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Nanofluid flow with autocatalytic chemical reaction over a curved surface with nonlinear thermal radiation and slip condition

Muhammad Ramzan^{1,2}, Abida Rafiq¹, Jae Dong Chung², Seifedine Kadry³ & Yu-Ming Chu^{4,5}✉

The study of nanofluids is the most debated subject for the last two decades. Researchers have shown great interest owing to the amazing features of nanofluids including heat transfer and thermal conductivity enhancement capabilities. Having such remarkable features of nanofluids in mind we have envisioned a mathematical model that discusses the flow of nanofluid comprising Nickel-Zinc Ferrite-Ethylene glycol (Ni-ZnFe₂O₄-C₂H₆O₂) amalgamation past an elongated curved surface with autocatalytic chemical reaction. The additional impacts added to the flow model are the heat generation/absorption with nonlinear thermal radiation. At the boundary, the slip and the convective conditions are added. Pertinent transformations are affianced to get the system of ordinary differential equations from the governing system in curvilinear coordinates. A numerical solution is found by applying MATLAB build-in function `bvp4c`. Graphical illustrations and the numerically computed estimates are discussed and analyzed properly. It is comprehended that velocity and temperature distributions have varied trends near and away from the curve when the curvature parameter is enhanced. Further, it is comprehended that the concentration field declines for both homogeneous and heterogeneous reaction parameters.

List of symbols

B_0	Magnetic field strength
Bi	Biot number
C_f	Surface drag force
c_1, c_2	Concentration of chemical species
C_p	Specific heat
Dc_1, Dc_2	Diffusion coefficient
f	Dimensionless stream function
Ha	Magnetic parameter
k	Thermal conductance
k_f	Fluid thermal conductivity
k_{nf}	Nanofluid thermal conductivity
K^*	Dimensionless slip parameter
k_1	Strength of homogenous reaction
k_c, k_s	Rate constants
k_2	Strength of heterogeneous reaction
K_1	Curvature parameter
L	Value of slip parameter
Nu_x	Nusselt number
P	Fluid pressure

¹Department of Computer Science, Bahria University, Islamabad Campus, Islamabad 44000, Pakistan. ²Department of Mechanical Engineering, Sejong University, Seoul 143-747, Korea. ³Department of Mathematics and Computer Science, Faculty of Science, Beirut Arab University, Beirut 115020, Lebanon. ⁴Department of Mathematics, Huzhou University, Huzhou 313000, People's Republic of China. ⁵Hunan Provincial Key Laboratory of Mathematical Modeling and Analysis in Engineering, Changsha University of Science and Technology, Changsha 410114, People's Republic of China. ✉email: chuyuming@zjhu.edu.cn

Pr	Prandtl number
Q_0	Heat generation/absorption volumetric rate
q_r	Nonlinear radiative heat flux
r	Axis coordinate
R^*	Radius of the circular surface
R_d	Radiation parameter
Re_x	Local Reynolds number
s	Positive stretching constant
Sc	Schmidt number
S_1, S_2	Chemical species
T_∞	Convective temperature at infinity
T_f	Fluid thermal conductivity
\bar{U}	Component of velocity
u_w	Stretching velocity along the x -direction
v	Component of velocity
x	Axis coordinates

Greek symbols

α	Dimensionless temperature difference
α^*	Thermal diffusivity
δ	The ratio of the diffusion coefficient
λ_1	Heat generation parameter
μ_f	Fluid dynamic viscosity
μ_{nf}	Nano-fluid dynamic viscosity
Φ	Nanoparticles solid volume fraction
ψ	Dimensionless concentration
ρ	Density of solid nanoparticles
ρ_{nf}	Nano-fluid thermal conductivity
$(\rho C_p)_f$	Fluid heat capacity
$(\rho C_p)_{nf}$	Nanofluid heat capacity
ρ_f	Fluid thermal conductivity
σ	Electrical conductivity
σ_{nf}	Modified thermal diffusion
τ_{yx}, τ_{rx}	Shear stress at the wall
θ	Dimensionless temperature
θ_w	Temperature difference
ξ	A scaled boundary layer coordinate

Nanofluids are characterized as a new type of nanotechnology centered fluids with enhanced thermal features, especially with regard to heat transfer. Nanofluids are the amalgamation of the metallic nanoparticles and some customary fluid like water or ethylene glycol. Choi and Eastman¹ were the pioneer who floated the idea of nanofluids by inserting nanosized (< 100 nm) metallic particles into the usual fluid. Nanofluids are used to improve the thermal performance of microelectronics, microchips in computers, and fuel cells. Nanofluids are also handy in numerous engineering applications including heat exchanger, electronic devices' cooling, reactors, biomedicine, transportation, and transformers' cooling, etc.². Maxwell³ proposed a model to examine the thermal conductivity effectiveness of nanofluids. This model includes the addition of spherical nanoparticles in the base fluid. Hamilton and Crosser⁴ suggested a model which is suitable for nanoparticles with non-spherical shape. Lately, Nadeem et al.⁵ numerically studied the hybrid nanofluid flow comprising two types of nanomaterials Copper and Aluminum Oxide immersed into water over a spongy exponentially stretched curved surface. It is determined in this study that nanofluids possess a higher heat transfer rate when compared with the ordinary fluid. The unsteady flow of the Sisko nanofluid with heat generation and thermal radiation past a curved surface is examined by Ali et al.⁶. It is comprehended here that the fluid velocity is enhanced for large curvature parameter. Khan et al.⁷ discussed numerically the dual solutions of a hybrid nanofluid flow containing silicon dioxide and Aluminum oxide as nanoparticles submerged into water over a curved surface near a stagnation point. It is witnessed here that thermal and velocity boundary layers are enriched when subject nanoparticles are inserted into the base fluid. The unsteady Casson Micropolar nanofluid flow in the region of a stagnation point over a curved surface is deliberated numerically by Amjad et al.⁸. The salient outcome of this study shows that higher estimates of the curvature parameter boost the fluid velocity and an opposite trend is noticed for the microrotation parameter. Some more recent studies featuring nanofluids may be found in⁹⁻¹¹.

