



Article

Investigation of SiO₂ Etch Characteristics by C₆F₆/Ar/O₂ Plasmas Generated Using Inductively Coupled Plasma and Capacitively Coupled Plasma

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Abstract: The etching properties of $C_6F_6/Ar/O_2$ in both an inductively coupled plasma (ICP) system and a capacitively coupled plasma (CCP) system were evaluated to investigate the effects of high C/F ratio of perfluorocarbon (PFC) gas on the etch characteristics of SiO_2 . When the SiO_2 masked with ACL was etched with C_6F_6 , for the CCP system, even though the etch selectivity was very high (20 ~ infinite), due to the heavy-ion bombardment possibly caused by the less dissociated high-mass ions from C_6F_6 , tapered SiO_2 etch profiles were observed. In the case of the ICP system, due to the higher dissociation of C_6F_6 and O_2 compared to the CCP system, the etching of SiO_2 required a much lower ratio of O_2/C_6F_6 (~1.0) while showing a higher maximum SiO_2 etch rate (~400 nm/min) and a lower etch selectivity (~6.5) compared with the CCP system. For the ICP etching, even though the etch selectivity was much lower than that by the CCP etching, due to less heavy-mass-ion bombardment in addition to an adequate fluorocarbon layer formation on the substrate caused by heavily dissociated species, highly anisotropic SiO_2 etch profiles could be obtained at the optimized condition of the O_2/C_6F_6 ratio (~1.0).

Keywords: inductively coupled plasma (ICP); capacitively coupled plasma (CCP); liquid fluorocarbon (PFC); L-FC; C_6F_6 ; plasma etching; high aspect ratio contact (HARC)



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1. Introduction

As the semiconductor device size has decreased to nanoscale due to the high integration of the circuit, the critical dimension has decreased to a few nanometers and the device structure has changed from 2D to 3D. To fabricate these devices, etching technologies such as pulsed plasma etching technology and multiple patterning technology are widely investigated [1–9] and applied using two different plasma etching systems, namely the capacitively coupled plasma (CCP) etching system and inductively coupled plasma (ICP) etching system.

The CCP system uses two facing electrodes, and multiple RF powers composed of high and low RF frequencies are generally applied to both the top and bottom electrodes or to the bottom electrode only; to provide ion energy to the substrate located at the bottom electrode, a lower frequency RF power is generally connected to the bottom electrode. Due to the electric field configuration of the CCP system, the CCP system tends to show a low plasma density of $\sim 109-10/{\rm cm}^3$ and a low gas dissociation. In the case of the ICP system, one RF power is connected to the inductive antenna located at the top of the chamber for the generation of time-varying azimuthal electric fields in the process chamber for the high-density plasma formation of $\sim 1010-11/{\rm cm}^3$ with a significant gas dissociation, and a low-frequency RF power is also connected to the bottom electrode to provide ion

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bombardment to the substrate [10]. The ICP system is generally operated at a low pressure of a few millitorr, and etch rates are generally higher than those by the CCP system operated at a few tens of millitorr due to the higher ion flux and higher radical flux of the ICP system during the etching. However, for the high aspect ratio contact (HARC) etching of SiO_2 using perfluorocarbon (PFC)-based etch gases, even though the etch rates are slower than the ICP system, the CCP system is generally used due to the higher etch selectivity over mask layers caused by low dissociation of fluorocarbon gases at the lower plasma density in addition to the higher ion bombardment energy at the same low-frequency power to the substrate.

Previously, to obtain higher etch selectivity over mask layers in addition to high HARC SiO₂ etch rates, researchers have investigated using the ICP system instead of the CCP system for the HARC etching [11–14]. Li et al. used C_4F_6 gas for the etching of SiO₂ masked with photoresist in an ICP system, and even though the etch selectivity of SiO₂/PR was higher than conventional PFC gas of C_4F_8 , the maximum etch selectivity was limited to 4 [11]. Nakamura et al. also etched SiO₂ masked with photoresist in an ICP system with various PFC gases having different C/F ratios such as C_3F_6 , C_4F_6 , C_4F_8 , and C_5F_8 and showed that the higher C/F ratio improved the etch selectivity but the maximum etch selectivity obtained with C_4F_6 was 2 [12]. Kim et al. used hydrofluoroether-based gases in the etching of SiO₂ with an ICP system, but no etch selectivity data were provided [13]. Therefore, even though studies have been carried out to etch SiO₂ selectively to mask layers using the ICP system, no sufficient investigation has been carried out and no results applicable to HARC SiO₂ etching have been reported.

