

# Enhanced N-Type Bismuth-Telluride-Based Thermoelectric Fibers via Thermal Drawing and Bridgman Annealing

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**Abstract:** N-type bismuth telluride (Bi<sub>2</sub>Te<sub>3</sub>) based thermoelectric (TE) fibers were fabricated by thermal drawing and Bridgman annealing, and the influence of Bridgman annealing on the TE properties of n-type Bi<sub>2</sub>Te<sub>3</sub>-based TE fibers was studied. The Bridgman annealing enhanced the electrical conductivity and Seebeck coefficient because of increasing crystalline orientation and decreasing detrimental elemental enrichment. The TE performance of n-type Bi<sub>2</sub>Te<sub>3</sub>-based TE fibers was improved significantly by enhancing the power factor. Hence the power factor increased from 0.14 to 0.93 mW/mK<sup>2</sup>, and the figure-of-merit value is from 0.11 to 0.43 at ~300 K, respectively.

**Keywords:** n-type Bi<sub>2</sub>Te<sub>3</sub>; thermoelectric fibers; thermal drawing; Bridgman annealing



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## 1. Introduction

The capacities of recycling heat for electricity generation or converting electricity for refrigeration have enabled the TE technique to be a promising way to recover the waste heat [1,2], a zero-carbon and ubiquitous resource. The efficiency of TE materials is gauged by its figure-of-merit value,  $ZT = S^2\sigma T/\kappa$ , where  $S$  is Seebeck coefficient,  $\sigma$  is electrical conductivity,  $T$  is absolute temperature, and  $\kappa$  is thermal conductivity. Layer-structure Bi<sub>2</sub>Te<sub>3</sub>-based materials have been reported to be the best room-temperature TE materials [3,4]. However, the commercial n-type Bi<sub>2</sub>Te<sub>3</sub>-based materials possess a  $ZT$  restricted to <1 at room temperature, owing to the common interdependence of electron-phonon transport and more sensitivity to texturing than their p-type counterparts [5,6]. Moreover, p-type and n-type Bi<sub>2</sub>Te<sub>3</sub>-based materials mostly compose TE devices together in block shapes, which are based on rigid design, so they cannot be used on heat sources with irregular shapes [7,8]. Current solutions focus on mainly embedding/coating the Bi<sub>2</sub>Te<sub>3</sub>-based materials into/on flexible substrates such as yarns, textiles, and papers [9–11]. But many drawbacks remain, such as low  $ZT$  and weak mechanical flexibility, which still impede their progress.

Hundred-kilometer-length silica fibers for optical communication are typically produced by thermal drawing a preform at the softening temperature of silica glass [12]. With the same facile technique, multiple materials with disparate properties, including semiconductors, metals, and insulators, can be co-drawn into a micro-nano scale [13,14]. It paves the way to multi-material fibers endowed with unique functionalities at fiber length scales and costs. In recent years, researchers have demonstrated ultralong TE fibers by the

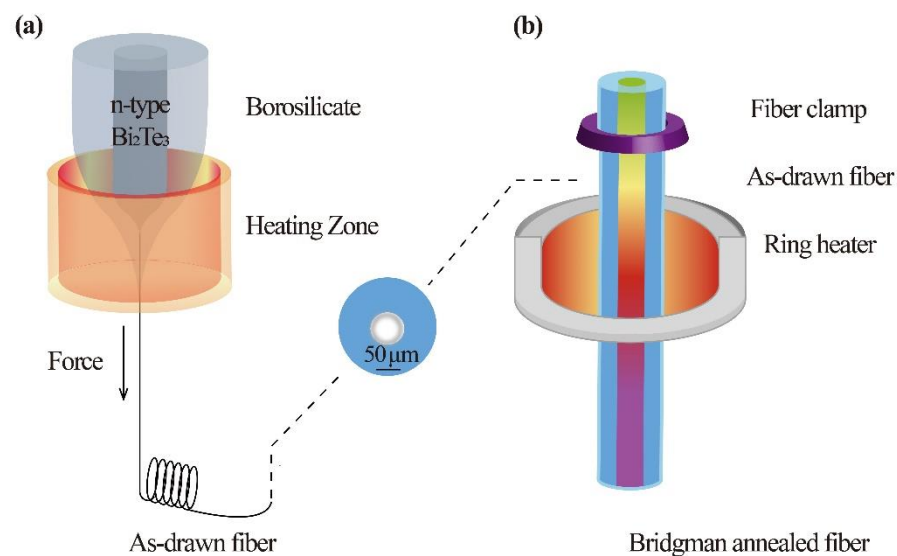
thermal drawing method to integrate crystalline TE micro/nanofibers into a glass-fiber template [15–19]. Although p-type  $\text{Bi}_2\text{Te}_3$  fibers are reported with a high  $ZT \sim 1.4$  at room temperature [20], n-type  $\text{Bi}_2\text{Te}_3$  fibers have not been systematically studied or improved  $ZT$  values effectively by thermal drawing or post-treatment, resulting in TE fiber devices with p-n pairs cannot be widely used. The p-n pair fibers then have the potential to be applied in the field of wearable self-powered devices and temperature-sensing fabrics [7,21–23].

