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Data Article

Dataset on flue gas composition during pyrolysis of polyoxymethylene in a fluidised bed with the possibility of incorporating CO₂



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ABSTRACT

The dataset presented in this article is the supplementary data for the research article titled "*The pyrolysis and combustion of polyoxymethylene in a fluidised bed with the possibility of incorporating CO2*" [1], in which possible paths of polyoxymethylene conversion in the fluidised bed made from cenospheres and by means of various fluidising gases (air, N₂, CO₂) were tested. The use of CO₂ as fluidising gases (air, N₂, CO₂) were tested. The use of CO₂ as fluidising gases was particularly interesting because above 600° C its incorporation into process products (i.e. CO-rich flue gas) was observed. The gaseous products were detected using Fourier Transform Infrared Spectroscopy (FTIR, Gasmet DX-4000) at intervals of a few seconds. The data on the concentration changes over time will allow to evaluate and verificate of new kinetic models of polyoxymethylene degradation with the possibility of incorporating CO₂.

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Subject	Environmental Engineering; Chemical Engineering
Tupe of data	Table
Type of data	IdDle The qualitative and quantitative analysis of the main second mediusts of
How data were acquired	the qualitative and qualitative analysis of the main gaseous products of thermal utilisation of polyoxymethylene in a CO ₂ atmosphere were performed by infrared absorption spectroscopy (FT-IR, DX-4000, Gasmet Technologies).
Data format	Raw
Parameters for data collection	Determination of the concentrations of components in a multi-component mixture of flue gases were made based on the recorded infrared absorbance spectra of the mixture. The spectra were generated in the range of 900 cm ⁻¹ to 4200 cm ⁻¹ . Measurement of each spectrum and its deconvolution lasted for 7-8 seconds. The explanation of mathematical deconvolution was included in the related research article as Appendix 1.
Description of data collection	Polyoxymethylene pyrolysis was carried out in a fluidised bed reactor. The fluidised bed was made of cenospheres and CO ₂ was used as fluidising medium. The bed was heated to 500-800°. The polyoxymethylene samples were dripped from the top of the reactor. The decomposing of the sample caused changes in the composition of the gases leaving the reactor. The FTIR analyser and deconvolution method (GASMET software) were used for the qualitative analysis of the flue gases.
Data source location	Cracow University of Technology, Faculty of Chemical Engineering and Technology, Cracow, Poland
Data accessibility	Data are accessible with the article.
Related research article	Witold Żukowski, Gabriela Berkowicz, Tomasz M. Majka, The pyrolysis and combustion of polyoxymethylene in a fluidised bed with the possibility of incorporating CO ₂ Energy Conversion and Management. 2020, in press [1]

Specifications Table

Value of the data

The data provides detail information on the quality and quantity of the gaseous products during the pyrolysis of polyoxymethylene by CO₂ in the fluidised bed made of cenospheres. This dataset will be helpful to develop the kinetic modesl of pyrolysis of polyoxymethylene

in CO₂ atmosphere.

This dataset will be helpful for mathematical modelling for chemical processes in fluidised bed or other types of reactors.

1. Data Description

The pyrolysis process is the subject of many works, because it is an attractive alternative to incineration for waste [2]. Studies on the pyrolysis of plastic waste are important for assembling the Circular Economy. To maximize plastic waste valorisation, it is suggested to study the recycling of each of the polymers separately. Most studies on plastic pyrolysis focus on polyolefins, PVC, PET [3]. There are only a few papers that focus on chemical recycling of polyoxymethylene [4].

This work present composition of flue gases recorded by the FTIR analyser obtained during the pyrolysis of polyoxymethylene in the atmosphere of CO_2 in a fluidised bed made of cenospheres. The waste polyoxymethylene is a source of valuable formaldehyde. However, when polyoxymethylene degradation was conducted in CO_2 atmosphere it was found that above $600^{\circ}C$ carbon from fluidising gas can be incorporated to products of POM decomposition. That kind of polyoxymethylene recycling lead to the CO-rich feedstock that may be associated with a negative CO_2 emission, if waste CO_2 is used to react with POM instead of being emitted to the atmosphere. Such a process is particularly important from an ecological point of view. Dataset on the composition of the exhaust gases during polyoxymethylene samples decomposition in CO_2 atmosphere is useful for the further development of modelling processes with CO_2 incorpora-

	Parameter, units	Magnitude
Fluidised bed reactor	Shape	tube
	Wall material	quartz
	Inner diameter, mm	96
	Height, mm	500
	Heating	electrical
	Sieve bottom	CrNi steel plate (1 mm thick), evenly
		distributed holes (diam. 0.6 mm; 6.25 cm ⁻²)
Fluidised bed	Material	cenospheres
	Shape	spherical
	Grain diameter, mm	0.25-0.30
	Mass, g	300
	Density, g/cm ³	845
	Static height, mm	115
	Temperature,°C	500 - 800
	Minimum fluidisation velocity, cm/s	1.24 (at 500°C)
		1.13 (at 600°C)
		1.04 (at 700°C)
Fluidising medium	Physical state	Gas
	Composition	CO ₂
	Inlet temperature,°C	20-25
	Flow Rate, L/min @STP	30 (40 for 500°C)

Parameters of fluidised bed reactor, bed material and fluidising medium.

tion. Numerical stimulation of chemical process is an interest of of many groups, among others, Combustion Group from University of Southern California [5], the CRECK Modeling Group from Politecnico di Milano [6], Lawrence Livermore National Laboratory [7], Combustion group from Berkeley University of California [8], The combustion research group from UC San Diego [9].

