

# *Article* **Mechanical and Electrical Characteristics of WB2 Synthesized at High Pressure and High Temperature**

### **Changchun Wang 1,\*, Lele Song <sup>2</sup> and Yupeng Xie <sup>1</sup>**

- <sup>1</sup> College of Science, Jilin Institute of Chemical Technology, Jilin 132022, China; xieyupeng1981@163.com
- 2 Institute of Atomic and Molecular Physics, Jilin University, Changchun 130012, China; songlele\_322@126.com
- **\*** Correspondence: wangcc@jlict.edu.cn; Tel.: +86-150-43216727

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Abstract: Single-phase tungsten diboride (WB<sub>2</sub>) was synthesized at high pressure and high temperature. The different grain sizes ranging from  $300 \text{ nm}$  to  $3 \mu \text{m}$  were successfully obtained in  $WB<sub>2</sub>$  by controlling the experimental conditions. The effects of grain size on hardness and resistivity properties were investigated. The Vickers hardness of WB<sub>2</sub> was modulated with grain size. The maximum asymptotic Vickers hardness is 25.5 GPa for WB<sup>2</sup> with a grain size of 300 nm which is a 10% increase compared to  $WB<sub>2</sub>$  with a grain size of 3  $\mu$ m. The optimal electrical resistivity of WB<sub>2</sub> was  $10^{-7}$   $\Omega$ m with the biggest grain size of 3 µm, which is ascribed to low grain boundary density. The superior properties of hardness and electrical resistivity demonstrate that  $WB<sub>2</sub>$  should be a new functional hard material replacing WC which is widely used in industrial production.

**Keywords:** hard material; electrical resistivity; tungsten diboride; Vickers hardness

#### **1. Introduction**

Recently, transition metal borides (TMBs) have been attracting considerable attention for their unique physicochemical properties, such as high melting point, hardness, electrical conductivity, wear resistance, thermal conductivity and chemical inertness, etc. [\[1–](#page-5-0)[4\]](#page-5-1). Due to their outstanding properties, TMB ceramics have been widely used in particular environments, such as abrasive, corrosion-resistant, conductive and electrode materials  $[5-8]$  $[5-8]$ . In TMBs, tungsten diboride (WB<sub>2</sub>) was predicted to have a very high hardness ranging from 36 to 40 GPa and good conductive properties by first-principle calculation [\[3](#page-5-2)[,9\]](#page-6-2). However, there is a paucity of reports about the hardness and conductive property of WB<sub>2</sub>. These reports about WB<sub>2</sub> are ascribed to the fact that bulk WB<sub>2</sub> is hard to synthesize at ambient temperature by traditional methods, such as self-propagating combustion synthesis [\[10\]](#page-6-3), chemical vapor deposition (CVD) [\[11\]](#page-6-4), and spark plasma sintering [\[7,](#page-6-5)[12\]](#page-6-6). Solid state WB<sub>2</sub> shows lower self-diffusion coefficients and so it is difficult to facilitate its densification in the process of sintering using powder as precursor. Even in high temperature sintering, WB<sub>2</sub> will not exhibit any shrinkage [\[13\]](#page-6-7). So, high quality bulk WB<sub>2</sub> samples cannot be synthesized by traditional methods so far. Therefore, an exploration of the mechanical properties of  $WB<sub>2</sub>$  has been hindered.

In this work, single-phase  $WB<sub>2</sub>$  was prepared under high pressure and high temperature. We measured its electrical resistivity and hardness. It is worth noting that we can modulate the hardness and electrical resistivity of WB<sub>2</sub> by controlling the experimental conditions. In addition, we also find that WB<sup>2</sup> shows excellent conductive properties. The high hardness and low electrical resistivity demonstrate that WB<sub>2</sub> can be used as conductor working under extreme conditions.

