728 (12)	-0.02905 (8)	0.0230 (3)	
HIOA	1.3191	0.9616	-0.0455	0.035*	
HI0B	1.4539	0.8408	-0.0779	0.035*	
HIOC	1.4557	0.8552	0.0159	0.035*	
C11	0.2901 (2)	0.75327 (12)	0.30102 (8)	0.0212 (3)	
H11A	0.1373	0.7463	0.3319	0.025*	
H11B	0.3117	0.8477	0.2696	0.025*	
C12	0.4496 (2)	0.71600 (12)	0.36448 (7)	0.0196 (3)	
C13	0.4619 (2)	0.79843 (13)	0.41841 (8)	0.0248 (3)	
H13	0.3700	0.8769	0.4156	0.030*	
C14	0.6069 (2)	0.76729 (14)	0.47622 (8)	0.0302 (3)	
H14	0.6149	0.8250	0.5122	0.036*	
C15	0.7402 (2)	0.65246 (15)	0.48175 (8)	0.0307 (3)	
H15	0.8390	0.6309	0.5215	0.037*	
C16	0.7282 (2)	0.56959 (14)	0.42883 (8)	0.0300 (3)	
H16	0.8186	0.4905	0.4325	0.036*	
C17	0.5845 (2)	0.60137 (13)	0.37025 (8)	0.0250 (3)	
H17	0.5786	0.5441	0.3338	0.030*	
C18	0.2112 (2)	0.36924 (12)	0.17230 (7)	0.0203 (3)	
H18	0.2905	0.3426	0.1244	0.024*	
C19	0.0490 (3)	0.28894 (14)	0.21750 (9)	0.0190 (3)	0.904 (2)
C20	0.0007 (2)	0.15731 (14)	0.19936 (9)	0.0204 (3)	0.904 (2)
H20	-0.0961	0.1753	0.1550	0.025*	0.904 (2)
01	0.20291 (17)	0.09447 (10)	0.16992 (7)	0.0268 (3)	0.904 (2)
H1A	0.1766	0.0378	0.1445	0.040*	0.904 (2)
C21	-0.1226 (3)	0.07182 (18)	0.28158 (11)	0.0203 (4)	0.904 (2)
H21	-0.1372	-0.0216	0.2763	0.024*	0.904 (2)
C22	0.0068 (3)	0.07145 (14)	0.35275 (9)	0.0237 (3)	0.904 (2)
H22A	0.1614	0.0414	0.3378	0.028*	0.904 (2)
H22B	-0.0598	0.0092	0.4054	0.028*	0.904 (2)
C23	-0.0005 (3)	0.2159 (2)	0.36551 (10)	0.0232 (3)	0.904 (2)

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(\hat{A}^2)$ 

H23A-0.09950.22010.41860.028*0.904 (2)H23B0.14880.23970.37030.028*0.904 (2)N2-0.0804 (3)0.31334 (13)0.29406 (9)0.0209 (3)0.904 (2)H24A-0.36570.34320.24470.031*0.904 (2)H24B-0.40540.31100.34550.031*0.904 (2)H25A-0.42590.09290.35630.029*0.904 (2)H25B-0.44080.13110.25750.029*0.904 (2)C20'0.808 (3)0.1336 (14)0.2189 (9)0.033 (4)*0.096 (2)C19'0.116 (2)0.2718 (12)0.2322 (7)0.013 (3)*0.096 (2)C19'0.1065 (19)0.1428 (11)0.1316 (6)0.035 (3)*0.096 (2)C11'0.1055 (19)0.1428 (11)0.1316 (6)0.035 (3)*0.096 (2)C11'0.1065 (19)0.1428 (11)0.1316 (6)0.035 (3)*0.096 (2)C21'-0.148 (3)0.0902 (19)0.2671 (11)0.039 (5)*0.096 (2)C21'-0.124 (3)0.0512 (14)0.3604 (9)0.036 (4)*0.096 (2)C22'-0.27110.04090.3737 (10)0.022 (4)*0.096 (2)C23'-0.005 (3)0.1654 (15)0.3737 (10)0.022 (4)*0.096 (2)C23'-0.005 (3)0.1654 (15)0.3737 (10)0.022 (4)*0.096 (2)C23'-0.00660.18030.37430.026*0.096 (2)C24'-0.016 (2)0.2938						
H23B $0.1488$ $0.2397$ $0.3703$ $0.028*$ $0.904 (2)$ N2 $-0.0804 (3)$ $0.31334 (13)$ $0.29406 (9)$ $0.0209 (3)$ $0.904 (2)$ C24 $-0.3148 (3)$ $0.28641 (16)$ $0.29584 (10)$ $0.0258 (4)$ $0.904 (2)$ H24A $-0.3657$ $0.3432$ $0.2447$ $0.031*$ $0.904 (2)$ C25 $-0.3496 (2)$ $0.13790 (14)$ $0.29981 (9)$ $0.0243 (3)$ $0.904 (2)$ C25 $-0.3496 (2)$ $0.13790 (14)$ $0.29981 (9)$ $0.0243 (3)$ $0.904 (2)$ L25A $-0.4259$ $0.0929$ $0.3563$ $0.029*$ $0.904 (2)$ C19' $0.116 (2)$ $0.2718 (12)$ $0.2322 (7)$ $0.013 (3)*$ $0.096 (2)$ C19' $0.180 (3)$ $0.1336 (14)$ $0.2189 (9)$ $0.033 (4)*$ $0.096 (2)$ H20' $0.905 (3)$ $0.1336 (14)$ $0.2189 (9)$ $0.033 (4)*$ $0.096 (2)$ C1' $0.1065 (19)$ $0.1428 (11)$ $0.1316 (6)$ $0.335 (3)*$ $0.096 (2)$ C1' $0.1065 (19)$ $0.1428 (11)$ $0.1316 (6)$ $0.335 (3)*$ $0.096 (2)$ C1' $-0.148 (3)$ $0.0902 (19)$ $0.2671 (11)$ $0.039 (5)*$ $0.096 (2)$ H21' $-0.1966$ $0.0125$ $0.2494$ $0.047*$ $0.096 (2)$ H22C $-0.2711$ $0.0409$ $0.3964$ $0.044*$ $0.096 (2)$ H22D $-0.05 (3)$ $0.654 (15)$ $0.3737 (10)$ $0.227 (4)*$ $0.096 (2)$ H22C $-0.0666$ $0.1803$ $0.4300$ $0.027*$ <	H23A	-0.0995	0.2201	0.4186	0.028*	0.904 (2)
N2 $-0.0804 (3)$ $0.31334 (13)$ $0.29406 (9)$ $0.0209 (3)$ $0.904 (2)$ C24 $-0.3148 (3)$ $0.28641 (16)$ $0.29584 (10)$ $0.0258 (4)$ $0.904 (2)$ H24A $-0.3657$ $0.3432$ $0.2447$ $0.031^*$ $0.904 (2)$ H24B $-0.4054$ $0.3110$ $0.3455$ $0.031^*$ $0.904 (2)$ C25 $-0.3496 (2)$ $0.13790 (14)$ $0.29981 (9)$ $0.0243 (3)$ $0.904 (2)$ H25A $-0.4259$ $0.0929$ $0.3563$ $0.029^*$ $0.904 (2)$ H25B $-0.4408$ $0.1311$ $0.2575$ $0.029^*$ $0.904 (2)$ C19' $0.116 (2)$ $0.2718 (12)$ $0.2322 (7)$ $0.013 (3)^*$ $0.096 (2)$ C20' $0.800 (3)$ $0.1336 (14)$ $0.2189 (9)$ $0.033 (4)^*$ $0.096 (2)$ H20' $0.1935$ $0.0690$ $0.2434$ $0.039^*$ $0.096 (2)$ C1' $0.1065 (19)$ $0.1428 (11)$ $0.1316 (6)$ $0.035 (3)^*$ $0.096 (2)$ C1' $-0.148 (3)$ $0.9092 (19)$ $0.2671 (11)$ $0.039 (5)^*$ $0.096 (2)$ C21' $-0.124 (3)$ $0.0512 (14)$ $0.3604 (9)$ $0.036 (4)^*$ $0.096 (2)$ H22D $-0.0383$ $-0.0339$ $0.3739$ $0.044^*$ $0.096 (2)$ H22D $-0.0533$ $-0.0399$ $0.3739$ $0.044^*$ $0.096 (2)$ H22C $-0.2711$ $0.4049$ $0.3743$ $0.027^*$ $0.096 (2)$ H22D $-0.0666$ $1.803$ $0.4300$ $0.027^*$ $0.096 (2)$ <tr<< td=""><td>H23B</td><td>0.1488</td><td>0.2397</td><td>0.3703</td><td>0.028*</td><td>0.904 (2)</td></tr<<>	H23B	0.1488	0.2397	0.3703	0.028*	0.904 (2)
