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# Flow field-flow fractionation coupled with multidetector: A robust approach for the separation and characterization of resistant starch

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# ABSTRACT

The unique properties of resistant starch (RS) have made it applicable in the formulation of a broad range of functional foods. The physicochemical properties of RS play a crucial role in its applications. Recently, flow field-flow fractionation (FIFFF) has attracted increasing interest in the separation and characterization of different categories of RS. In this review, an overview of the theory behind FIFFF is introduced, and the controllable factors, including FIFFF channel design, sample separation conditions, and the choice of detector, are discussed in detail. Furthermore, the applications of FIFFF for the separation and characterization of RS at both the granule and molecule levels are critically reviewed. The aim of this review is to equip readers with a fundamental understanding of the theoretical principle of FIFFF and to highlight the potential for expanding the application of RS through the valuable insights gained from FIFFF coupled with multidetector analysis.

# 1. Introduction

Resistant starch (RS) is defined by the Food and Agriculture Organization (FAO) in accordance with the recommendations of Englyst and EURESTA (European Food-Linked Agro-Industrial Research-Concerted Action on Resistant Starch) as the starches and their degradation products that remain unabsorbed in the small intestine of healthy individuals (Asp, 1992). RS is categorized into five distinct groups (RS1-RS5) based on its morphology and physicochemical properties (Table 1) (Brown, 1996; Englyst, Kingman, & Cummings, 1992; Evans, 2016). RS exhibits dietary fiber functional properties, including prevention of gastrointestinal and cardiovascular diseases, improvement of immunity, and enhancement of mineral absorption. RS has been applied in the food industry, medical care, material science, and other fields (Fig. 1) (Hernandez-Hernandez, Julio-Gonzalez, Doyagüez, & Gutiérrez, 2023; Liang et al., 2023; Tekin & Dincer, 2023; Thongsomboon, Srihanam, & Baimark, 2023; Wang et al., 2023; Wen, Li, & Nie, 2023).

Starch consists of homogeneous glucan components: amylose (AM), mainly linear chains with a molecular weight  $(M_w)$  of approximately

 $10^{5}$ – $10^{6}$ , and amylopectin (AP), branched chains with  $M_{\rm w}$  of approximately 10<sup>7</sup>–10<sup>9</sup> (Lu, Zhu, Bao, Liu, Yu, & Chen, 2020; Tester, Karkalas, & Qi, 2004). Several factors affect RS content in starch, including AM content, plant genotypes and mutations, the physical form of grains and seeds, the size of starch granules and molecules, and food processing techniques (Lopez-Silva, Bello-Perez, Castillo-Rodriguez, Agama-Acevedo, & Alvarez-Ramirez, 2020; Ma, Yin, Hu, Li, Liu, & Boye, 2018; Yee et al., 2021). Among these factors, the characteristics of starch granules (such as AM/AP ratio, crystal structure, and gelatinization) play a vital role in evaluating the digestive properties and functional mechanisms of RS (Ding, Luo, & Lin, 2019; Gong, Cheng, Gilbert, & Li, 2019). French (1984) investigated the crystal structure of starch granules by the X-ray diffraction (XRD) technique. Three possible crystalline structures of starch granules were identified by XRD: type A, type B, and type C. Type A starch contains a digestible additional spiral in the center of its hexagonal array (Imberty, Chanzy, Pérez, Buléon, & Tran, 1987), while type B starch has water occupying the central hexagonal array, making it difficult to digest (Brown, 1996). Type C starch is considered the combination of type A and type B crystallization and has resistance

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#### Table 1

Classification of resistant starch and structural characteristics of resistance to enzymatic digestion.

Classification of RS	Structure affecting digestion	Reference
Physically inaccessible starch (RS1)	Starch granules encased by a thick cell wall and matrix	(Brown, 1996)
Non-gelatinized	Semicrystalline properties of starch	(Gallant, Bouchet,
starch granules	granules, susceptibility of the	Buléon, & Pérez,
(RS2)	granules to gelatinization	1992)
Retrograded starch	The more orderly internal structure	(Englyst, Kingman,
(RS3)	of the rearranged starch with stable	& Cummings, 1992)
	hydrogen bonds	
Chemically	High hydrophobicity, increased	(Dong & Vasanthan,
modified starch	intergranular connections density,	2020)
(RS4)	crosslinks, and steric hindrance	
Starch complex	Helical molecular structure formed	(Panyoo &
(RS5)	by amylose and long branched	Emmambux, 2017)
	chains of amylopectin bound with	
	different substances	

to enzymatic hydrolysis. Another significant factor affecting the resistance of natural starch granules to enzymatic hydrolysis is the sensitivity to gelatinization. Gelatinization can lead to the breakdown and dissolution of the compact crystal structure of starch granules, making them more susceptible to digestion by enzymes. Although the AOAC (Association of Official Analytical Communities) method is commonly used for determining RS content, it cannot provide structural insights into RS. Recently, Guo et al. (2022) developed a novel approach for the structural characterization and quantitative analysis of RS by offline coupling of asymmetrical flow field-flow fractionation (AF4) and liquid chromatography (LC). The results showed that the digestibility of starch is closely related to its crystal structure. The AM molecules in type C starch play a crucial role in the anti-digestion process. The results demonstrated that AF4 × LC is a powerful method for informative structural detection and quantitative analysis of RS over its entire  $M_w$  distribution.