Over the last two decades, investigations emphasizing the boundary layer flow over the stretched surfaces has gained remarkable attention by the scientists and the engineers owing to its numerous uses in varied manufacturing and industrial processes. These procedures include liquid films in concentration processes, production of paper, designs of plastic wires and films, crystal glowing, glass blowing, food industries, coatings, drug delivery systems, paints, ceramics, and manufacturing of rubber sheets, etc. The pioneering work studying the fluid flow over a stretched surface was done by Crane¹². Later, many researchers examined flows over stretching surfaces under different configurations. Gupta and Gupta¹³ examined the fluid flow over the spongy surface. Hydromagnetic flow past a stretching surface is assumed by Charabakti and Gupta¹⁴. Anderson et al.¹⁵ examined Power-law

fluid flow under the impact of magnetic forces past a linearly stretching sheet. An Oldroyd-B fluid flow under the influence of generation or absorption of heat is depicted by Hayat et al.¹⁶. Sajid et al.¹⁷ investigated the first time the fluid flow through a straining/stretching surface with a curved shape applying curvilinear coordinates. The impact of the thermal stratification phenomenon in the ferromagnetic fluid over a stretched sheet is scrutinized by Muhammad et al.¹⁸. Ramzan and Yousaf¹⁹ determined the elastic viscid nanofluid flow in view of Newtonian heating past a two-dimensional straining sheet. Sanni et al.²⁰ proposed a computational analysis on the viscous fluid flow past a stretchable curved surface. Hussain et al.²¹ analyzed the flow of Jeffery nano-fluid along with radiation effects past an exponentially stretching sheet. Some recent research work on different types of fluid flows over a stretching surface is given at^{22–26}.

Homogeneous-heterogeneous reactions are entangled in the various bio-chemical reacting systems e.g., biochemical systems and hydrolysis. The association between homogenous and heterogeneous reactions is quite complicated. Some reactions can continue steadily without a catalyst. Homogenous and heterogeneous reactions are unpredictable in the case of reactant species creation and are consumed on the surface of the catalyst. These types of reactions are witnessed in fog formation, processing and diffusion of food, polymer production, hydro-metallurgical industry, and ceramics. Homogenous and heterogeneous reactions impact in a viscous fluid flow past an extended surface is investigated by Merkin²⁷. It is observed here that heterogeneous reaction appears on the surface of the catalyst and homogenous reaction for cubic autocatalysis. Chaudhary and Markin²⁸ reported the same diffusivities of homogenous and heterogeneous reactions. Bachok et al.²⁹ determined the homogenous and heterogeneous reactions in stretching fluid flow. Stretching viscous fluid flow with homogenous-heterogeneous reactions is assumed by Khan and Pop³⁰. Recently, Saif et al.³¹ analyzed analytically the boundary layer flow over a nonlinear curved stretched surface in the presence of autocatalytic reactions and the convective boundary condition at the surface using the Homotopy Analysis Method. The outcome of the analysis revealed that the fluid temperature is enhanced for large estimates of Biot number, nevertheless, an opposing behavior is noted for autocatalytic chemical reactions. The flow of the nanofluid comprising nanomaterials with autocatalytic reactions and second-order boundary condition accompanied by entropy minimization analysis is numerically explored by Muhammad et al.³². It is disclosed in this study that the fluid velocity is diminished for decreasing value of the slip condition. The Peristaltic MHD hybrid Carreau nanofluid flow comprising copper and silver nanoparticles with autocatalytic reactions is studied by Bibi and Xu³³. The salient outcome of this model is that the increasing values of the Weissenberg and the Hartmann numbers affect the fluid velocity. Homogenous and heterogeneous reactions are also conferred through the several studies given at^{34–41}.

From the above literature review, it is noted that very little work is available on the fluid flow over curved surfaces as compared to linear/non-linear/exponential stretching surfaces. Further, this difference gets narrower if we speak about the study of nanofluid with homogenous and heterogeneous reactions past a curved surface. Our aim in this exploration is to numerically analyze the flow of nanofluid containing ferromagnetic nanoparticles i.e., Nickel zinc ferrite ($\text{NiZnFe}_2\text{O}_4$) and the base fluid, ethylene glycol ($\text{C}_2\text{H}_6\text{O}_2$) with impacts of autocatalytic reactions, heat generation/absorption, and nonlinear thermal radiation. The analysis is supported by the slip and convective conditions at the boundary of the curved surface that also boosts the novelty of the envisioned mathematical model. The numerical solution of the proposed problem is attained by invoking *bvp4c* from MATLAB, and characteristics of all arising parameters are discussed thoroughly by keeping their physical justification in mind.

Mathematical modeling

Consider an incompressible 2D nanofluid flow over a spiral steady stretched sheet coiled in a semi-circle of the radius R^* . The sheet is stretched with the velocity $U = u_w$ in the x -direction. The induced magnetic field B_0 is enforced in r -direction *i.e.*, perpendicular to the fluid flow. The temperature T of the sheet is kept invariable while T_∞ is the ambient temperature of the fluid. The heat transfer process is examined through heat absorption/generation influences (Fig. 1).