C24 $-0.3148$ (3) $0.28641$ (16) $0.29584$ (10) $0.0258$ (4) $0.904$ (2)H24A $-0.3657$ $0.3432$ $0.2447$ $0.031^*$ $0.904$ (2)H24B $-0.4054$ $0.3110$ $0.3455$ $0.031^*$ $0.904$ (2)C25 $-0.3496$ (2) $0.13790$ (14) $0.29981$ (9) $0.0243$ (3) $0.904$ (2)H25A $-0.4259$ $0.0929$ $0.3563$ $0.029^*$ $0.904$ (2)C19' $0.116$ (2) $0.2718$ (12) $0.2322$ (7) $0.013$ (3)* $0.096$ (2)C20' $0.800$ (3) $0.1336$ (14) $0.2189$ (9) $0.033$ (4)* $0.096$ (2)C19' $0.165$ (19) $0.1428$ (11) $0.1316$ (6) $0.035$ (3)* $0.096$ (2)C10' $0.1065$ (19) $0.1428$ (11) $0.1316$ (6) $0.035$ (3)* $0.096$ (2)C1' $-0.166$ (300) $0.2434$ $0.039^*$ $0.096$ (2)H1' $0.0220$ $0.0896$ $0.1222$ $0.052^*$ $0.096$ (2)C1' $-0.148$ (3) $0.0902$ (19) $0.2671$ (11) $0.039$ (5)* $0.096$ (2)H21' $-0.1966$ $0.0125$ $0.2494$ $0.047^*$ $0.096$ (2)H22D $-0.0383$ $-0.0339$ $0.3739$ $0.044^*$ $0.096$ (2)H22D $-0.005$ (3) $0.1654$ (15) $0.3737$ (10) $0.022$ (4)* $0.096$ (2)H22D $-0.0666$ $0.1803$ $0.4300$ $0.027^*$ $0.096$ (2)H22D $-0.0666$ $0.1803$ $0.3733$ $0.027^*$ $0.096$ (2)H22D	N2	-0.0804 (3)	0.31334 (13)	0.29406 (9)	0.0209 (3)	0.904 (2)
H24A $-0.3657$ $0.3432$ $0.2447$ $0.031*$ $0.904 (2)$ H24B $-0.4054$ $0.3110$ $0.3455$ $0.031*$ $0.904 (2)$ C25 $-0.3496 (2)$ $0.13790 (14)$ $0.29981 (9)$ $0.0243 (3)$ $0.904 (2)$ H25A $-0.4259$ $0.0929$ $0.3563$ $0.029*$ $0.904 (2)$ H25B $-0.4408$ $0.1311$ $0.2575$ $0.029*$ $0.906 (2)$ C19' $0.116 (2)$ $0.2718 (12)$ $0.2322 (7)$ $0.013 (3)*$ $0.096 (2)$ C20' $0.080 (3)$ $0.1335 (14)$ $0.2189 (9)$ $0.033 (4)*$ $0.096 (2)$ H20' $0.1935$ $0.6690$ $0.2434$ $0.039*$ $0.096 (2)$ C1' $0.1065 (19)$ $0.1428 (11)$ $0.1316 (6)$ $0.35 (3)*$ $0.096 (2)$ C1' $-0.148 (3)$ $0.0902 (19)$ $0.2671 (11)$ $0.039 (5)*$ $0.096 (2)$ C2' $-0.148 (3)$ $0.0902 (19)$ $0.2671 (11)$ $0.039 (5)*$ $0.096 (2)$ C22' $-0.124 (3)$ $0.0512 (14)$ $0.3604 (9)$ $0.036 (4)*$ $0.096 (2)$ H21' $-0.1966$ $0.0125$ $0.2494$ $0.047*$ $0.096 (2)$ H22D $-0.0383$ $-0.0339$ $0.3739$ $0.044*$ $0.096 (2)$ H22D $-0.0383$ $-0.0339$ $0.3739$ $0.044*$ $0.096 (2)$ H22D $-0.0383$ $-0.0339$ $0.3737 (10)$ $0.022 (4)*$ $0.096 (2)$ H23D $0.1519$ $0.1378$ $0.3743$ $0.027*$ $0.096 (2)$ H23D $0.1519$	C24	-0.3148 (3)	0.28641 (16)	0.29584 (10)	0.0258 (4)	0.904 (2)
H24B $-0.4054$ $0.3110$ $0.3455$ $0.031^*$ $0.904 (2)$ C25 $-0.3496 (2)$ $0.13790 (14)$ $0.29981 (9)$ $0.0243 (3)$ $0.904 (2)$ H25A $-0.4259$ $0.0929$ $0.3563$ $0.029^*$ $0.904 (2)$ H25B $-0.4408$ $0.1311$ $0.2575$ $0.029^*$ $0.904 (2)$ C19' $0.116 (2)$ $0.2718 (12)$ $0.2322 (7)$ $0.013 (3)^*$ $0.096 (2)$ C20' $0.080 (3)$ $0.1336 (14)$ $0.2189 (9)$ $0.033 (4)^*$ $0.096 (2)$ D1' $0.1065 (19)$ $0.1428 (11)$ $0.1316 (6)$ $0.035 (3)^*$ $0.096 (2)$ C1' $0.1065 (19)$ $0.1428 (11)$ $0.1316 (6)$ $0.035 (3)^*$ $0.096 (2)$ C1' $0.1065 (19)$ $0.1428 (11)$ $0.1316 (6)$ $0.035 (3)^*$ $0.096 (2)$ C21' $-0.148 (3)$ $0.0902 (19)$ $0.2671 (11)$ $0.039 (5)^*$ $0.096 (2)$ C21' $-0.148 (3)$ $0.0902 (19)$ $0.2671 (11)$ $0.036 (4)^*$ $0.096 (2)$ C22' $-0.124 (3)$ $0.512 (14)$ $0.3604 (9)$ $0.36 (4)^*$ $0.096 (2)$ H22D $-0.0333$ $-0.0339$ $0.3737 (10)$ $0.022 (4)^*$ $0.096 (2)$ H23C $-0.0666$ $0.1803$ $0.3737 (10)$ $0.022 (4)^*$ $0.096 (2)$ H23D $0.1519$ $0.1378$ $0.3743$ $0.027^*$ $0.096 (2)$ H23D $0.1519$ $0.3146 (15)$ $0.2931 (10)$ $0.026 (*)$ $0.096 (2)$ H24C $-0.240 (3)$ $0.3146 (15)$ $0.2931 ($	H24A	-0.3657	0.3432	0.2447	0.031*	0.904 (2)