#### **2. Materials and Methods**

In this study, powdery tungsten (200 mesh, 99.95% in purity) and amorphous boron powder (500 mesh, 99.99% in purity) were used as the starting materials. Powder mixtures which contained



W:B atomic ratios of 1:2 and 1:2.2 were mixed in an agate mortar for 3.5 h. The mixed powders were then cold-pressed into cylindrical samples of 4 mm in diameter and 3 mm in height. Finally, the samples were prepared in a cubic anvil HPHT apparatus (SPD-6  $\times$  600, Xianyang, China) at a target temperature (in this study temperatures were 1600 ◦C, 1700 ◦C, 1800 ◦C and 1900 ◦C, respectively), and a pressure of 5.2 GPa for a holding time of 15 min. The detailed process is as follows: firstly, the samples were put into the HPHT apparatus and the pressure was then raised to 5.2 GPa; secondly, the samples were heated to the target temperature in 15 seconds and the samples were kept at the target pressure and target temperature for 15 min; finally, the samples were cooled naturally to room temperature and removed from the apparatus. The phase analyses of the as-synthesized samples were examined by an X-ray diffractometer (XRD) using Cu-Ka  $(I = 1.5404 \text{ Å})$  radiation in a Rigaku D/max-2500 X-ray diffractometer (Japan). The morphological properties of the samples were analyzed with a scanning electron microscope (JEOL JSM-6700F, Japan). The electrical resistivity of  $WB<sub>2</sub>$  was measured using a four-point probe system. The Vickers microhardness measurements were performed by a Micro-Hardness Tester (HV-1000ZDT), and the applied load P and Vickers hardness (H<sub>V</sub>) were determined using equation:

$$
H_V = 1854.4P/d^2,
$$
 (1)

Here, d is the mean of the two diagonals of the indent and the holding time under the peak load was 15 s. The drainage method was used to measure density. The density ρ was determined using equation:

$$
\rho = m/v \tag{2}
$$

Here, m is the mass of the sample and V is the volume of boiling water discharged from the sample.

#### **3. Results and Discussion**

In order to synthesize the stoichiometric phase in pure WB<sub>2</sub>, powder mixtures that contained W/B atomic ratios of  $1/2$  were used as a precursor. We found that single phase WB<sub>2</sub> without impurity is hard to synthesize. Figure [1a](#page-2-0) shows the XRD patterns of  $WB<sub>2</sub>$  samples synthesized at 5.2 GPa and temperatures of 1600 °C to 1900 °C for 15 min. We can detect that WB<sub>2</sub> space group: P6<sub>3</sub>/mmc; ICSD Number: 023716 is the major phase and coexists with WB space group: I41/amd; ICSD Number: 024281). The phenomenon that stoichiometric phase pure  $WB<sub>2</sub>$  cannot be synthesized by using a stoichiometric W/B atomic ratios precursor, often appears in TMBs synthesis, and may be caused by an inadequate proportion of B. In the process of mixing the precursor, boron powder was easily absorbed by mortar and spread in the air. The loss of boron samples led to the precursor exhibiting a nonstoichiometric ratio. In order to synthesize phase pure WB2, the proportion of B in the precursor should be increased. When we changed the atomic ratios of W/B to 1/2.2, phase pure  $WB<sub>2</sub>$  was synthesized easily. Figure [1b](#page-2-0) shows the XRD patterns of WB<sub>2</sub> samples synthesized using the mixed precursor with W/B atomic ratios of 1/2.2 at 5.2 GPa and temperatures of 1600 ◦C to 1900 ◦C for 15 min. All the materials were confirmed to be phase pure.

<span id="page-2-0"></span>

Figure 1. XRD patterns of the samples fabricated (a) W/B atomic ratios of 1/2 at 5.2 GPa and different temperatures (1600–1900 °C) for 15 min, (b)  $W/B$  atomic ratios of 1/2.2 at 5.2 GPa and different temperatures (1600–1900 °C) for 15 min. Solid rhombus represents tungsten diboride ( $WB<sub>2</sub>$ ). Hollow rhombus represents WB. rhombus represents WB. rhombus represents WB. temperatures (1600–1900–1901–15 min<sub>t</sub>) W/B atomic ratios of 1/2.2 at 5.1 GPa and different

The stoichiometry ratio of the compound was checked by EDS and the results are shown in The stoichiometry ratio of the compound was checked by EDS and the results are shown in Figure [2.](#page-2-1) The picture is one of the images we have taken. The atomic ratio of  $W/B$  shown in Figure 2 is the average value of ten measurements. In measurement, we chose different parts to measure. The molar ratio of W and B for the compound was approximately confirmed to be 1:2.0. So, single phase  $WB<sub>2</sub>$  without impurity cannot be synthesized with W/B atomic ratios of 1/2 because the proportion of B B is inadequate. is inadequate. B is inadequate.  $\mathbb{R}^n$  with  $\mathbb{R}^n$  at  $\mathbb{R}^n$  at  $\mathbb{R}^n$  atomic ratios of  $\mathbb{R}^n$  because the proportion of

<span id="page-2-1"></span>

**Figure 2.** EDS images of as-synthesized compound fabricated at 5.2 GPa and different temperatures Figure 2. EDS images of as-synthesized compound fabricated at 5.2 GPa and different temperatures (1600–1900 °C) for 15 min using W powder and B powder (with W/B atomic ratios of 1/2.2) as precursor.