During the etching of SiO₂ using the PFC gases, PFC gases are dissociated/ionized, and the characteristics of the dissociation/ionization affect the etch characteristics of SiO₂ such as etch rates, etch selectivity over mask layers, and etch profile. Because the characteristics of the dissociation/ionization of the PFCs by ICP and CCP systems are different, the HARC SiO₂ etch characteristics will be different; however, currently, no detailed research results can be found in the literature on the differences between the ICP system and the CCP system for the dissociation/ionization of PFCs and their relationship to the etching of HARC SiO₂ using the same PFC gases. Moreover, the reason for the use of the CCP system for the HARC etching instead of the ICP system is due to the lower dissociation of the fluorocarbon gas to have high C/F ratio radicals/ions in the plasma for the higher etch selectivity over mask layers, but no research has been carried out using a perfluorocarbon gas with the high C/F ratio ≥ 1.0 such as C_6F_6 for higher C/F ratio radicals/ions even for the higher gas dissociation. In this study, using a PFC gas having a high C/F ratio of C_6F_6 , the differences in the plasma characteristics of the C_6F_6 and the etch characteristics such as etch rate, etch selectivity over a hard mask layer, and etch profile were compared between the ICP system and the CCP system. In addition, the possibility of using the ICP system in HARC SiO₂ etching masked with an amorphous carbon layer (ACL) was investigated. In the case of C_6F_6 , in addition to a high C/F ratio, the global warming potential (GWP) is very low compared to some of PFC gases generally used for HARC SiO₂ etching such as CF_4 and C_4F_8 [15–17], as shown in Table 1, and its boiling point is lower than 0 $^{\circ}$ C (a liquid PFC); therefore, if required, the undissociated C_6F_6 can be collected at the exhaust line, which can reduce the global warming effect further.

Table 1. The lifetimes and 100-year GWPs of perfluorocarbon gases CF_4 , c- C_4F_8 , C_2F_6 , and C_6F_6 based on the IPCC reports [18].

Gas Species	Chemical Formula	Lifetime (Years)	GWP _{100 years}
Perfluoromethane	CF ₄	50,000	6500
Perfluorocyclobutane	$c-C_4F_8$	3200	8700
Perfluoroethane	C_2F_6	10,000	9200
Hexafluorobenzene	C_6F_6	0.23	7

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2. Materials and Methods

Figure 1 shows the schematics of the ICP etching system and CCP etching system used in the experiment. The ICP system used in this study was composed of a spiral gold-coated copper coil separated by a 1 cm thick quartz window located on the top of the process chamber for the generation of ICP with a 13.56 MHz RF power and the substrate holder biased with a separate 13.56 MHz RF power for the control of the ion energy to the substrate. The distance between the ICP source and the substrate was ~7 cm, and the ICP antenna and substrate were also cooled at room temperature by a chiller. In the case of the CCP system, one 60 MHz RF power was connected to the top electrode with a showerhead for the control of plasma density, and a 2 MHz RF power source was connected to the bottom electrode holding the substrate for the control of ion energy to the substrate. The distance between the two electrodes was ~30 mm, and both top and bottom electrodes were cooled at room temperature by a chiller. For the vacuum environments, a turbo molecular pump backed by a dry pump was used for both systems. To use liquid state C_6F_6 , heating systems were connected to the gas lines of ICP and CCP systems. C_6F_6 (boiling point: 76 °C) was vaporized and delivered from a canister to the process chambers. Gas lines were maintained at 80 °C using heating systems. A quartz viewport window was located on the sidewall of the process chambers for the plasma analysis using an optical emission spectrometer (OES).