Herein, n-type  $\text{Bi}_2\text{Te}_3$ -based TE fibers with mechanical flexibility were fabricated by optical-fiber-template thermal drawing and Bridgman annealing, also called the Bridgman–Stockbarger method for single-crystal growth and is recently applied in the fabrication of multi-material single-crystal fibers [24,25]. Through Bridgman annealing, the detrimental elemental enrichment in the fiber cores can be reduced, and crystalline orientation along  $(00l)$  can be increased, so they possess enhanced electrical transport. The  $ZT$  value of fibers is measured to be  $\sim 0.43$  at 300 K, approaching four times their as-drawn fiber counterparts.

## 2. Experimental Procedure

### 2.1. Fabrication

As shown in Figure 1a, the two-step method of thermal drawing and Bridgman annealing was applied for n-type  $\text{Bi}_2\text{Te}_3$ -based fibers fabrication. First,  $\text{Bi}_2\text{Te}_3$  and  $\text{Bi}_2\text{Se}_3$  powders (99.999% purity, Aladdin, Shanghai, China) are sealed by a ratio of 5:1 into a Pyrex3.3-borosilicate-glass tube with a 3-mm inner diameter and a 7-mm outer diameter. It is special that the preforms before drawing endured  $700\text{ }^\circ\text{C}$  for one-hour preheating time to form a wetting interface of the core and the cladding by elemental diffusion.  $\text{Bi}_2\text{Te}_3$ -based-core and glass-cladding fibers were then drawn at  $\sim 900\text{ }^\circ\text{C}$  using an optical fiber drawing tower. All fibers maintain a complete core-cladding structure, and the fiber cores show a relative density of  $\sim 97\%$ . N-type  $\text{Bi}_2\text{Te}_3$  cores were produced into meters of continuous fibers.



**Figure 1.** Schematic of the process of (a) fiber drawing and (b) Bridgman annealing.

Figure 1b shows the schematic of the Bridgman annealing technique. Only one ring-shaped resistance was used as a heater to offer a temperature gradient field, which is beneficial to maintaining the stability of the crystal growth interface [24]. The as-drawn fiber gradually descended and crossed the high-temperature zone to recrystallize the core at a constant speed of  $10\text{ mm/h}$ , referencing the growth of single-crystal  $\text{Bi}_2\text{Te}_3$  bulks. The high-temperature zone is  $\sim 60\text{ }^\circ\text{C}$  higher than the melting point of the  $\text{Bi}_2\text{Te}_3$  ( $585\text{ }^\circ\text{C}$ ) and lower than the softening point of the silicate cladding glass ( $719\text{ }^\circ\text{C}$ ).

## 2.2. Measurements

The Bi<sub>2</sub>Te<sub>3</sub>-based core was obtained by etching the as-drawn and annealed fibers in HF acid solution to strip the glass cladding and then identified by an X-ray diffractometer (XRD, X'Pert PROX, Cu K $\alpha$ , PANalytical Corp., Almelo, The Netherlands). Energy-dispersive X-ray spectroscopy (EDS) elemental studies were performed on the fiber cross-section by using scanning electron microscopy (SEM, Zeiss Merlin, ZEISS Corp., Oberkochen, Germany).