This dataset contains 5 Tables. The features of the fluidised bed reactor, bed material, and fluidising air gas are presented in Table 1. Tables 2-5 contain flue gas composition during thermal utilisation of polyoxymethylene in a CO2 atmosphere at different temperatures.

2. Experimental Design, Materials, and Methods

Thermal degradation of polyoxymethylene was performed in the fluidised bed reactor which was made from a quartz tube and chrome-nickel plate with evenly distributed holes. 300 g of cenospheres with diam. 0.25-0.3m mm were placed into reactor. The cenospheres were introduced into a stable fluidized state by means of a gaseous CO₂. The parameters of the reactor, bed material and fluidising gas are summarized in Table 1. Studies on fluidization of cenospheric material can be found in the paper [10].

The cenospheric bed was electrically heated to a given temperature in the range 500-800°C. At specified temperature, samples of polyoxymethylene pellets were dripped into the bed from an open space at the top of reactor. Three types of polyoxymethylene were used: pure polymer (POM-P); recyclate (POM-R), and waste polymer (POM-O). The masses of individual samples were around 200 mg. Due to low density of fluidised bed, polyoxymethylene pellets sank into the bed.

Released during degradation of polyoxymethylene sample gases were sampled by a probe and their infrared spectrum was recorded every few seconds by FTIanalyser. The deconvolution of multi-component spectra was performed using Gasmet Software, using the least squares method. Recording the spectrum with its deconvolution lasted 7-8 seconds. Concentrations of the exhaust gases resulting from the analysis components are shown in Tables 2–5.

Composition of flue gases during thermal utilisation of polyoxymethylene in a CO₂ atmosphere at 800°C.

Temp., C	Canada	Mass	Time	CO	CH4	НСНО	СНЗОН	нсоон	СН3СОСН3
[°C]	Sample	[mg]	[s]			[pi	om]		
			0	0.00	0.00	0.00	0.00	0.00	0.00
			6	396.23	27.54	2.78	0.00	0.00	0.00
			13	18711.14	401.05	65.33	6.40	0.00	0.00
			20	41211.64	625.28	157.91	16.45	0.00	0.00
			27	15355.21	414.74	76.46	10.33	0.00	0.00
			33	3745.73	169.93	22.54	9.92	0.00	0.00
			40	1010.44	54.11	7.50	5.04	0.00	0.00
			47	300,56	16.62	1.97	0.00	0.00	0.00
			54	91.72	5.63	0.90	0.00	0.00	0.00
			60	34.97	1.83	0.60	0.00	0.00	0.00
	POM-P	201	67	17.81	0.00	0.00	0.00	0.00	0.00
			74	9.53	0.00	0.00	0.00	0.00	0.00
			81	5.99	0.00	0.00	0.00	0.00	0.00
			87	3 93	0.00	0.00	0.00	0.00	0.00
			94	4 19	0.00	0.00	0.00	0.00	0.00
			101	4.15	0.00	0.00	0.00	0.00	0.00
			101	2.75	0.00	0.00	0.00	0.00	0.00
			114	2.60	0.00	0.00	0.00	0.00	0.00
			114	2.34	0.00	0.00	0.00	0.00	0.00
			121	1.74	0.00	0.00	0.00	0.00	0.00
			128	0.00	0.00	0.00	0.00	0.00	0.00
			0	0.00	0.00	0.00	0.00	0.00	0.00
			/	5.92	1.10	0.49	0.00	0.00	0.00
			14	9859.06	253.44	62.47	6.65	0.00	0.00
			20	43599.53	593.31	182.02	11.67	0.00	0.00
			27	<u>2822</u> 5.48	512.62	<u>119</u> .21	10.65	0.00	0.00
			34	7144.14	238.65	37.87	6.01	0.00	0.00
			41	1787.77	83.79	11.01	0.00	0.00	0.00
800		203	47	527.49	24.72	3.30	0.00	0.00	0.00
	РОМ-Р		54	160.01	7.52	0.94	0.00	0.00	0.00
			61	52.83	1.96	0.00	0.00	0.00	0.00
			68	23.50	0.66	0.00	0.00	0.00	0.00
			74	14.93	0.00	0.00	0.00	0.00	0.00
			81	8.54	0.00	0.00	0.00	0.00	0.00
			88	5.88	0.00	0.00	0.00	0.00	0.00
			96	4.27	0.00	0.00	0.00	0.00	0.00
			103	2.28	0.00	0.00	0.00	0.00	0.00
			109	2.35	0.00	0.00	0.00	0.00	0.00
			116	2.81	0.00	0.00	0.00	0.00	0.00
			12 <mark>3</mark>	2.19	0.00	0.00	0.00	0.00	0.00
			130	2.45	0.00	0.00	0.00	0.00	0.00
			0	0.00	0.00	0.00	0.00	0.00	0.00
			7	1031.49	79.43	9.00	0.35	0.00	0.00
			14	52368.60	709.82	94.50	21.64	0.00	0.00
			20	20746.37	495.41	39.91	14.75	0.00	0.00
			27	4725.81	210 43	11 16	8 68	0.00	0.00
			34	1253 91	69 17	3 34	0.00	0.00	0.00
			41	371.24	20.97	0.54	0.00	0.00	0.00
			41	107 72	6 /12	0.34	0.00	0.00	0.00
	POM-R	198	5/	207.75	1 92	0.29	0.00	0.00	0.00
			54 61	15 50	1.00	0.00	0.00	0.00	0.00
			10	15.50	0.00	0.00	0.00	0.00	0.00
			58	7.91	0.00	0.00	0.00	0.00	0.00
			/5	5.29	0.00	0.00	0.00	0.00	0.00
			81	3.21	0.00	0.00	0.00	0.00	0.00
			88	1.94	0.00	0.00	0.00	0.00	0.00
			95	1.42	0.00	0.00	0.00	0.00	0.00
			102	0.29	0.00	0.00	0.00	0.00	0.00