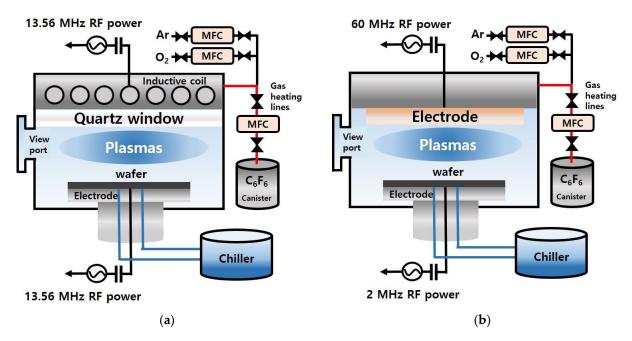


Figure 1. Schematic drawings of (a) the inductively coupled plasma (ICP) etching system and (b) the capacitively coupled plasma (CCP) etching system used in this experiment with C_6F_6 (liquid state at RT)/Ar/O₂.

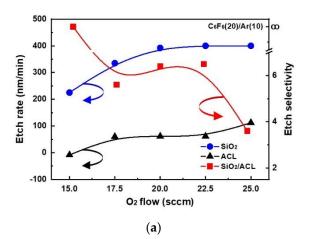
As the sample, 2.4 μ m thick SiO₂ on Si masked by 1.4 μ m thick ACL with 160 nm hole patterns was used. In addition to C₆F₆, Ar and O₂ were added for the processing, and the O₂ flow rates were varied to control the fluorocarbon layer formed on the sample surface. For the ICP system, 500 W of RF power and -1500 V of bias voltage were applied to the ICP source and substrate while keeping 6 mTorr of operating pressure, and oxygen flow rate was varied from 15 to 25 sccm while keeping the gas flow rates of C₆F₆ and Ar at 20 and 10 sccm. In the case of the CCP system, 400 W of RF power and -1700 V of bias voltage were applied to the top electrode and substrate while keeping 30 mTorr of operating pressure, and the oxygen flow rate was varied from 150 to 200 sccm while maintaining the gas flow rates of C₆F₆ and Ar at 50 and 150 sccm.

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The etch depths of SiO_2/ACL and the SiO_2 etch profiles were observed using field emission scanning electron microscopy (FE-SEM, Hitachi S-4700) after the etching using ICP and CCP, and the etch rates and etch selectivity were calculated. The compositions and binding states of the etched SiO_2 surfaces were observed using X-ray photoelectron spectroscopy (XPS, Fisons Instruments Surface Systems ESCALAB 220i). Then, to fit the spectrum of the C1s peak and to calculate the atomic percentages on the SiO_2 surfaces, an XPS peak-fitting software (software name: Thermo Scientific Avantage) and the Origin program (Origin Lab Corporation) were used. The differences in the dissociation species of C_6F_6 in the ICP and CCP used in our experimental conditions were observed using an optical emission spectroscope (OES, Isoplane SCT3200, Andor iStar 734).

3. Results and Discussion

Using $C_6F_6/Ar/O_2$, ACL-masked SiO_2 was etched in the ICP and CCP systems, and the etch rates and etch selectivities estimated from the etch depths of ACL and SiO₂ are shown in Figure 2a for the ICP system and Figure 2b for the CCP system. As shown in Figure 2a, for the ICP system, until the oxygen flow rate was higher than 15.0 sccm, no etching of ACL was observed, and from the oxygen flow rate higher than 17.5 sccm, the ACL etch rate was increased with oxygen flow rate. In the case of SiO₂, the etching was observed even at 15.0 sccm, and with an increase in the oxygen flow rate, the SiO_2 etch rate was increased to ~400 nm/min at 20 sccm, and the further increase in oxygen flow rate nearly saturated the SiO₂ etch rate. The etch selectivity of SiO₂/ACL was infinite at 15 sccm and ~6.5 at 20-22.5 sccm, and the further increase in oxygen flow rate to 25 sccm decreased the etch selectivity to ~3.6. In the case of the CCP system, for the oxygen flow rate from 150 to 180 sccm, deposition of a fluorocarbon layer instead of etching was observed on the ACL, and when the oxygen flow rate was 200 sccm, ~12 nm/min of ACL etching was observed. In the case of SiO₂, the etch rate ~244 nm/min was observed even at 150 sccm; with increasing oxygen flow rates, the etch rate was slightly increased (or nearly saturated) to 200 sccm by showing the etch rate of ~267 nm/min. However, when the oxygen flow rate was lower than 150 sccm, SiO₂ etching was also decreased to ~0 for the CCP system (not shown). Therefore, the etch selectivity of SiO₂/ACL was infinite from 150 to 180 sccm, and the etch selectivity of ~23 could be obtained at 200 sccm. From the above results, it can be concluded that the etching of SiO₂ requires a much lower ratio of O₂/C₆F₆ (0.75–1.25 for ICP and 3-4 for CCP) for the ICP system, the maximum SiO₂ etch rate is higher for the ICP system (~400 nm/min for ICP and ~267 nm/min for CCP), and the etch selectivity is much higher for the CCP system at the maximum SiO₂ etch rate (~6.5 for ICP and ~23 for CCP).