Size exclusion chromatography (SEC), fluorophore-assisted carbohydrate electrophoresis (FACE), and high performance anion exchange chromatography (HPAEC) are commonly used to characterize starch (Gilbert, Witt, & Hasjim, 2013). HPAEC coupled with a pulsed amperometric detector (PAD) can provide information on the chain length distribution (CLD) of starch (Li, Li, & Gilbert, 2019). Longer CLDs are associated with a more ordered physical structure, especially in retrograded starches (RS3), which contributes to higher resistance to enzymatic digestion (Zhu & Liu, 2020). SEC, a size-based separation method, can be used to separate AM and AP molecules. Furthermore, SEC coupled with multiangle light scattering (MALS) is commonly used to determine the  $M_w$  and radius of gyration ( $R_g$ ) distributions of the starch components (Bello-Perez, Agama-Acevedo, Lopez-Silva, & Alvarez-Ramirez, 2019). However, obtaining an accurate detection of AP molecules can be challenging due to column adsorption and shear degradation of AP molecules (Cave, Seabrook, Gidley, & Gilbert, 2009). Flow field-flow fractionation (FIFFF) is a valuable technique for separating starch with ultrahigh  $M_w$  due to its rapid and gentle separation



Fig. 1. Classification and application of RS.

mechanism (Giddings, 1966). Notably, FIFFF lacks a stationary phase and packing material in the channel, which minimizes shear degradation risks, especially for AP molecules (González-Espinosa, Sabagh, Moldenhauer, Clarke, & Goycoolea, 2019). FIFFF coupled with online MALS and differential refractive index (dRI) detectors can provide the entire size distribution and molecular conformation information about RS (Zhang, Shen, Song, Chen, Zhang, & Dou, 2021). Wahlund et al. (2011) studied a wide range of starches from different plant sources by AF4-MALS-dRI. The results showed that the relative quantity,  $M_w$ ,  $R_g$ , and hydrodynamic diameter ( $d_h$ ) of starch molecules from different plant sources and varieties varied greatly. AF4-MALS-dRI has been proven to be a valuable tool for characterizing RS.

In a previous review, the dissolution, structure, and functions of starch characterized by AF4-MALS-dRI were summarized (Guo, Li, An, Shen, & Dou, 2019). Compared to SEC, FIFFF analysis of starches involves a greater number of controllable factors. To our knowledge, there is a notable absence of comprehensive reviews on the separation and characterization of RS by using FIFFF. In this review, the theory of FIFFF and the controllable factors affecting the sample separation of FIFFF are introduced in detail. The applications of FIFFF in the separation and characterization of RS are critically reviewed.

#### 2. Flow field-flow fractionation (FIFFF)

FIFFF, an important sub-technique of field-flow fractionation, was proposed by Giddings in 1976. FIFFF has the widest separation range and the best compatibility with various carrier liquids, supporting extensive applications to multi-sized analytes from diverse sources (Wu et al., 2023). In this review, the theory and operation modes and the variant of FIFFF are reviewed.

# 2.1. Principle of flow field-flow fractionation (FIFFF)

In FIFFF, a ribbon-like separation channel (as shown in Fig. 2(a)) is usually assembled by sandwiching a thin spacer between two blocks (top and base in Fig. 2(b)). The shape of the spacer determines the shape of the FIFFF separation channel. In the FIFFF channel, the fluid can be approximated as a Poiseuille flow between two infinite planes, and the flow phase velocity distribution within the separation channel can be approximated as a parabolic flow profile (Fig. 2(c)). From the edge of the channel to its center, the flow velocity of the fluid gradually increases and reaches a maximum at the centerline. An applied external force, called cross-flow, is introduced in the direction perpendicular to the separation channel, which persists throughout the separation process. When the sample is injected into the separation channel, the sample particles accumulate on its bottom wall (acting as an accumulation wall) under the combined action of the applied external force and its own diffusion force. When the applied external force is balanced with the diffusion force of the particles, the samples can be separated in the channel. FIFFF maintains the integrity of the structure and properties of the sample, and the collected fractions can be further analyzed online or offline using other characterization methods (e.g., ultraviolet (UV),



Fig. 2. Schematic diagram of the channel (a and b) and separation process (c) of FIFFF.

fluorescence, dRI, MALS, etc.).

