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2-(3-Cyano-4-methyl-5,5-diphenyl-5Hfuran-2-ylidene)malononitrile

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Key indicators: single-crystal X-ray study; T = 123 K; mean σ (C–C) = 0.002 Å; R factor = 0.045; wR factor = 0.119; data-to-parameter ratio = 21.9.

The title compound, C₂₁H₁₃N₃O, crystallizes with two independent molecules with similar conformations per asymmetric unit. The dihydrofuran rings are essentially planar with maximum deviations of 0.017 (1) and 0.006 (1) Å for the O atoms. The dihedral angles between the dihydrofuran ring and the attached phenyl rings are 79.90 (6) and 82.07 (6) $^{\circ}$ in one molecule and 79.36 (6) and 72.26 (6) $^{\circ}$ in the other. In the crystal, the molecules are linked by weak $C-H\cdots\pi$ and C-H...N interactions similar to those in other closely related crystals. The replacement of appended methyl by phenyl groups has not significantly affected the dihydrofuran ring structure or the crystal packing interactions.

Related literature

For general background to NLO chromophores, see: Smith et al. (2006, 2010); Carey et al. (2002); Kay et al. (2004). For details of the synthesis, see: Anderson (2009). For related structures, see: Anderson (2009); Gainsford et al. (2011); Li et al. (2005); Liao et al. (2005). For geometric analysis of structures, see: Spek (2009). For a description of the Cambridge Structural Database, see: Allen (2002).



mm

45305 measured reflections 9930 independent reflections

 $R_{\rm int} = 0.042$

7329 reflections with $I > 2\sigma(I)$

Experimental

Crystal data

•	
C ₂₁ H ₁₃ N ₃ O	$\gamma = 79.233 \ (2)^{\circ}$
$M_r = 323.34$	V = 1634.07 (9) Å ²
Triclinic, P1	Z = 4
a = 9.2308 (3) Å	Mo $K\alpha$ radiation
b = 12.5991 (4) Å	$\mu = 0.08 \text{ mm}^{-1}$
c = 14.3043 (4) Å	T = 123 K
$\alpha = 89.954 \ (2)^{\circ}$	$0.36 \times 0.32 \times 0.29$
$\beta = 89.052 \ (2)^{\circ}$	

Data collection

Bruker APEXII CCD
diffractometer
Absorption correction: multi-scan
(SADABS; Bruker, 2005)
$T_{\min} = 0.651, \ T_{\max} = 0.746$

Refinement

ł

v

S g

$R[F^2 > 2\sigma(F^2)] = 0.045$	453 parameters
$vR(F^2) = 0.119$	H-atom parameters constrained
S = 1.04	$\Delta \rho_{\rm max} = 0.35 \ {\rm e} \ {\rm \AA}^{-3}$
930 reflections	$\Delta \rho_{\rm min} = -0.24 \text{ e } \text{\AA}^{-3}$

Table 1

Hydrogen-bond geometry (Å, °).

Cg1 is the centroid of the C10-C15 phenyl ring

$D - H \cdots A$	D-H	$H \cdot \cdot \cdot A$	$D \cdots A$	$D - \mathbf{H} \cdot \cdot \cdot A$		
$C20' - H20' \cdots Cg1^i$	0.95	2.69	3.4041 (14)	133		
$C9 - H9B \cdots N3'$	0.98	2.70	3.4560 (14)	134		
Summatry and (i) $x + 1$ $y + 1$						

Symmetry code: (i) -x + 1, -y + 1, -z.

Data collection: APEX2 (Bruker, 2005); cell refinement: SAINT (Bruker, 2005); data reduction: SAINT; program(s) used to solve structure: SHELXS97 (Sheldrick, 2008); program(s) used to refine structure: SHELXL97 (Sheldrick, 2008); molecular graphics: ORTEP-3 for Windows (Farrugia, 2012) and Mercury (Macrae et al., 2006); software used to prepare material for publication: SHELXL97 and PLATON (Spek, 2009).

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: RZ5081).

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supplementary materials

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2-(3-Cyano-4-methyl-5,5-diphenyl-5H-furan-2-ylidene)malononitrile

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Comment

Organic non-linear optical (NLO) chromophores consist of donor and acceptor units connecting through π -conjugation. To realise a strong NLO response, chromophores need to be in uniform alignment. Unfortunately organic chromophores have a tendency to aggregate rather than align due to their highly polar nature (Smith *et al.*, 2006). These push-pull chromophores can also exist as two rotomeric (*cis* and *trans*) forms (Kay *et al.*, 2004). As a result, these chromophores are difficult to crystallize, therefore they may not be able to be used in devices that require crystals such as terahertz wave emitters (Carey *et al.*, 2002). Consequently it is of interest to design and synthesize molecules which will be much less prone to aggregation and isomerization. It has been found that through changing the shape of the chromophore molecules, aggregation can be minimized. The most successful strategy has been to add bulky pendant groups onto the donor end (Smith *et al.*, 2010). We have reported our previous attempts with two benzyloxyphenyl groups (Gainsford *et al.*, 2011; Anderson, 2009) and report here the structure of a related acceptor unit with two phenyl groups.

The asymmetric unit of the title compound (I) contains two independent, nearly identical, 2-(3-cyano-4-methyl-5,5-diphenyl-5*H*-furan-2-ylidene)malononitrile molecules (Fig. 1). The second molecule (1') has identical labels with an appended prime (*e.g.* C10 and C10'); the r.m.s. bond and angle fits are 0.003 Å and 0.48° (Spek, 2009). The fivemembered dihydrofuran rings (atoms C4-C7/O1, hereafter plane 1) are planar (maximum deviation 0.017 (1) Å for O1) with the appended cyano groups almost coplanar (maximum deviation 0.093 (1) Å for N1). The 5,5-dimethyl adduct (Li *et al.*, 2005; CSD refcode PANLUM), in which plane 1 was constrained to a crystallographic mirror plane, has identical ring dimensions with the exception of the C4–C5 bond which is just significantly longer here (by 0.013 (4) Å). This marginally longer distance seems the exception and is not observed in related molecules [Allen (2002); CSD version 5.34 with May 2013 updates: *e.g.* KAJCII and KATCEE, 1.518 and 1.536, 1.537 Å respectively (Liao *et al.*, 2005); YAHKUP 1.512 Å (Gainsford *et al.*, 2011)].

The only significant conformational differences between the two molecules concern the interplanar angles between the phenyl rings and plane 1, corresponding to the different torsion angles $(C4-C5-C10-C15 = -21.21 (15)^\circ; O1-C5-C16-C17 = -30.62 (13)^\circ; C4'-C5'-C10'-C15' = -30.22 (14)^\circ; O1'-C5'-C16'-C17' = -21.91 (15)^\circ)$. The plane 1 angle to phenyl plane (C10-C15) is 79.90 (6) and 82.07 (6)° for molecules 1 and 1' while the other phenyl plane (C16-C21) makes interplane angle of 79.36 (6) and 72.26 (6)° for molecules 1 and 1'.

Lattice binding is provided mainly by one non-classical C–H··· π interaction (Table 1, Figure 2 where Cg1 is the centroid of the C10–C15 ring), the dominant binding interaction type in related compound YAHKUP (Gainsford *et al.*, 2011). As in PANLUM, a weak methyl*C*–H···*N*(cyano) interaction is observed. Other *C*–H···*N*(cyano), C–H··· π and cyano···cyano very weak interactions even closer to van der Waal's contact distances are also present. Overall, the effect of the phenyl for methyl replacement on C5 has given insignificant molecular structural and cystal packing alignment affects.

Experimental

The title compound was prepared by the condensation of 1-hydroxy-1,1-diphenylpropan-2-one with 4 equivalents of malononitrile over 10 days as described in Anderson (2009). A small portion was recrystallized in dichloromethane and acetone (1:1) mixture to give colourless crystals. M.p. 223 °C. Found: C, 77.70; H, 3.91; N, 13.06, C₂₁H₁₃N₃O requires C, 78.00; H, 4.05; N, 13.00%. Found: M^+ m/z 323.1059 C₂₁H₁₃N₃O requires: M+ m/z 323.1056 (Δ 0.9 p.p.m.). ¹H NMR– (300 MHz, CDCl₃) δ (p.p.m.): 2.41 (s, 3H), 7.18 (d, *J* 9.6 Hz, 4H), 7.51–7.47 (m, 6H). ¹³C NMR– (75 MHz, CDCl₃) δ (p.p.m.): 16.2 (CH₃), 59.5 (C_Q), 105.6 (C_Q), 106.4 (C_Q), 109.0 (C_Q), 110.2 (C_Q), 110.7 (C_Q), 127.3 (CH), 129.5 (CH), 130.6 (CH), 134.9 (C_Q), 175.1 (C_Q), 180.2 (C_Q).

Refinement

All carbon-bound H atoms were constrained to their expected geometries [C—H 0.95, 0.98 Å] and refined with U_{iso} 1.2 times the U_{eq} of their parent atom. All other non-hydrogen atoms were refined with anisotropic thermal parameters.

Computing details

Data collection: *APEX2* (Bruker, 2005); cell refinement: *SAINT* (Bruker, 2005); data reduction: *SAINT* (Bruker, 2005); program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *ORTEP-3 for Windows* (Farrugia, 2012) and *Mercury* (Macrae *et al.*, 2006); software used to prepare material for publication: *SHELXL97* (Sheldrick, 2008) and *PLATON* (Spek, 2009).



Figure 1

Content of the asymmetric unit of the title compound with displacement ellipsoids drawn at the 50% probability level. The partially obscured atom C15 is not labelled.



Figure 2

Packing diagram of the title compound with one C–H $\cdots\pi$ and C(methyl)–H \cdots N(cyano) interaction shown as dashed blue lines. H atoms not involved in intermolecular contacts are excluded except on methyl C9. *Cg*1 is the centroid of the phenyl ring (C10–C15) at symmetry 1-*x*, 1-*y*, -*z*. Symmetry code: (i) -1+*x*, *y*, *z*.