The well-sintered bulk samples possessed high densification. We performed Vickers hardness The well-sintered bulk samples possessed high densification. We performed Vickers hardness (Hv) measurement after polishing. The measurement details are described in the experiment section. (Hv) measurement after polishing. The measurement details are described in the experiment section. The obtained hardness results are shown in Figure [3.](#page-3-0) The hardness decreased as the loading pressure The obtained hardness results are shown in Figure 3. The hardness decreased as the loading pressure increased. The load-dependent Vickers hardness data for WB<sub>2</sub> are shown in Figure [3.](#page-3-0) A maximum measured hardness of 43.875 GPa at 0.49 N was obtained and this value was higher than the threshold measured hardness of 43.875 GPa at 0.49 N was obtained and this value was higher than the threshold value of superhard material [\[14\]](#page-6-8). It is reported that hardness in the asymptotic-hardness region may value of superhard material [14]. It is reported that hardness in the asymptotic-hardness region may occur because it is closer to the intrinsic hardness [\[15](#page-6-9)[,16\]](#page-6-10). As shown in Figure [3,](#page-3-0) the asymptotic-hardness occur because it is closer to the intrinsic hardness [15,16]. As shown in Figure 3, the of WB<sub>2</sub> synthesized at temperatures of 1600 °C is about 25.5 GPa. This is higher than that of WC  $(22.0\ \text{GPa})$  [\[17\]](#page-6-11), which is most widely used as a hard material in industrial applications, under the same applied load. The high hardness of WB<sub>2</sub> suggests that WB<sub>2</sub> is a promising candidate for use as a hard material.

<span id="page-3-0"></span>

**Figure 3.** The asymptotic-hardness of WB<sup>2</sup> synthesized at temperatures of 1600 °C to 1900 °C with the **Figure 3.** The asymptotic-hardness of WB<sup>2</sup> synthesized at temperatures of 1600 ◦C to 1900 ◦C with the pressure at 5.2 GPa for 15 min. pressure at 5.2 GPa for 15 min.

It is worth noting that the maximum asymptotic Vickers hardness of WB<sub>2</sub> synthesized at 1600  $^{\circ}$ C increased by 10% compared to WB<sub>2</sub> synthesized at 1900 °C. It is known that increasing temperature could improve the densification of a sample, and the densification could affect the hardness. So, the could improve the densification of a sample, and the densification could affect the hardness. So, the hardness should increase with the synthesis temperature increasing at a certain pressure. However, hardness should increase with the synthesis temperature increasing at a certain pressure. However, in our result, the hardness of WB<sub>2</sub> synthesized at a low temperature was higher than that of WB<sub>2</sub> synthesized at a high temperature. In order to find why our conclusion was contrary to other findings, SEM tests were performed. SEM images of phase-pure WB<sub>2</sub> synthesized at different temperatures are shown in Figure 4. As is shown in the SEM images,  $WB<sub>2</sub>$  has different grain sizes in the range of 200 nm−3 µm. As temperature accelerates grain growth, it was found that the grain size increased as the temperature increased at a certain pressure. In the conventional synthesis method, temperature could improve the densification of sample ceramics. The denseness of a sample has an obvious effect on its hardness, and the hardness increases as the temperature increases. That is to say, the denseness of sample is the main factor in affecting hardness. In the HPHT method, the denseness of sample does not change obviously. So, the denseness of WB<sub>2</sub> is not the main factor in affecting hardness. It is reported that grain size can affect hardness. Smaller grains have more grain boundaries which can impede the propagation of stress during the hardness test. This increase in hardness with a decrease in crystal size is known as the Ha[ll-P](#page-6-12)[etc](#page-6-13)h effect  $[18,19]$ . In our study, the largest grain size was more than tenfold that of the smallest grain size. So, the grain size of WB<sub>2</sub> has an obvious effect on hardness. This requires more force to make the crystal slip, and so the smaller the grain size, the greater the yield limit of the material. However, in this work, the grain size was not at the nanoscale. So, WB<sub>2</sub> cannot have a rapid increase in hardness. It can be concluded from the above that the grain size had an obvious influence on the hardness of WB<sub>2</sub> synthesized in our experiment.