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(continued on next page)

Table 2 (continued)

			0	0.00	0.00	0.00	0.00	0.00	0.00
			7	1513.56	102.68	12.35	0.22	0.00	0.00
			14	67582.36	767.65	152 30	36.91	0.00	0.00
				07302.30	500.05	152.50	30.51	0.00	0.00
			21	25444.63	526.45	68.58	24.97	0.00	0.00
		201	27	5964.57	233.55	20.07	11.57	0.00	0.00
			34	1525.81	81.91	5.59	5.18	0.00	0.00
			41	454.53	24.45	1.04	0.00	0.00	0.00
			19	127 77	7.62	0.00	0.00	0.00	0.00
	POM-R		40	137.77	7.03	0.00	0.00	0.00	0.00
			54	53.45	2.23	0.00	0.00	0.00	0.00
			61	25.62	0.00	0.00	0.00	0.00	0.00
			68	12.16	0.00	0.00	0.00	0.00	0.00
			75	8.08	0.00	0.00	0.00	0.00	0.00
			02	E 00	0.00	0.00	0.00	0.00	0.00
			02	5.66	0.00	0.00	0.00	0.00	0.00
			88	4.19	0.00	0.00	0.00	0.00	0.00
			95	2.74	0.00	0.00	0.00	0.00	0.00
			102	3.15	0.00	0.00	0.00	0.00	0.00
			0	0.00	0.00	0.00	0.00	0.00	0.00
			0	105.50	0.00	12.42	0.00	0.00	0.00
			0	105.52	9.61	12.43	6.26	0.00	0.00
			13	30534.40	472.99	471.73	18.47	0.00	0.00
			20	49867.17	619.05	453.35	31.27	0.00	0.00
			27	13265.45	334.06	152.55	10.37	0.00	0.00
			22	3344.01	125 41	46.27	7 47	0.00	0.00
				1042.00	27.71	14.02	7.47	0.00	0.00
			40	1043.66	37.67	14.92	8.69	0.00	0.00
			47	355.43	11.26	5.52	7.51	0.00	0.00
			54	135.10	3.26	2.79	0.00	0.00	0.00
		200	60	59.85	1.47	1.90	0.00	0.00	0.00
	POM-O		67	35.15	0.56	0.00	0.00	0.00	0.00
			74	21.40	0.00	0.00	0.00	0.00	0.00
			74	21.40	0.00	0.00	0.00	0.00	0.00
			81	17.03	0.00	0.00	0.00	0.00	0.00
800			87	9.99	0.00	0.00	0.00	0.00	0.00
800			94	8.18	0.00	0.00	0.00	0.00	0.00
			101	5.08	0.00	0.00	0.00	0.00	0.00
			101	4 54	0.00	0.00	0.00	0.00	0.00
			108	4.54	0.00	0.00	0.00	0.00	0.00
			114	3.35	0.00	0.00	0.00	0.00	0.00
			121	2.44	0.00	0.00	0.00	0.00	0.00
			128	1.97	0.00	0.00	0.00	0.00	0.00
			135	1 29	0.00	0.00	0.00	0.00	0.00
			141	0.45	0.00	0.00	0.00	0.00	0.00
			141	0.45	0.00	0.00	0.00	0.00	0.00
			0	0.00	0.00	0.00	0.00	0.00	0.00
			7	302.76	23.90	9.86	0.00	0.00	0.00
			14	42813.83	553.72	414.32	27.66	0.00	0.00
			21	38283 70	552.09	317 08	27.25	0.00	0.00
			21	0720.04	270.02	102.01	10 50	0.00	0.00
			2/	9/30.84	270.92	102.81	10.56	0.00	0.00
			34	2624.01	98.61	32.44	9.72	0.00	0.00
			41	834.55	29.34	11.15	9.50	0.00	0.00
			48	291.46	7.93	3.90	0.00	0.00	0.00
			54	109.60	2 69	2 09	0.00	0.00	0.00
				105.00	1.05	1.40	0.00	0.00	0.00
			61	53.48	1.05	1.46	0.00	0.00	0.00
	POM-O	198	68	28.91	0.00	0.97	0.00	0.00	0.00
	101010		75	17.39	0.00	1.17	0.00	0.00	0.00
			81	11.29	0.00	1.05	0.00	0.00	0.00
			20	6./1	0.00	0.00	0.00	0.00	0.00
			00	0.41	0.00	0.00	0.00	0.00	0.00
			95	5.50	0.00	0.00	0.00	0.00	0.00
			102	2.94	0.00	0.00	0.00	0.00	0.00
			108	1.82	0.00	0.00	0.00	0.00	0.00
			115	3.98	0.00	0.00	0.00	0.00	0.00
			122	1 22	0.00	0.00	0.00	0.00	0.00
			122	1.23	0.00	0.00	0.00	0.00	0.00
			129	0.00	0.00	0.00	0.00	0.00	0.00
			136	0.00	0.00	0.00	0.00	0.00	0.00
			142	0.00	0.00	0.00	0.00	0.00	0.00