2-(3-Cyano-4-methyl-5,5-diphenyl-5*H*-furan-2-ylidene)malononitrile

Crystal data	
$C_{21}H_{13}N_{3}O$ $M_{r} = 323.34$ Triclinic, <i>P</i> 1 Hall symbol: -P 1 a = 9.2308 (3) Å b = 12.5991 (4) Å c = 14.3043 (4) Å a = 89.954 (2)° $\beta = 89.052$ (2)° $\gamma = 79.233$ (2)° V = 1634.07 (9) Å ³	Z = 4 F(000) = 672 $D_x = 1.314 \text{ Mg m}^{-3}$ Mo K\alpha radiation, \lambda = 0.71073 \mathbf{A} Cell parameters from 9027 reflections $\theta = 2.2-30.5^{\circ}$ $\mu = 0.08 \text{ mm}^{-1}$ T = 123 K Block, colourless $0.36 \times 0.32 \times 0.29 \text{ mm}$
Data collection	
Bruker APEXII CCD diffractometer Radiation source: fine-focus sealed tube Graphite monochromator Detector resolution: 8.333 pixels mm ⁻¹ φ and ω scans	Absorption correction: multi-scan (<i>SADABS</i> ; Bruker, 2005) $T_{min} = 0.651$, $T_{max} = 0.746$ 45305 measured reflections 9930 independent reflections 7329 reflections with $I > 2\sigma(I)$ $R_{int} = 0.042$

$\theta_{\rm max} = 30.7^{\circ}, \theta_{\rm min} = 1.4^{\circ}$	$k = -18 \rightarrow 18$
$h = -13 \rightarrow 13$	$l = -20 \rightarrow 20$
Refinement	
Refinement on F^2	Secondary atom site location: difference Fourier
Least-squares matrix: full	map
$R[F^2 > 2\sigma(F^2)] = 0.045$	Hydrogen site location: inferred from
$wR(F^2) = 0.119$	neighbouring sites
S = 1.04	H-atom parameters constrained
9930 reflections	$w = 1/[\sigma^2(F_o^2) + (0.0512P)^2 + 0.3811P]$
453 parameters	where $P = (F_o^2 + 2F_c^2)/3$
0 restraints	$(\Delta/\sigma)_{ m max} < 0.001$
Primary atom site location: structure-invariant	$\Delta ho_{ m max} = 0.35 \ { m e} \ { m \AA}^{-3}$
direct methods	$\Delta \rho_{\min} = -0.24 \text{ e} \text{ Å}^{-3}$

Special details

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters $(Å^2)$

	x	у	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	
01	0.34806 (9)	0.80434 (6)	0.09747 (5)	0.01913 (17)	
N1	0.71127 (14)	0.64480 (10)	-0.12562 (9)	0.0387 (3)	
N2	0.41086 (13)	0.95957 (10)	-0.09834 (8)	0.0315 (3)	
N3	0.68541 (13)	0.46791 (10)	0.06030 (8)	0.0320 (3)	
C1	0.62087 (14)	0.70061 (10)	-0.08395 (9)	0.0255 (3)	
C2	0.50822 (13)	0.77028 (10)	-0.03197 (8)	0.0204 (2)	
C3	0.45366 (13)	0.87575 (10)	-0.06807 (8)	0.0228 (2)	
C4	0.40415 (12)	0.64052 (9)	0.17749 (8)	0.0194 (2)	
C5	0.30203 (12)	0.74917 (9)	0.18178 (8)	0.0176 (2)	
C6	0.45279 (12)	0.73785 (9)	0.04999 (8)	0.0183 (2)	
C7	0.49044 (12)	0.63614 (9)	0.10052 (8)	0.0193 (2)	
C8	0.60060 (13)	0.54476 (10)	0.07557 (8)	0.0225 (2)	
C9	0.40783 (15)	0.55820 (10)	0.25144 (9)	0.0269 (3)	
H9A	0.4637	0.4889	0.2288	0.032*	
H9B	0.3069	0.5502	0.2677	0.032*	
H9C	0.4553	0.5808	0.3069	0.032*	
C10	0.14038 (12)	0.74436 (9)	0.16821 (8)	0.0188 (2)	
C11	0.03222 (13)	0.83316 (10)	0.19229 (8)	0.0225 (2)	
H11	0.0589	0.8940	0.2219	0.027*	
C12	-0.11448 (14)	0.83266 (11)	0.17303 (9)	0.0278 (3)	
H12	-0.1884	0.8930	0.1899	0.033*	
C13	-0.15301 (14)	0.74430 (12)	0.12926 (9)	0.0301 (3)	
H13	-0.2535	0.7441	0.1162	0.036*	
C14	-0.04624 (15)	0.65645 (11)	0.10437 (9)	0.0288 (3)	

H14	-0.0733	0.5963	0.0738	0.035*
C15	0.10062 (14)	0.65600 (10)	0.12400 (9)	0.0238 (2)
H15	0.1740	0.5953	0.1072	0.029*
C16	0.33659 (12)	0.80840 (9)	0.26874 (8)	0.0186 (2)
C17	0.45540 (13)	0.86160 (10)	0.26897 (9)	0.0226 (2)
H17	0.5119	0.8654	0.2134	0.027*
C18	0.49144 (15)	0.90922 (11)	0.35082 (9)	0.0287 (3)
H18	0.5728	0.9456	0.3512	0.034*
C19	0.40914 (17)	0.90379 (12)	0.43177 (9)	0.0337 (3)
H19	0.4334	0.9371	0.4875	0.040*
C20	0.29189 (17)	0.85014 (12)	0.43188 (9)	0.0329 (3)
H20	0.2352	0.8468	0.4875	0.040*
C21	0.25681(15)	0.80120 (10)	0.35100 (8)	0.0255(3)
H21	0.1778	0.7625	0.3517	0.031*
01'	0.98981 (9)	0 20107 (6)	0.40488(5)	0 01929 (17)
N1′	1 26942 (15)	0.36533(11)	0.10100(9)	0.0397(3)
N2'	1.20912(19) 1.13037(14)	0.05064 (10)	0.60095 (8)	0.0397(3)
N3'	1.15037(14) 1.16038(13)	0.53580 (9)	0.00093(8) 0.43102(8)	0.0340(3) 0.0302(2)
C1'	1.10030(13) 1.20774(14)	0.30913(11)	0.43102(0) 0.57926(9)	0.0302(2)
C1	1.20774(14) 1.13161(13)	0.30913(11) 0.23860(10)	0.57920(9) 0.53017(8)	0.0205(3)
C_2'	1.13101(13) 1.12000(14)	0.23800(10) 0.13375(10)	0.55017 (8)	0.0214(2) 0.0236(2)
CJ	1.12990(14)	0.15575(10) 0.35081(0)	0.30893(8)	0.0230(2)
C4 C5/	0.97037(12)	0.35981(9) 0.25122(0)	0.31831(8) 0.21821(8)	0.0192(2)
CS	1.06105(12)	0.23132(9) 0.26850(0)	0.31831(8) 0.44854(8)	0.0181(2)
C0	1.00105(12) 1.05045(12)	0.20830(9) 0.26764(0)	0.44634(8) 0.20470(8)	0.0183(2)
C^{γ}	1.03043(12) 1.11272(12)	0.30704(9)	0.39479(8)	0.0194(2)
	1.115/5(15)	0.43944(10) 0.420(0(10))	0.41079(8)	0.0220(2)
	0.95505 (15)	0.43900 (10)	0.24239 (9)	0.0202 (3)
П9 А 110/Д	0.9034	0.3077	0.2007	0.031*
	0.8289	0.4320	0.2309	0.031*
HYC C10/	0.9893	0.4120	0.1855	0.031^{+}
	0.75078(12)	0.20000 (9)	0.33075(8)	0.0187(2)
	0.08589(15)	0.18118 (10)	0.29681 (9)	0.0231(2)
HII	0.7401	0.1214	0.2630	0.028*
C12'	0.53511 (14)	0.18933 (11)	0.31243 (9)	0.0276 (3)
HI2'	0.4859	0.1359	0.2879	0.033*
C13'	0.45660 (14)	0.27472 (11)	0.36351 (10)	0.0290 (3)
H13'	0.3537	0.2798	0.3741	0.035*
C14′	0.52747 (14)	0.35269 (11)	0.39920 (10)	0.0291 (3)
H14′	0.4737	0.4106	0.4353	0.035*
C15′	0.67724 (14)	0.34638 (10)	0.38225 (9)	0.0241 (2)
H15′	0.7256	0.4007	0.4059	0.029*
C16′	0.99343 (13)	0.18644 (9)	0.23453 (8)	0.0189 (2)
C17′	1.13164 (13)	0.12020 (9)	0.24063 (9)	0.0217 (2)
H17'	1.1791	0.1096	0.2992	0.026*
C18′	1.19993 (14)	0.06974 (10)	0.16117 (9)	0.0262 (3)
H18′	1.2949	0.0254	0.1654	0.031*
C19′	1.13090 (16)	0.08335 (10)	0.07570 (9)	0.0288 (3)
H19′	1.1776	0.0478	0.0216	0.035*
C20′	0.99357 (15)	0.14899 (11)	0.06954 (9)	0.0287 (3)

supplementary materials

H20′	0.9458	0.1584	0.0110	0.034*	
C21′	0.92545 (14)	0.20087 (10)	0.14786 (8)	0.0252 (3)	
H21′	0.8317	0.2467	0.1428	0.030*	