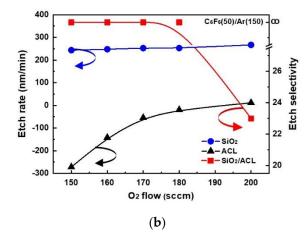
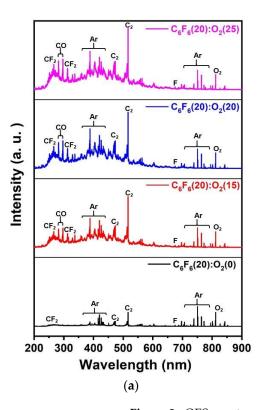


Figure 2. SiO_2 etch rates and SiO_2 etch selectivities over ACL in $C_6F_6/Ar/O_2$ plasmas as a function of O_2 gas flow rate in (a) ICP and (b) CCP systems. The flow rates of C_6F_6 and Ar were 20 and 10 sccm for the ICP system and 50 and 150 sccm for the CCP system.

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To understand the differences in the etch characteristics of ACL-masked SiO₂ with C₆F₆/Ar/O₂ gas mixtures between the ICP and CCP systems, the dissociation characteristics of C₆F₆/Ar/O₂ for different oxygen flow rates were investigated with OES for the wavelength range of 200-900 nm, and the results are shown in Figure 3a for the ICP system from 0 to 25 sccm of oxygen flow rate and Figure 3b for the CCP system from 0 to 250 sccm of oxygen flow rate. For easier comparison, the OES data were normalized by the Ar peak at 750.4 nm. As shown in Figure 3a,b, optical emission peaks from O (777.3, 844.8 nm), F (685.7, 703.8 nm), Ar (696,7, 706.8, 738.6, 750.4, 772.5, 794.9, 800.7, 801.6, 811.6, and 826.5 nm), CO (282.7, 296.8 nm), C₂ (473.7, 516.7, 563.6 nm), CF₂ (245–321 nm), etc., could be observed [19]. Among these peaks, the emission peaks related to CF₂ (247 nm), CO (297.7 nm), C₂ (516.5 nm), and F (703.7 nm) normalized by Ar (750. 4 nm) measured as a function of oxygen flow rate are shown in Figure 4a for the ICP system and b for the CCP system. In general, during the etching of SiO₂ by fluorocarbon plasmas, F radicals react with Si on the SiO₂ surface and are removed from the surface as SiF_x while C radicals react with O on the SiO_2 surface and are removed from the surface as CO_x [20]. As shown in Figure 4a,b, the increase in densities of radicals such as CF₂, CO, C₂, and F with increasing oxygen flow rate could be observed in both the ICP system and the CCP system due to the increased dissociation of fluorocarbon by oxygen radicals in the plasmas. However, a more significant increase in the radicals with increasing oxygen flow rate was observed for the ICP system even with lower oxygen flow rates. When the radical ratios of CF₂/F, CO/F, and C_2/F were compared between the ICP and CCP systems, significantly high ratios of CF₂/F (5.0–7.1 for ICP and 0.8–1.1 for CCP), CO/F (0–8.8 for ICP and 0–1.5 for CCP), and C_2/F (15.5–41.5 for ICP and 1.4–1.8 for CCP) were observed for the ICP system due to the significantly higher radical densities of CF₂, CO, and C₂ compared to F density for the ICP system, indicating more significant dissociation of the C₆F₆ of the ICP system compared to the CCP system.