Composition of flue gases during thermal utilisation of polyoxymethylene in a CO₂ atmosphere at 700°C.

Temp.	Sample	Mass	Time	CO	CH4	НСНО	CH3OH	нсоон	СНЗСОСНЗ
[°C]		[mg]	[s]			[p	pm]		
			0	0.00	0.00	0.00	0.00	0.00	0.00
			6	234.27	17.02	24.95	0.00	0.00	0.00
			13	15490.34	389.59	331.57	26.44	0.00	0.00
			20	43154.60	660.84	1044.66	112.56	0.00	0.00
			27	25146.90	569.05	649.39	70.61	0.00	0.00
			33	6462.63	270.01	213.05	21.23	0.00	0.00
			40	1717.58	95.59	65.36	1.92	0.00	0.00
			47	551.98	28.34	20.67	0.00	0.00	0.00
			54	195.88	9.98	7.56	0.00	0.00	0.00
			60	78.26	3.51	3.26	0.00	0.00	0.00
	POM-P	201	5/	37.85	0.97	1.77	0.00	0.00	0.00
			01	27.43	1.18	1.30	0.00	0.00	0.00
			81	13.25	0.48	0.00	0.00	0.00	0.00
			0/	6 24	0.00	0.00	0.00	0.00	0.00
			101	5.92	0.00	0.00	0.00	0.00	0.00
			101	J.82	0.00	0.00	0.00	0.00	0.00
			114	3.81	0.00	0.00	0.00	0.00	0.00
			121	3 32	0.00	0.00	0.00	0.00	0.00
			121	2.64	0.00	0.00	0.00	0.00	0.00
			135	2.04	0.00	0.00	0.00	0.00	0.00
			141	1.94	0.00	0.00	0.00	0.00	0.00
			0	0.00	0.00	0.00	0.00	0.00	0.00
			6	38.71	2.12	8.80	0.00	0.00	0.00
			13	8284.30	241.21	352.33	17.90	0.00	0.00
			20	37694.64	617.27	1275.90	115.51	0.00	0.00
			27	29671.66	612.54	906.67	88.80	0.00	0.00
			33	8437.51	319.48	316.12	27.65	0.00	0.00
			40	2183.80	119.72	99.89	12.02	0.00	0.00
			47	710.07	37.71	32.29	0.97	0.00	0.00
			54	259.83	10.80	11.36	0.00	0.00	0.00
		P 203	61	105.30	3.50	4.25	0.00	0.00	0.00
700	POM-P		67	48.79	1.09	2.60	0.00	0.00	0.00
			74	26.20	0.00	0.00	0.00	0.00	0.00
			81	18.12	0.00	0.00	0.00	0.00	0.00
			88	10.73	0.00	0.00	0.00	0.00	0.00
			95	8.35	0.00	0.00	0.00	0.00	0.00
			102	6.62	0.00	0.00	0.00	0.00	0.00
			108	4.39	0.00	0.00	0.00	0.00	0.00
			115	6.92	0.00	0.00	0.00	0.00	0.00
			122	3.84	0.00	0.00	0.00	0.00	0.00
			129	5.45	0.00	0.00	0.00	0.00	0.00
			135	2.19	0.00	0.00	0.00	0.00	0.00
			0	0.00	0.00	0.00	0.00	0.00	0.00
			6	2.96	0.58	0.32	0.00	0.00	0.00
			20	11660.05	712.20	202 22	129.95	0.00	0.00
			20	25282.22	502 56	493.33	20.95	0.00	0.00
			27	62/19/29	292.20	497.03	24.01	0.00	0.00
			40	1733.66	101.82	48.67	4 03	0.00	0.00
DOM D			40	598.49	30.58	15.07	1.04	0.00	0.00
			54	225 55	9 68	5 95	0.00	0.00	0.00
			60	97.61	3.41	2.64	0.00	0.00	0.00
		67	50.07	1.13	1.55	0.00	0.00	0.00	
	POM-R	203	74	27.94	0.00	0.00	0.00	0.00	0.00
		81	16.27	0.00	0.00	0.00	0.00	0.00	
		87	11.68	0.00	0.00	0.00	0.00	0.00	
			94	7.28	0.00	0.00	0.00	0.00	0.00
			101	5.59	0.00	0.00	0.00	0.00	0.00
			108	4.68	0.00	0.00	0.00	0.00	0.00
			115	3.23	0.00	0.00	0.00	0.00	0.00