Atomic displacement parameters $(Å^2)$

	U^{11}	U^{22}	U^{33}	U^{12}	U^{13}	<i>U</i> ²³
01	0.0182 (4)	0.0211 (4)	0.0176 (4)	-0.0025 (3)	0.0024 (3)	0.0021 (3)
N1	0.0364 (7)	0.0400 (7)	0.0369 (7)	-0.0012 (6)	0.0125 (5)	-0.0044 (6)
N2	0.0309 (6)	0.0339 (6)	0.0282 (6)	-0.0025 (5)	0.0041 (5)	0.0049 (5)
N3	0.0288 (6)	0.0323 (6)	0.0317 (6)	0.0029 (5)	-0.0057 (5)	-0.0042 (5)
C1	0.0244 (6)	0.0287 (6)	0.0235 (6)	-0.0057 (5)	0.0027 (5)	0.0005 (5)
C2	0.0182 (5)	0.0246 (6)	0.0184 (5)	-0.0042 (4)	0.0005 (4)	-0.0005 (4)
C3	0.0206 (6)	0.0305 (6)	0.0177 (5)	-0.0060 (5)	0.0025 (4)	-0.0003 (5)
C4	0.0180 (5)	0.0202 (5)	0.0208 (5)	-0.0057 (4)	-0.0035 (4)	0.0002 (4)
C5	0.0172 (5)	0.0196 (5)	0.0160 (5)	-0.0039 (4)	0.0017 (4)	0.0020 (4)
C6	0.0153 (5)	0.0216 (5)	0.0184 (5)	-0.0045 (4)	-0.0021 (4)	-0.0018 (4)
C7	0.0171 (5)	0.0206 (5)	0.0204 (5)	-0.0039 (4)	-0.0027 (4)	-0.0016 (4)
C8	0.0193 (5)	0.0258 (6)	0.0225 (6)	-0.0045 (5)	-0.0035 (4)	-0.0022 (5)
C9	0.0306 (7)	0.0238 (6)	0.0258 (6)	-0.0040 (5)	-0.0005 (5)	0.0060 (5)
C10	0.0170 (5)	0.0241 (5)	0.0161 (5)	-0.0055 (4)	-0.0003 (4)	0.0021 (4)
C11	0.0203 (5)	0.0264 (6)	0.0211 (5)	-0.0049 (5)	0.0002 (4)	-0.0015 (5)
C12	0.0188 (6)	0.0365 (7)	0.0265 (6)	-0.0013 (5)	0.0000 (5)	0.0007 (5)
C13	0.0187 (6)	0.0440 (8)	0.0297 (6)	-0.0110 (5)	-0.0043 (5)	0.0040 (6)
C14	0.0281 (6)	0.0318 (7)	0.0301 (6)	-0.0146 (5)	-0.0055 (5)	0.0011 (5)
C15	0.0234 (6)	0.0238 (6)	0.0254 (6)	-0.0070 (5)	-0.0015 (5)	0.0000 (5)
C16	0.0180 (5)	0.0197 (5)	0.0180 (5)	-0.0032 (4)	-0.0026 (4)	0.0010 (4)
C17	0.0188 (5)	0.0234 (6)	0.0259 (6)	-0.0047 (4)	-0.0024 (5)	0.0033 (5)
C18	0.0287 (6)	0.0274 (6)	0.0330 (7)	-0.0121 (5)	-0.0109 (5)	0.0032 (5)
C19	0.0466 (8)	0.0355 (7)	0.0231 (6)	-0.0175 (6)	-0.0107 (6)	-0.0007 (5)
C20	0.0451 (8)	0.0385 (7)	0.0185 (6)	-0.0164 (6)	0.0006 (6)	0.0005 (5)
C21	0.0287 (6)	0.0306 (6)	0.0204 (5)	-0.0135 (5)	-0.0011 (5)	0.0015 (5)
O1′	0.0198 (4)	0.0208 (4)	0.0176 (4)	-0.0045 (3)	-0.0035 (3)	0.0023 (3)
N1′	0.0412 (7)	0.0389 (7)	0.0397 (7)	-0.0079 (6)	-0.0131 (6)	-0.0056 (6)
N2′	0.0397 (7)	0.0325 (6)	0.0303 (6)	-0.0033 (5)	-0.0062 (5)	0.0042 (5)
N3′	0.0302 (6)	0.0310 (6)	0.0312 (6)	-0.0109 (5)	0.0057 (5)	-0.0038 (5)
C1′	0.0250 (6)	0.0289 (6)	0.0243 (6)	-0.0013 (5)	-0.0044 (5)	-0.0013 (5)
C2′	0.0192 (5)	0.0246 (6)	0.0195 (5)	-0.0020 (4)	-0.0017 (4)	-0.0006 (4)
C3′	0.0229 (6)	0.0276 (6)	0.0184 (5)	-0.0002 (5)	-0.0034 (5)	-0.0010 (5)
C4′	0.0154 (5)	0.0209 (5)	0.0203 (5)	-0.0016 (4)	0.0033 (4)	0.0007 (4)
C5′	0.0175 (5)	0.0201 (5)	0.0158 (5)	-0.0011 (4)	-0.0022 (4)	0.0023 (4)
C6′	0.0141 (5)	0.0214 (5)	0.0188 (5)	-0.0019 (4)	0.0020 (4)	-0.0018 (4)
C7′	0.0161 (5)	0.0213 (5)	0.0208 (5)	-0.0036 (4)	0.0030 (4)	-0.0005 (4)
C8′	0.0188 (5)	0.0251 (6)	0.0219 (6)	-0.0042 (5)	0.0032 (4)	-0.0009 (5)
C9′	0.0293 (6)	0.0250 (6)	0.0241 (6)	-0.0046 (5)	-0.0004 (5)	0.0061 (5)
C10′	0.0167 (5)	0.0215 (5)	0.0172 (5)	-0.0015 (4)	-0.0001 (4)	0.0031 (4)
C11′	0.0214 (6)	0.0240 (6)	0.0234 (6)	-0.0030 (5)	0.0003 (5)	-0.0010 (5)
C12′	0.0221 (6)	0.0299 (6)	0.0325 (7)	-0.0087 (5)	-0.0021 (5)	0.0027 (5)
C13′	0.0177 (6)	0.0339 (7)	0.0344 (7)	-0.0025 (5)	0.0028 (5)	0.0059 (6)
C14′	0.0225 (6)	0.0284 (6)	0.0335 (7)	0.0019 (5)	0.0060 (5)	0.0001 (5)

supplementary materials

C15′	0.0215 (6)	0.0234 (6)	0.0268 (6)	-0.0029 (5)	0.0013 (5)	-0.0013 (5)
C16′	0.0185 (5)	0.0196 (5)	0.0187 (5)	-0.0037 (4)	0.0012 (4)	0.0004 (4)
C17′	0.0196 (5)	0.0208 (5)	0.0244 (6)	-0.0029 (4)	0.0004 (4)	0.0020 (5)
C18′	0.0235 (6)	0.0215 (6)	0.0313 (6)	0.0008 (5)	0.0060 (5)	0.0021 (5)
C19′	0.0347 (7)	0.0257 (6)	0.0245 (6)	-0.0023 (5)	0.0103 (5)	-0.0019 (5)
C20′	0.0331 (7)	0.0337 (7)	0.0183 (5)	-0.0035 (6)	0.0014 (5)	0.0000 (5)
C21′	0.0220 (6)	0.0308 (6)	0.0208 (6)	0.0002 (5)	-0.0012 (5)	0.0022 (5)

Geometric parameters (Å, °)