Homogenous and heterogeneous reactions with two synthesized species S_1 and S_2 are considered. For cuboid autocatalysis, the homogenous reaction can be defined as²⁸:



whereas the heterogeneous reaction on the reactant surface is depicted as²⁸:



Here, c_1 , c_2 are the concentrations for the chemical species S_1 and S_2 whereas rate constants are k_c and k_s . The assumed system of equations comprising continuity, momentum, energy, and homogeneous-heterogeneous reactions is governed by the subsequent boundary layer equations⁹.

$$R^* \left(\frac{\partial U}{\partial x} \right) + \frac{\partial}{\partial r} \{ (r + R^*) v \} = 0, \quad (3)$$

$$\frac{U^2}{r + R^*} = \frac{1}{\rho_{nf}} \left(\frac{\partial p}{\partial r} \right), \quad (4)$$

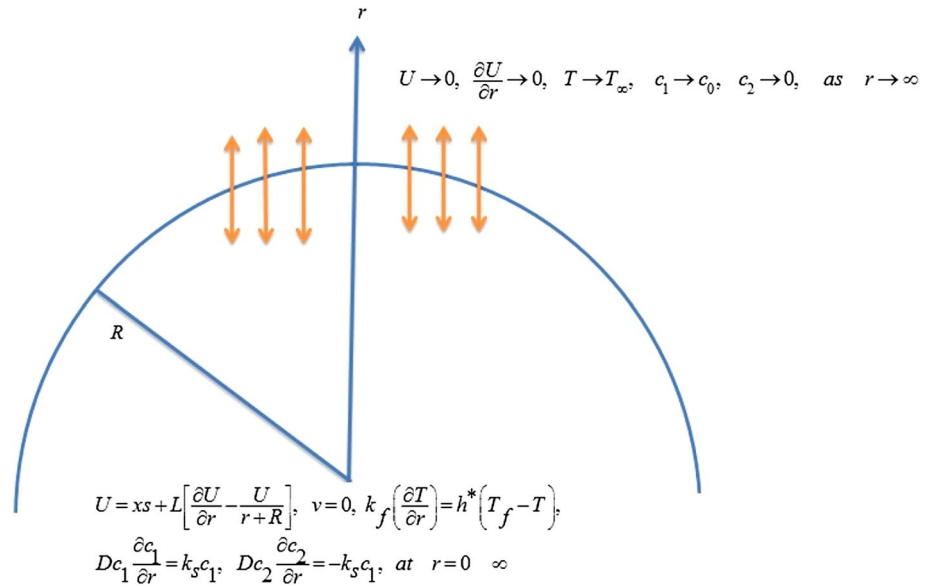


Figure 1. Geometry of the envisioned nanoflow.

$$v \left(\frac{\partial U}{\partial r} \right) + \frac{UR^*}{r + R^*} \left(\frac{\partial U}{\partial x} \right) + \frac{Uv}{r + R^*} = -\frac{1}{\rho_{nf}} \left(\frac{R^*}{R^* + r} \right) \left(\frac{\partial p}{\partial x} \right) + \frac{\mu_{nf}}{\rho_{nf}} \left\{ \frac{\partial^2 U}{\partial r^2} + \frac{1}{R^* + r} \left(\frac{\partial U}{\partial r} \right) - \frac{U}{(R^* + r)^2} \right\} - \frac{\sigma}{\rho_{nf}} B_0^2 U, \tag{5}$$

$$v \left(\frac{\partial T}{\partial r} \right) + \left(\frac{UR^*}{R^* + r} \right) \left(\frac{\partial T}{\partial x} \right) = \alpha_{nf} \left\{ \frac{\partial^2 T}{\partial r^2} + \frac{1}{R^* + r} \left(\frac{\partial T}{\partial r} \right) \right\} + \frac{Q_0}{(\rho C_p)_{nf}} (T_\infty - T) + \frac{1}{(\rho C_p)_{nf}} \left(\frac{1}{r + R^*} \right) \frac{\partial}{\partial r} (r + R^*) q_r, \tag{6}$$

$$v \left(\frac{\partial c_1}{\partial r} \right) + \frac{R^* U}{R^* + r} \left(\frac{\partial c_1}{\partial x} \right) = Dc_1 \left\{ \frac{\partial^2 c_1}{\partial r^2} + \frac{1}{R^* + r} \left(\frac{\partial c_1}{\partial r} \right) \right\} - k_c c_1 c_2^2, \tag{7}$$

$$v \left(\frac{\partial c_2}{\partial r} \right) + \frac{R^* U}{R^* + r} \left(\frac{\partial c_2}{\partial x} \right) = Dc_2 \left\{ \frac{\partial^2 c_2}{\partial r^2} + \frac{1}{R^* + r} \left(\frac{\partial c_2}{\partial r} \right) \right\} + k_c c_1 c_2^2. \tag{8}$$

With the subject conditions:

$$U = xs + L \left[\frac{\partial U}{\partial r} - \frac{U}{r + R^*} \right], v = 0, k_f \left(\frac{\partial T}{\partial r} \right) = h^* (T_f - T), Dc_1 \frac{\partial c_1}{\partial r} = k_s c_1, Dc_2 \frac{\partial c_2}{\partial r} = -k_s c_1, \text{ at } r = 0, U \rightarrow 0, \frac{\partial U}{\partial r} \rightarrow 0, T \rightarrow T_\infty, c_1 \rightarrow c_0, c_2 \rightarrow 0, \text{ as } r \rightarrow \infty. \tag{9}$$