C25 $-0.3496 (2)$ $0.13790 (14)$ $0.29981 (9)$ $0.0243 (3)$ $0.904 (2)$ H25A $-0.4259$ $0.0929$ $0.3563$ $0.029^*$ $0.904 (2)$ H25B $-0.4408$ $0.1311$ $0.2575$ $0.029^*$ $0.904 (2)$ C19' $0.116 (2)$ $0.2718 (12)$ $0.2322 (7)$ $0.013 (3)^*$ $0.096 (2)$ C20' $0.080 (3)$ $0.1336 (14)$ $0.2189 (9)$ $0.033 (4)^*$ $0.096 (2)$ H20' $0.1935$ $0.0690$ $0.2434$ $0.039^*$ $0.096 (2)$ O1' $0.1065 (19)$ $0.1428 (11)$ $0.1316 (6)$ $0.035 (3)^*$ $0.096 (2)$ H1' $0.0220$ $0.0896$ $0.1222$ $0.052^*$ $0.096 (2)$ C21' $-0.148 (3)$ $0.0902 (19)$ $0.2671 (11)$ $0.039 (5)^*$ $0.096 (2)$ H21' $-0.1966$ $0.0125$ $0.2494$ $0.047^*$ $0.096 (2)$ H22C $-0.2711$ $0.0409$ $0.3964$ $0.044^*$ $0.096 (2)$ H22D $-0.0383$ $-0.0339$ $0.3737 (10)$ $0.22 (4)^*$ $0.096 (2)$ H23C $-0.0666$ $0.1803$ $0.4300$ $0.27^*$ $0.096 (2)$ H23D $0.1519$ $0.1378$ $0.3743$ $0.027^*$ $0.096 (2)$ H23D $0.1519$ $0.3146 (15)$ $0.2931 (10)$ $0.022 (4)^*$ $0.096 (2)$ H23D $0.1519$ $0.3146 (15)$ $0.2931 (10)$ $0.026^*$ $0.096 (2)$ H24C $-0.240 (3)$ $0.3146 (15)$ $0.2931 (10)$ $0.026^*$ $0.096 (2)$ H24C </td <td>H24B</td> <td>-0.4054</td> <td>0.3110</td> <td>0.3455</td> <td>0.031*</td> <td>0.904 (2)</td>	H24B	-0.4054	0.3110	0.3455	0.031*	0.904 (2)
H25A $-0.4259$ $0.0929$ $0.3563$ $0.029^*$ $0.904$ (2)H25B $-0.4408$ $0.1311$ $0.2575$ $0.029^*$ $0.904$ (2)C19' $0.116$ (2) $0.2718$ (12) $0.2322$ (7) $0.013$ (3)* $0.096$ (2)C20' $0.080$ (3) $0.1336$ (14) $0.2189$ (9) $0.033$ (4)* $0.096$ (2)H20' $0.1935$ $0.0690$ $0.2434$ $0.039^*$ $0.096$ (2)O1' $0.1065$ (19) $0.1428$ (11) $0.1316$ (6) $0.035$ (3)* $0.096$ (2)H1' $0.0220$ $0.0896$ $0.1222$ $0.052^*$ $0.096$ (2)C21' $-0.148$ (3) $0.0902$ (19) $0.2671$ (11) $0.039$ (5)* $0.096$ (2)H21' $-0.1966$ $0.0125$ $0.2494$ $0.047^*$ $0.096$ (2)H22C $-0.2711$ $0.0409$ $0.3604$ (9) $0.036$ (4)* $0.096$ (2)H22D $-0.0383$ $-0.0339$ $0.3739$ $0.044^*$ $0.096$ (2)H23C $-0.05$ (3) $0.1654$ (15) $0.3737$ (10) $0.022$ (4)* $0.096$ (2)H23D $0.1519$ $0.1378$ $0.3743$ $0.027^*$ $0.096$ (2)H23D $0.1519$ $0.3748$ $0.3743$ $0.027^*$ $0.096$ (2)L24' $-0.240$ (3) $0.3146$ (15) $0.2931$ (10) $0.022$ (4)* $0.096$ (2)L24C $-0.2543$ $0.4049$ $0.2558$ $0.026^*$ $0.096$ (2)L24C $-0.3418$ $0.3118$ $0.3465$ $0.026^*$ $0.096$ (2)L25C $-0.3010$ (2)<	C25	-0.3496 (2)	0.13790 (14)	0.29981 (9)	0.0243 (3)	0.904 (2)
H25B-0.44080.13110.25750.029*0.904 (2)C19'0.116 (2)0.2718 (12)0.2322 (7)0.013 (3)*0.096 (2)C20'0.080 (3)0.1336 (14)0.2189 (9)0.033 (4)*0.096 (2)H20'0.19350.06900.24340.039*0.096 (2)O1'0.1065 (19)0.1428 (11)0.1316 (6)0.035 (3)*0.096 (2)H1'0.02200.08960.12220.052*0.096 (2)C21'-0.148 (3)0.0902 (19)0.2671 (11)0.039 (5)*0.096 (2)H21'-0.19660.01250.24940.047*0.096 (2)C22'-0.124 (3)0.0512 (14)0.3604 (9)0.036 (4)*0.096 (2)H22D-0.0383-0.03390.37390.044*0.096 (2)H23D-0.05 (3)0.1654 (15)0.3737 (10)0.022 (4)*0.096 (2)H23D0.15190.13780.37430.027*0.096 (2)H23D0.15190.13780.37430.027*0.096 (2)H24D-0.240 (3)0.3146 (15)0.2931 (10)0.022 (4)*0.096 (2)H24D-0.240 (3)0.3146 (15)0.2931 (10)0.022 (4)*0.096 (2)H24D-0.34180.31180.34650.026*0.096 (2)H24D-0.34180.31180.34650.026*0.096 (2)H25D-0.46290.18160.27520.043*0.096 (2)	H25A	-0.4259	0.0929	0.3563	0.029*	0.904 (2)
C19' $0.116 (2)$ $0.2718 (12)$ $0.2322 (7)$ $0.013 (3)^*$ $0.096 (2)$ C20' $0.080 (3)$ $0.1336 (14)$ $0.2189 (9)$ $0.033 (4)^*$ $0.096 (2)$ H20' $0.1935$ $0.0690$ $0.2434$ $0.039^*$ $0.096 (2)$ O1' $0.1065 (19)$ $0.1428 (11)$ $0.1316 (6)$ $0.035 (3)^*$ $0.096 (2)$ H1' $0.0220$ $0.0896$ $0.1222$ $0.052^*$ $0.096 (2)$ C21' $-0.148 (3)$ $0.0902 (19)$ $0.2671 (11)$ $0.039 (5)^*$ $0.096 (2)$ H21' $-0.1966$ $0.0125$ $0.2494$ $0.047^*$ $0.096 (2)$ C22' $-0.124 (3)$ $0.0512 (14)$ $0.3604 (9)$ $0.036 (4)^*$ $0.096 (2)$ H22D $-0.0383$ $-0.0339$ $0.3739$ $0.044^*$ $0.096 (2)$ H22D $-0.005 (3)$ $0.1654 (15)$ $0.3737 (10)$ $0.022 (4)^*$ $0.096 (2)$ H23C $-0.005 (3)$ $0.1654 (15)$ $0.3737 (10)$ $0.022 (4)^*$ $0.096 (2)$ H23D $0.1519$ $0.1378$ $0.3743$ $0.027^*$ $0.096 (2)$ H24D $-0.240 (3)$ $0.3146 (15)$ $0.2931 (10)$ $0.022 (4)^*$ $0.096 (2)$ H24D $-0.3418$ $0.3118$ $0.3465$ $0.026^*$ $0.096 (2)$ H24D $-0.3418$ $0.3118$ $0.3465$ $0.026^*$ $0.096 (2)$ H24D $-0.3418$ $0.3118$ $0.3465$ $0.026^*$ $0.096 (2)$ H25D $-0.3038$ $0.2475$ $0.1893$ $0.043^*$ $0.096 (2)$ <td>H25B</td> <td>-0.4408</td> <td>0.1311</td> <td>0.2575</td> <td>0.029*</td> <td>0.904 (2)</td>	H25B	-0.4408	0.1311	0.2575	0.029*	0.904 (2)