The Seebeck coefficients ( $S$ ) or the electrical conductivities ( $\sigma$ ) of some fibers were measured by the four-probe method [20]. For each sample, 3-time fiber measurements were carried out under the same conditions, and we used the average values of 3-time fiber measurements as the measuring value. All absolute values of these relative deviations are lower than 5% and can be negligible, showing the setup is effective, and the measuring results are reliable and reproducible. The thermal conductivity ( $\kappa$ ) was measured using the time-domain thermal-reflection method, and the relative deviation was lower than 10%.

## 3. Results and Discussion

### 3.1. Microstructure

The XRD patterns of the as-drawn fibers and the Bridgman annealed fibers are shown in Figure 2. It is observed that all XRD peaks can be indexed to the Bi<sub>2</sub>Te<sub>2.5</sub>Se<sub>0.5</sub> hexagonal phase (JCPDS No. 51-0643). After thermal drawing, the as-drawn fiber underwent a flash cooling process so that the fiber core would consist of polycrystals. Then the average particle size of as-drawn crystals was calculated to be ~29 nm according to the XRD peaks width using the Scherrer formula [17]. Still, the average particle size of Bridgman annealed crystals is >100 nm. There exist differences in XRD peak intensities between the as-drawn and annealed fibers. The annealed fibers show larger diffraction intensities than the as-drawn fibers at many lattice planes, including (0 0 6) and (0 0 15). These differences in diffraction peak intensities illustrate that the annealed fiber crystals would exhibit a more preferred orientation than the as-drawn fiber crystals do. Based on the Lotgering method [19], the orientation degree  $F$  of the (0 0  $l$ ) planes of polycrystals can be calculated:

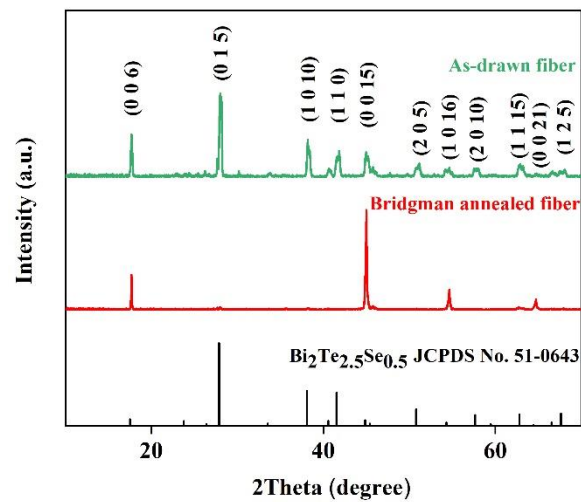
$$F = \frac{P - P_0}{1 - P_0} \quad (1)$$

$$P_0 = \frac{I_0(0\ 0\ l)}{\sum I_0(h\ k\ l)} \quad (2)$$

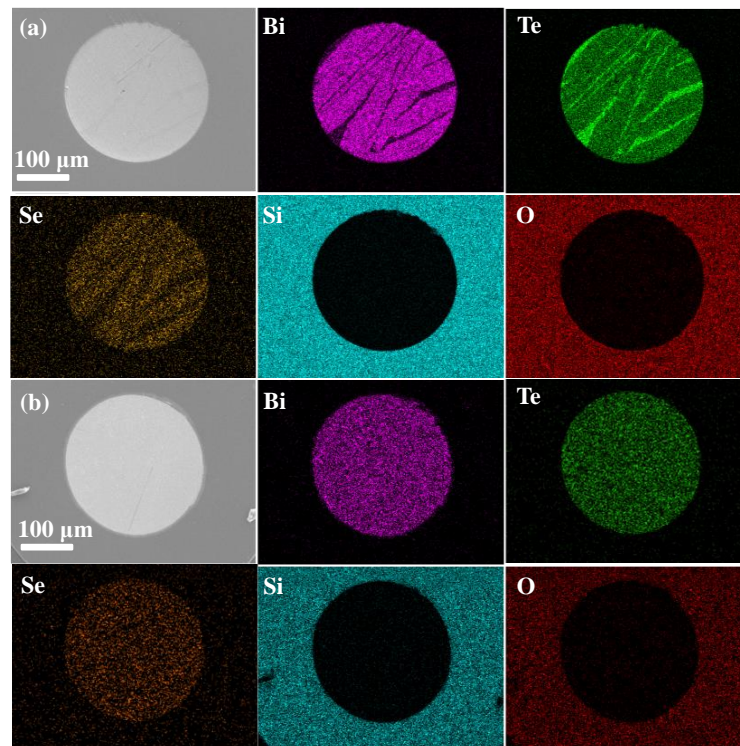
$$P = \frac{I(0\ 0\ l)}{\sum I(h\ k\ l)} \quad (3)$$