Invoking the following transformations:

$$\xi = \sqrt{\frac{s}{\nu_f}} r, p = \rho_f s^2 x^2 P(\xi), T = T_\infty (1 + (\theta_w - 1)\theta), U = sx f'(\xi), c_1 = c_0 \phi(\xi), c_2 = c_0 g(\xi), v = -\frac{R^*}{r + R^*} \sqrt{sv_f} f(\xi). \tag{10}$$

After using boundary layer approximation and invoking here, Eq. (3) is automatically equated and Eqs. (4)–(10) take the form:

$$P' = \left(1 - \Phi + \Phi \frac{\rho_s}{\rho_f} \right) \frac{f'^2}{\xi + K_1}. \tag{11}$$

Material	C_p (J kg ⁻¹ K ⁻¹)	ρ (kg m ⁻³)	k (W m ⁻¹ K ⁻¹)
Ethylene-glycol C ₂ H ₆ O ₂	2382.0	1116.6	0.2490
Nickel-zinc ferrite (NiZnFe ₂ O ₄)	710.0	4800.0	6.3

Table 1. Mathematical values of physical properties C_p , ρ , and k for Ethylene glycol and Nickel-zinc ferrite (Ni-ZnFe₂O₄-C₂H₆O₂)⁹.

$$\frac{1}{(1 - \Phi + \Phi \frac{\rho_s}{\rho_f})} \frac{2K_1}{\xi + K_1} P = \frac{1}{(1 - \Phi)^{\frac{25}{10}} (1 - \Phi + \Phi \frac{\rho_s}{\rho_f})} \left(f''' - \frac{f'}{(\xi + K_1)^2} + \frac{f''}{\xi + K_1} \right) - \frac{K_1}{K_1 + \xi} f''' + \frac{K_1}{(K_1 + \xi)^2} f'' - \frac{Ha}{(1 - \Phi + \Phi \frac{\rho_s}{\rho_f})} f' \tag{12}$$

$$\frac{1}{Pr} \left\{ \frac{k_{nf}}{k_f} + R_d(1 + \theta(\theta_w - 1))^3 \right\} \left(\theta'' + \frac{1}{K_1 + \xi} \theta' \right) + \left(1 - \Phi + \Phi \frac{(\rho C_p)_s}{(\rho C_p)_f} \right) \left(\frac{K_1}{\xi + K_1} f \theta' \right) - \lambda_1 \theta + \frac{3}{Pr} R_d(1 + (\theta_w - 1)\theta)^2 \theta^2 (\theta_w - 1) = 0 \tag{13}$$

$$\frac{1}{S_c} \left(\psi'' + \frac{1}{\xi + K_1} \psi' \right) + \frac{K_1}{\xi + K_1} f \psi' - k_1 \psi g^2 = 0 \tag{14}$$

$$\frac{\delta}{S_c} \left(g'' + \frac{1}{\xi + K_1} g' \right) + \frac{K_1}{\xi + K_1} f g' + k_1 \psi g^2 = 0 \tag{15}$$

$$f(\xi) = 0, f'(\xi) = 0, f''(\xi) = 1 + K^* [f''(\xi) - f'(\xi)], \theta'(\xi) = Bi(1 - \theta(\xi)), \psi'(\xi) = k_2 \psi(\xi), \delta g'(\xi) = -k_2 \psi(\xi), \text{ at } \xi = 0, \tag{16}$$

$$f'(\infty) \rightarrow 0, f''(\infty) \rightarrow 0, \theta(\infty) \rightarrow 0, \text{ as } \xi \rightarrow \infty \tag{17}$$

The arising parameters are mathematically defined as:

$$K_1 = R^* \sqrt{\frac{s}{\nu_f}}, Bi = h^* \sqrt{\frac{\nu_f}{s}}, S_c = \frac{\nu_f}{Dc_1}, R_d = \frac{16\sigma^* T_\infty^3}{3k^* k}, Pr = \frac{\nu_f}{\alpha}, K^* = L \sqrt{\frac{s}{\nu_f}}, \lambda_1 = \frac{Q_0^*}{s(\rho C_p)_f}, Ha = \sigma \frac{B_0^2}{s \rho_f}, k_1 = c_0^2 \frac{k_c}{s}, k_2 = \frac{k_s \sqrt{\frac{\nu_f}{s}}}{Dc_1}, \delta = \frac{Dc_2}{Dc_1} \tag{18}$$

Eliminating pressure from Eqs. (11)–(12), we get

$$f^{iv} + \frac{2f'''}{K_1 + \xi} - \frac{f''}{(K_1 + \xi)^2} + \frac{f'}{(K_1 + \xi)^3} + (1 - \Phi)^{2.5} \left(1 - \Phi + \Phi \frac{\rho_s}{\rho_f} \right) \left[\frac{K_1}{(\xi + K_1)^2} (f'^2 - f'') \right] - (1 - \Phi)^{2.5} Ha \left(\frac{f'}{\xi + K_1} + f'' \right) = 0 \tag{19}$$