$\begin{array}{cccccccccccccccccccccccccccccccccccc$	O1—C6	1.3320 (14)	O1'—C6'	1.3295 (14)
N1C11.1450 (17)N1'C1'1.1469 (18)N2C31.1437 (16)N2'C3'1.1417 (17)N3C81.1443 (16)N3'C8'1.1448 (16)C1C21.4280 (18)C1'-C2'1.4239 (18)C2C61.3642 (16)C2'-C6'1.3647 (15)C2C31.4295 (16)C2'-C3'1.4351 (17)C4C71.3432 (17)C4'-C7'1.3432 (16)C4C71.3432 (16)C4'-C5'1.5180 (16)C5C161.5197 (16)C4'-C5'1.5180 (16)C5C161.5197 (16)C5'-C16'1.5180 (16)C5C101.5202 (16)C5'-C16'1.5180 (16)C5C101.5202 (16)C5'-C16'1.5180 (16)C7C81.4277 (17)C7'-C8'1.4273 (17)C9H9A0.9800C9'-H9'A0.9800C9-H9A0.9800C9'-H9'A0.9800C9-H9B0.9800C9'-H9'A0.9800C10C111.3962 (17)C10'-C15'1.3911 (17)C10-C111.3926 (17)C10'-C15'1.3911 (17)C10-C111.3875 (17)C11'-C12'1.3806 (17)C10-C111.3842 (2)C12'-C13'1.3816 (19)C12-C131.384 (2)C12'-C13'1.3816 (19)C12-C131.384 (2)C12'-C13'1.3816 (19)C12-C141.380 (2)C13'-C14'1.380 (2)C13-H130.9500C13'-C14'1.3816 (18)C14-H140.9500C13'-C14'1.3816 (18)C14-H140.9500C13'-	O1—C5	1.4866 (13)	O1′—C5′	1.4808 (12)
N2-C3 1.1437 (16) N2'-C3' 1.1417 (17) N3-C8 1.1443 (16) N3'-C8' 1.1448 (16) C1-C2 1.4280 (18) C1'-C2' 1.4239 (18) C2-C6 1.3642 (16) C2'-C6' 1.3647 (15) C2-C3 1.4295 (16) C2'-C3' 1.4351 (17) C4-C7 1.3432 (17) C4'-C7' 1.3432 (16) C4-C5 1.5107 (16) C4'-C9' 1.4779 (15) C4-C5 1.5107 (16) C5'-C16' 1.518 (16) C5-C10 1.5202 (16) C5'-C10' 1.5243 (15) C6-C7 1.4580 (15) C6'-C7' 1.4547 (17) C7-C8 1.4277 (17) C7'-C8' 1.4273 (17) C9-H9A 0.9800 C9'-H9'A 0.9800 C9-H9B 0.9800 C9'-H9'A 0.9800 C9-H9B 0.9800 C9'-H9'A 0.9800 C10-C15 1.3912 (17) C10'-C15' 1.3911 (17) C11-C12 1.3875 (17) C11'-C12' 1.386 (17) C10-C11 1.3926 (17) C10'-C15' 1.3816 (19) C12-C13 1.384 (2) <td>N1—C1</td> <td>1.1450 (17)</td> <td>N1′—C1′</td> <td>1.1469 (18)</td>	N1—C1	1.1450 (17)	N1′—C1′	1.1469 (18)
N3-C81.1443 (16)N3'-C8'1.1448 (16)C1-C21.4280 (18)C1'-C2'1.4239 (18)C2-C61.3642 (16)C2'-C6'1.3647 (15)C2-C31.4295 (16)C2'-C3'1.4351 (17)C4-C71.3432 (17)C4'-C7'1.3432 (16)C4-C91.4772 (16)C4'-C9'1.4779 (15)C4-C51.5197 (16)C5'-C16'1.518 (16)C5-C161.5197 (16)C5'-C16'1.518 (16)C5-C101.5202 (16)C5'-C16'1.5233 (15)C6-C71.4580 (15)C6'-C7'1.4547 (15)C7-C81.4277 (17)C7'-C8'1.4273 (17)C9-H9A0.9800C9'-H9'A0.9800C9-H9B0.9800C9'-H9'A0.9800C9-H9C0.9800C9'-H9'C0.9800C9-H9C0.9800C9'-H9'C0.9800C10-C151.3912 (17)C10'-C15'1.3917 (17)C11-C121.3875 (17)C11'-C12'1.3907 (17)C11-C121.3875 (17)C11'-C12'1.3907 (17)C11-H110.9500C12'-C13'1.3816 (19)C12-C131.384 (2)C12'-C13'1.3816 (19)C12-C131.384 (2)C12'-C13'1.3816 (19)C12-C141.380 (2)C13'-H14'0.9500C14-C151.3879 (17)C14'-C15'1.3872 (18)C14-C151.3879 (17)C14'-C15'1.3812 (18)C14-C151.3898 (17)C16'-C21'1.3919 (16)C15-H150.9500C13'-H14'0.9500 <td>N2—C3</td> <td>1.1437 (16)</td> <td>N2′—C3′</td> <td>1.1417 (17)</td>	N2—C3	1.1437 (16)	N2′—C3′	1.1417 (17)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	N3—C8	1.1443 (16)	N3′—C8′	1.1448 (16)
C2-C61.3642 (16) $C2'-C6'$ 1.3647 (15) $C2-C3$ 1.4295 (16) $C2'-C3'$ 1.4351 (17) $C4-C7$ 1.3432 (17) $C4'-C7'$ 1.3432 (16) $C4-C9$ 1.4772 (16) $C4'-C7'$ 1.3432 (16) $C4-C5$ 1.5107 (16) $C4'-C5'$ 1.5118 (16) $C5-C16$ 1.5197 (16) $C5'-C16'$ 1.5180 (16) $C5-C10$ 1.5202 (16) $C5'-C10'$ 1.5243 (15) $C6-C7$ 1.4580 (15) $C6'-C7'$ 1.4547 (15) $C7-C8$ 1.4277 (17) $C7'-C8'$ 1.4273 (17) $C9-H9A$ 0.9800 $C9'-H9'A$ 0.9800 $C9-H9B$ 0.9800 $C9'-H9'C$ 0.9800 $C9-H9B$ 0.9800 $C9'-H9'C$ 0.9800 $C9-H9B$ 0.9800 $C9'-H9'C$ 0.9800 $C10-C15$ 1.3912 (17) $C10'-C15'$ 1.3911 (17) $C11-C12$ 1.3875 (17) $C11'-C12'$ 1.3907 (17) $C11-C12$ 1.3875 (17) $C11'-C12'$ 1.3907 (17) $C12-C13$ 1.384 (2) $C12'-C13'$ 1.3816 (19) $C12-C14$ 1.380 (2) $C13'-C14'$ 1.380 (2) $C13-C14$ 1.380 (2) $C13'-C14'$ 1.380 (2) $C13-C14$ 1.380 (2) $C13'-C14'$ 1.380 (2) $C13-C14$ 1.389 (17) $C14'-C15'$ 1.3872 (18) $C14-C15$ 1.3879 (17) $C14'-C15'$ 1.3872 (18) $C14-C15$ 1.3894 (18) $C17'-C18'$ 1.3861 (18) $C1-C11$ 1.3894 (18) $C17'-C18'$ 1.3851 (19) $C14-C14$ 1.3800 $C16$	C1—C2	1.4280 (18)	C1′—C2′	1.4239 (18)
C2-C3 $1.4295 (16)$ $C2'-C3'$ $1.4351 (17)$ $C4-C7$ $1.3432 (17)$ $C4'-C7'$ $1.3432 (16)$ $C4-C9$ $1.4772 (16)$ $C4'-C9'$ $1.4779 (15)$ $C4-C5$ $1.5107 (16)$ $C4'-C9'$ $1.5118 (16)$ $C5-C16$ $1.5197 (16)$ $C5'-C16'$ $1.5180 (16)$ $C5-C16$ $1.5202 (16)$ $C5'-C10'$ $1.5243 (15)$ $C6-C7$ $1.4580 (15)$ $C6'-C7'$ $1.4547 (15)$ $C7-C8$ $1.4277 (17)$ $C7-C8'$ $1.4273 (17)$ $C9-H9A$ 0.9800 $C9'-H9'A$ 0.9800 $C9-H9B$ 0.9800 $C9'-H9'B$ 0.9800 $C9-H9C$ 0.9800 $C9'-H9'B$ 0.9800 $C10-C15$ $1.3912 (17)$ $C10'-C15'$ $1.3911 (17)$ $C10-C11$ $1.3926 (17)$ $C10'-C15'$ $1.3911 (17)$ $C11-C12$ $1.3875 (17)$ $C11'-C12'$ $1.3907 (17)$ $C12-C13$ $1.384 (2)$ $C12'-C13'$ $1.3816 (19)$ $C12-C13$ $1.384 (2)$ $C12'-C13'$ $1.3816 (19)$ $C12-H12$ 0.9500 $C12'-H12'$ 0.9500 $C13-H13$ 0.9500 $C13'-H13'$ 0.9500 $C14-C15$ $1.3879 (17)$ $C14'-C15'$ $1.3872 (18)$ $C14-H14$ 0.9500 $C15'-H15'$ 0.9500 $C14-C14$ $1.380 (2)$ $C15'-H15'$ 0.9500 $C14-C15$ $1.3881 (16)$ $C17'-C18'$ $1.3861 (18)$ $C17-H17$ 0.9500 $C15'-H15'$ 0.9500 $C14-C18$ $1.3894 (18)$ $C17'-C18'$ <	C2—C6	1.3642 (16)	C2'—C6'	1.3647 (15)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C2—C3	1.4295 (16)	C2'—C3'	1.4351 (17)
C4-C9 $1.4772 (16)$ $C4'-C9'$ $1.4779 (15)$ C4-C5 $1.5107 (16)$ $C4'-C5'$ $1.5118 (16)$ C5-C16 $1.5197 (16)$ $C5'-C16'$ $1.518 (16)$ C5-C10 $1.5202 (16)$ $C5'-C10'$ $1.5243 (15)$ C6-C7 $1.4580 (15)$ $C6'-C7'$ $1.4547 (15)$ C7-C8 $1.4277 (17)$ $C7'-C8'$ $1.4273 (17)$ C9-H9A 0.9800 $C9'-H9'B$ 0.9800 C9-H9B 0.9800 $C9'-H9'C$ 0.9800 C9-H9C 0.9800 $C9'-H9'C$ 0.9800 C10-C15 $1.3912 (17)$ $C10'-C11'$ $1.3866 (17)$ C10-C11 $1.3926 (17)$ $C10'-C15'$ $1.3911 (17)$ C11-C12 $1.3875 (17)$ $C11'-C12'$ $1.3907 (17)$ C11-C12 $1.3875 (17)$ $C11'-C12'$ $1.3907 (17)$ C12-C13 $1.384 (2)$ $C12'-C13'$ $1.3816 (19)$ C12-C13 $1.384 (2)$ $C12'-C14'$ $1.380 (2)$ C13-C14 $1.380 (2)$ $C13'-C14'$ 0.9500 C14-C15 $1.3879 (17)$ $C14'-C15'$ $1.3872 (18)$ C14-C15 $1.3879 (17)$ $C14'-C15'$ $1.3872 (18)$ C14-C14 0.9500 $C14'-H14'$ 0.9500 C15-H15 0.9500 $C15'-H15'$ 0.9500 C16-C17 $1.3894 (18)$ $C17'-C18'$ $1.3861 (18)$ C17-H17 0.9500 $C16'-C1'$ $1.3892 (16)$ C16-C21 $1.3894 (18)$ $C17'-C18'$ $1.3821 (19)$ C18-H18 0.9500 $C18'-H18'$ 0.9500 <td< td=""><td>C4—C7</td><td>1.3432 (17)</td><td>C4′—C7′</td><td>1.3432 (16)</td></td<>	C4—C7	1.3432 (17)	C4′—C7′	1.3432 (16)
C4—C51.5107 (16)C4'—C5'1.5118 (16)C5—C161.5197 (16)C5'—C16'1.5180 (16)C5—C101.5202 (16)C5'—C10'1.5243 (15)C6—C71.4580 (15)C6'—C7'1.4547 (15)C7—C81.4277 (17)C7'—C8'1.4273 (17)C9—H9A0.9800C9'—H9'A0.9800C9—H9B0.9800C9'—H9'B0.9800C9—H9C0.9800C9'—H9'C0.9800C10—C151.3912 (17)C10'—C15'1.3911 (17)C11—C121.3875 (17)C11'—C12'1.3966 (17)C11—C121.3875 (17)C11'—C12'1.3907 (17)C11—H110.9500C12'—C13'1.3816 (19)C12—H120.9500C12'—C13'1.3816 (19)C13—C141.380 (2)C12'—C14'1.380 (2)C13—C141.380 (2)C13'—C14'1.380 (2)C13—H130.9500C13'—H13'0.9500C14—H140.9500C14'—H14'0.9500C14—H140.9500C14'—H14'0.9500C14—C151.381 (16)C16'—C17'1.3812 (18)C14—H140.9500C14'—H14'0.9500C16—C211.3898 (17)C16'—C21'1.3837 (19)C16—C211.3894 (18)C17'—C18'1.3837 (19)C18—C191.383 (2)C18'—C19'1.3837 (19)C18—C191.382 (18)C17'—H17'0.9500C19—H190.9500C19'—H18'0.9500C19—H190.9500C19'—H18'0.9500C19—H19 <td>C4—C9</td> <td>1.4772 (16)</td> <td>C4′—C9′</td> <td>1.4779 (15)</td>	C4—C9	1.4772 (16)	C4′—C9′	1.4779 (15)
C5-C161.5197 (16)C5'-C16'1.5180 (16)C5-C101.5202 (16)C5'-C10'1.5243 (15)C6-C71.4580 (15)C6'-C7'1.4547 (15)C7-C81.4277 (17)C7'-C8'1.4273 (17)C9-H9A0.9800C9'-H9'A0.9800C9-H9B0.9800C9'-H9'C0.9800C9-H9C0.9800C9'-H9'C0.9800C10-C151.3912 (17)C10'-C11'1.3866 (17)C11-C121.3926 (17)C10'-C15'1.3911 (17)C11-C121.3875 (17)C11'-C12'1.3907 (17)C11-H110.9500C12'-H12'0.9500C12-C131.384 (2)C12'-C13'1.3816 (19)C12-H120.9500C12'-H12'0.9500C13-C141.380 (2)C13'-C14'1.380 (2)C13-H130.9500C14'-H14'0.9500C14-C151.3879 (17)C14'-C15'1.3872 (18)C14-H140.9500C15'-H15'0.9500C15-H150.9500C15'-H15'0.9500C16-C211.3881 (16)C16'-C21'1.3919 (16)C16-C211.3894 (18)C17'-C18'1.3861 (18)C17-C181.3832 (2)C18'-C19'1.3837 (19)C18-C191.383 (2)C18'-C19'1.3837 (19)C18-H180.9500C18'-H18'0.9500C19-C201.379 (2)C19'-C20'1.3822 (19)C19-H190.9500C18'-H18'0.9500C19-H190.9500C19'-H19'0.9500C20-H20 <td>C4—C5</td> <td>1.5107 (16)</td> <td>C4′—C5′</td> <td>1.5118 (16)</td>	C4—C5	1.5107 (16)	C4′—C5′	1.5118 (16)
C5-C101.5202 (16)C5'-C10'1.5243 (15)C6-C71.4580 (15)C6'-C7'1.4547 (15)C7-C81.4277 (17)C7'-C8'1.4273 (17)C9-H9A0.9800C9'-H9'A0.9800C9-H9B0.9800C9'-H9'C0.9800C9-H9C0.9800C9'-H9'C0.9800C10-C151.3912 (17)C10'-C11'1.3866 (17)C10-C111.3926 (17)C10'-C15'1.3911 (17)C11-C121.3875 (17)C11'-C12'1.3907 (17)C11-C121.3875 (17)C11'-C12'0.9500C12-C131.384 (2)C12'-C13'1.3816 (19)C12-C131.384 (2)C12'-H12'0.9500C13-C141.380 (2)C13'-C14'1.380 (2)C13-C141.380 (2)C13'-C14'1.380 (2)C14-H130.9500C14'-H14'0.9500C15-H150.9500C15'-H15'0.9500C15-H150.9500C15'-H15'0.9500C16-C171.3881 (16)C16'-C17'1.3919 (16)C16-C211.3898 (17)C16'-C21'1.3851 (18)C17-C181.3894 (18)C17'-C18'1.3861 (18)C17-H170.9500C18'-H18'0.9500C18-C191.383 (2)C18'-C19'1.3837 (19)C18-H180.9500C18'-H18'0.9500C19-C201.379 (2)C19'-C20'1.3822 (19)C19-H190.9500C19'-H19'0.9500C19-C201.3826 (18)C20'-C21'1.3822 (19)C20	C5—C16	1.5197 (16)	C5'—C16'	1.5180 (16)
C6-C71.4580 (15)C6'-C7'1.4547 (15)C7-C81.4277 (17)C7'-C8'1.4273 (17)C9-H9A0.9800C9'-H9'A0.9800C9-H9B0.9800C9'-H9'C0.9800C9-H9C0.9800C9'-H9'C0.9800C10-C151.3912 (17)C10'-C11'1.3866 (17)C10-C111.3926 (17)C10'-C15'1.3911 (17)C11-C121.3875 (17)C11'-C12'1.3907 (17)C11-H110.9500C11'-H11'0.9500C12-C131.384 (2)C12'-C13'1.3816 (19)C12-H120.9500C13'-H13'0.9500C13-C141.380 (2)C13'-C14'1.380 (2)C13-H130.9500C13'-H13'0.9500C14-C151.3879 (17)C14'-C15'1.3872 (18)C14-H140.9500C15'-H15'0.9500C15-H150.9500C15'-H15'0.9500C16-C171.3881 (16)C16'-C17'1.3919 (16)C16-C211.3894 (18)C17'-C18'1.3851 (18)C17-C181.3894 (18)C17'-C18'1.3813 (18)C17-H170.9500C18'-H18'0.9500C18-C191.383 (2)C18'-C19'1.3837 (19)C18-C191.383 (2)C18'-C19'1.3822 (19)C18-H180.9500C19'-H19'0.9500C19-C201.379 (2)C19'-C20'1.3822 (19)C19-H190.9500C19'-H19'0.9500C20-C211.3826 (18)C20'-C21'1.3792 (18)C20-H20	C5—C10	1.5202 (16)	C5'—C10'	1.5243 (15)
C7-C8 $1.4277(17)$ $C7'-C8'$ $1.4273(17)$ $C9-H9A$ 0.9800 $C9'-H9'A$ 0.9800 $C9-H9B$ 0.9800 $C9'-H9'B$ 0.9800 $C9-H9C$ 0.9800 $C9'-H9'C$ 0.9800 $C10-C15$ $1.3912(17)$ $C10'-C11'$ $1.3866(17)$ $C10-C11$ $1.3926(17)$ $C10'-C15'$ $1.3911(17)$ $C11-C12$ $1.3875(17)$ $C11'-C12'$ $1.3907(17)$ $C11-H11$ 0.9500 $C11'-H11'$ 0.9500 $C12-C13$ $1.384(2)$ $C12'-C13'$ $1.3816(19)$ $C12-H12$ 0.9500 $C13'-H12'$ 0.9500 $C13-C14$ $1.380(2)$ $C13'-C14'$ $1.380(2)$ $C14-C15$ $1.3879(17)$ $C14'-C15'$ $1.3872(18)$ $C14-C15$ $1.3879(17)$ $C14'-C15'$ $1.3872(18)$ $C14-H14$ 0.9500 $C15'-H15'$ 0.9500 $C15-H15$ 0.9500 $C15'-H15'$ 0.9500 $C16-C21$ $1.3898(17)$ $C16'-C21'$ $1.3919(16)$ $C16-C21$ $1.3898(17)$ $C16'-C18'$ $1.3837(19)$ $C18-C19$ $1.383(2)$ $C18'-C19'$ $1.3837(19)$ $C18-C19$ $1.383(2)$ $C18'-C19'$ $1.3837(19)$ $C18-C19$ $1.383(2)$ $C18'-C19'$ $1.3822(19)$ $C19-C20$ $1.379(2)$ $C19'-C20'$ $1.3822(19)$ $C19-L10$ 0.9500 $C12'-H19'$ 0.9500 $C20-C21$ $1.3826(18)$ $C20'-C21'$ $1.3792(18)$ $C20-L21$ 0.9500 $C21'-H21'$ 0.9500 </td <td>C6—C7</td> <td>1.4580 (15)</td> <td>C6'—C7'</td> <td>1.4547 (15)</td>	C6—C7	1.4580 (15)	C6'—C7'	1.4547 (15)
C9—H9A0.9800C9'—H9'A0.9800C9—H9B0.9800C9'—H9'B0.9800C9—H9C0.9800C9'—H9'C0.9800C10—C151.3912 (17)C10'—C1'1.3866 (17)C10—C111.3926 (17)C10'—C1'1.3911 (17)C11—C121.3875 (17)C11'—C12'1.3907 (17)C11—H110.9500C11'—H11'0.9500C12—C131.384 (2)C12'—C13'1.3816 (19)C12—H120.9500C12'—H12'0.9500C13—C141.380 (2)C13'—C14'1.380 (2)C13—H130.9500C13'—H13'0.9500C14—C151.3879 (17)C14'—C15'1.3872 (18)C14—H140.9500C15'—H15'0.9500C15—H150.9500C15'—H15'0.9500C16—C171.3881 (16)C16'—C17'1.3919 (16)C16—C211.3898 (17)C16'—C17'1.3919 (16)C16—C211.3894 (18)C17'—C18'1.3861 (18)C17—H170.9500C17'—H17'0.9500C18—C191.383 (2)C18'—C19'1.3837 (19)C18—H180.9500C18'—H18'0.9500C18—H180.9500C18'—H18'0.9500C19—H190.9500C19'—H19'0.9500C19—H190.9500C19'—H19'0.9500C19—H190.9500C19'—H19'0.9500C19—H190.9500C19'—H19'0.9500C19—H190.9500C20'—C21'1.3792 (18)C20—C211.3826 (18)C20'—C	C7—C8	1.4277 (17)	C7′—C8′	1.4273 (17)