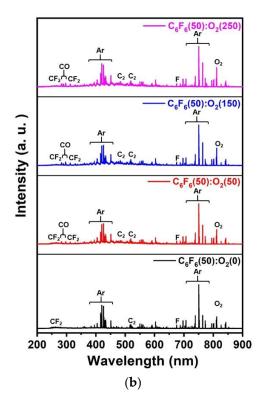
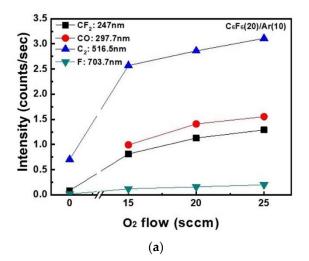


Figure 3. OES spectra of $C_6F_6/Ar/O_2$ plasmas: (a) $C_6F_6(20)/Ar(10)/O_2(0-25)$ sccm for the ICP system and (b) $C_6F_6(50)/Ar(150)/O_2(0-250)$ sccm for the CCP system. The spectral peaks were normalized by the Ar peak intensity (750.4 nm).

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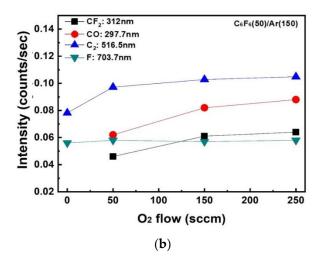


Figure 4. OES intensities of CF_2 (247–312 nm), CO (297.7 nm), C_2 (516.5 nm), and F (703.7 nm) normalized by Ar (750.4 nm) as a function of O_2 gas flow rate for (a) the ICP system and (b) the CCP system.

Figure 5 shows the XPS narrow scan data of C 1s on the SiO₂ surfaces etched with $C_6F_6/Ar/O_2$ for different oxygen flow rates for (a) the ICP system with $C_6F_6(20)/Ar(10)/O_2$ (15-25 sccm) and (b) the CCP system with $C_6F_6(50)/Ar(150)/O_2(160\sim200 \text{ sccm})$. The other conditions are the same as those in Figure 2. The carbon bonding peaks such as C-C (285.5 eV), C-CF (287.8 eV), C-F (290.0 eV), and C-F₂ (291.3 eV) could be observed [21]. For the ICP system, as shown in Figure 5a, the increase in oxygen flow rate from 15 to 25 sccm decreased C-C bonding and C-CF bonding slightly possibly due to the greater dissociation of species from the plasmas as shown in Figure 4a. In the case of the CCP system, the increase in oxygen flow rate from 160 to 200 sccm did not change the carbon bonding peaks on the SiO₂ surface noticeably possibly due to no significant change of radical ratios with increasing oxygen flow rate as shown in Figure 4b. When C 1s bonding peaks on the etched SiO₂ surfaces between the ICP system and the CCP systems are compared, the SiO₂ surfaces etched by the CCP system show slightly higher C-CF bonding intensities compared to those by the ICP system. Table 2 shows the composition of the SiO₂ surface etched using $C_6F_6/Ar/O_2$ as a function of O_2 gas flow rates for the ICP and CCP systems for the conditions in Figure 5. As shown in Table 2, even though the ratio of C_6F_6/O_2 in the gas mixture was much higher for the SiO₂ etching using the CCP system, similar compositions of fluorocarbon polymer layers were observed between the ICP system and the CCP system on the etched SiO₂ surfaces; however, a more significant increase in Si percentage (0% to 2.5% for ICP and 0% to 0.7% for CCP) and a more significant decrease in C percentage (48.6% to 42.6% for ICP and 47.8% to 45.7% for CCP) were observed on the etched SiO₂ surfaces for the ICP system compared to those for the CCP system, indicating thinner fluorocarbon layers on the SiO2 surface etched by the ICP system, which could increase SiO₂ etch rate with increasing oxygen flow rate. In fact, the SiO₂ etch rate was increased with oxygen flow rate from 15 to 22.5 sccm for the ICP system, while that for the CCP system was almost saturated with increasing oxygen flow rate from 150 to 200 sccm.