Table 3 (continued)

			0	0.00	0.00	0.00	0.00	0.00	0.00
			6	45.14	5.04	11.45	0.00	0.00	0.00
			13	28531.70	582.57	689.19	106.08	0.00	0.00
			20	33267.88	669.24	585 59	112.69	0.00	0.00
			27	8573.08	348.64	107 55	30 71	0.00	0.00
			27	2202.42	122.06	E0 20	14.46	0.00	0.00
			33	2205.42	152.00	10.53	14.40	0.00	0.00
			40	740.65	39.75	18.53	7.89	0.00	0.00
			4/	263.95	12.19	6.03	0.00	0.00	0.00
			54	106.85	3.16	2.95	0.00	0.00	0.00
			60	54.87	1.09	1.08	0.00	0.00	0.00
		201	67	30.37	0.00	0.00	0.00	0.00	0.00
	TOWER	201	74	20.15	0.00	0.00	0.00	0.00	0.00
			81	12.84	0.00	0.00	0.00	0.00	0.00
			87	9.26	0.00	0.00	0.00	0.00	0.00
			94	7.23	0.00	0.00	0.00	0.00	0.00
			101	6.48	0.00	0.00	0.00	0.00	0.00
			101	4 87	0.00	0.00	0.00	0.00	0.00
			114	2 72	0.00	0.00	0.00	0.00	0.00
			114	3.73	0.00	0.00	0.00	0.00	0.00
			121	2.39	0.00	0.00	0.00	0.00	0.00
			128	3.01	0.00	0.00	0.00	0.00	0.00
			135	0.91	0.00	0.00	0.00	0.00	0.00
			141	0.00	0.00	0.00	0.00	0.00	0.00
			0	0.00	0.00	0.00	0.00	0.00	0.00
			6	275.86	16.12	51.60	0.00	0.00	0.00
			13	21456.45	408.89	1388.85	76.46	0.00	0.00
			20	36253.03	602.28	1804.23	115.58	0.00	0.00
			27	10674.01	333.96	676.33	38.83	0.00	0.00
			33	2996.19	130.93	221.51	12.95	0.00	0.00
			40	1067.77	41.35	71.40	6.48	0.00	0.00
			47	486 11	12.60	25.02	4 63	0.00	0.00
			54	302.04	4.08	0.57	1.03	0.00	0.00
			60	302.04	4.00	3.37	4.02	0.00	0.00
			60	209.00	1.41	4.60	2.77	0.00	0.00
			6/	140.67	1.13	2.80	3.42	0.00	0.00
			/5	99.23	0.00	2.07	0.00	0.00	0.00
	POM-O	199	82	78.36	0.00	0.00	0.00	0.00	0.00
700			89	63.82	0.00	0.00	0.00	0.00	0.00
			96	45.06	0.00	0.00	0.00	0.00	0.00
			102	36.50	0.00	0.00	0.00	0.00	0.00
			109	28.31	0.00	0.00	0.00	0.00	0.00
			116	23.25	0.00	0.00	0.00	0.00	0.00
			123	21.54	0.00	0.00	0.00	0.00	0.00
			129	17.69	0.00	0.00	0.00	0.00	0.00
			136	16.41	0.00	0.00	0.00	0.00	0.00
			1/3	15.46	0.00	0.00	0.00	0.00	0.00
			140	10.40	0.00	0.00	0.00	0.00	0.00
			150	10.82	0.00	0.00	0.00	0.00	0.00
			150	12.11	0.00	0.00	0.00	0.00	0.00
			163	7.40	0.00	0.00	0.00	0.00	0.00
			1/0	6.68	0.00	0.00	0.00	0.00	0.00
			0	0.00	0.00	0.00	0.00	0.00	0.00
			7	4178.22	127.69	477.00	14.44	0.00	0.00
			14	32889.40	556.34	2132.45	127.17	0.00	0.00
			20	17118.87	441.96	1148.24	48.43	0.00	0.00
			27	4658.25	197.28	396.87	21.98	0.00	0.00
			34	1464.79	64.32	127.90	9.44	0.00	0.00
			41	586.56	19.88	42.59	6.91	0.00	0.00
			48	273.65	6.31	16.34	4.75	0.00	0.00
			54	190.61	2.10	6.73	7.53	0.00	0.00
			61	141 47	0.00	3 63	0.00	0.00	0.00
			69	118 00	0.00	1 59	0.00	0.00	0.00
	POM O	200	75	110.09	0.00	1.38	0.00	0.00	0.00
	FOIVI-U	200	/5	88.42	0.00	1.14	0.00	0.00	0.00
			81	64.29	0.00	1.29	0.00	0.00	0.00
			88	52.71	0.00	0.00	0.00	0.00	0.00
			95	39.29	0.00	0.00	0.00	0.00	0.00
			102	33.98	0.00	0.00	0.00	0.00	0.00

Composition of flue gases during thermal utilisation of polyoxymethylene in a CO₂ atmosphere at 600°C.