C9—H9B0.9800C9'—H9'B0.9800C9—H9C0.9800C9'—H9'C0.9800C10—C151.3912 (17)C10'—C11'1.3866 (17)C10—C111.3926 (17)C10'—C15'1.3911 (17)C11—C121.3875 (17)C11'—C12'1.3907 (17)C11—H110.9500C11'—H11'0.9500C12—C131.384 (2)C12'—C13'1.3816 (19)C12—H120.9500C12'—H12'0.9500C13—C141.380 (2)C13'—C14'1.380 (2)C14—C151.3879 (17)C14'—C15'1.3872 (18)C14—C151.3879 (17)C14'—C15'1.3872 (18)C14—H140.9500C15'—H15'0.9500C15—H150.9500C15'—H15'0.9500C16—C171.3881 (16)C16'—C17'1.3919 (16)C16—C211.3898 (17)C16'—C17'1.3919 (16)C17—C181.3894 (18)C17'—C18'1.3861 (18)C17—H170.9500C17'—H17'0.9500C18—C191.383 (2)C18'—C19'1.3837 (19)C18—H180.9500C19'—H18'0.9500C19—H190.9500C19'—H19'0.9500C19—C201.379 (2)C19'—C20'1.3792 (18)C20—C211.3826 (18)C20'—C21'1.3792 (18)C20—H200.9500C21'—H21'0.9500C21—H210.9500C21'—H21'0.9500	С9—Н9А	0.9800	С9′—Н9′А	0.9800
C9-H9C 0.9800 C9'-H9'C 0.9800 C10-C15 $1.3912 (17)$ $C10'-C11'$ $1.3866 (17)$ C10-C11 $1.3926 (17)$ $C10'-C15'$ $1.3911 (17)$ C11-C12 $1.3875 (17)$ $C11'-C12'$ $1.3907 (17)$ C11-H11 0.9500 $C11'-H11'$ 0.9500 C12-C13 $1.384 (2)$ $C12'-C13'$ $1.3816 (19)$ C12-H12 0.9500 $C12'-H12'$ 0.9500 C13-C14 $1.380 (2)$ $C13'-C14'$ $1.380 (2)$ C14-H13 0.9500 $C13'-H13'$ 0.9500 C14-C15 $1.3879 (17)$ $C14'-C15'$ $1.3872 (18)$ C14-H14 0.9500 $C15'-H15'$ 0.9500 C15-H15 0.9500 $C15'-H15'$ 0.9500 C16-C17 $1.3881 (16)$ $C16'-C17'$ $1.3919 (16)$ C16-C21 $1.3898 (17)$ $C16'-C21'$ $1.3861 (18)$ C17-C18 $1.3894 (18)$ $C17'-C18'$ $1.3861 (18)$ C17-H17 0.9500 $C18'-H18'$ 0.9500 C18-C19 $1.383 (2)$ $C18'-C19'$ $1.3822 (19)$ C19-C20 $1.379 (2)$ $C19'-C20'$ $1.3822 (19)$ C19-C21 $1.3826 (18)$ $C20'-C21'$ $1.3792 (18)$ C20-H20 0.9500 $C21'-H21'$ 0.9500 C21-H21 0.9500 $C21'-H21'$ 0.9500	С9—Н9В	0.9800	С9′—Н9′В	0.9800
C10—C15 $1.3912 (17)$ C10'—C11' $1.3866 (17)$ C10—C11 $1.3926 (17)$ C10'—C15' $1.3911 (17)$ C11—C12 $1.3875 (17)$ C11'—C12' $1.3907 (17)$ C11—H11 0.9500 C11'—H11' 0.9500 C12—C13 $1.384 (2)$ C12'—C13' $1.3816 (19)$ C12—C13 $1.384 (2)$ C12'—H12' 0.9500 C13—C14 $1.380 (2)$ C13'—C14' $1.380 (2)$ C13—C14 $1.380 (2)$ C13'—H13' 0.9500 C14—C15 $1.3879 (17)$ C14'—C15' $1.3872 (18)$ C14—H14 0.9500 C14'—H14' 0.9500 C15—H15 0.9500 C15'—H15' 0.9500 C16—C17 $1.3881 (16)$ C16'—C17' $1.3919 (16)$ C16—C21 $1.3894 (18)$ C17'—C18' $1.3861 (18)$ C17—C18 $1.384 (2)$ C18'—C19' $1.3837 (19)$ C18—C19 $1.383 (2)$ C18'—C19' $1.3837 (19)$ C18—H18 0.9500 C18'—H18' 0.9500 C19—C20 $1.379 (2)$ C19'—C20' $1.3822 (19)$ C19—H19 0.9500 C19'—H19' 0.9500 C20—C21 $1.3826 (18)$ C20'—C21' $1.3792 (18)$ C20—H20 0.9500 C21'—H21' 0.9500	С9—Н9С	0.9800	С9′—Н9′С	0.9800
C10C11 $1.3926 (17)$ C10'C15' $1.3911 (17)$ C11C12 $1.3875 (17)$ C11'C12' $1.3907 (17)$ C11H11 0.9500 C11'H11' 0.9500 C12C13 $1.384 (2)$ C12'C13' $1.3816 (19)$ C12H12 0.9500 C12'H12' 0.9500 C13C14 $1.380 (2)$ C13'C14' $1.380 (2)$ C13H13 0.9500 C13'H13' 0.9500 C14C15 $1.3879 (17)$ C14'C15' $1.3872 (18)$ C14H14 0.9500 C14'H14' 0.9500 C15H15 0.9500 C15'H15' 0.9500 C16C17 $1.3881 (16)$ C16'C17' $1.3919 (16)$ C16C21 $1.3898 (17)$ C16'C21' $1.3861 (18)$ C17C18 $1.3894 (18)$ C17'C18' $1.3861 (18)$ C17H17 0.9500 C18'H18' 0.9500 C18C19 $1.383 (2)$ C18'H18' 0.9500 C18C19 $1.383 (2)$ C18'H18' 0.9500 C18H18 0.9500 C19'C20' $1.3822 (19)$ C19H19 0.9500 C19'C20' $1.3822 (19)$ C19H19 0.9500 C19'H19' 0.9500 C20C21 $1.3826 (18)$ C20'C21' $1.3792 (18)$ C20H20 0.9500 C20'-H20' 0.9500 C21H21 0.9500 C21'-H21' 0.9500	C10—C15	1.3912 (17)	C10'—C11'	1.3866 (17)
C11C121.3875 (17)C11'C12'1.3907 (17)C11H110.9500C11'-H11'0.9500C12C131.384 (2)C12'C13'1.3816 (19)C12H120.9500C12'H12'0.9500C13C141.380 (2)C13'C14'1.380 (2)C13H130.9500C13'H13'0.9500C14C151.3879 (17)C14'C15'1.3872 (18)C14H140.9500C14'H14'0.9500C15H150.9500C15'H15'0.9500C16C171.3881 (16)C16'C17'1.3919 (16)C16C211.3898 (17)C16'C21'1.3952 (16)C17C181.3894 (18)C17'C18'1.3861 (18)C17H170.9500C18'H17'0.9500C18C191.383 (2)C18'C19'1.3837 (19)C18H180.9500C18'H18'0.9500C19C201.379 (2)C19'C20'1.3822 (19)C19H190.9500C19'H19'0.9500C20C211.3826 (18)C20'-C21'1.3792 (18)C20H200.9500C21'H21'0.9500	C10-C11	1.3926 (17)	C10'—C15'	1.3911 (17)
C11H110.9500C11'H11'0.9500C12C131.384 (2)C12'C13'1.3816 (19)C12H120.9500C12'H12'0.9500C13C141.380 (2)C13'C14'1.380 (2)C13H130.9500C13'H13'0.9500C14C151.3879 (17)C14'C15'1.3872 (18)C14H140.9500C14'H14'0.9500C15H150.9500C15'H15'0.9500C16C171.3881 (16)C16'C17'1.3919 (16)C16C211.3898 (17)C16'C21'1.3952 (16)C17C181.3894 (18)C17'C18'1.3861 (18)C17H170.9500C18'C19'1.3837 (19)C18C191.383 (2)C18'C19'1.3837 (19)C18H180.9500C18'H18'0.9500C19C201.379 (2)C19'C20'1.3822 (19)C19H190.9500C19'H19'0.9500C20C211.3826 (18)C20'C21'1.3792 (18)C20H200.9500C20'-H20'0.9500C21H210.9500C21'-H21'0.9500	C11—C12	1.3875 (17)	C11'—C12'	1.3907 (17)
C12—C13 $1.384 (2)$ $C12'-C13'$ $1.3816 (19)$ C12—H12 0.9500 $C12'-H12'$ 0.9500 C13—C14 $1.380 (2)$ $C13'-C14'$ $1.380 (2)$ C13—H13 0.9500 $C13'-H13'$ 0.9500 C14—C15 $1.3879 (17)$ $C14'-C15'$ $1.3872 (18)$ C14—H14 0.9500 $C14'-H14'$ 0.9500 C15—H15 0.9500 $C15'-H15'$ 0.9500 C16—C17 $1.3881 (16)$ $C16'-C17'$ $1.3919 (16)$ C16—C21 $1.3898 (17)$ $C16'-C21'$ $1.3952 (16)$ C17—C18 $1.3894 (18)$ $C17'-C18'$ $1.3861 (18)$ C17—H17 0.9500 $C18'-H17'$ 0.9500 C18—C19 $1.383 (2)$ $C18'-C19'$ $1.3837 (19)$ C18—H18 0.9500 $C19'-C20'$ $1.3822 (19)$ C19—C20 $1.379 (2)$ $C19'-C20'$ $1.3822 (19)$ C19—H19 0.9500 $C19'-H19'$ 0.9500 C20—C21 $1.3826 (18)$ $C20'-C21'$ $1.3792 (18)$ C20—H20 0.9500 $C21'-H21'$ 0.9500	C11—H11	0.9500	C11'—H11'	0.9500
C12—H12 0.9500 $C12'$ —H12' 0.9500 C13—C14 1.380 (2) $C13'$ —C14' 1.380 (2)C13—H13 0.9500 $C13'$ —H13' 0.9500 C14—C15 1.3879 (17) $C14'$ —C15' 1.3872 (18)C14—H14 0.9500 $C14'$ —H14' 0.9500 C15—H15 0.9500 $C15'$ —H15' 0.9500 C16—C17 1.3881 (16) $C16'$ —C17' 1.3919 (16)C16—C21 1.3898 (17) $C16'$ —C21' 1.3952 (16)C17—C18 1.3894 (18) $C17'$ —C18' 1.3861 (18)C17—H17 0.9500 $C18'$ —C19' 1.3837 (19)C18—C19 1.383 (2) $C18'$ —C19' 1.3837 (19)C18—H18 0.9500 $C18'$ —H18' 0.9500 C19—C20 1.379 (2) $C19'$ —C20' 1.3822 (19)C19—H19 0.9500 $C19'$ —H19' 0.9500 C20—C21 1.3826 (18) $C20'$ —C21' 1.3792 (18)C20—H20 0.9500 $C21'$ —H21' 0.9500	C12—C13	1.384 (2)	C12'—C13'	1.3816 (19)
C13—C14 $1.380 (2)$ C13'—C14' $1.380 (2)$ C13—H130.9500C13'—H13'0.9500C14—C15 $1.3879 (17)$ C14'—C15' $1.3872 (18)$ C14—H140.9500C14'—H14'0.9500C15—H150.9500C15'—H15'0.9500C16—C17 $1.3881 (16)$ C16'—C17' $1.3919 (16)$ C16—C21 $1.3898 (17)$ C16'—C21' $1.3952 (16)$ C17—C18 $1.3894 (18)$ C17'—C18' $1.3861 (18)$ C17—H170.9500C18"—C19' $1.3837 (19)$ C18—C19 $1.383 (2)$ C18'—C19' $1.3822 (19)$ C19—C20 $1.379 (2)$ C19'—C20' $1.3822 (19)$ C19—H190.9500C19'—H19'0.9500C20—C21 $1.3826 (18)$ C20'—C21' $1.3792 (18)$ C20—H200.9500C20'—H20'0.9500C21—H210.9500C21'—H21'0.9500	C12—H12	0.9500	C12'—H12'	0.9500
C13—H13 0.9500 $C13'$ —H13' 0.9500 C14—C15 $1.3879 (17)$ $C14'$ —C15' $1.3872 (18)$ C14—H14 0.9500 $C14'$ —H14' 0.9500 C15—H15 0.9500 $C15'$ —H15' 0.9500 C16—C17 $1.3881 (16)$ $C16'$ —C17' $1.3919 (16)$ C16—C21 $1.3898 (17)$ $C16'$ —C21' $1.3952 (16)$ C17—C18 $1.3894 (18)$ $C17'$ —C18' $1.3861 (18)$ C17—H17 0.9500 $C18'$ —C19' $1.3837 (19)$ C18—C19 $1.383 (2)$ $C18'$ —C19' $1.3837 (19)$ C18—H18 0.9500 $C18'$ —H18' 0.9500 C19—C20 $1.379 (2)$ $C19'$ —C20' $1.3822 (19)$ C19—H19 0.9500 $C19'$ —H19' 0.9500 C20—C21 $1.3826 (18)$ $C20'$ —C21' $1.3792 (18)$ C20—H20 0.9500 $C21'$ —H21' 0.9500	C13—C14	1.380 (2)	C13'—C14'	1.380 (2)
C14-C15 $1.3879 (17)$ $C14'-C15'$ $1.3872 (18)$ $C14-H14$ 0.9500 $C14'-H14'$ 0.9500 $C15-H15$ 0.9500 $C15'-H15'$ 0.9500 $C16-C17$ $1.3881 (16)$ $C16'-C17'$ $1.3919 (16)$ $C16-C21$ $1.3898 (17)$ $C16'-C21'$ $1.3952 (16)$ $C17-C18$ $1.3894 (18)$ $C17'-C18'$ $1.3861 (18)$ $C17-H17$ 0.9500 $C17'-H17'$ 0.9500 $C18-C19$ $1.383 (2)$ $C18'-C19'$ $1.3837 (19)$ $C18-H18$ 0.9500 $C18'-H18'$ 0.9500 $C19-C20$ $1.379 (2)$ $C19'-C20'$ $1.3822 (19)$ $C19-H19$ 0.9500 $C19'-H19'$ 0.9500 $C20-C21$ $1.3826 (18)$ $C20'-C21'$ $1.3792 (18)$ $C20-H20$ 0.9500 $C20'-H20'$ 0.9500 $C21'-H21'$ 0.9500 $C21'-H21'$ 0.9500	C13—H13	0.9500	C13'—H13'	0.9500
C14—H14 0.9500 C14'—H14' 0.9500 C15—H15 0.9500 C15'—H15' 0.9500 C16—C17 1.3881 (16)C16'—C17' 1.3919 (16)C16—C21 1.3898 (17)C16'—C21' 1.3952 (16)C17—C18 1.3894 (18)C17'—C18' 1.3861 (18)C17—H17 0.9500 C17'—H17' 0.9500 C18—C19 1.383 (2)C18'—C19' 1.3837 (19)C18—H18 0.9500 C18'—H18' 0.9500 C19—C20 1.379 (2)C19'—C20' 1.3822 (19)C19—H19 0.9500 C19'—H19' 0.9500 C20—C21 1.3826 (18)C20'—C21' 1.3792 (18)C20—H20 0.9500 C21'—H21' 0.9500	C14—C15	1.3879 (17)	C14'—C15'	1.3872 (18)
C15—H15 0.9500 $C15'$ —H15' 0.9500 C16—C17 1.3881 (16) $C16'$ —C17' 1.3919 (16)C16—C21 1.3898 (17) $C16'$ —C21' 1.3952 (16)C17—C18 1.3894 (18) $C17'$ —C18' 1.3861 (18)C17—H17 0.9500 $C17'$ —H17' 0.9500 C18—C19 1.383 (2) $C18'$ —C19' 1.3837 (19)C18—H18 0.9500 $C18'$ —H18' 0.9500 C19—C20 1.379 (2) $C19'$ —C20' 1.3822 (19)C19—H19 0.9500 $C19'$ —H19' 0.9500 C20—C21 1.3826 (18) $C20'$ —C21' 1.3792 (18)C20—H20 0.9500 $C21'$ —H21' 0.9500	C14—H14	0.9500	C14'—H14'	0.9500
C16—C17 $1.381(16)$ C16'—C17' $1.3919(16)$ C16—C21 $1.3898(17)$ C16'—C21' $1.3952(16)$ C17—C18 $1.3894(18)$ C17'—C18' $1.3861(18)$ C17—H17 0.9500 C17'—H17' 0.9500 C18—C19 $1.383(2)$ C18'—C19' $1.3837(19)$ C18—H18 0.9500 C18'—H18' 0.9500 C19—C20 $1.379(2)$ C19'—C20' $1.3822(19)$ C19—H19 0.9500 C19'—H19' 0.9500 C20—C21 $1.3826(18)$ C20'—C21' $1.3792(18)$ C20—H20 0.9500 C21'—H21' 0.9500	C15—H15	0.9500	C15'—H15'	0.9500
C16—C21 $1.3898(17)$ C16'—C21' $1.3952(16)$ C17—C18 $1.3894(18)$ C17'—C18' $1.3861(18)$ C17—H17 0.9500 C17'—H17' 0.9500 C18—C19 $1.383(2)$ C18'—C19' $1.3837(19)$ C18—H18 0.9500 C18'—H18' 0.9500 C19—C20 $1.379(2)$ C19'—C20' $1.3822(19)$ C19—H19 0.9500 C19'—H19' 0.9500 C20—C21 $1.3826(18)$ C20'—C21' $1.3792(18)$ C20—H20 0.9500 C21'—H21' 0.9500	C16—C17	1.3881 (16)	C16'—C17'	1.3919 (16)
C17—C18 $1.3894 (18)$ C17'—C18' $1.3861 (18)$ C17—H17 0.9500 $C17'$ —H17' 0.9500 C18—C19 $1.383 (2)$ $C18'$ —C19' $1.3837 (19)$ C18—H18 0.9500 $C18'$ —H18' 0.9500 C19—C20 $1.379 (2)$ $C19'$ —C20' $1.3822 (19)$ C19—H19 0.9500 $C19'$ —H19' 0.9500 C20—C21 $1.3826 (18)$ $C20'$ —C21' $1.3792 (18)$ C20—H20 0.9500 $C21'$ —H20' 0.9500 C21—H21 0.9500 $C21'$ —H21' 0.9500	C16—C21	1.3898 (17)	C16'—C21'	1.3952 (16)
C17—H170.9500C17'—H17'0.9500C18—C191.383 (2)C18'—C19'1.3837 (19)C18—H180.9500C18'—H18'0.9500C19—C201.379 (2)C19'—C20'1.3822 (19)C19—H190.9500C19'—H19'0.9500C20—C211.3826 (18)C20'—C21'1.3792 (18)C20—H200.9500C21'—H20'0.9500C21—H210.9500C21'—H21'0.9500	C17—C18	1.3894 (18)	C17'—C18'	1.3861 (18)
C18—C191.383 (2)C18'—C19'1.3837 (19)C18—H180.9500C18'—H18'0.9500C19—C201.379 (2)C19'—C20'1.3822 (19)C19—H190.9500C19'—H19'0.9500C20—C211.3826 (18)C20'—C21'1.3792 (18)C20—H200.9500C20'—H20'0.9500C21—H210.9500C21'—H21'0.9500	C17—H17	0.9500	C17'—H17'	0.9500
C18—H180.9500C18'—H18'0.9500C19—C201.379 (2)C19'—C20'1.3822 (19)C19—H190.9500C19'—H19'0.9500C20—C211.3826 (18)C20'—C21'1.3792 (18)C20—H200.9500C20'—H20'0.9500C21—H210.9500C21'—H21'0.9500	C18—C19	1.383 (2)	C18′—C19′	1.3837 (19)
C19—C201.379 (2)C19'—C20'1.3822 (19)C19—H190.9500C19'—H19'0.9500C20—C211.3826 (18)C20'—C21'1.3792 (18)C20—H200.9500C20'—H20'0.9500C21—H210.9500C21'—H21'0.9500	C18—H18	0.9500	C18'—H18'	0.9500
C19—H190.9500C19'—H19'0.9500C20—C211.3826 (18)C20'—C21'1.3792 (18)C20—H200.9500C20'—H20'0.9500C21—H210.9500C21'—H21'0.9500	C19—C20	1.379 (2)	C19'—C20'	1.3822 (19)
C20—C211.3826 (18)C20'—C21'1.3792 (18)C20—H200.9500C20'—H20'0.9500C21—H210.9500C21'—H21'0.9500	С19—Н19	0.9500	C19'—H19'	0.9500
C20—H200.9500C20'—H20'0.9500C21—H210.9500C21'—H21'0.9500	C20—C21	1.3826 (18)	C20'—C21'	1.3792 (18)
C21—H21 0.9500 C21'—H21' 0.9500	С20—Н20	0.9500	C20'—H20'	0.9500
	C21—H21	0.9500	C21'—H21'	0.9500