The etch profiles of 160 nm ACL hole masked SiO_2 with different O_2 gas flow rates of $C_6F_6(20)/Ar(10)/O_2(15-25$ sccm) for the ICP system are shown in Figure 6a–e, and those with $C_6F_6(50)/Ar(150)/O_2(150-200$ sccm) for the CCP system are shown in Figure 6f–j. White dotted lines are the ACL mask bottom positions and red arrows show ACL mask top positions. For the ICP etching with $C_6F_6/Ar/O_2$, for 15–17.5 sccm of oxygen flow rate, the ACL mask was clogged by the fluorocarbon layer after etching 1.4–2.0 μ m depth of SiO_2 . After using the oxygen flow rate of 20 sccm or higher, ~2.4 μ m thick SiO_2 could be fully etched with highly anisotropic etch profiles even though the etched amount of ACL mask was increased with the increase in oxygen flow rate. In the case of the CCP etching with

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 $C_6F_6/Ar/O_2$, for the oxygen flow rates of 150–180 sccm, a thick fluorocarbon layer was deposited on the top of the ACL mask while etching ~2.4 µm thick SiO₂ anisotropically; therefore, infinite etch selectivity of SiO₂/ACL could be obtained. For the oxygen flow rate of 200 sccm, the top of the ACL mask was etched while etching ~2.4 µm thick SiO₂. Therefore, as shown in Figure 2b, the infinite etch selectivity of SiO₂/ACL was observed for the oxygen flow rate of 150–180 sccm, and the etch selectivity of 23 was observed for the oxygen flow rate of 200 sccm. However, for the SiO₂ etching with the CCP system, even though deposition of a fluorocarbon layer on the top of the ACL was observed during the etching of SiO₂, the ACL sidewall was etched for the oxygen flow rates of 150–180 sccm; therefore, triangular-shaped ACL was observed after the etching.

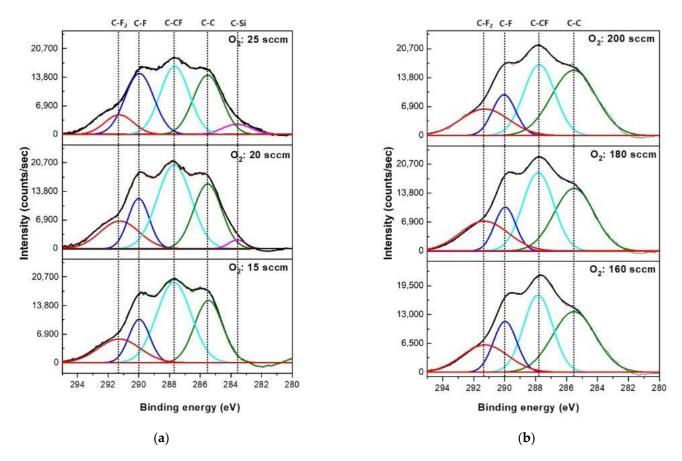


Figure 5. C1s XPS narrow scan spectra of SiO_2 surface after etching using $C_6F_6/O_2/Ar$ plasmas as a function of O_2 gas flow rates with (a) the ICP system and (b) the CCP system.

Table 2. Composition of the SiO_2 surface etched using $C_6F_6/Ar/O_2$ as a function of O_2 gas flow rate for the ICP and CCP systems.

System Type	Etch Gas	Si 2p (%)	O 1s (%)	F 1s (%)	C 1s (%)	Total (%)
ICP	C ₆ F ₆ (20)/O ₂ (2 C ₆ F ₆ (20)/O ₂ (2 C ₆ F ₆ (20)/O ₂ (2	20) 1.1	4.6 5.5 7.1	46.8 45.8 47.7	48.6 47.6 42.6	100 100 100
ССР	C ₆ F ₆ (50)/O ₂ (7 C ₆ F ₆ (50)/O ₂ (7 C ₆ F ₆ (50)/O ₂ (7	180) -	6.9 7.0 7.4	45.3 46.0 46.2	47.8 47.0 45.7	100 100 100