#### 2.2. Variants of flow field-flow fractionation (FIFFF)

Several variants of FIFFF have been developed, each with different characteristics as summarized in Table 2. Symmetrical FIFFF (SF4) channel has a permeable top wall, and the flow conditions are set at low flow rates with identical inlet and outlet flow velocities. However, SF4 presented certain challenges, including prolonged injection time, peak broadening, and low resolution (Giddings, Yang, & Myers, 1977). It was improved by AF4 (Wahlund & Giddings, 1987; Wahlund, Winegarner, Caldwell, & Giddings, 1986). In AF4, the top wall of the channel is impermeable, and the bottom wall is permeable, allowing the cross-flow to pass through the channel. Subsequently, the trapezoidal asymmetrical parallel plate channel (TrAF4) was developed (Litzen, 1993; Litzen & Wahlund, 1991). AF4 is suitable for the characterization of synthetic and natural polymers, including proteins and polysaccharides. In addition to soluble polymers, AF4 can separate colloidal particles in the range of approximately 1 nm to 1 µm in diameter (in the normal mode) (Podzimek. 2012).

Hollow fiber FIFFF (HF5) was developed with some advantages such as low sample loading, high sensitivity, short analysis time, and potential disposability (Joensson & Carlshaf, 1989). However, it is worth noting that low sample loading and disposability also represent disadvantages for this method. To solve the overloading effect observed with HF5, the tandem HF5 approach was developed to enhance the detection of low abundance components (Zattoni, Rambaldi, Casolari, Roda, & Reschiglian, 2011). Commercially manufactured AF4 instruments equipped with frit inlet and frit outlet channel came into existence in the 1990s. The key advantage of the frit inlet FIFFF channel is the elimination of the focusing step, enabling a higher injection mass compared to a conventional channel, thereby mitigating the risk of sample overloading (Fuentes, Choi, Zielke, Peñarrieta, Lee, & Nilsson, 2019). The frit outlet FIFFF channel enhances mass detection sensitivity (Clark & Zika, 2001).

# 2.3. Elution modes of flow field-flow fractionation (FIFFF)

The sample separation in FIFFF occurs within a ribbon-like channel. According to the elution order of the samples, elution modes of FIFFF are categorized into normal mode and steric/hyperlayer mode (Fig. 3).

# 2.3.1. Normal mode

The field force ( $F_F$ ) employed in FIFFF makes the sample components spread uniformly to the accumulation wall, which is expressed as Eq. (1) (Giddings, Ratanathanawongs, & Moon, 1991):

# Table 2

Characteristics of FIFFF variants.

FlFFF variant	Characteristic	Reference
Symmetrical FlFFF (SF4) Asymmetrical FlFFF (AF4)	Low flow conditions, stop-flow relaxation period Most used, high resolution	(Giddings, Yang, & Myers, 1977) (Wahlund & Giddings, 1987)
Hollow fiber FlFFF (HF5)	Low sample loading, high sensitivity due to lower dilution, short analysis time, potentially disposable	(Joensson & Carlshaf, 1989)
Frit inlet FlFFF	On-the-fly sample relaxation so no stop-flow or focusing flow step, generally lower separation resolution than AF4, good for samples prone to undesirable interactions with the membrane accumulation wall	(Fuentes, Choi, Zielke, Peñarrieta, Lee, & Nilsson, 2019)
Frit outlet FlFFF	Enhancement in detector signal intensity due to lower dilution	(Clark, & Zika, 2001)



Fig. 3. Main separation modes of FIFFF.

$$F_{\rm F} = \frac{3\pi\eta d_h w V_{\rm c}}{V^0} \tag{1}$$

where  $\eta$  is the viscosity of the carrier liquid,  $d_h$  is the hydrodynamic diameter of the particle,  $V_c$  is the cross-flow rate, w is the channel thickness, and  $V^0$  is the void volume. Eq. (1) shows that  $F_F$  is proportional to  $V_c$ . At the same time, the sample components diffuse away from the accumulation wall under the action of Brownian motion and finally form an equilibrium layer between the two opposing transport processes. For the sample with  $d_h$  smaller than 1 µm, separation occurs in the normal mode, and retention time ( $t_r$ ) is inversely proportional to the diffusion coefficient *D* and proportional to  $d_h$  (Ratanathanawongs Williams & Lee, 2006). The carrier liquid enters the channel from the inlet and forms a parabolic profile inside the channel, with the highest velocity at the center of the channel (Fig. 3). As a result, the smaller particles are eluted earlier than larger ones, which is the so-called normal mode, as shown in Fig. 3(c).