C20' $0.080(3)$ $0.1336(14)$ $0.2189(9)$ $0.033(4)*$ $0.096(2)$ H20' $0.1935$ $0.0690$ $0.2434$ $0.039*$ $0.096(2)$ O1' $0.1065(19)$ $0.1428(11)$ $0.1316(6)$ $0.035(3)*$ $0.096(2)$ H1' $0.0220$ $0.0896$ $0.1222$ $0.052*$ $0.096(2)$ C21' $-0.148(3)$ $0.0902(19)$ $0.2671(11)$ $0.039(5)*$ $0.096(2)$ H21' $-0.1966$ $0.0125$ $0.2494$ $0.047*$ $0.096(2)$ C22' $-0.124(3)$ $0.0512(14)$ $0.3604(9)$ $0.036(4)*$ $0.096(2)$ H22C $-0.2711$ $0.0409$ $0.3964$ $0.044*$ $0.096(2)$ H22D $-0.0383$ $-0.0339$ $0.3739$ $0.044*$ $0.096(2)$ H23C $-0.005(3)$ $0.1654(15)$ $0.3737(10)$ $0.022(4)*$ $0.096(2)$ H23D $0.1519$ $0.1378$ $0.3743$ $0.027*$ $0.096(2)$ H23D $0.1519$ $0.378(14)$ $0.3109(8)$ $0.021(3)*$ $0.096(2)$ H24C $-0.240(3)$ $0.3146(15)$ $0.2931(10)$ $0.022(4)*$ $0.096(2)$ H24D $-0.3418$ $0.3118$ $0.3465$ $0.026*$ $0.096(2)$ H24D $-0.310(2)$ $0.2096(15)$ $0.2506(10)$ $0.036(4)*$ $0.096(2)$ H25D $-0.3038$ $0.2475$ $0.1893$ $0.043*$ $0.096(2)$	C19′	0.116 (2)	0.2718 (12)	0.2322 (7)	0.013 (3)*	0.096 (2)
H20'0.19350.06900.24340.039*0.096 (2)O1'0.1065 (19)0.1428 (11)0.1316 (6)0.035 (3)*0.096 (2)H1'0.02200.08960.12220.052*0.096 (2)C21'-0.148 (3)0.0902 (19)0.2671 (11)0.039 (5)*0.096 (2)H21'-0.19660.01250.24940.047*0.096 (2)C22'-0.124 (3)0.0512 (14)0.3604 (9)0.036 (4)*0.096 (2)H22D-0.27110.04090.39640.044*0.096 (2)H22D-0.0383-0.03390.37390.044*0.096 (2)C23'-0.005 (3)0.1654 (15)0.3737 (10)0.022 (4)*0.096 (2)H23D0.15190.13780.37430.027*0.096 (2)H23D0.15190.13780.37430.027*0.096 (2)K2'-0.016 (2)0.2938 (14)0.3109 (8)0.021 (3)*0.096 (2)H24C-0.25430.40490.25580.026*0.096 (2)H24D-0.34180.31180.34650.026*0.096 (2)H24D-0.310 (2)0.2096 (15)0.2506 (10)0.036 (4)*0.096 (2)H25D-0.30380.24750.18930.043*0.096 (2)	C20′	0.080 (3)	0.1336 (14)	0.2189 (9)	0.033 (4)*	0.096 (2)
$O1'$ $0.1065(19)$ $0.1428(11)$ $0.1316(6)$ $0.035(3)^*$ $0.096(2)$ $H1'$ $0.0220$ $0.0896$ $0.1222$ $0.052^*$ $0.096(2)$ $C21'$ $-0.148(3)$ $0.0902(19)$ $0.2671(11)$ $0.039(5)^*$ $0.096(2)$ $H21'$ $-0.1966$ $0.0125$ $0.2494$ $0.047^*$ $0.096(2)$ $C22'$ $-0.124(3)$ $0.0512(14)$ $0.3604(9)$ $0.036(4)^*$ $0.096(2)$ $H22C$ $-0.2711$ $0.0409$ $0.3964$ $0.044^*$ $0.096(2)$ $H22D$ $-0.0383$ $-0.0339$ $0.3739$ $0.044^*$ $0.096(2)$ $C23'$ $-0.005(3)$ $0.1654(15)$ $0.3737(10)$ $0.022(4)^*$ $0.096(2)$ $H23D$ $0.1519$ $0.1378$ $0.3743$ $0.027^*$ $0.096(2)$ $H24C$ $-0.240(3)$ $0.3146(15)$ $0.2931(10)$ $0.022(4)^*$ $0.096(2)$ $H24D$ $-0.3418$ $0.3118$ $0.3465$ $0.026^*$ $0.096(2)$ $H24D$ $-0.3418$ $0.3118$ $0.3465$ $0.026^*$ $0.096(2)$ $H25D$ $-0.3038$ $0.2475$ $0.1893$ $0.43^*$ $0.096(2)$	H20′	0.1935	0.0690	0.2434	0.039*	0.096 (2)
H1'0.02200.08960.12220.052*0.096 (2)C21'-0.148 (3)0.0902 (19)0.2671 (11)0.039 (5)*0.096 (2)H21'-0.19660.01250.24940.047*0.096 (2)C22'-0.124 (3)0.0512 (14)0.3604 (9)0.036 (4)*0.096 (2)H22C-0.27110.04090.39640.044*0.096 (2)H22D-0.0383-0.03390.37390.044*0.096 (2)C23'-0.005 (3)0.1654 (15)0.3737 (10)0.022 (4)*0.096 (2)H23D-0.15190.13780.37430.027*0.096 (2)H23D0.15190.13780.37430.021 (3)*0.096 (2)N2'-0.016 (2)0.2938 (14)0.3109 (8)0.021 (3)*0.096 (2)H24C-0.25430.40490.25580.026*0.096 (2)H24D-0.34180.31180.34650.026*0.096 (2)H25D-0.30380.24750.18930.043*0.096 (2)	O1′	0.1065 (19)	0.1428 (11)	0.1316 (6)	0.035 (3)*	0.096 (2)
C21' $-0.148(3)$ $0.0902(19)$ $0.2671(11)$ $0.039(5)^*$ $0.096(2)$ H21' $-0.1966$ $0.0125$ $0.2494$ $0.047^*$ $0.096(2)$ C22' $-0.124(3)$ $0.0512(14)$ $0.3604(9)$ $0.036(4)^*$ $0.096(2)$ H22C $-0.2711$ $0.0409$ $0.3964$ $0.044^*$ $0.096(2)$ H22D $-0.0383$ $-0.0339$ $0.3739$ $0.044^*$ $0.096(2)$ C23' $-0.005(3)$ $0.1654(15)$ $0.3737(10)$ $0.022(4)^*$ $0.096(2)$ H23C $-0.6666$ $0.1803$ $0.4300$ $0.027^*$ $0.096(2)$ H23D $0.1519$ $0.1378$ $0.3743$ $0.027^*$ $0.096(2)$ N2' $-0.016(2)$ $0.2938(14)$ $0.3109(8)$ $0.021(3)^*$ $0.096(2)$ H24C $-0.2543$ $0.4049$ $0.2558$ $0.026^*$ $0.096(2)$ H24D $-0.3418$ $0.3118$ $0.3465$ $0.026^*$ $0.096(2)$ H25C $-0.4629$ $0.1816$ $0.2752$ $0.43^*$ $0.096(2)$ H25D $-0.3038$ $0.2475$ $0.1893$ $0.043^*$ $0.096(2)$	H1′	0.0220	0.0896	0.1222	0.052*	0.096 (2)