C6—O1—C5	110.17 (8)	C6'—O1'—C5'	110.25 (8)
N1—C1—C2	179.94 (19)	N1′—C1′—C2′	179.47 (14)
C6—C2—C1	121.39 (11)	C6'—C2'—C1'	121.78 (11)
C6—C2—C3	120.28 (11)	C6'—C2'—C3'	120.02 (11)
C1—C2—C3	118.33 (11)	C1'—C2'—C3'	118.20 (10)
N2—C3—C2	178.90 (14)	N2′—C3′—C2′	178.76 (14)
C7—C4—C9	127.97 (11)	C7′—C4′—C9′	127.80 (11)
C7—C4—C5	109.10 (10)	C7'—C4'—C5'	109.09 (10)
C9—C4—C5	122.86 (11)	C9'—C4'—C5'	123.09 (10)
01	102.37 (9)	O1′—C5′—C4′	102.35 (9)
01-C5-C16	109.19 (9)	01'-C5'-C16'	109.11 (8)
C4-C5-C16	108.53 (9)	C4'—C5'—C16'	108.89 (9)
01 - C5 - C10	105 72 (8)	01'-05'-010'	106 34 (8)
C4-C5-C10	114 22 (10)	C4' - C5' - C10'	112.82 (9)
$C_{16} - C_{5} - C_{10}$	115.82(10)	$C_{16} - C_{5} - C_{10}$	112.02(9)
01 - C6 - C2	120.36(10)	01'-C6'-C2'	120.27(10)
01 - C6 - C7	109 26 (10)	01' - C6' - C7'	120.27(10) 109.49(9)
C_{2} C_{6} C_{7}	130.38(11)	C2' - C6' - C7'	130.22(11)
$C_{2} = C_{0} = C_{1}$	123 65 (11)	$C_{2}^{4} - C_{3}^{7} - C_{3}^{8}$	130.22(11) 124.09(11)
$C_{4} - C_{7} - C_{6}$	123.03(11) 109.02(10)	C4' - C7' - C6'	124.09(11) 108.81(10)
C^{*}	107.02(10) 127.34(11)	$C_{1}^{*} - C_{1}^{*} - C_{0}^{*}$	100.01(10) 127.10(10)
$N_3 C_8 C_7$	127.34(11) 175.48(14)	$N_{3'} = C_{3'} = C_{0}$	176 62 (13)
C_{4} C_{9} H0A	1/0.5	$A^{\prime} = C^{\prime} = C^{\prime}$	1/0.02 (13)
$C_4 = C_9 = H_9R$	109.5	C4' = C9' = H9'R	109.5
H_{0} C_{0} H_{0} H_{0}	109.5	H_{0}^{\prime} C_{0}^{\prime} H_{0}^{\prime} H_{0}^{\prime}	109.5
$C_{A} = C_{A} = H_{A}C_{A}$	109.5	$A = C_{3} = H_{3} B$	109.5
	109.5	H_{0}^{\prime} C_{0}^{\prime} H_{0}^{\prime} C_{0}^{\prime}	109.5
	109.5	H_{0}^{\prime} R_{-}^{\prime} C_{0}^{\prime} H_{0}^{\prime} C_{0}^{\prime}	109.5
$119D - C_{2} - 119C$	110.65 (11)	$113 \text{ B} - C_3 - 113 \text{ C}$	109.3 110.72(11)
C15 - C10 - C11	119.03(11) 120.27(11)	$C_{11} = C_{10} = C_{13}$	119.72(11)
$C_{13} = C_{10} = C_{5}$	120.37(11) 110.70(11)	C11 - C10 - C3	120.81(10)
C12 C11 C10	119.70 (11)	C13 - C10 - C3	119.32(11)
C12 - C11 - C10	119.95 (12)	$C10^{\circ}$ $-C11^{\circ}$ $-C12^{\circ}$	119.71 (12)
CI2—CII—HII	120.0		120.1
	120.0		120.1
C13 - C12 - C11	119.97 (12)		120.31 (12)
C13-C12-H12	120.0	C13 - C12 - H12	119.8
CII—CI2—HI2	120.0	$C11^{2}$ $-C12^{2}$ $-H12^{2}$	119.8
C14 - C13 - C12	120.39 (12)	C14' - C13' - C12'	120.11 (12)
C14—C13—H13	119.8	C14' - C13' - H13'	119.9
C12—C13—H13	119.8	C12'— $C13'$ — $H13'$	119.9
C13—C14—C15	119.99 (12)	C13' - C14' - C15'	119.93 (12)
C13—C14—H14	120.0	C13'—C14'—H14'	120.0
C15—C14—H14	120.0	C15'—C14'—H14'	120.0
C14—C15—C10	120.03 (12)	C14'-C15'-C10'	120.18 (12)
C14—C15—H15	120.0	C14'-C15'-H15'	119.9
C10—C15—H15	120.0	C10'—C15'—H15'	119.9
C17—C16—C21	119.62 (11)	C17'—C16'—C21'	119.14 (11)
C17—C16—C5	120.49 (11)	C17'—C16'—C5'	120.97 (10)