<span id="page-4-0"></span>

Figure 4. SEM results of as as-synthesized sample. (a), (b), (c) and (d) show the SEM results of WB<sub>2</sub> synthesized at 5.2 GPa for 15 min, with different temperatures of 1600 °C, 1700 °C, 1800 °C, 1900 $\degree$ C, respectively.

<span id="page-4-1"></span>In order to further confirm that the changes in the hardness of  $WB<sub>2</sub>$  were caused by grain size but not density, density measurements were performed on the as-synthesized samples. Density results are sho[wn](#page-4-1) in Figure 5. The density increased with the increase in the temperature in the entire temperature range. Considering that materials with a high density always show high hardness, the high hardness of WB<sub>2</sub> synthesized at low temperatures could be caused by small grain size.



Figure 5. Density of WB<sub>2</sub> samples versus temperature at pressures of 5.2 GPa for 15 min.

The Electrical resistivity of WB<sub>2</sub> synthesized at different temperatures was measured, and the rice Electrical resistivity of WEZ synthesized at different temperatures was inclusively and the results are shown in Figure [6.](#page-5-3) As the synthesized temperature increased, the electrical resistivity of WB<sub>2</sub> decreased from 9.164  $\times$  10<sup>-7</sup>  $\Omega$ m to 2.349  $\times$  10<sup>-7</sup>  $\Omega$ m. According to the electron scattering  $t_{\rm c}$  is supposed to electrical conductivity is supposed to be approximately proportional to the grain size  $[20]$ . theory, [the](#page-6-14) electrical conductivity is supposed to be approximately proportional to the grain size [20]. As the volume fraction of the interface in crystalline materials is roughly inversely proportional to the<br>service in the dense dense of mai deal maintimity or a majority can complete deviate of the interfacial fraction. In Figure 4, we show that the grain size increases with the temperature in the entire in the entire  $\frac{1}{2}$ volume fraction. In Figure 4, we s[how](#page-4-0) that the grain size increases with the temperature in the entire temperature range. This result can explain why the electrical resistivity decreased while the temperature in means of  $F_{\text{reflected}}$ grain size, the dependence of residual resistivity on grain size correlated with that of the interfacial temperature increased. temperature increased.

<span id="page-5-3"></span>

Figure 6. The variation of electrical resistivity with temperature for WB<sub>2</sub> synthesized at 5.2 GPa and temperatures of 1600℃ to 1900 °C for 15 min. temperatures of 1600 ◦C to 1900 ◦C for 15 min.

Furthermore, from the analysis of the density measurement results, we found that the density In this work, different which the interested temperature in the children temperature range. This is not been demonstrated, density can influence resistivity. So the electrical resistivity is not only determined by electron microscope and electron microscope and the density measurements, we have a matter of the matter of properties of a material are not only dependent on its high density, but also on a large grain size. increased concurrent with the increased temperature in the entire temperature range. As has been the single condition of grain size. It can be concluded from the above results that the high conductive

# Vickers hardness of WB<sup>2</sup> decreased as the grain size grew larger. The maximum asymptotic Vickers **4. Conclusions**

In this work, different grain size samples of  $WB$ <sub>2</sub> were synthesized through a high pressure and electron microscope and electrical resistivity measurements, we found that both density and grain size had a direct connection with electrical resistivity. The Vickers indentation test showed that the Vickers predict different preparation, S.L.; writing and editing, W.C.; writing and editing and editing the victorision, W.C.; projection, W.C.; projection, W.C.; projection, W.C.; projection, W.C.; projection, W.C.; projection, W hardness of WB<sub>2</sub> decreased as the grain size grew larger. The maximum asymptotic Vickers hardness is 25.5 GPa. Comparatively, WC has a hardness of 22.0 GPa, which is lower than that of WB<sub>2</sub>. Results **Funding:** This research was funded by Scientific Research Fund of Jilin Provincial Education Department, grant high temperature reaction sintering method. Through an analysis of density, the use of a scanning indicate that  $WB<sub>2</sub>$  would be a new functional hard material.

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**Conflicts of Interest:** The authors declare no conflict of interest.

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