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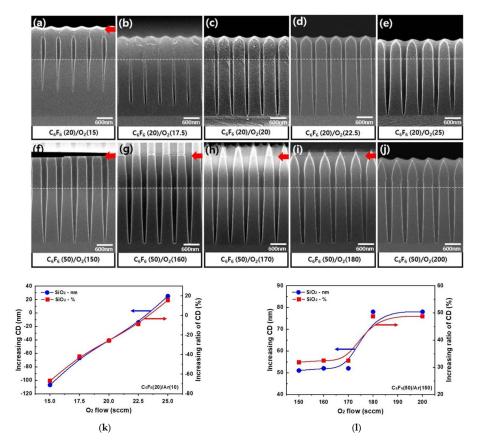


Figure 6. Etch profiles of 160 nm ACL hole masked SiO_2 with different O_2 gas flow rates of $C_6F_6(20)/Ar(10)/O_2(15-25$ sccm) for the ICP system (**a-e**) and with $C_6F_6(50)/Ar(150)/O_2(150-200$ sccm) for the CCP system (**f-j**). (**k,l**) The changes of pattern hole width (CD) and its changed percentages of SiO_2 after the etching of ~2.4 μ m thick SiO_2 on Si masked by 1.4 μ m thick ACL with 160 nm hole patterns for (**a-e**) the ICP system and (**f-j**) the CCP system, respectively, except for the cases when the ACL mask holes were clogged by a fluorocarbon layer. White dotted lines are the ACL mask bottom positions and red arrows show ACL mask top positions.

The changes of SiO₂ hole diameter critical dimension (CD) and its changed percentages after the etching of \sim 2.4 µm thick SiO₂ on Si masked by 1.4 µm thick ACL with 160 nm hole patterns for Figure 6a-e the ICP system and Figure 6f-j the CCP system were showed in Figure 6k,l, respectively, except for the cases when the ACL mask holes were clogged by a fluorocarbon layer. As shown in Figure 6k, for the ICP system, due to the clogging of the ACL mask top area at the lower oxygen flow rates, the hole pattern diameter smaller than the ACL mask hole diameter was observed for the oxygen flow rate from 15 to 20 sccm (from -66% at 15 sccm to -25% at 20 sccm), but due to the increase in hole diameter with increasing oxygen flow rate, the hole diameter equal to the ACL mask hole diameter CD or higher was observed with the further increase in oxygen flow rate from 22.5 to 25 sccm (from -8% at 22.5 sccm to +15% at 25 sccm). Therefore, for the oxygen flow rate of 20~22.5 sccm, highly anisotropic SiO₂ etch profiles with no significant hole diameter CD variation were observed for the etching by the ICP system with $C_6F_6/Ar/O_2$, which could be applied for the HARC SiO₂ etching. However, as shown in Figure 6l, for the etching by the CCP system with $C_6F_6/Ar/O_2$, even though the etch selectivity of SiO_2/ACL was infinite, due to the etching of ACL sidewall, for the oxygen flow rates of 150~200 sccm, an increase in hole diameter percentage from +31% to +48% was observed with less anisotropic SiO₂ etch profiles compared to those etched by the ICP system.

For the CCP system, the ratio of Ar/C_6F_6 used in the etching of ACL-masked SiO_2 was much higher than that for the ICP system (10/20 for ICP and 150/50 for CCP); therefore, the widening of the SiO_2 hole diameter CD could be related to the enhanced ion bombardment