Table 1 characterizes the physical characteristics of Ethylene glycol- Nickel-zinc ferrite (Ni-ZnFe₂O₄-C₂H₆O₂). Thermophysical properties in the mathematical form are given as⁴²:

$$\mu_{nf} = \frac{\mu_f}{(1 - \Phi)^{\frac{25}{10}}}, \tag{20}$$

$$\alpha_{nf} = \frac{k_{nf}}{(\rho C_p)_{nf}}, \tag{21}$$

$$\rho_{nf} = (1 - \Phi)\rho_f + \Phi\rho_s. \tag{22}$$

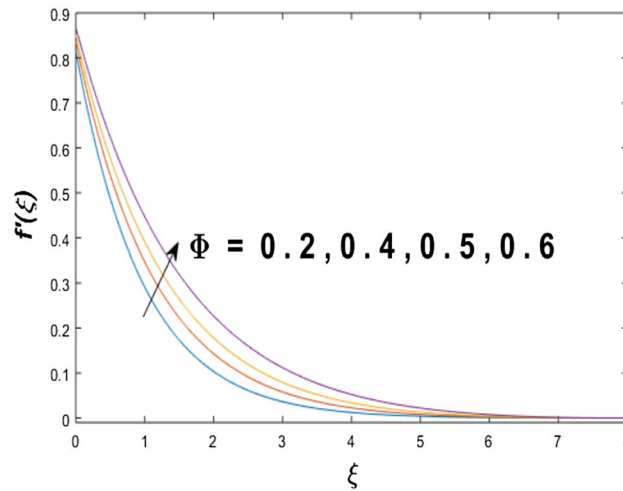


Figure 2. Variations of Φ to $f'(\xi)$.

$$(\rho C_p)_{nf} = \Phi(\rho C_p)_s + (1 - \Phi)(\rho C_p)_f. \tag{23}$$

$$\frac{k_{nf}}{k_f} = \frac{k_s + 2k_f + 2\Phi(k_s - k_f)}{k_s + 2k_f - 2\Phi(k_s - k_f)}. \tag{24}$$

When the diffusion coefficients $D_{c1} = D_{c2}$, then $\delta = 1$, we have

$$\psi(\xi) + g(\xi) = 1. \tag{25}$$

Then Eqs. (14) and (15) become

$$\frac{1}{S_c} \left(\psi'' + \frac{1}{\xi + K_1} \psi' \right) + \frac{K_1}{\xi + K_1} f \psi' - k_1 \psi (1 - \psi)^2 = 0, \tag{26}$$

with boundary conditions

$$\psi'(0) = k_2 \psi(0), \quad \psi(0) \rightarrow 1. \tag{27}$$

Along x -direction, Nusselt number (Nu_x), surface drag force coefficient (C_f) is:

$$Nu_x = \frac{xq_r}{k_f(T_f - T_\infty)}, \quad C_f = \frac{2\tau_{rx}}{u_w^2 \rho}, \tag{28}$$

$$(q_r)_w = q_w + \left(\frac{\partial T}{\partial r} \right), \quad \tau_{rx} = \mu_{nf} \left(\frac{\partial U}{\partial r} - \frac{U}{r + R^*} \right), \text{ at } r = 0 \tag{29}$$

Nusselt number and surface drag force in the dimensionless form are appended as follows:

$$Nu_x (Re_x)^{-\frac{1}{2}} = - \left\{ \frac{k_{nf}}{k_f} + R_d [1 + (\theta_w - 1)\theta(0)]^3 \right\} \theta(0), \tag{30}$$

$$\frac{1}{2} C_f (Re_x)^{\frac{1}{2}} = f''(0) - \frac{f'(0)}{K_1}.$$

The local Reynolds number is expressed as $Re_x = \frac{sx^2}{\nu_f}$.

Results and discussion

The velocity profile, temperature distribution, and rate of heat transfer are characterized by solving Eqs. (12), (13), (19), (26) subject to boundary conditions (16), (17), and (27), and are solved by using MATLAB built-in function bvp4c. This particular section is dedicated to envisioning the impact of distinct parameters, on the velocity $f'(\xi)$, temperature $\theta(\xi)$, and concentration $\psi(\xi)$ profiles. The parameters with their fixed values are defined as $Pr = K_1 = 10, S_c = 0.5, R_d = 1.5, \lambda_1 = 10.5, k_1 = Bi = k_2 = 0.1, \Phi = Ha = 0.1$. Figures 2 and 3 are illustrated to see the effects of volume fraction Φ on the velocity and temperature fields respectively. The magnitude of fluid velocity and temperature field upsurge with increasing values of Φ . For large values of Φ , the momentum, and the boundary layer thicknesses are getting thicker. The nanoparticles volume fraction and convective flow are in direct proportionate with each other. So, an increase in the volume fraction boosts the velocity of the fluid

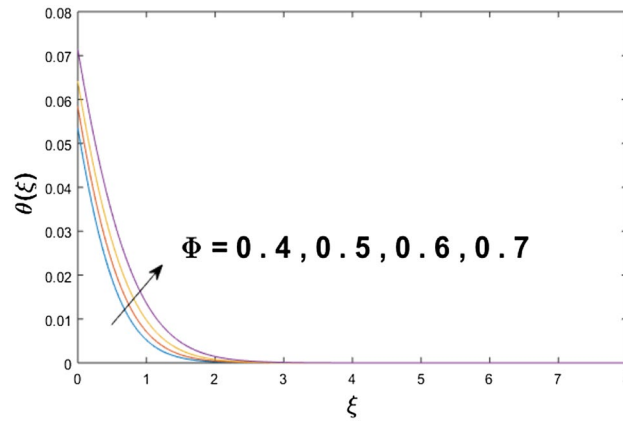


Figure 3. Variations of Φ to $\theta(\xi)$.

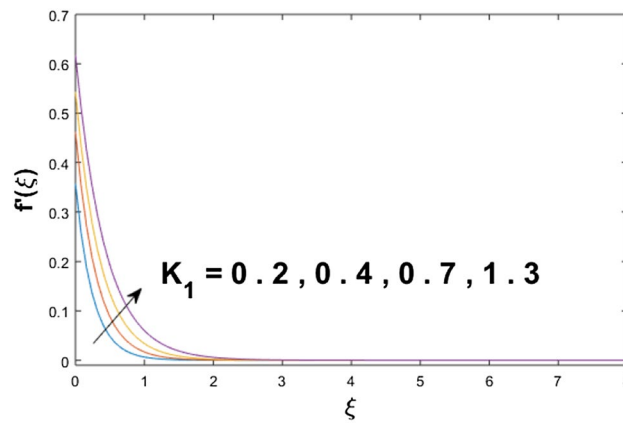


Figure 4. Variations of K_1 to $f'(\xi)$.