where  $P$  and  $P_0$  are the ratios of the integrated intensities ( $I$ ) of (0 0  $l$ ) planes to those of ( $h\ k\ l$ ) planes for preferentially and randomly oriented samples, respectively. Hence the calculated  $F$  of the as-drawn fiber and annealed fiber polycrystals is 0.48 and 0.85, respectively, which means both possess a preferred orientation, and the annealed fiber exhibits a larger preferred orientation.

EDS mappings of the Bi, Te, Se, Si, and O elements on the polished cross-section samples of the as-drawn and the Bridgman annealed fibers are shown in Figure 3. For two samples, there is a little diffusion of Bi, Te, and Se from the core into the cladding region, and there is little diffusion of Si and O from the cladding into the core. Meanwhile, it is noted that there are Te enrichments in the as-drawn fiber core, but no enrichment is found in the Bridgman annealed fiber core. The Te enrichments should be reduced after a slow annealing process with a 10 mm/h recrystallization speed. As the Te enrichments might affect the electrical and thermal transport [26], the fiber cores with/without Te enrichments will exhibit different TE properties.



**Figure 2.** XRD patterns of the as-drawn and Bridgman annealed n-type  $\text{Bi}_2\text{Te}_3$ -based fiber.

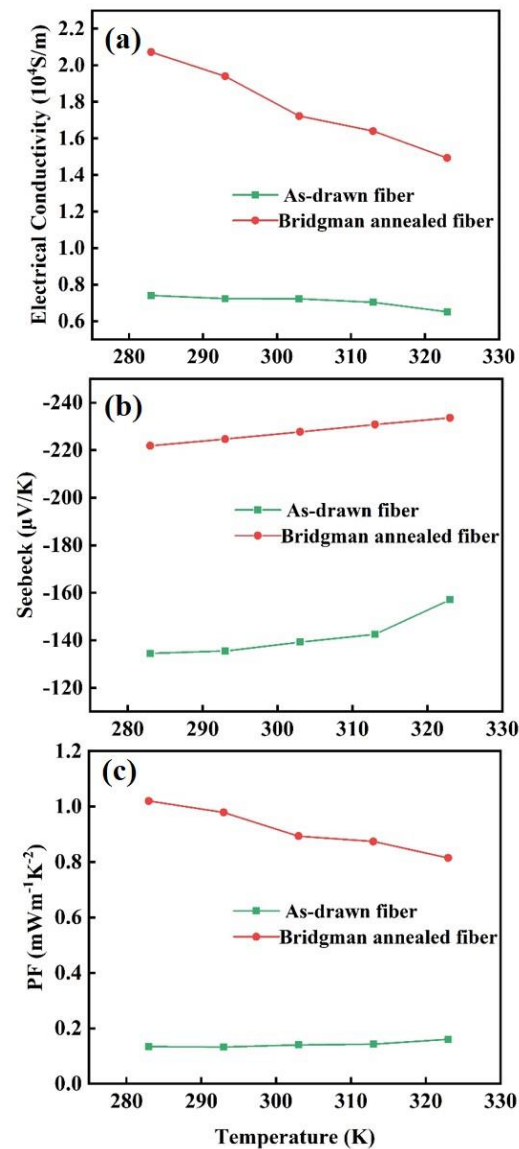


**Figure 3.** Cross-section SEM image and EDS elemental mapping of (a) the as-drawn and (b) the Bridgman annealed n-type  $\text{Bi}_2\text{Te}_3$ -based fiber.