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by Ar⁺ ions for the CCP system. In fact, in the experiment, the different Ar flow rates used for the ICP and CCP systems were related to the optimized process for the SiO₂ etching with the ICP and CCP systems. However, to clearly show the effect of Ar gas flow rate on the etching, the SiO₂ masked by ACL mask was also etched with and without the Ar flow rates for each of the ICP/CCP etching conditions. Figure 7 shows the etch rates of SiO₂ and ACL and the etch selectivity of SiO₂/ACL for (a) the ICP system and (b) the CCP system with and without Ar flow in $C_6F_6/Ar/O_2$. (c) and (d) are the SEM etch profiles of ACL-masked SiO₂ with and without Ar flow for the ICP etching, respectively, and (e) and (f) are those with and without Ar flow for the CCP etching, respectively. The gas mixtures of $C_6F_6(20)/Ar(0)/O_2(22.5)$ and $C_6F_6(20)/Ar(10)/O_2(22.5)$ were used for the ICP etching, and the gas mixtures of $C_6F_6(50)/Ar(0)/O2(200)$ and $C_6F_6(50)/Ar(150)/O2(200)$ were used for the CCP etching. As shown in Figure 7, the etch rates of SiO₂ and the etch selectivities of SiO₂/ACL were not significantly different for the etching with and without Ar flow for both the ICP system and the CCP system. In fact, there were some differences in the SiO₂ etch profiles between the gas mixtures with and without Ar, as shown in Figure 7c-f; however, also, no significant differences could be observed. Therefore, the more significant etching of the ACL sidewall and the more significant widening of SiO₂ hole diameter for the CCP system with $C_6F_6/Ar/O_2$ are not related to the higher Ar+ ion bombardment flux to the substrate due to the higher Ar gas flow rate in the gas mixture. In fact, in the case of the CCP etching, due to the low dissociation of C_6F_6 , higher-mass ions such as C_xF_v + (x = 3-6, y = 4-5) having the ion mass higher than 100 (while the mass of Ar+ is ~40) can exist in the plasmas more than those formed during the ICP etching. The ion bombardment by those partially dissociated high-mass ions can etch the ACL sidewall more and widen the SiO₂ hole diameter more, which can result in more tapered etch profiles as shown in Figure 6f-j.

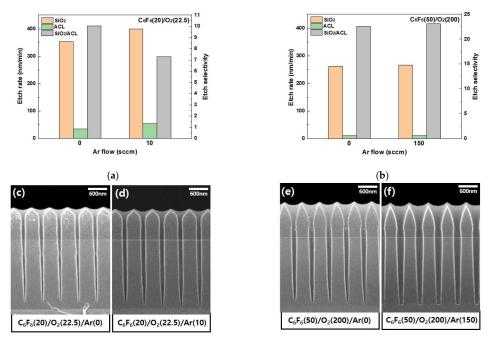


Figure 7. Etch rates of SiO_2 and ACL and the etch selectivity of SiO_2/ACL for (a) the ICP system and (b) the CCP system with and without Ar flow in $C_6F_6/Ar/O_2$. (c,d) The SEM etch profiles of ACL-masked SiO_2 with and without Ar flow for the ICP etching, respectively; (e,f) those with and without Ar flow for the CCP etching, respectively. The gas mixtures of $C_6F_6(20)/Ar(0)/O_2(22.5)$ and $C_6F_6(20)/Ar(10)/O_2(22.5)$ were used for the ICP etching and the gas mixtures of $C_6F_6(50)/Ar(0)/O_2(200)$ and $C_6F_6(50)/Ar(150)/O_2(200)$ were used for the CCP etching. White dotted lines in (c-f) are ACL mask lines and red dotted circle shows the bowed area in the SiO_2 hole.

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4. Conclusions

In this study, using a perfluorocarbon (PFC) gas having a high C/F ratio of C_6F_6 and low GWP of 7, the differences in the plasma characteristics and the etch characteristics were compared between an ICP system and a CCP system. In addition, the possibility of using an ICP system instead of a conventional CCP system in HARC SiO₂ etching masked with ACL was investigated for $C_6F_6/Ar/O_2$ gas mixtures. It was found that, due to the higher dissociation of C₆F₆ and O₂ for the ICP system compared to the CCP system, the SiO₂ etching required a much lower ratio of O₂/C₆F₆ while showing a higher maximum SiO₂ etch rate and lower etch selectivity. However, in the case of the ICP etching with C_6F_6 , even though the etch selectivity was much lower than that of the CCP etching with C₆F₆, due to less heavy-mass-ion bombardment in addition to an adequate fluorocarbon layer formation on the substrate, highly anisotropic SiO₂ etch profiles could be obtained at certain oxygen gas flow rates added to C₆F₆. The high gas dissociation of the ICP system could be identified from higher densities of CF₂, CO, and C₂ radicals in the ICP system compared to the CCP system. It is believed that the ICP system could be also applied to the HARC SiO₂ etching with higher etch rates and vertical etch profiles by using high C/F ratio PFCs and by controlling etch parameters adequately.

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