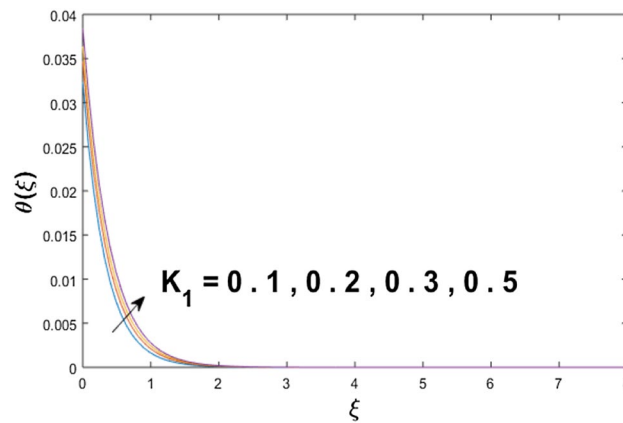


Figure 5. Variations of K_1 to $\theta(\xi)$.

flow. In Fig. 3, the increase in the temperature is because of the thermal conductivity of nanoparticles that is enhanced with growing estimates of nanoparticles volume fraction. This why the high temperature of the fluid is witnessed for large estimates of nanoparticle volume fraction. Figure 4 is drawn to check the inspiration of the curvature parameter K_1 on the velocity profile $f'(\xi)$. The velocity of the fluid raises with large values of K_1 . The surface radius increases for higher estimates of curvature parameter K_1 , which enhances the fluid velocity. Figure 5 demonstrates the behavior of the temperature field for distinct estimates of K_1 . It is observed that the

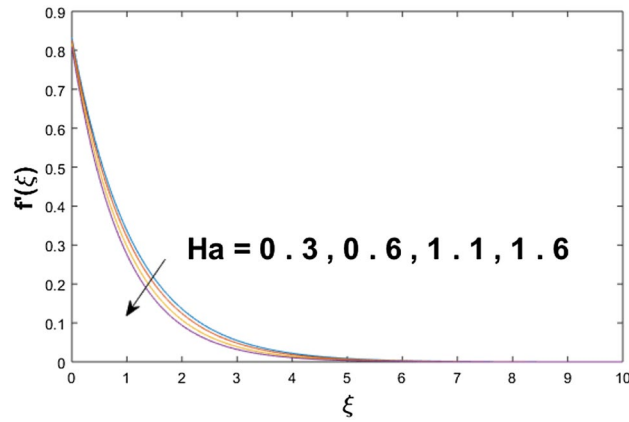


Figure 6. Variations of Ha to $f'(\xi)$.

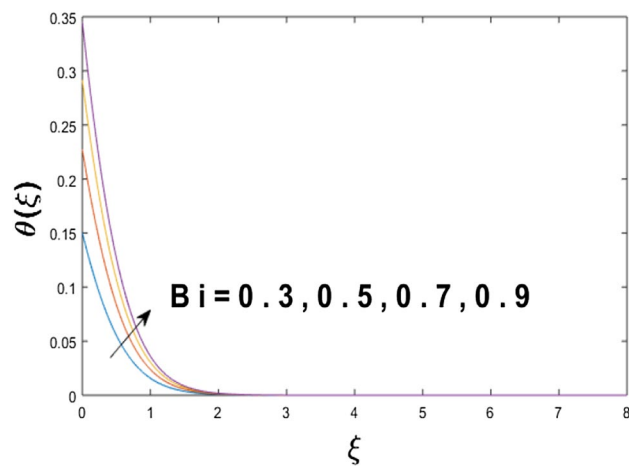


Figure 7. Variations of Bi to $\theta(\xi)$.

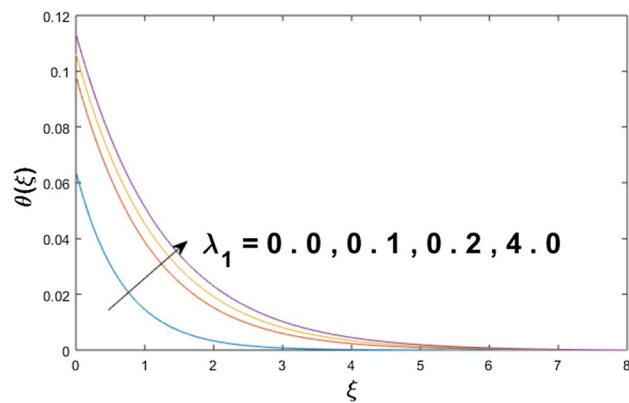


Figure 8. Variations of λ_1 to $\theta(\xi)$.

higher values of K_1 initiates an increase in temperature and the thermal boundary layer. An increase in heat transport is witnessed as values of the curvature parameter is improved. Figure 6 elucidates the influence of the magnetic parameter M on velocity distribution $f'(\xi)$. A decline in the magnitude of velocity is dependent on the enhancement of Hartman's number Ha . This is because the external magnetic field acts as a resistive force (Lorentz force) to the fluid velocity. Figures 7 and 8 illustrate the characteristic of Bi (Biot number) and heat source (generation of heat or absorption) parameter λ_1 on temperature distribution $\theta(\xi)$, respectively. Figure 7 depicts