Temp.	Sample	Mass	Time	CO	CH4	НСНО	CH3OH	НСООН	СНЗСОСНЗ
		[mg]	[5]	0.00	0.00	0.00		0.00	0.00
			7	9.85	0.00	9.00	0.00	0.00	0.00
			14	2381.80	120.53	851.42	66.82	5.04	6.15
			21	11682.76	468.70	2256.72	314 20	12.75	23.10
			27	19950 90	489.55	4287.01	465.66	16 21	31.73
			34	11889 11	505.61	1963.91	214 53	12 46	17 75
			41	3605.98	237.87	729 79	71.66	4 78	3 32
			48	1082.04	83.75	236.22	24.91	3 21	0.83
			54	391.65	24.43	76.92	4 4 2	2 99	0.00
			61	168 20	6.89	26.79	0.55	2.55	0.00
			68	84.23	2.02	12.05	0.55	1.83	0.00
	POM-P	204	75	50.72	0.00	7.48	0.20	1.05	0.00
	10111	201	82	37.61	0.00	5.02	0.04	0.00	0.00
			02	29.06	0.00	2.02	0.00	0.00	0.00
			00	23.00	0.00	2.07	0.00	0.00	0.00
			102	19.40	0.00	0.00	0.00	0.00	0.00
			102	18.40	0.00	0.00	0.00	0.00	0.00
			110	13.93	0.00	0.00	0.00	0.00	0.00
			116	10.94	0.00	0.00	0.00	0.00	0.00
			123	12.60	0.00	0.00	0.00	0.00	0.00
			130	10.80	0.00	0.00	0.00	0.00	0.00
			137	6.79	0.00	0.00	0.00	0.00	0.00
			144	4.52	0.00	0.00	0.00	0.00	0.00
			150	3.93	0.00	0.00	0.00	0.00	0.00
			0	0.00	0.00	0.00	0.00	0.00	0.00
			7	138.76	5.22	101.03	0.00	0.00	0.00
			14	4526.83	205.49	1137.32	85.73	5.64	7.95
			20	13837.48	495.19	2798. <mark>8</mark> 2	326.44	12.05	27.21
			27	15963.47	566.65	3804.14	369.12	11.43	32.42
			34	10608.48	422.59	2230.95	224.85	11.49	21.75
			41	4577.51	230.87	1030.37	79.85	5.63	6.11
			47	1529.59	85.09	360.46	29.87	3.34	0.74
			54	524.90	25.42	119.56	6.28	2.54	0.00
			61	215.55	7.53	42.36	2.36	2.51	0.00
			68	106.47	2.44	16.83	0.33	2.59	0.00
	POM-P	205	74	67.05	0.00	8.36	0.00	0.00	0.00
600	FONFF	205	81	47.24	0.00	5.19	0.00	0.00	0.00
			88	35.34	0.00	4.34	0.00	0.00	0.00
			95	28.61	0.00	3.79	0.00	0.00	0.00
			101	27.00	0.00	2.37	0.00	0.00	0.00
			108	20.25	0.00	2.56	0.00	0.00	0.00
			115	15.11	0.00	2.54	0.00	0.00	0.00
			122	12.07	0.00	1.76	0.00	0.00	0.00
			128	10.66	0.00	1.46	0.00	0.00	0.00
			135	8.90	0.00	1.40	0.00	0.00	0.00
			142	7.10	0.00	1.18	0.00	0.00	0.00
			149	5.31	0.00	1.35	0.00	0.00	0.00
			155	3.80	0.00	1.34	0.00	0.00	0.00
			0	0.00	0.00	0.00	0.00	0.00	0.00
			7	2.39	0.00	2.08	0.00	0.00	0.00
			13	4873.10	210.68	949.76	121.22	4.08	6.99
			20	26449.96	348.70	4499.24	511.07	8.83	26.32
			27	12247.27	554.56	1973.44	218.51	10.28	13.16
			34	3960.81	283.13	760.34	83.04	3.06	3.35
			41	1275.77	105.04	250.90	18.81	2.26	0.00
			47	477.84	31.28	81.10	5.16	2.13	0.00
			54	235.67	9.71	27.44	2.20	1.73	0.00
			61	130.06	3.16	11.66	0.00	0.07	0.00
			68	83.50	1.03	6.57	0.00	0.00	0.00
			74	63.29	0.64	3.91	0.00	0.00	0.00
	POM-R	199	81	47.76	0.00	3.81	0.00	0.00	0.00
			88	42.98	0.00	2.59	0.00	0.00	0.00
			95	33.83	0.00	2.36	0.00	0.00	0.00
			101	26.98	0.00	0.00	0.00	0.00	0.00
			108	25.10	0.00	0.00	0.00	0.00	0.00
			115	21.10	0.00	0.00	0.00	0.00	0.00
			113	21.00	0.00	0.00	0.00	0.00	0.00

Table 4 (continued)