# 2.3.2. Steric/hyperlayer mode

As the sample diameter increases, the elution mode shifts from the normal mode to the steric/hyperlayer mode with an opposite elution order (Kim, Yang, & Moon, 2018). When the particle size is larger than 1  $\mu$ m, the diffusion force of the particle can be ignored. In this case, the particles are driven downward by the  $F_{\rm F}$  to (or close to) the accumulation wall, where the centers of the large particles are in a faster stratosphere and then are eluted first (Fig. 3(d)) (Giddings, 1993; Myers & Giddings, 1982). When the force of hydrodynamic lift ( $F_{HL}$ ) is sufficient to counteract the  $F_{\rm F}$ , a particle-focusing layer is formed at a distance from the accumulation wall (Mélin et al., 2012).  $F_{\rm HL}$  is caused by inertia and other factors of liquid carriers (Reschiglian et al., 2000). There is the "steric transition" phenomenon when the sample elution mode changes from the normal mode to the steric/hyperlayer mode (Dou, Lee, Jung, Lee, & Lee, 2013; Kim, Yang, & Moon, 2018). When the sample's size range spans the steric transition region (i.e., the particle size range overlaps between the normal mode and steric/hyperlayer mode), it can lead to simultaneous elution of particles with different sizes. This makes it challenging to determine the accurate size distribution of the sample components (Dou, Jung, & Lee, 2015; Perez-Rea, Zielke, & Nilsson, 2017; Zielke, Fuentes, Piculell, & Nilsson, 2018). The particles with large size are generally formed during starch retrogradation process. Therefore, when FIFFF is employed for the separation of RS3, great care

# is needed, as steric phenomenon may occur (Zhang et al., 2019).

# 2.4. Resolution and retention ratio in flow field-flow fractionation (FIFFF)

Resolution ( $R_s$ ) is one term for evaluating the separation efficiency between two analyte components. During the separation process of two components, two distinct types of dispersion need to be considered: selective dispersion ( $\Delta t_r$ ) and random dispersion (Schimpf, Myers, & Giddings, 1987).  $\Delta t_r$  is beneficial to the separation of two components, whereas random dispersion is not.  $\Delta t_r$  is quantified by the selectivity (S), which reflects the difference in retention volume (or  $t_r$ ) with  $M_w$  or particle diameter. Random dispersion is quantified by plate height (H). Therefore, the resolution depends on both H and S, and can be expressed as Eq. (2):

$$R_s = \frac{\Delta z}{2(\sigma_1 + \sigma_2)} = \frac{\Delta z}{4\overline{\sigma}}$$
(2)

where  $\Delta z$  is the gap between the centers of gravity of neighboring zones and  $\sigma$  is the standard deviation of the zones. The subscripts on  $\sigma$  refer to components 1 and 2, and  $\overline{\sigma}$  refers to an average value for two zones. Consequently,  $\Delta z$  reflects selective dispersion, while  $\sigma$  indicates the extent to which the gap is filled by cross-contamination due to random dispersion. It is well known that the  $M_w$  of AM and AP molecules has an overlap (Dou, Zhou, Jang, & Lee, 2014; Zhang et al., 2019). Thus, a baseline separation for starch samples by FIFFF is still a challenge.

The retention ratio (R) is defined as the ratio of the times associated with the void time and retention time, and it is expressed as Eq. (3):

$$R = 6\gamma \alpha (1 - \alpha) + \left[ \left( 1 - 2\alpha) coth \left( \frac{1 - 2\alpha}{2\lambda} \right) - 2\lambda \right]$$
(3)

where  $\gamma$  is a dimensionless parameter that depends on the field strength, migration velocity, and particle size (Kim, Yang, & Moon, 2018).  $\alpha$  is the ratio of particle radius (*a*) to *w*,  $\lambda$  is the ratio of the mean layer thickness (*l*) to *w*, which can be expressed as (Wahlund & Giddings, 1987):

$$\lambda = \frac{kTV^0}{3\pi\eta w^2 d_h V_c} \tag{4}$$

where *k* is the Boltzmann constant and *T* is the absolute temperature. When  $\lambda$  is very small, Eq. (3) can be reduced to Eq. (5):

$$R = 6\gamma \alpha + 6\lambda \tag{5}$$

In the Eq. (5), the first term of the equation is proportional to the particle size, while the second term is inversely proportional to the particle size. As a result, *R* decreases with increasing  $d_h$  and reaches the minimum value ( $R_i$ ). The diameter corresponding to  $R_i$  is called the "steric transition point" ( $d_i$ ).  $d_i$  and  $R_i$  are expressed as Eqs. (6) and (7), respectively:

$$d_i = \sqrt{\frac{2kTV^0}{3\pi\eta w\gamma V_c}} \tag{6}$$

and

$$R_i = \frac{6\gamma d_i}{w} \tag{7}$$

For highly retained components in FIFFF ( $l \ll w$  or  $\lambda \rightarrow 0$ ), Eq. (5) can be approximated to yield a so-called "simplified" retention equation (Eq. (8) for the normal mode and Eq. (9) for the steric/hyperlayer mode):

$$R = 6\lambda \tag{8}$$

$$R = 6\gamma\alpha \tag{9}$$

In the normal mode, R is inversely proportional to the particle size, while in the steric/hyperlayer mode, R is proportional to the particle

size. The value of  $\gamma$  is related to the information of the elution mode (steric or hyperlayer mode) (Moon & Giddings, 1992). When the sample size ranges in the steric transition region, the elution mode can be adjusted by changing the elution parameters. For FIFFF analysis of polydisperse samples (such as RS), it is crucial to optimize the elution conditions to avoid steric transition.