### 3.2. TE Properties

The Seebeck coefficients ( $S$ ) and the electrical conductivities ( $\sigma$ ) of fibers were examined by a self-built setup as shown in the previous study [25] and presented in Figure 4a,b. Both the as-drawn fiber and the Bridgman-annealed fiber exhibit a metallic resistance characteristic in Figure 4a, meaning that the  $\sigma$  decreases with the increasing temperature, 283–323 K. The  $\sigma$  of the Bridgman-annealed fiber is more than double of the as-drawn fiber at the same temperature. In Figure 4b, The  $S$  of the Bridgman-annealed fiber is more than 150% of the as-drawn fiber at the same temperature. The power factors ( $PF = S^2\sigma$ ) of fibers were calculated and presented in Figure 4c. The  $PF$  of the Bridgman-annealed fiber is more than four times the as-drawn fiber, and the highest value is obtained at 283 K,

$\sim 1 \text{ mW/mK}^2$ . It should be mainly derived from Bridgman annealing of reducing detrimental Te enrichment to increase  $S$  and larger orientation to enhance  $\sigma$ .



**Figure 4.** (a) Electrical conductivities, (b) Seebeck coefficients, and (c) power factors of the as-drawn fibers and the Bridgman-annealed fibers at 283–323 K.

As the fiber-axis thermal conductivities ( $\kappa_{||}$ ) were measured on the fiber cross-section using the time-domain thermal-reflection (TDTR) method, the measured  $\sigma$ ,  $S$ ,  $\kappa_{||}$ , and  $ZT$  of the two samples are listed in Table 1. It is observed that the  $\kappa_{||}$  of the as-drawn fiber is ultralow, which could be induced by enhanced phonon scattering from the low relative density of  $\sim 97\%$  and the interface nanograins as reported in the previous study [17]. The  $ZT$  of the Bridgman-annealed fiber core is the highest in the table, three times larger than the as-drawn fiber. The  $ZT$  is also about twice as large as the reported  $ZT$  of  $\text{Bi}_2\text{Se}_3$  fibers, while the Bridgman-annealed fiber core exhibits lower  $\sigma$  but a much higher  $S$  than other fibers [16,27]. The high  $ZT$  of the annealed fiber core comes from enhanced  $PF$ , which benefits from the preferential orientation and the elimination of the Te enrichments. Beyond these, the bending radius minimum ( $r$ ) of the 200- $\mu\text{m}$ -diameter annealed fibers is tested to be 2 cm, and their flexibility is estimated by the maximum bending strain ( $\varepsilon = D/2r \sim 0.5$ ) [28].



**Table 1.** Electrical conductivity, Seebeck coefficient, thermal conductivity, and  $ZT$  of the n-type  $\text{Bi}_2\text{Te}_3$ -based fibers at  $\sim 300$  K.

Samples	Electrical Conductivity $\sigma$ (S/cm)	Seebeck Coefficient $S$ ( $\mu\text{V/K}$ )	Thermal Conductivity $\kappa_{  }$ (W/mK)	$ZT$
Bridgman-annealed fiber	$180 \pm 7$	$-227 \pm 11$	$0.64 \pm 0.06$	0.43
As-drawn fiber	$71 \pm 3$	$-138 \pm 6$	$0.39 \pm 0.04$	0.11
$\text{Bi}_2\text{Se}_3$ fiber [16]	$763 \pm 35$	$-92 \pm 6$	$0.84 \pm 0.08$	0.23
$\text{Bi}_2\text{Se}_3$ core fiber [27]	$319 \pm 15$	$-150 \pm 7$	$1.25 \pm 0.12$	0.18

#### 4. Conclusions

Herein, n-type  $\text{Bi}_2\text{Te}_3$ -based-core glass-clad fibers have been fabricated via thermal drawing and Bridgman annealing. All the polycrystalline  $\text{Bi}_2\text{Te}_3$ -based cores possess a preferential orientation, and the orientation factors of the as-drawn fiber and the annealed fiber are 0.48 and 0.85, respectively. The preferential orientation increases the fiber cores' electrical and thermal conductivity. Importantly, the Te enrichments in the as-drawn fiber core are improved in the annealed fiber core, remarkably enhancing the Seebeck coefficient. Finally, the Bridgman annealed  $\text{Bi}_2\text{Te}_3$ -based core shows an enhanced  $ZT = 0.43$ , and our future work will be enhancing density and regulating the component and the microstructure of the fibers. In addition, the 200- $\mu\text{m}$ -diameter annealed fibers can reversibly bend into a 2-cm curvature radius to show their flexibility. Such a proof-of-concept fiber drawing and annealing method have promising applications in fiber-based TE conversion.

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