H21' $-0.1966$ $0.0125$ $0.2494$ $0.047*$ $0.096(2)$ C22' $-0.124(3)$ $0.0512(14)$ $0.3604(9)$ $0.036(4)*$ $0.096(2)$ H22C $-0.2711$ $0.0409$ $0.3964$ $0.044*$ $0.096(2)$ H22D $-0.0383$ $-0.0339$ $0.3739$ $0.044*$ $0.096(2)$ C23' $-0.005(3)$ $0.1654(15)$ $0.3737(10)$ $0.022(4)*$ $0.096(2)$ H23C $-0.0666$ $0.1803$ $0.4300$ $0.027*$ $0.096(2)$ H23D $0.1519$ $0.1378$ $0.3743$ $0.027*$ $0.096(2)$ N2' $-0.016(2)$ $0.2938(14)$ $0.3109(8)$ $0.021(3)*$ $0.096(2)$ C24' $-0.240(3)$ $0.3146(15)$ $0.2931(10)$ $0.022(4)*$ $0.096(2)$ H24D $-0.3418$ $0.3118$ $0.3465$ $0.026*$ $0.096(2)$ H24D $-0.310(2)$ $0.2096(15)$ $0.2506(10)$ $0.036(4)*$ $0.096(2)$ H25C $-0.4629$ $0.1816$ $0.2752$ $0.043*$ $0.096(2)$ H25D $-0.3038$ $0.2475$ $0.1893$ $0.043*$ $0.096(2)$	C21′	-0.148 (3)	0.0902 (19)	0.2671 (11)	0.039 (5)*	0.096 (2)
C22' $-0.124 (3)$ $0.0512 (14)$ $0.3604 (9)$ $0.036 (4)^*$ $0.096 (2)$ H22C $-0.2711$ $0.0409$ $0.3964$ $0.044^*$ $0.096 (2)$ H22D $-0.0383$ $-0.0339$ $0.3739$ $0.044^*$ $0.096 (2)$ C23' $-0.005 (3)$ $0.1654 (15)$ $0.3737 (10)$ $0.022 (4)^*$ $0.096 (2)$ H23C $-0.0666$ $0.1803$ $0.4300$ $0.027^*$ $0.096 (2)$ H23D $0.1519$ $0.1378$ $0.3743$ $0.027^*$ $0.096 (2)$ N2' $-0.016 (2)$ $0.2938 (14)$ $0.3109 (8)$ $0.021 (3)^*$ $0.096 (2)$ C24' $-0.240 (3)$ $0.3146 (15)$ $0.2931 (10)$ $0.022 (4)^*$ $0.096 (2)$ H24C $-0.2543$ $0.4049$ $0.2558$ $0.026^*$ $0.096 (2)$ H24D $-0.3418$ $0.3118$ $0.3465$ $0.026^*$ $0.096 (2)$ H25C $-0.4629$ $0.1816$ $0.2752$ $0.043^*$ $0.096 (2)$ H25D $-0.3038$ $0.2475$ $0.1893$ $0.043^*$ $0.096 (2)$	H21′	-0.1966	0.0125	0.2494	0.047*	0.096 (2)
H22C $-0.2711$ $0.0409$ $0.3964$ $0.044*$ $0.096(2)$ H22D $-0.0383$ $-0.0339$ $0.3739$ $0.044*$ $0.096(2)$ C23' $-0.005(3)$ $0.1654(15)$ $0.3737(10)$ $0.022(4)*$ $0.096(2)$ H23C $-0.0666$ $0.1803$ $0.4300$ $0.027*$ $0.096(2)$ H23D $0.1519$ $0.1378$ $0.3743$ $0.027*$ $0.096(2)$ N2' $-0.016(2)$ $0.2938(14)$ $0.3109(8)$ $0.021(3)*$ $0.096(2)$ C24' $-0.240(3)$ $0.3146(15)$ $0.2931(10)$ $0.022(4)*$ $0.096(2)$ H24C $-0.2543$ $0.4049$ $0.2558$ $0.026*$ $0.096(2)$ H24D $-0.3418$ $0.3118$ $0.3465$ $0.026*$ $0.096(2)$ H25C $-0.4629$ $0.1816$ $0.2752$ $0.043*$ $0.096(2)$ H25D $-0.3038$ $0.2475$ $0.1893$ $0.043*$ $0.096(2)$	C22′	-0.124 (3)	0.0512 (14)	0.3604 (9)	0.036 (4)*	0.096 (2)
H22D $-0.0383$ $-0.0339$ $0.3739$ $0.044*$ $0.096(2)$ C23' $-0.005(3)$ $0.1654(15)$ $0.3737(10)$ $0.022(4)*$ $0.096(2)$ H23C $-0.0666$ $0.1803$ $0.4300$ $0.027*$ $0.096(2)$ H23D $0.1519$ $0.1378$ $0.3743$ $0.027*$ $0.096(2)$ N2' $-0.016(2)$ $0.2938(14)$ $0.3109(8)$ $0.021(3)*$ $0.096(2)$ C24' $-0.240(3)$ $0.3146(15)$ $0.2931(10)$ $0.022(4)*$ $0.096(2)$ H24C $-0.2543$ $0.4049$ $0.2558$ $0.026*$ $0.096(2)$ H24D $-0.3418$ $0.3118$ $0.3465$ $0.026*$ $0.096(2)$ H25C $-0.4629$ $0.1816$ $0.2752$ $0.043*$ $0.096(2)$ H25D $-0.3038$ $0.2475$ $0.1893$ $0.043*$ $0.096(2)$	H22C	-0.2711	0.0409	0.3964	0.044*	0.096 (2)
C23' $-0.005(3)$ $0.1654(15)$ $0.3737(10)$ $0.022(4)*$ $0.096(2)$ H23C $-0.0666$ $0.1803$ $0.4300$ $0.027*$ $0.096(2)$ H23D $0.1519$ $0.1378$ $0.3743$ $0.027*$ $0.096(2)$ N2' $-0.016(2)$ $0.2938(14)$ $0.3109(8)$ $0.021(3)*$ $0.096(2)$ C24' $-0.240(3)$ $0.3146(15)$ $0.2931(10)$ $0.022(4)*$ $0.096(2)$ H24C $-0.2543$ $0.4049$ $0.2558$ $0.026*$ $0.096(2)$ H24D $-0.3418$ $0.3118$ $0.3465$ $0.026*$ $0.096(2)$ C25' $-0.310(2)$ $0.2096(15)$ $0.2506(10)$ $0.036(4)*$ $0.096(2)$ H25D $-0.3038$ $0.2475$ $0.1893$ $0.043*$ $0.096(2)$	H22D	-0.0383	-0.0339	0.3739	0.044*	0.096 (2)
H23C $-0.0666$ $0.1803$ $0.4300$ $0.027^*$ $0.096(2)$ H23D $0.1519$ $0.1378$ $0.3743$ $0.027^*$ $0.096(2)$ N2' $-0.016(2)$ $0.2938(14)$ $0.3109(8)$ $0.021(3)^*$ $0.096(2)$ C24' $-0.240(3)$ $0.3146(15)$ $0.2931(10)$ $0.022(4)^*$ $0.096(2)$ H24C $-0.2543$ $0.4049$ $0.2558$ $0.026^*$ $0.096(2)$ H24D $-0.3418$ $0.3118$ $0.3465$ $0.026^*$ $0.096(2)$ C25' $-0.310(2)$ $0.2096(15)$ $0.2506(10)$ $0.036(4)^*$ $0.096(2)$ H25C $-0.4629$ $0.1816$ $0.2752$ $0.043^*$ $0.096(2)$ H25D $-0.3038$ $0.2475$ $0.1893$ $0.043^*$ $0.096(2)$	C23′	-0.005 (3)	0.1654 (15)	0.3737 (10)	0.022 (4)*	0.096 (2)
H23D $0.1519$ $0.1378$ $0.3743$ $0.027^*$ $0.096(2)$ N2' $-0.016(2)$ $0.2938(14)$ $0.3109(8)$ $0.021(3)^*$ $0.096(2)$ C24' $-0.240(3)$ $0.3146(15)$ $0.2931(10)$ $0.022(4)^*$ $0.096(2)$ H24C $-0.2543$ $0.4049$ $0.2558$ $0.026^*$ $0.096(2)$ H24D $-0.3418$ $0.3118$ $0.3465$ $0.026^*$ $0.096(2)$ C25' $-0.310(2)$ $0.2096(15)$ $0.2506(10)$ $0.036(4)^*$ $0.096(2)$ H25C $-0.4629$ $0.1816$ $0.2752$ $0.043^*$ $0.096(2)$ H25D $-0.3038$ $0.2475$ $0.1893$ $0.043^*$ $0.096(2)$	H23C	-0.0666	0.1803	0.4300	0.027*	0.096 (2)