# 3. Factors affecting sample separation of flow field-flow fractionation

Despite the excellent separation performance of FIFFF, the retention and accumulation of samples on the surface of the accumulation wall can result in low sample recovery, which may limit the potential applications of this technology. Additionally, the retention capacity of ultrafiltration membranes imposes constraints on the minimum sample size in FIFFF. Therefore, prior to conducting sample separation using FIFFF, a series of parameters need to be optimized to attain ideal separation conditions for the given sample. The primary factors that influence sample separation and characterization in FIFFF include the composition of the separation channel, the conditions used for sample separation, and the sensitivity of the detectors.

# 3.1. Performance of the FIFFF channel

The channel profile in FIFFF is usually designed with diverse dimensions and shapes (Kang & Moon, 2004). The channel dimensions are described by w, the breadth (b), and the length (L). The w is controlled by the thickness of the spacer. The actual thickness of the FIFFF channel is typically 50 µm smaller than the spacer thickness due to the compression of the semipermeable membrane. In comparison to a rectangular channel, the trapezoidal channel design serves to partially compensate for the reduction in axial flow velocity, resulting from the loss of crossflow through the membrane. This, in turn, mitigates peak dilution and enhances detector responsiveness. At a consistent cross-flow rate, the actual field force is contingent on the area of the semipermeable wall, comprising the channel length L, the channel breadths  $b_0$  (inlet breadth of trapezoidal FIFFF channel), and  $b_{\rm L}$  (outlet breadth of the trapezoidal FlFFF channel), and the areas of tapered ends. Shorter and/or narrower channels are employed to achieve higher field force, which reduces solvent consumption and enhances sample separation efficiency. The lower size limit is determined by the molecular weight cut off (MWCO) of the membrane, while the upper size limit is assessed by a threshold of 20 % of the FIFFF channel thickness.

Ultrafiltration membranes made of regenerated cellulose (RC), polvether sulfone (PES), and cellulose triacetate (CT) with MWCO of 0.3-100 kDa are commonly employed as accumulation walls in FIFFF. Since smaller monosaccharides and oligosaccharides can pass through the ultrafiltration membrane, oligosaccharides with sizes comparable to the MWCO may be blocked in the pores of the ultrafiltration membrane, and large starch molecules can interact with the membrane through chemical (adsorption) or physical (rough surface) interactions, which may result in lower sample recovery and potential membrane contamination. To mitigate these issues, the selection of an appropriate ultrafiltration membrane type and MWCO is crucial to minimize the interactions between the sample and the surface of the membrane, which can ensure a higher sample recovery. In practical applications, when dealing with charged samples, it is essential to choose a suitable carrier liquid to eliminate the interaction between the samples and the ultrafiltration membrane (González-Espinosa, Sabagh, Moldenhauer, Clarke, & Goycoolea, 2019).

# 3.2. Sample separation conditions

Mudalige et al. (2015) reported that sample modification can alter sample retention within FIFFF. In addition to altering the nature of the sample, optimizing the separation conditions of FIFFF (e.g., external

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forces, the nature of the carrier liquid, injection mass, and focusing time) can enhance sample recovery.

# 3.2.1. External force

During the FIFFF separation process, the choice of external force is critical, as a lower external force can lead to decreased  $R_s$ , while a higher external force may increase the risk of sample aggregation and interaction with the surface of the membrane. Optimizing the external force is essential to achieve good sample resolution. For heterogeneous samples with a wide size distribution, it is recommended to employ gradient external force to shorten the analysis time. In the FIFFF elution process, the external force action can be categorized into three main modes: constant mode, linear attenuation mode, and exponential attenuation mode. Among them, the combination of exponentially attenuated external force with other external force modes is frequently employed for the separation of starch samples (Ma, Buschmann, & Winnik, 2010).

# 3.2.2. Selection of carrier liquid

Ideally, the carrier liquid should be compatible with properties of the sample (such as pH and ionic strength) to inhibit the instability of the sample molecules (such as degradation, aggregation, and adsorption) during FIFFF separation (Kammer, Legros, Hofmann, Larsen, & Loeschner, 2011). Generally, it is recommended to use electrolyte solutions with ionic strength and pH conditions similar to those of the sample. Additionally, in some cases, surfactants are needed to maximize sample recovery, and a bactericide (e.g., sodium azide) can be added to prevent bacterial growth. For starch samples from different plant sources, a carrier liquid composed of diluted electrolytes (such as 1-50 mM NaNO<sub>3</sub>) is recommended (Nilsson, 2013). When separating polysaccharides (such as chitosan complex and dextran), deionized water is sometimes chosen as the carrier liquid (Faucard et al., 2018; Fraunhofer, Jakob, & Vogel, 2018). To separate the mixture of starches and other biomacromolecules, buffer solutions such as acetate buffer, phosphate buffer, and sodium citrate buffer are commonly used as carrier liquids. Ideally, on the premise of ensuring the stability of the sample, a carrier liquid with a pH value that maximizes repulsion between the sample and the surface of the accumulation wall and an appropriate ionic strength to prevent starch aggregation and/or adsorption should be selected.