			0	0.00	0.00	0.00	0.00	0.00	0.00																							
			6	2143.64	100.68	539.55	48.34	2.85	5.22																							
			13	26523.34	338.84	4727.21	554.95	9.47	28.07																							
			20	13257.65	571.12	2099.95	265.87	11.48	15.39																							
			27	3872.47	281.21	764.91	82.92	4.12	1.61																							
			33	1202.91	103.42	250.96	19.27	2.56	0.00																							
			40	479.19	30.66	79.52	5.98	3.43	0.00																							
			47	223.55	9.63	27.96	2.26	2.52	0.00																							
			54	126.74	2.38	11.40	0.49	2.04	0.00																							
			60	90,40	0.76	5.46	0.00	0.00	0.00																							
			67	60.46	0.00	3.81	0.00	0.00	0.00																							
			74	48.47	0.00	2.94	0.00	0.00	0.00																							
	POM-R	207	81	41.93	0.00	2.50	0.00	0.00	0.00																							
			87	33.57	0.00	1.95	0.00	0.00	0.00																							
			94	29.13	0.00	1 35	0.00	0.00	0.00																							
			101	23.28	0.00	2.09	0.00	0.00	0.00																							
			108	19.95	0.00	1.80	0.00	0.00	0.00																							
			115	17.28	0.00	0.00	0.00	0.00	0.00																							
			121	1/.20	0.00	0.00	0.00	0.00	0.00																							
			121	10.85	0.00	0.00	0.00	0.00	0.00																							
			125	8.03	0.00	0.00	0.00	0.00	0.00																							
			142	6.05	0.00	0.00	0.00	0.00	0.00																							
			142	7 11	0.00	0.00	0.00	0.00	0.00																							
			140	6.52	0.00	0.00	0.00	0.00	0.00																							
600			155	0.52	0.00	0.00	0.00	0.00	0.00																							
				642.20	10.00	205.67	0.00	1 51	0.00																							
			14	10820 50	19.05	295.07	4.11	1.51	0.00																							
																										14	10820.56	282.40	3192.21	181.30	4.33	27.77
			21	16938.90	269.20	1000 75	280.61	4.31	33.93																							
			2/	6040.58	268.30	1860.75	85.25	6.54	9.91																							
			34	1///.32	105.41	650.23	29.21	4.09	3.03																							
			41	623.29	33.36	216.53	12.55	2.54	0.00																							
			48	258.26	10.34	74.50	7.71	2.42	0.00																							
			54	139.16	2.31	28.37	0.00	0.00	0.00																							
			61	101.91	0.00	12.15	0.00	0.00	0.00																							
			68	80.10	0.00	7.89	0.00	0.00	0.00																							
	POM-O	198	75	69.28	0.00	5.28	0.00	0.00	0.00																							
			81	56.22	0.00	4.28	0.00	0.00	0.00																							
			88	48.50	0.00	4.23	0.00	0.00	0.00																							
			95	41.54	0.00	3.89	0.00	0.00	0.00																							
			102	38.90	0.00	0.00	0.00	0.00	0.00																							
			108	39.15	0.00	0.00	0.00	0.00	0.00																							
			115	35.47	0.00	0.00	0.00	0.00	0.00																							
			122	34.90	0.00	0.00	0.00	0.00	0.00																							
			129	33.34	0.00	0.00	0.00	0.00	0.00																							
			135	29.72	0.00	0.00	0.00	0.00	0.00																							
			142	23.05	0.00	0.00	0.00	0.00	0.00																							
			149	20.45	0.00	0.00	0.00	0.00	0.00																							
				1812-625 25 26	500 Stores	1 1021 001003			0.00																							

Composition of flue gases during thermal utilisation of polyoxymethylene in a CO₂ atmosphere at 500°C.