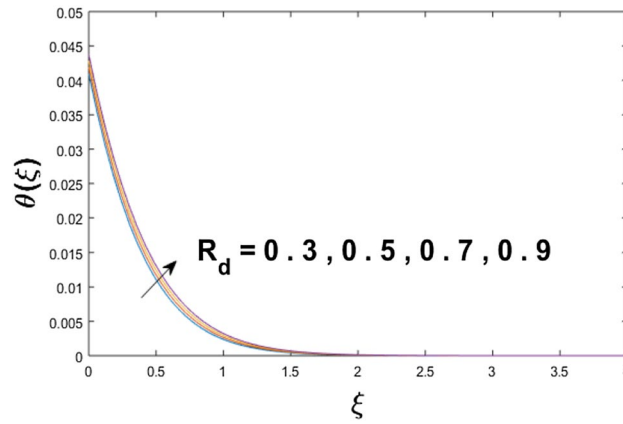


Figure 9. Variations of R_d to $\theta(\xi)$.

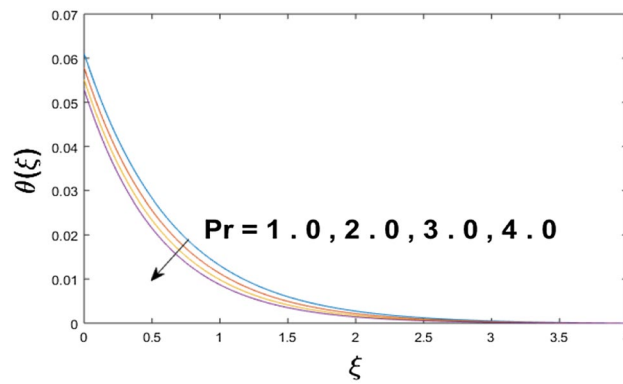


Figure 10. Variations of Pr to $\theta(\xi)$.

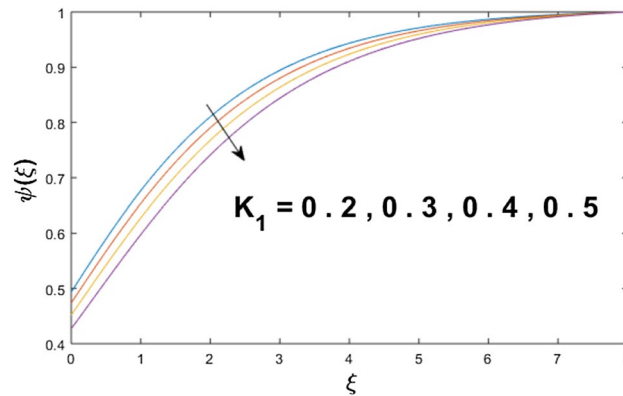


Figure 11. Variations of K_1 to $\psi(\xi)$.

that the convective heat transfer coefficient augments for higher values of Bi and the temperature eventually boosted. Figure 8 demonstrates the temperature field affected by λ_1 . So, augmentation in λ_1 leads to an increment in the temperature and thickness of the thermal boundary layer. Figure 9 depicts the change of radiation parameter R_d on the dimensionless temperature profile $\theta(\xi)$. Augmentation in temperature profile is noted for increasing values of R_d . Substantially, the conduction effects are enhanced for cumulative values of R_d , hence; increase in temperature of the fluid can be noticed. Figure 10 displays the effect of the Prandtl number Pr on temperature distribution. It is obvious from this figure that the temperature profile declines with the increasing values of Pr , as the thermal diffusivity and Prandtl number are associated reciprocally. As the increase in Pr causes a reduction in temperature as well as in boundary layer thickness. The effect of the curvature parameter K_1 on concentration distribution is depicted in Fig. 11. It shows that the concentration field reduces for higher values

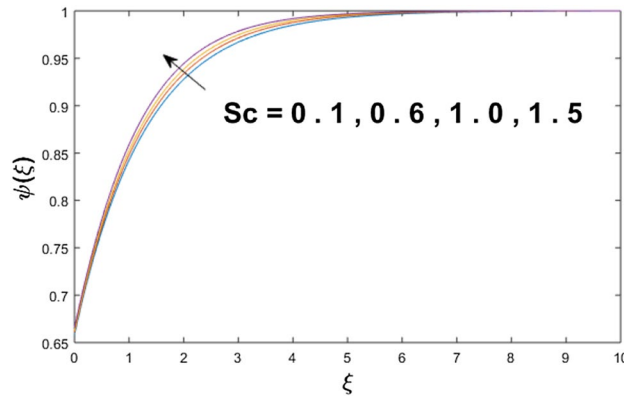


Figure 12. Variations of S_c to $\psi(\xi)$.

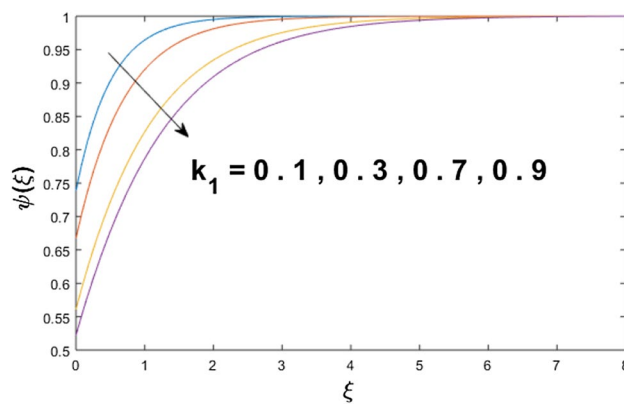


Figure 13. Variations of k_1 to $\psi(\xi)$.