# 3.2.3. Injection mass

FIFFF can provide precise sample characterization with relatively small sample amounts, typically approximately 10 µg or less, depending on the sensitivity of the detection method (Caldwell, Brimhall, Gao, & Giddings, 1988). It is important to be aware of the phenomenon of "sample overloading." Sample overloading results in an excessively high concentration of sample components in the concentration region of the accumulation wall. Sample overloading involves multiple concentration-dependent phenomena, which can lead to an unstable retention ratio (increase or decrease) and asymmetrical peak (tail or front). During the elution process, the interaction between samples or between the sample and the surface of the accumulation wall increases, which results in sample aggregation and/or adsorption (Benincasa & Giddings, 1992; Schimpf, Caldwell, & Giddings, 2000). AP with an ultrahigh  $M_w$  is particularly susceptible to sample overloading due to chain entanglement and viscosity effects. Arfvidsson and Wahlund (2003) found that a large injection volume with a low sample concentration is superior to using a small injection volume with a high sample concentration. Therefore, the key to avoid sample overloading is to reduce the maximum sample concentration, which can be achieved by decreasing the injected sample mass.

# 3.2.4. Focusing time

Regarding the focusing time, during the FIFFF injection and focusing process, it is essential to extend the focusing time to enrich the sample. This ensures that the sample concentration surpasses the detection limit of the detector and minimizes peak broadening. If the focusing time is too short, the sample equilibrium layer distribution is wide, and some sample components may elute within the void peak. On the other hand, an excessively long focusing time can increase the interaction between samples and between samples and the surface of the membrane, potentially leading to sample aggregation and excessive retention (Wahlund, 2013). Therefore, selecting an appropriate focusing time is also a crucial factor in the separation and characterization of RS using FIFFF.

# 3.3. Sensitivity of the detectors

The sensitivity and detection limit of the detector play a crucial role in the accuracy of characterizing samples by FIFFF. AF4 coupled with a mass detector (typically MALS) and a concentration detector (usually dRI) is primarily used for the separation and characterization of starch molecules in the normal mode. AP molecules with higher  $M_{\rm w}$  and viscosity tend to be closer to the accumulation wall during AF4 separation and are prone to absorb on the surface of the accumulation wall. To achieve optimal separation for AP molecules, it is essential to operate at a lower concentration (Chiaramonte, Rhazi, Aussenac, & White, 2012). The intensity of the MALS signal is influenced by both the concentration and the size of the sample components. According to Rayleigh's approximation, the intensity of light scattering by a particle is proportional to the sixth power of the particle's diameter ( $I \propto d^6$ ), making it more challenging to detect scattered light from smaller particles. Consequently, when a mixture of particles with different sizes is present in the suspension, the data tend to be skewed toward larger particle sizes (Doyle & Wang, 2019; Guisbiers et al., 2016). However, MALS signal detection is particularly challenging for AM molecules with a lower  $t_r$ due to their smaller size (Yoo, Choi, Zielke, Nilsson, & Lee, 2017). The sample recovery is determined from the ratio of the mass eluted from the separation channel (integration of the dRI signal) to the injected mass (based on the starch content). However, at a lower injection mass, the dRI detector may exhibit a low signal-to-noise ratio, making it difficult to accurately determine sample recovery and  $M_{\rm w}$ . In such cases, averaging multiple injections can be a reliable method to enhance the accuracy of starch characterization (Leeman, Islam, & Haseltine, 2007). This approach can improve the accuracy of quantitative analysis of AM but may not provide detailed M<sub>w</sub> and conformational information about AP. Thus, the subsequent improvements of FIFFF technique (such as modified membranes, coupled with precision detection methods) are necessary to address the characterization challenges of AP molecules.

# 4. Application of FIFFF for the structural characterization of RS

The characterization of starch at both the granule and molecule levels by direct measurement of physicochemical parameters in association with MALS and dRI is a key feature of the FIFFF technique. The information about the RS obtained from FIFFF is outlined in Table 3.