N2' $-0.016(2)$ $0.2938(14)$ $0.3109(8)$ $0.021(3)^*$ $0.096(2)$ C24' $-0.240(3)$ $0.3146(15)$ $0.2931(10)$ $0.022(4)^*$ $0.096(2)$ H24C $-0.2543$ $0.4049$ $0.2558$ $0.026^*$ $0.096(2)$ H24D $-0.3418$ $0.3118$ $0.3465$ $0.026^*$ $0.096(2)$ C25' $-0.310(2)$ $0.2096(15)$ $0.2506(10)$ $0.036(4)^*$ $0.096(2)$ H25C $-0.4629$ $0.1816$ $0.2752$ $0.043^*$ $0.096(2)$ H25D $-0.3038$ $0.2475$ $0.1893$ $0.043^*$ $0.096(2)$	H23D	0.1519	0.1378	0.3743	0.027*	0.096 (2)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	N2′	-0.016 (2)	0.2938 (14)	0.3109 (8)	0.021 (3)*	0.096 (2)
H24C-0.25430.40490.25580.026*0.096 (2)H24D-0.34180.31180.34650.026*0.096 (2)C25'-0.310 (2)0.2096 (15)0.2506 (10)0.036 (4)*0.096 (2)H25C-0.46290.18160.27520.043*0.096 (2)H25D-0.30380.24750.18930.043*0.096 (2)	C24′	-0.240 (3)	0.3146 (15)	0.2931 (10)	0.022 (4)*	0.096 (2)
H24D-0.34180.31180.34650.026*0.096 (2)C25'-0.310 (2)0.2096 (15)0.2506 (10)0.036 (4)*0.096 (2)H25C-0.46290.18160.27520.043*0.096 (2)H25D-0.30380.24750.18930.043*0.096 (2)	H24C	-0.2543	0.4049	0.2558	0.026*	0.096 (2)
C25'-0.310 (2)0.2096 (15)0.2506 (10)0.036 (4)*0.096 (2)H25C-0.46290.18160.27520.043*0.096 (2)H25D-0.30380.24750.18930.043*0.096 (2)	H24D	-0.3418	0.3118	0.3465	0.026*	0.096 (2)
H25C-0.46290.18160.27520.043*0.096 (2)H25D-0.30380.24750.18930.043*0.096 (2)	C25′	-0.310 (2)	0.2096 (15)	0.2506 (10)	0.036 (4)*	0.096 (2)
<u>H25D</u> -0.3038 0.2475 0.1893 0.043* 0.096 (2)	H25C	-0.4629	0.1816	0.2752	0.043*	0.096 (2)
	H25D	-0.3038	0.2475	0.1893	0.043*	0.096 (2)

Atomic displacement parameters  $(Å^2)$ 

	$U^{11}$	$U^{22}$	$U^{33}$	$U^{12}$	$U^{13}$	$U^{23}$
N1	0.0196 (5)	0.0182 (5)	0.0198 (5)	-0.0002 (4)	-0.0017 (4)	-0.0068 (4)
O2	0.0274 (5)	0.0277 (5)	0.0337 (5)	-0.0079 (4)	-0.0019 (4)	-0.0166 (4)
03	0.0178 (4)	0.0223 (4)	0.0242 (4)	-0.0048 (3)	-0.0004 (3)	-0.0073 (3)
C1	0.0183 (6)	0.0188 (6)	0.0211 (6)	-0.0006 (4)	-0.0034 (5)	-0.0034 (5)
C2	0.0179 (6)	0.0178 (5)	0.0182 (5)	-0.0005 (4)	-0.0045 (4)	-0.0027 (4)
C3	0.0180 (6)	0.0162 (5)	0.0174 (5)	0.0000 (4)	-0.0057 (4)	-0.0023 (4)
C4	0.0208 (6)	0.0173 (5)	0.0177 (5)	-0.0005 (4)	-0.0047 (4)	-0.0061 (4)
C5	0.0176 (6)	0.0194 (6)	0.0182 (5)	0.0007 (4)	-0.0028 (4)	-0.0058 (4)
C6	0.0177 (6)	0.0165 (5)	0.0178 (5)	-0.0008 (4)	-0.0060 (4)	-0.0033 (4)
C7	0.0209 (6)	0.0156 (5)	0.0192 (6)	0.0006 (4)	-0.0063 (5)	-0.0055 (4)
C8	0.0181 (6)	0.0169 (5)	0.0163 (5)	0.0018 (4)	-0.0039 (4)	-0.0038 (4)
C9	0.0186 (6)	0.0181 (6)	0.0194 (6)	0.0008 (4)	-0.0061 (5)	-0.0048 (4)
C10	0.0173 (6)	0.0235 (6)	0.0273 (6)	-0.0051 (5)	-0.0028 (5)	-0.0037 (5)
C11	0.0233 (6)	0.0190 (6)	0.0223 (6)	0.0025 (5)	-0.0014 (5)	-0.0088(5)
C12	0.0206 (6)	0.0184 (6)	0.0179 (5)	-0.0025 (4)	0.0014 (4)	-0.0034 (4)
C13	0.0289 (7)	0.0210 (6)	0.0245 (6)	-0.0008 (5)	-0.0021 (5)	-0.0070 (5)

C14	0.0375 (8)	0.0316 (7)	0.0244 (7)	-0.0059 (6)	-0.0052 (6)	-0.0106 (5)
C15	0.0287 (7)	0.0395 (8)	0.0236 (6)	-0.0015 (6)	-0.0069 (5)	-0.0052 (6)
C16	0.0288 (7)	0.0320 (7)	0.0263 (7)	0.0078 (6)	-0.0034 (5)	-0.0049 (6)
C17	0.0300 (7)	0.0230 (6)	0.0218 (6)	0.0029 (5)	-0.0030 (5)	-0.0069 (5)
C18	0.0220 (6)	0.0209 (6)	0.0191 (6)	-0.0019 (5)	-0.0033 (5)	-0.0062 (5)
C19	0.0175 (7)	0.0211 (7)	0.0195 (7)	0.0005 (6)	-0.0064 (6)	-0.0048 (5)
C20	0.0179 (7)	0.0246 (7)	0.0207 (7)	-0.0037 (5)	-0.0028 (6)	-0.0082 (5)
01	0.0232 (5)	0.0290 (6)	0.0325 (6)	-0.0072 (4)	0.0033 (4)	-0.0194 (5)
C21	0.0188 (7)	0.0180 (7)	0.0250 (8)	-0.0030 (5)	-0.0025 (6)	-0.0066 (6)
C22	0.0238 (8)	0.0230 (7)	0.0233 (7)	0.0025 (6)	-0.0058 (6)	-0.0035 (5)
C23	0.0242 (8)	0.0260 (9)	0.0215 (8)	-0.0027 (7)	-0.0035 (5)	-0.0095 (7)
N2	0.0193 (8)	0.0196 (6)	0.0230 (7)	-0.0018 (5)	-0.0001 (6)	-0.0055 (5)
C24	0.0156 (8)	0.0233 (8)	0.0344 (9)	0.0021 (6)	-0.0008 (6)	-0.0025 (6)
C25	0.0174 (7)	0.0251 (7)	0.0302 (8)	-0.0037 (5)	-0.0030 (5)	-0.0059 (6)

Geometric parameters (Å, °)

N1—C1	1.3772 (15)	C19—C20	1.5204 (18)
N1—C8	1.3787 (15)	C20—O1	1.4296 (18)
N1-C11	1.4510 (15)	C20—C21	1.536 (2)
О2—С9	1.2174 (14)	C20—H20	1.0000
О3—С9	1.3334 (14)	O1—H1A	0.8400
O3—C10	1.4450 (14)	C21—C25	1.528 (2)
C1—C2	1.3771 (17)	C21—C22	1.533 (2)
C1—H1	0.9500	C21—H21	1.0000
C2—C3	1.4419 (16)	C22—C23	1.552 (2)
C2—C18	1.4583 (16)	C22—H22A	0.9900
C3—C4	1.4042 (16)	C22—H22B	0.9900
С3—С8	1.4185 (15)	C23—N2	1.483 (2)
C4—C5	1.3784 (16)	C23—H23A	0.9900