C21—C16—C5	119.64 (10)	C21'—C16'—C5'	119.62 (10)
C16—C17—C18	119.77 (12)	C18′—C17′—C16′	119.95 (11)
С16—С17—Н17	120.1	C18'—C17'—H17'	120.0
C18—C17—H17	120.1	C16'—C17'—H17'	120.0
C19—C18—C17	120.14 (12)	C19'—C18'—C17'	120.54 (11)
C19—C18—H18	119.9	C19'—C18'—H18'	119.7
C17—C18—H18	119.9	C17'—C18'—H18'	119.7
C20—C19—C18	120.17 (13)	C20'—C19'—C18'	119.58 (12)
С20—С19—Н19	119.9	С20'—С19'—Н19'	120.2
C18—C19—H19	119.9	C18'—C19'—H19'	120.2
C19—C20—C21	119.97 (13)	C21'—C20'—C19'	120.41 (12)
С19—С20—Н20	120.0	C21'—C20'—H20'	119.8
C21—C20—H20	120.0	C19'—C20'—H20'	119.8
C20—C21—C16	120.30 (12)	C20'—C21'—C16'	120.36 (11)
C20—C21—H21	119.9	C20'—C21'—H21'	119.8
C16—C21—H21	119.9	C16'—C21'—H21'	119.8
C6-01-C5-C4	2.74 (11)	C6'-01'-C5'-C4'	1.01 (11)
C6-01-C5-C16	117.63 (10)	C6'	116.26 (10)
C6-01-C5-C10	-117 13 (10)	C6' - 01' - C5' - C10'	-11754(10)
C7-C4-C5-O1	-1.50(12)	C7' - C4' - C5' - O1'	-0.64(12)
C9-C4-C5-O1	175 57 (10)	C9' - C4' - C5' - 01'	177.60(10)
C7-C4-C5-C16	-116.87(11)	C7'-C4'-C5'-C16'	-116.05(10)
$C_{1}^{0} = C_{1}^{0} = C_{1}^{0} = C_{1}^{0}$	60.21 (14)	$C_{1}^{0} = C_{1}^{0} = C_{1}^{0} = C_{1}^{0}$	62 10 (13)
$C_{7} = C_{4} = C_{5} = C_{10}$	112 25 (11)	$C_{3} = C_{4} = C_{3} = C_{10}$	113 21 (11)
$C^{0} = C^{4} = C^{5} = C^{10}$	-70.67(14)	$C_{1}^{0} = C_{1}^{0} = C_{1}^{0}$	-68.54(14)
$C_{5} = C_{4} = C_{5} = C_{10}$	177.72(10)	$C_{3} = C_{4} = C_{3} = C_{10}$	-170.82(14)
$C_{5} = 01 = C_{6} = C_{7}$	177.73(10)	$C_{3} = 0_{1} = 0_{0} = 0_{2}$	-1/9.83(10)
$C_{1} = C_{1} = C_{1} = C_{1}$	-2.93(12)	$C_{3} = 0_{1} = 0_{0} = 0_{1}$	-1.00(12)
$C_1 = C_2 = C_0 = O_1$	1/9.78(11)	C1 - C2 - C0 - 01	-1/9.38(11)
$C_3 = C_2 = C_0 = O_1$	-0.43(17)	$C_{3} = C_{2} = C_{6} = O_{1}$	0.38(17)
C1 = C2 = C6 = C7	0.6(2)	C1' - C2' - C6' - C7'	2.1 (2)
$C_3 = C_2 = C_6 = C_7$	-1/9.61(11)	$C_{3}^{\prime} = C_{2}^{\prime} = C_{6}^{\prime} = C_{7}^{\prime}$	-1/8.1/(12)
C9—C4—C7—C8	2.6 (2)	C9'	1.5 (2)
C5-C4-C7-C8	179.51 (11)	C5'—C4'—C'/'—C8'	179.64 (11)
C9—C4—C7—C6	-177.01 (11)	C9'—C4'—C7'—C6'	-178.04 (11)
C5—C4—C7—C6	-0.12 (13)	C5'—C4'—C7'—C6'	0.10 (13)
O1—C6—C7—C4	1.95 (13)	O1'—C6'—C7'—C4'	0.57 (13)
C2—C6—C7—C4	-178.82 (12)	C2'—C6'—C7'—C4'	179.24 (12)
O1—C6—C7—C8	-177.67 (11)	O1'C6'C7'C8'	-178.96 (11)
C2—C6—C7—C8	1.6 (2)	C2'—C6'—C7'—C8'	-0.3 (2)
O1—C5—C10—C15	90.54 (12)	O1'-C5'-C10'-C11'	-94.48 (12)
C4—C5—C10—C15	-21.21 (15)	C4'—C5'—C10'—C11'	154.11 (10)
C16—C5—C10—C15	-148.43 (10)	C16'—C5'—C10'—C11'	27.23 (14)
O1-C5-C10-C11	-83.48 (12)	O1'-C5'-C10'-C15'	81.20 (12)
C4—C5—C10—C11	164.77 (10)	C4'—C5'—C10'—C15'	-30.22 (14)
C16—C5—C10—C11	37.56 (14)	C16'—C5'—C10'—C15'	-157.09 (10)
C15—C10—C11—C12	0.68 (17)	C15'—C10'—C11'—C12'	1.69 (17)
C5-C10-C11-C12	174.74 (11)	C5'—C10'—C11'—C12'	177.34 (10)
C10-C11-C12-C13	-0.52 (18)	C10'—C11'—C12'—C13'	-1.61 (18)