# 4.1. Physically inaccessible starch (RS1)

Song et al. (2021) utilized AF4-MALS-dRI to separate and characterize starch granules and starch molecules extracted from various plant sources. The AF4 results were validated by a combination of optical microscopy (OM), scanning electron microscopy (SEM), and dynamic light scattering (DLS) techniques. The size distributions of starch granules determined by AF4 were in reasonable agreement with those obtained from OM. However, OM measurement is time-consuming. The results suggested that AF4 is an appropriate method for determining the sizes of starch granules. Meanwhile, the relationships between the size of starch at nano- to microscale and its functional properties (i.e., digestibility, retrogradation, and thermal properties) were studied by Pearson correlation analysis. The results showed that the sizes of starch granules and starch molecules from different plant sources were related to their digestibility. The information about RS obtained from FIFFF.

Source of RS	Type of RS	Type of FlFFF	FIFFF operation condition			Detection	The information	Reference	
			Carrier liquid	Membrane	Cross-flow rate	Injection mass		gained by FlFFF	
Rice, lotus	RS1	AF4	3 mM NaN <sub>3</sub> , 0.35 mM SDS	RC	$1.2 \rightarrow 0.05$ mL/min Half-time $t_{1/2} = 3$ min	100 µg	UV, MALS, dRI	M <sub>w</sub> , R <sub>g</sub>	(Song et al., 2021)
Mung bean, yam, banana	RS2	AF4	5 mM NaNO <sub>3</sub>	RC	$1.2 \rightarrow 0.05$ mL/min $t_{1/2} = 3$ min	10 µg	MALS, dRI, LC	<i>M</i> <sub>w</sub> , <i>R</i> <sub>g</sub> , content of RS	(Guo, Zhang, Sun, Ye, Shen, & Dou, 2022)
Potato	RS2	AF4	3 mM NaN <sub>3</sub> , 5 mM NaNO <sub>3</sub>	RC	$1.2 \rightarrow 0.05$ mL/min $t_{1/2} = 3$ min	25 µg	MALS, dRI	$M_{ m w},R_{ m g}, ho_{ m app},R_{ m g}/R_{ m h}$	(Zhang, Shen, Song, Chen, Zhang, & Dou, 2021)
Maize, wheat, rice potato, tapioca, pea	RS2	AF4	-	RC	$1.0 \rightarrow 0$ mL/min $t_{1/2} = 4$ min	40 µg	MALS, dRI	$M_{\rm w},R_{\rm g},R_{\rm h}$	(Wahlund, Leeman, & Santacruz, 2011)
Potato, maize, wheat	RS2	AF4	$3 \text{ mM NaN}_3$	-	-	-	MALS, QELS, dRI	$M_{\rm w},R_{\rm g},R_{\rm h}$	(Rolland-Sabaté, Guilois, Jaillais, & Colonna, 2011)
Potato, maize	RS3	AF4	3 mM NaN <sub>3</sub> , 50 mM NaNO <sub>3</sub>	RC	$1.4 \rightarrow 0.05$ mL/min $t_{1/2} = 2$ min	100 µg	MALS, dRI	$M_{ m w},R_{ m g}, ho_{ m app},R_{ m g}/R_{ m h}$	(Zhang et al., 2019)
Wheat	RS3	AF4	-	RC	$2.0 \rightarrow 0.12$ mL/min $t_{1/2} = 4$ min	1.25–15 μg	MALS, dRI	$M_{ m w},R_{ m g}, ho_{ m app},R_{ m g}/R_{ m h}$	(Fuentes, Castañeda, Rengel, Peñarrieta, & Nilsson, 2019)
Maize	RS4	AF4	3 mM NaN <sub>3</sub> , 50 mM NaNO <sub>3</sub>	RC	0.2 mL/ min	100 µg	MALS, dRI	$M_{ m w}$	(Lee et al., 2010)
-	RS4	AF4	3 mM NaN <sub>3</sub> , 1 M NaCl	RC	1.0 or 2.0 mL/min	40–300 µg	MALS, dRI	$M_{\rm w},R_{\rm g},R_{\rm g}/R_{\rm h}$	(Wittgren, Wahlund, Andersson, & Arfvidsson, 2002)
Barley	RS4	EAF4	10 mM PBS	RC	$2.0 \rightarrow 0.25$ mL/min $t_{1/2} = 3$ min	60 µg	MALS, dRI	$M_{\rm w}$ , Zeta potential	(Fuentes, Choi, Wahlgren, & Nilsson, 2023)

# 4.2. Non-gelatinized starch granules (RS2)

Rolland-Sabaté et al. (2011) utilized AF4 coupled with MALS, guasielastic light scattering (QELS), and dRI (AF4-MALS-QELS-dRI) to analyze the structure of varying AM/AP ratios and natural starches from different plant sources. The results showed that AF4 could effectively separate AP molecules and obtain more structural information about branched macromolecules. Zhang et al. (2021) explored the capability of AF4-MALS-dRI for monitoring structural and conformational changes in potato starch during enzymatic hydrolysis. The results revealed that the gelatinization process induced a loose and random coil conformation in potato AM molecules, accelerating enzymatic hydrolysis of potato starch. Guo et al. (2022) conducted structural characterization and quantification of RS extracted from various plant sources (i.e., mung bean, yam, and banana) by offline coupling AF4-MALS-dRI with LC. The results demonstrated that the combination of AF4-MALS-dRI and LC is an effective method for rapid, quantitative, and comprehensive structural information detection of RS over the entire  $M_w$  distribution.