C4—H4	0.9500	C23—H23B	0.9900
С5—С6	1.4100 (15)	N2—C24	1.484 (2)
С5—Н5	0.9500	C24—C25	1.545 (2)
C6—C7	1.3890 (16)	C24—H24A	0.9900
С6—С9	1.4819 (16)	C24—H24B	0.9900
С7—С8	1.3907 (16)	C25—H25A	0.9900
С7—Н7	0.9500	C25—H25B	0.9900
C10—H10A	0.9800	C19′—N2′	1.473 (13)
C10—H10B	0.9800	C19′—C20′	1.532 (14)
C10—H10C	0.9800	C20'—O1'	1.410 (14)
C11—C12	1.5245 (17)	C20′—C21′	1.525 (16)
C11—H11A	0.9900	С20'—Н20'	1.0000
C11—H11B	0.9900	O1′—H1′	0.8400
C12—C17	1.3894 (17)	C21′—C22′	1.530 (16)
C12—C13	1.3924 (17)	C21′—C25′	1.534 (16)
C13—C14	1.3871 (19)	C21'—H21'	1.0000
С13—Н13	0.9500	C22′—C23′	1.511 (15)
C14—C15	1.386 (2)	C22′—H22C	0.9900
C14—H14	0.9500	C22′—H22D	0.9900
C15—C16	1.382 (2)	C23'—N2'	1.474 (14)

C15—H15	0.9500	C23′—H23C	0.9900
C16—C17	1.3906 (18)	C23′—H23D	0.9900
C16—H16	0.9500	N2'—C24'	1.449 (14)
С17—Н17	0.9500	C24′—C25′	1.552 (15)
C18—C19′	1.317 (11)	C24′—H24C	0.9900
C18—C19	1.3414 (18)	C24′—H24D	0.9900
C18—H18	0.9500	C25′—H25C	0.9900
C19—N2	1.4473 (17)	C25′—H25D	0.9900
C1—N1—C8	108.58 (10)	C25—C21—C20	107.91 (15)
C1—N1—C11	125.67 (10)	C22—C21—C20	108.15 (13)
C8—N1—C11	124.84 (10)	C25—C21—H21	110.5
C9—O3—C10	116.16 (9)	C22—C21—H21	110.5
C2—C1—N1	110.67 (11)	C20—C21—H21	110.5
C2—C1—H1	124.7	C21—C22—C23	108.31 (12)
N1—C1—H1	124.7	C21—C22—H22A	110.0
C1—C2—C3	105.81 (10)	C23—C22—H22A	110.0
C1-C2-C18	129.80 (11)	C21—C22—H22B	110.0
$C_{3}$ — $C_{2}$ — $C_{18}$	124.28 (11)	C23—C22—H22B	110.0
C4-C3-C8	118 63 (10)	H22A - C22 - H22B	108.4
C4-C3-C2	134.05 (11)	$N_2 - C_2 $	110.86 (12)
C8-C3-C2	107 24 (10)	N2-C23-H23A	109 5
$C_{5} - C_{4} - C_{3}$	119 14 (10)	$C^{22}$ $C^{23}$ $H^{23}$	109.5
$C_5 - C_4 - H_4$	120.4	N2_C23_H23B	109.5
$C_3 - C_4 - H_4$	120.4	$C^{22}$ $C^{23}$ $H^{23B}$	109.5
C4-C5-C6	120.4	$H_{23}A = C_{23} = H_{23}B$	109.5
$C_{4} = C_{5} = H_{5}$	119.4	C19 N2 C23	107.06 (13)
C6-C5-H5	119.4	C19 N2 C24	107.00(13) 109.12(13)
$C_{0} - C_{0} - C_{0}$	121.04 (10)	$C_{13} = N_2 = C_{24}$	109.12(13) 108.13(12)
C7 - C6 - C9	121.04(10) 117.76(10)	$N_2 - C_2 - C_2 + C_2 - C_2 $	100.13(12) 112.14(12)
$C_{2}^{-} = C_{2}^{-} = C_{2}^{-}$	121 20 (10)	$N_2 = C_2 - C_2 $	109.2
$C_{5} = C_{5} = C_{5}$	121.20(10) 117 38 (10)	12 - C24 - 1124A C25 - C24 - H24A	109.2
C6 C7 H7	121.3	$N_2 C_2 H_2 A_3 H_2 H_2 H_2 H_2 H_2 H_2 H_2 H_2 H_2 H_2$	109.2
$C_{0}$	121.3	$\frac{112}{124}$	109.2
$C_{0} = C_{1} = 117$	121.3 120.70 (10)	$C_{23}$ $C_{24}$ $C$	107.0
N1 - C8 - C7	129.70(10) 107.67(10)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	107.9 107.50(12)
11 - 6 - 63	107.07(10) 122.56(11)	$C_{21} = C_{23} = C_{24}$	107.39(12)
$C_{}C_{-$	122.30(11) 122.10(11)	$C_{21}$ $C_{25}$ $H_{25A}$	110.2
02 - 03 - 03	125.10(11) 124.16(11)	$C_{24}$ $C_{25}$ $H_{25}$ $H_{25}$	110.2
02 - 03 - 06	124.10(11) 112.74(0)	$C_{21} = C_{23} = H_{23} = H$	110.2
03 - 09 - 00	112.74 (9)	$C_{24}$ $C_{25}$ $C$	110.2
03-C10-H10A	109.5	H25A = C25 = H25B	108.5
	109.5	$C18 - C19 - N2^{\circ}$	123.0(10)
HIUA—CIU—HIUB	109.5	C18 - C19 - C20	123.3 (9)
	109.5	$N2^{-}$ $C19^{-}$ $C20^{-}$	112.0 (9)
HIVA-CIV-HIVC	109.5	$01^{-}-0.20^{-}-0.21^{-}$	114./(13)
HIUB-CIU-HIUC	109.5	$01^{-}-0.20^{-}-0.19^{\prime}$	108.5 (11)
NI-CII-CI2	113.30 (10)	$C_2 I^{*} - C_2 U^{*} - C_1 9^{*}$	107.0 (12)
NI-CII-HIIA	108.9	UT - C20' - H20'	108.8
UI2—UII—HIIA	108.9	$U_{21} - U_{20} - H_{20}$	108.8

N1—C11—H11B	108.9	C19'—C20'—H20'	108.8
C12—C11—H11B	108.9	C20'—O1'—H1'	109.5
H11A—C11—H11B	107.7	C20'—C21'—C22'	106.2 (13)
C17—C12—C13	118.55 (11)	C20'—C21'—C25'	108.6 (14)
C17—C12—C11	121.83 (11)	C22'—C21'—C25'	109.8 (14)
C13—C12—C11	119.62 (11)	C20'—C21'—H21'	110.7
C14—C13—C12	120.72 (12)	C22'—C21'—H21'	110.7
С14—С13—Н13	119.6	C25'—C21'—H21'	110.7
С12—С13—Н13	119.6	C23'—C22'—C21'	104.9 (12)
C15—C14—C13	120.31 (12)	C23'—C22'—H22C	110.8
C15—C14—H14	119.8	C21′—C22′—H22C	110.8
C13—C14—H14	119.8	C23'—C22'—H22D	110.8
C16—C15—C14	119.39 (12)	C21′—C22′—H22D	110.8
С16—С15—Н15	120.3	H22C—C22′—H22D	108.8
C14—C15—H15	120.3	N2'—C23'—C22'	116.0 (12)
C15—C16—C17	120.38 (13)	N2'—C23'—H23C	108.3
$C_{15}$ $C_{16}$ $H_{16}$	119.8	C22' - C23' - H23C	108.3
C17 - C16 - H16	119.8	N2'-C23'-H23D	108.3
C12-C17-C16	120.65 (12)	C22' - C23' - H23D	108.3
C12 - C17 - H17	119.7	$H_{23}C_{}C_{23'}-H_{23}D$	107.4
C16—C17—H17	119.7	C24' - N2' - C23'	107.8 (12)