C11—C12—C13—C14	-0.1(2)	C11'-C12'-C13'-C14'	0.16 (19)
C12—C13—C14—C15	0.6 (2)	C12'—C13'—C14'—C15'	1.22 (19)
C13—C14—C15—C10	-0.41 (19)	C13'—C14'—C15'—C10'	-1.13 (19)
C11—C10—C15—C14	-0.22 (17)	C11′—C10′—C15′—C14′	-0.33 (17)
C5-C10-C15-C14	-174.24 (11)	C5'—C10'—C15'—C14'	-176.05 (11)
O1-C5-C16-C17	-30.62 (13)	O1'—C5'—C16'—C17'	-21.91 (15)
C4—C5—C16—C17	80.23 (12)	C4'—C5'—C16'—C17'	89.06 (12)
C10-C5-C16-C17	-149.77 (10)	C10'—C5'—C16'—C17'	-142.14 (11)
O1-C5-C16-C21	155.10 (10)	O1'—C5'—C16'—C21'	164.16 (10)
C4—C5—C16—C21	-94.05 (12)	C4'—C5'—C16'—C21'	-84.88 (13)
C10-C5-C16-C21	35.95 (15)	C10'—C5'—C16'—C21'	43.92 (15)
C21—C16—C17—C18	-1.44 (17)	C21'—C16'—C17'—C18'	0.08 (18)
C5-C16-C17-C18	-175.72 (10)	C5'—C16'—C17'—C18'	-173.88 (11)
C16—C17—C18—C19	-0.09 (19)	C16'—C17'—C18'—C19'	-0.94 (19)
C17—C18—C19—C20	0.7 (2)	C17'—C18'—C19'—C20'	0.8 (2)
C18—C19—C20—C21	0.3 (2)	C18′—C19′—C20′—C21′	0.1 (2)
C19—C20—C21—C16	-1.8 (2)	C19′—C20′—C21′—C16′	-1.0 (2)
C17—C16—C21—C20	2.41 (18)	C17'—C16'—C21'—C20'	0.86 (19)
C5—C16—C21—C20	176.74 (11)	C5'—C16'—C21'—C20'	174.90 (12)

Hydrogen-bond geometry (Å, °)

Cg1 is the centroid of the C10–C15 phenyl ring

D—H···A	D—H	H···A	D···A	<i>D</i> —H··· <i>A</i>
C20'—H20'…Cg1 ⁱ	0.95	2.69	3.4041 (14)	133
C9—H9 <i>B</i> ···N3′	0.98	2.70	3.4560 (14)	134

Symmetry code: (i) -x+1, -y+1, -z.