# 4.3. Retrograded starch (RS3)

Starch retrogradation is an inevitable transformation during processing and storage, and often accompanies with structural and conformational changes, especially under low-temperature or cooling conditions. Zhang et al. (2019) studied the influence of the plant source, AM/AP ratio, storage conditions (temperature and time), and salt on starch retrogradation by using AF4-MALS-dRI. The results revealed that nitrate ions retarded starch retrogradation behavior by inhibiting the formation of hydrogen bonds between AM molecules. Moreover, the results highlighted the significant role played by small AM aggregates in starch retrogradation and maize AP degradation, offering valuable insights into the mechanism of starch retrogradation. Fuentes et al. (2019a) analyzed the molecular properties (such as  $M_w$ ,  $R_g$ , and apparent density ( $\rho_{app}$ )) of wheat starch in three different types of bread by AF4-MALS-dRI. The results showed that the higher the water content of the bread was, the higher the  $R_g$ ,  $M_w$ ,  $\rho_{app}$ , and content of RS. The content of AM in bread may be related to  $\rho_{app}$ , suggesting that the content of RS might be related to the difference in structural and conformational properties of starch. Furthermore, the results also indicated that characterizing non-solvent precipitated starch led to insights into how changes in molecular properties may be associated with the presence of RS (Fuentes et al., 2019b).

# 4.4. Chemically modified starch (RS4)

RS4 can impact its original structure and lead to changes in  $M_w$  via chemical alterations. Several methods, including acid hydrolysis, crosslinking, acetylation/esterification, dual modification, and oxidation, have been employed for the chemical modification of starch (Haq et al., 2019). Lee et al. (2010) investigated the effect of carboxymethylation on the  $M_w$  and size distribution of corn starch using AF4-MALS-dRI. The results demonstrated that carboxymethylation of starch resulted in a reduction in  $M_w$  due to molecular degradation by the alkaline treatment. The results suggested that AF4-MALS-dRI is a useful tool for monitoring the changes in  $M_w$  and the size of starch during derivatization. Additionally, Wittgren et al. (2002) explored the  $M_w$  of four commercial hydroxypropyl and hydroxyethyl-modified starches using AF4-MALS-dRI. The results highlighted the ability of AF4-MALS- dRI to provide a rapid size characterization of modified starches. Recently, Fuentes et al. (2023) investigated the capability of electrical asymmetrical flow field-flow fractionation (EAF4) for determining the charge properties over the  $M_w$  distribution of barley starch modified with octenyl succinic anhydride (OSA). The results revealed that EAF4 facilitated the estimation of the zeta potential and net charge of OSAstarch. Furthermore, the results suggested that OSA substituents were not evenly distributed at or near the "surface" of the starch, potentially affecting the adsorption behavior and functionality of OSA-starch in emulsions.

# 4.5. Starch complex (RS5)

RS5 is a starch complex formed by the combination of long branched chains of AM and AP with different nutrients, which prevents digestive enzymes from binding and hydrolyzing starch by forming a helical molecular structure. Several studies have reported that RS5 is formed when AM or AP is processed with fatty acids or fatty alcohols (Panyoo & Emmambux, 2017). Magnusson and Nilsson (2011) studied the interaction between hydrophobically modified starch, with octenyl succinic anhydride (OSA), and  $\alpha$ - $\beta$ -livetin, which is the water-soluble fraction of egg yolk. Although, AF4-UV-MALS-dRI has been proven to be a useful tool for studying the complex of polysaccharides and proteins (Chen et al., 2022), few studies have reported on the application of FIFFF for RS5.

# 5. Summary and outlook

In summary, FIFFF is a useful tool for the separation of RS that can aid in optimizing the production process of starch and elucidating the factors that contribute to their resistance to enzymatic digestion. Coupling FIFFF with multidetector (such as MALS and dRI detectors) can serve as a powerful tool to comprehensively understand the structure and conformation of RS. The FIFFF channel with a frit outlet could enhance the signal intensity of AP molecules due to lower dilution and achieve structural characterization even at low RS concentrations. Although, AF4-UV-MALS-dRI has shown its capability for the separation and characterization of RS and would open a new avenue for studying RS5, more exploration is needed regarding the structure of RS and its resistance to enzymatic digestion.

# CRediT authorship contribution statement

Mu Wang: Writing – original draft, Conceptualization. Wenhui Zhang: Writing – original draft, Conceptualization. Liu Yang: Visualization. Yueqiu Li: Data curation. Hailiang Zheng: Writing – review & editing, Project administration. Haiyang Dou: Writing – review & editing, Supervision, Funding acquisition.

# Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

#### Data availability

Data will be made available on request.

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