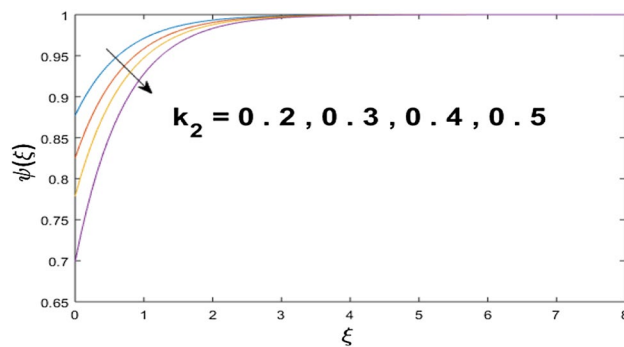


Figure 14. Variations of k_2 to $\psi(\xi)$.

of the curvature parameter K_1 . Large estimates of the curvature parameter increase the space for the collision of the molecules. Thus, decreasing the concentration of the fluid. Figure 12 portrays a decline in concentration $\psi(\xi)$ with increasing estimates of the Schmidt number. The relation between mass diffusivity and viscosity is called the Schmidt number S_c . Then mass diffusivity declines with increasing Schmidt number. Consequently, a reduction in the concentration of fluid is seen. Figure 13 specifies that the concentration field $\psi(\xi)$ decreases with the high strength of the homogenous reaction parameter k_1 . Actually, the reactants are consumed during the homogenous reaction. Thus, a decline in concentration is observed. The concentration profile for a larger strength of heterogeneous reaction parameter k_2 is explained in Fig. 14. When k_2 increases, the concentration profile decreases because of a reduction in diffusion.

Table 2 shows the impact of prominent parameters on the Skin drag coefficient and Nusselt number. The drag strength coefficient rises for large values of Ha (Hartman number), Φ (solid volume fraction of nanofluid)

K_1	Ha	Φ	Bi	R_d	λ_1	θ_w	$-\frac{1}{2}C_f(Re_x)^{\frac{1}{2}}$	$Nu(Re_x)^{-1/2}$
0.8	0.4	0.5	0.7	0.5	0.5	0.5	1.9567	0.3221
1.0							2.0963	0.3215
1.3							2.1979	0.3210
1.5							2.2344	0.3208
0.8	0.1						1.9369	0.3221
	0.3						1.9501	0.3221
	0.5						1.9633	0.3221
	1.0						1.9960	0.3221
	0.1	0.02					0.3837	0.1013
		0.2					0.6297	0.1577
		0.5					1.9369	0.3221
		0.5	0.7				–	1.7136
			1.0				–	2.1923
			1.5				–	2.8072
			2.0	0.1			–	3.2456
				0.3			–	3.2582
				0.5			–	3.2706
				0.7	0.7		–	3.4474
					0.9		–	3.5804
					1.0		–	3.6385
					0.7	0.5	–	3.4474
						0.7	–	3.4319
						0.9	–	3.4075

Table 2. Values of Nusselt number $Nu(Re_x)^{-1/2}$ and Skin drag coefficient $-\frac{1}{2}C_f(Re_x)^{\frac{1}{2}}$.

and K_1 (curvature parameter). A gradual reduction in Nusselt number is noted for higher values of K_1 . Both the Nusselt number and Skin friction coefficient raises for larger values of solid volume fraction Φ of nanofluid. For high radiation parameter R_d , Biot number Bi , λ_1 and θ_w heat transmission rate enhance and no influence on the Skin drag coefficient.

Final remarks. In this study, we have studied the flow of the nanofluid comprising an amalgamation of the Nickel-Zinc ferrite and Ethylene glycol ($Fe_2O_4-C_2H_6O_2$) past an elongated curved surface with the autocatalytic chemical reactions. The associated effects considered in the exploration are the heat generation/absorption and nonlinear thermal radiation with slip and convective conditions are taken at the boundary. The numerical solution of the envisaged problem is obtained via the bvp4c method, a MATLAB software tool. This fluid model is unique as it comprises the combined impacts of autocatalytic chemical reaction with heat generation/absorption and nonlinear thermal radiation with slip and convective conditions. No study so far has been carried out that discusses the combined impacts of the aforementioned impacts. The key observations of the presented model are:

- The autocatalyst chemical reactions affect the fluid concentration significantly.
- The fluid temperature is enhanced for growing estimates of Biot number, heat generation parameter, and solid volume fraction.
- The impacts of the solid volume fraction and the Hartmann number are opposite on the fluid velocity.
- The fluid concentration is augmented for large estimates of the radiation parameter.
- The Schmidt and the Prandtl numbers lower the fluid concentration.
- The impact of the Surface drag force is strengthened for growing values of the Hartmann and Biot numbers.
- The rate of heat transfer is augmented when numerical estimates of the radiation parameter and Biot number.

Future possibilities. The subject manuscript may be extended to a hybrid nanofluid form with varied nanomaterials and fluids. The melting heat boundary conditions may also be adopted.

Received: 5 July 2020; Accepted: 10 September 2020

Published online: 27 October 2020

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Acknowledgements

This work was supported by Korea Institute of Energy Technology Evaluation and Planning (KETEP) Grant funded by the Korea government (MOTIE) (No. 20192010107020, Development of hybrid adsorption chiller using unutilized heat source of low temperature).

Author contributions

M.R. conceived the idea of this manuscript; A.R. did software work, J.D.C. wrote the manuscript S.K. and Y.M.C. vetted the manuscript.

Competing interests

The authors declare no competing interests.

Additional information

Correspondence and requests for materials should be addressed to Y.-M.C.

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