C19'-C18-C2	123.8 (5)	C24' - N2' - C19'	107.0(12) 104 4 (11)
C19-C18-C2	128.40(12)	$C_{23'} = N_{2'} = C_{19'}$	105.6(11)
C19'-C18-H18	115.1	N2' - C24' - C25'	103.0(11) 113.8(11)
C19—C18—H18	115.1	N2' - C24' - H24C	108.8
$C_{2}$ $C_{18}$ $H_{18}$	115.8	$C_{25'} = C_{24'} = H_{24C}$	108.8
$C_{18} = C_{19} = N_2^2$	122 23 (12)	N2' - C24' - H24D	108.8
C18 - C19 - C20	122.23(12) 123.71(12)	$C_{25'} = C_{24'} = H_{24D}$	108.8
$N_{2}$ $C_{19}$ $C_{20}$	123.71(12) 113.72(11)	$H_{24}C_{}C_{24}'_{}H_{24}D$	107.7
$01 - C_{20} - C_{19}$	109.43(11)	C21' - C25' - C24'	107.7 106.2(12)
$01 - C_{20} - C_{21}$	112 52 (13)	$C_{21} = C_{23} = C_{24}$	110.5
C19-C20-C21	112.32(13) 106.93(11)	$C_{21} = C_{23} = H_{25}C$	110.5
$C_{1}^{-1} = C_{2}^{-1} = C_{$	100.35 (11)	$C_{24} = C_{23} = H_{25}C$	110.5
$C_{10}$ $C_{20}$ $H_{20}$	109.3	$C_{21} = C_{23} = H_{25D}$	110.5
$C_{19} = C_{20} = H_{20}$	109.3	$H_{25} = C_{25} = H_{25} = H_{25}$	108.7
$C_{21} = C_{20} = H_{20}$	109.3 100.07(13)	H23C-C23-H23D	108.7
C25-C21-C22	109.07 (13)		
C8—N1—C1—C2	-1.61 (13)	$C_{2}$ $C_{18}$ $C_{19}$ $C_{20}$	-17548(13)
$C_1 = N_1 = C_1 = C_2$	-171.05(10)	$C_{18} - C_{19} - C_{20} - C_{10}$	350(2)
N1 - C1 - C2 - C3	0.62(13)	$N_{2}$ $C_{19}$ $C_{20}$ $O_{1}$	-13842(14)
N1 = C1 = C2 = C18	176.88(11)	$C_{18} = C_{19} = C_{20} = C_{11}$	157.16(17)
$C_1 = C_2 = C_1 = C_2$	170.00(11) 177.33(12)	$N_2 = C_{19} = C_{20} = C_{21}$	-16.20(10)
C1 = C2 = C3 = C4	177.33(12)	$N_2 - C_{19} - C_{20} - C_{21}$	-171.58(11)
$C_{10} = C_{2} = C_{3} = C_{4}$	0.8(2)	$C_{1}^{$	68 25 (16)
$C_1 = C_2 = C_3 = C_8$	-175.06(12)	$C_{19} = C_{20} = C_{21} = C_{23}$	70.56(15)
$C_{10} C_2 C_3 C_4 C_5$	1/3.50(10)	$C_1 = C_2 $	-40.00(13)
$C_{2} = C_{3} = C_{4} = C_{5}$	-176 11 (12)	$C_{17} - C_{20} - C_{21} - C_{22}$	+7.00(17) -51.22(16)
$C_2 = C_3 = C_4 = C_5$	1/0.11(12) 0.04(17)	$C_{23} = C_{21} = C_{22} = C_{23}$	51.52 (10) 65 70 (16)
$C_{3} - C_{4} - C_{5} - C_{6} - C_{7}$	-1.10(17)	$C_{20} = C_{21} = C_{22} = C_{23}$	$-12 \ 47 \ (10)$
	1.10(1/)	UZ1-UZZ-UZJ-INZ	13.4/(1/)

C4—C5—C6—C9	178.01 (11)	C18—C19—N2—C23	-104.06 (18)
C5—C6—C7—C8	-0.11 (16)	C20-C19-N2-C23	69.50 (18)
C9—C6—C7—C8	-179.26 (10)	C18—C19—N2—C24	139.14 (17)
C1—N1—C8—C7	-175.07 (12)	C20-C19-N2-C24	-47.30 (18)
C11—N1—C8—C7	-5.52 (19)	C22—C23—N2—C19	-50.65 (16)
C1—N1—C8—C3	1.92 (12)	C22—C23—N2—C24	66.81 (15)
C11—N1—C8—C3	171.47 (10)	C19—N2—C24—C25	64.01 (16)
C6—C7—C8—N1	178.07 (11)	C23—N2—C24—C25	-52.12 (16)
C6—C7—C8—C3	1.47 (16)	C22—C21—C25—C24	65.38 (16)
C4—C3—C8—N1	-178.88 (10)	C20—C21—C25—C24	-51.89 (16)
C2-C3-C8-N1	-1.52 (12)	N2-C24-C25-C21	-12.01 (18)
C4—C3—C8—C7	-1.63 (17)	C19—C18—C19'—N2'	-82.4 (17)
C2—C3—C8—C7	175.73 (10)	C2-C18-C19'-N2'	27.3 (16)
C10—O3—C9—O2	-0.86 (16)	C19—C18—C19′—C20′	81.5 (17)
C10—O3—C9—C6	178.94 (9)	C2-C18-C19'-C20'	-168.7 (10)
C7—C6—C9—O2	1.15 (17)	C18—C19′—C20′—O1′	-16.1 (19)
C5—C6—C9—O2	-177.99 (11)	N2'—C19'—C20'—O1'	149.4 (13)
C7—C6—C9—O3	-178.65 (10)	C18—C19′—C20′—C21′	-140.4 (14)
C5—C6—C9—O3	2.21 (15)	N2'—C19'—C20'—C21'	25.1 (17)
C1—N1—C11—C12	98.55 (13)	O1'—C20'—C21'—C22'	165.5 (13)
C8—N1—C11—C12	-69.23 (14)	C19'—C20'—C21'—C22'	-74.1 (15)
N1—C11—C12—C17	-8.29 (16)	O1'—C20'—C21'—C25'	-76.4 (17)
N1-C11-C12-C13	171.63 (11)	C19'—C20'—C21'—C25'	44.0 (16)
C17—C12—C13—C14	0.46 (19)	C20'—C21'—C22'—C23'	48.1 (17)
C11—C12—C13—C14	-179.46 (12)	C25'—C21'—C22'—C23'	-69.2 (17)
C12—C13—C14—C15	-0.7 (2)	C21'—C22'—C23'—N2'	21 (2)
C13—C14—C15—C16	0.3 (2)	C22'—C23'—N2'—C24'	42.2 (18)
C14—C15—C16—C17	0.3 (2)	C22'—C23'—N2'—C19'	-68.9 (17)
C13—C12—C17—C16	0.21 (19)	C18—C19'—N2'—C24'	92.0 (15)
C11—C12—C17—C16	-179.87 (12)	C20'—C19'—N2'—C24'	-73.5 (15)
C15—C16—C17—C12	-0.6 (2)	C18—C19'—N2'—C23'	-154.4 (13)
C1—C2—C18—C19′	-32.0 (8)	C20'—C19'—N2'—C23'	40.0 (15)
C3—C2—C18—C19′	143.6 (8)	C23'—N2'—C24'—C25'	-64.7 (16)
C1—C2—C18—C19	-5.1 (2)	C19'—N2'—C24'—C25'	47.2 (16)
C3—C2—C18—C19	170.57 (14)	C20'—C21'—C25'—C24'	-67.2 (16)
C19'—C18—C19—N2	83.7 (14)	C22'—C21'—C25'—C24'	48.5 (17)
C2-C18-C19-N2	-2.6 (2)	N2'-C24'-C25'-C21'	18.4 (18)
<u>C19'—C18—C19—C20</u>	-89.2 (14)		

Hydrogen-bond geometry (Å, °)

D—H···A	D—H	H···A	D····A	<i>D</i> —H··· <i>A</i>
01—H1A····O2 <sup>i</sup>	0.84	1.97	2.7989 (13)	169

Symmetry code: (i) x-1, y-1, z.