Temp.	Sample	Mass	Time	CO	CH4	HCHO	СНЗОН	НСООН	СНЗСОСНЗ
[°C]	Sample	[mg]	[s]			[p	pm]		
			0	0.00	0.00	0.00	0.00	0.00	0.00
			6	12.11	0.00	41.95	0.00	0.04	0.00
			13	315.73	0.00	1008.71	38.39	3.49	0.36
			20	32\$4.08	187.31	<u>3916.</u> 52	474.78	9.77	27.92
			27	5114.56	416.76	5409.35	931.94	15.33	29.33
			33	4327.85	396.18	4739.63	782.99	18.10	24,26
			40	2531.91	194.87	1792.96	289.69	9.59	6.75
			4/	884.37	76.09	653.41	99.72	5.01	1.10
			54	317.78	23.31	216.30	24.10	4.60	0.00
			60	121.57	7.92	72.22	7.95	4.05	0.00
	POM-P	203	7/	31 35	3.00	13 52	0.72	2.54	0.00
			81	20.83	0.66	8.07	0.72	2.33	0.00
			88	15.40	0.00	5.95	0.00	0.00	0.00
			94	11.90	0.00	4.21	0.00	0.00	0.00
			101	11.65	0.00	3.38	0.00	0.00	0.00
			108	9.90	0.00	3.35	0.00	0.00	0.00
			115	8.99	0.00	2.21	0.00	0.00	0.00
			121	7.74	0.00	0.00	0.00	0.00	0.00
			128	7.38	0.00	0.00	0.00	0.00	0.00
			135	6.32	0.00	0.00	0.00	0.00	0.00
			142	6.35	0.00	0.00	0.00	0.00	0.00
			0	0.00	0.00	0.00	0.00	0.00	0.00
			7	105.89	0.51	377.79	5.84	2.62	0.00
			14	1199.16	68.72	2280.15	182.99	4.32	23.26
			20	3393.21	310.76	5519.35	660.79	11.55	36.97
			27	3538.66	317.22	6668.24	816.39	12.80	37.54
			34	2280.69	269.18	1720.00	619.59	17.15	31.37
			41	1334.56	20.81	1/29.66	208.73	7.86	12.68
			4/	4/1.38	39.81	202.05	16.90	4.50	3.02
			61	75.06	12.44	67.08	6.18	3.02	0.00
			68	39.67	9.52	24 79	2 45	2 90	0.00
			74	27.03	0.00	10.22	0.63	2.50	0.00
	POM-P	201	81	18.05	0.00	4.43	0.00	0.00	0.00
500			88	13.92	0.00	2.29	0.00	0.00	0.00
			95	10.69	0.00	1.25	0.00	0.00	0.00
			101	9.16	0.00	0.00	0.00	0.00	0.00
			108	6.97	0.00	0.00	0.00	0.00	0.00
			115	5.87	0.00	0.00	0.00	0.00	0.00
			122	4.49	0.00	0.00	0.00	0.00	0.00
			128	3.48	0.00	0.00	0.00	0.00	0.00
			135	2.52	0.00	0.00	0.00	0.00	0.00
			142	1.68	0.00	0.00	0.00	0.00	0.00
			149	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			0	0.00	0.00	0.00	0.00	0.00	0.00
			7	12.92	0.07	61.37	0.00	0.00	0.17
			14	1659 54	20.45	6457 07	201 00	4.39 5 1 F	22.09
			20	1770 61	112 51	9076 81	415 65	71 /2	18 20
			3/	1820.21	83 66	5875 71	221 12	5 09	6.58
			41	614 49	37.23	1687.02	73 41	5.62	3 14
PC			47	280.41	15.67	608.58	26.90	4.44	0.00
			54	107.90	4.25	205.47	14.84	2.70	0.00
			61	57.96	1.67	72.35	2.09	3.47	0.00
			68	36.38	0.26	29.45	0.00	0.00	0.00
			74	27.01	0.00	15.27	0.00	0.00	0.00
	POM-O	203	81	23.32	0.00	9.39	0.00	0.00	0.00
			88	19.26	0.00	7.52	0.00	0.00	0.00
			95	18.35	0.00	7.49	0.00	0.00	0.00
			101	14.06	0.00	5.01	0.00	0.00	0.00
			108	14.10	0.00	4.58	0.00	0.00	0.00
			115	13.34	0.00	3.61	0.00	0.00	0.00
			122	11.77	0.00	3.35	0.00	0.00	0.00
			128	9.93	0.00	3.05	0.00	0.00	0.00

Table 5 (continued)

			0	0.00	0.00	0.00	0.00	0.00	0.00																	
			6	10.69	0.50	49.65	0.00	0.00	0.00																	
			13	299.34	24.87	1165.05	32.47	5.42	12.34																	
			20	1734. <mark>43</mark>	82.67	6878.80	267.54	5.83	30.22																	
			27	2118.44	119.56	9537.80	308.20	82.35	14.28																	
			34	1688.37	70.00	4760.22	187.90	9.43	1.68																	
			40	618.52	16.41	1333.04	52.71	6.23	0.00																	
			47	212.56	7.29	465.64	20.10	4.78	0.00																	
			54	86.97	2.57	157.11	13.20	3.60	0.00																	
		M-O 201	61	46.15	0.00	57.86	0.57	3.67	0.00																	
			67	32.82	0.00	25.46	7.37	3.55	0.00																	
																				74	23.37	0.00	14.44	6.75	3.53	0.00
			81	20.37	0.00	9.76	0.00	0.00	0.00																	
500	POM-O		88	14.66	0.00	6.26	0.00	0.00	0.00																	
500	101110		201	95	13.89	0.00	5.19	0.00	0.00	0.00																
				102	11.87	0.00	4.74	0.00	0.00	0.00																
			108	9.87	0.00	5.24	0.00	0.00	0.00																	
			115	9.56	0.00	4.03	0.00	0.00	0.00																	
			122	9.01	0.00	3.16	0.00	0.00	0.00																	
			129	6.77	0.00	0.00	0.00	0.00	0.00																	
			1 <mark>35</mark>	8.17	0.00	0.00	0.00	0.00	0.00																	
			142	5.14	0.00	0.00	0.00	0.00	0.00																	
			149	5.32	0.00	0.00	0.00	0.00	0.00																	
			15 <mark>6</mark>	4.36	0.00	0.00	0.00	0.00	0.00																	
			162	3.81	0.00	0.00	0.00	0.00	0.00																	
																169	3.80	0.00	0.00	0.00	0.00	0.00				
			176	3.13	0.00	0.00	0.00	0.00	0.00																	
			183	3.27	0.00	0.00	0.00	0.00	0.00																	

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships which have, or could be perceived to have, influenced the work reported in this article.

Supplementary materials

Supplementary material associated with this article can be found, in the online version, at doi:10.1016/j.dib.2020.105703.

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