

# Toward Predicting Interfacial Tension of Impure and Pure CO<sub>2</sub>-Brine Systems Using Robust Correlative Approaches

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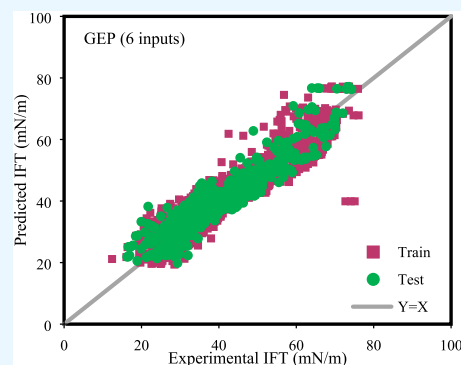
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**ABSTRACT:** In the context of global climate change, significant attention is being directed toward renewable energy and the pivotal role of carbon capture and storage (CCS) technologies. These innovations involve secure CO<sub>2</sub> storage in deep saline aquifers through structural and capillary processes, with the interfacial tension (IFT) of the CO<sub>2</sub>-brine system influencing the storage capacity of formations. In this study, an extensive data set of 2811 experimental data points was compiled to model the IFT of impure and pure CO<sub>2</sub>-brine systems. Three white-box machine learning (ML) methods, namely, genetic programming (GP), gene expression programming (GEP), and group method of data handling (GMDH) were employed to establish accurate mathematical correlations. Notably, the study utilized two distinct modeling approaches: one focused on impurity compositions and the other incorporating a pseudocritical temperature variable ( $T_{cm}$ ) offering a versatile predictive tool suitable for various gas mixtures. Among the correlation methods explored, GMDH, employing five inputs, exhibited exceptional accuracy and reliability across all metrics. Its mean absolute percentage error (MAPE) values for testing, training, and complete data sets stood at 7.63, 7.31, and 7.38%, respectively. In the case of six-input models, the GEP correlation displayed the highest precision, with MAPE values of 9.30, 8.06, and 8.31% for the testing, training, and total data sets, respectively. The sensitivity and trend analyses revealed that pressure exerted the most significant impact on the IFT of CO<sub>2</sub>-brine, showcasing an adverse effect. Moreover, an impurity possessing a critical temperature below that of CO<sub>2</sub> resulted in an elevated IFT. Consequently, this relationship leads to higher impurity concentrations aligning with lower  $T_{cm}$  values and subsequently elevated IFT. Also, monovalent and divalent cation molalities exhibited a growing influence on the IFT, with divalent cations exerting approximately double the influence of monovalent cations. Finally, the Leverage approach confirmed both the reliability of the experimental data and the robust statistical validity of the best correlations established in this study.



## 1. INTRODUCTION

The escalation of carbon dioxide (CO<sub>2</sub>) levels within the Earth's atmospheric composition stands as a pressing concern, given its profound impact on the dynamics of global climate alteration.<sup>1</sup> To this end, diverse strategies have been initiated to counteract the swift increase in CO<sub>2</sub> concentrations. Among these strategies, carbon capture and storage (CCS) emerges as a propitious method for addressing CO<sub>2</sub> emissions.<sup>2–4</sup> Underground geological structures, encompassing saline aquifers, depleted oil and gas reservoirs, and coal seams have emerged as robust candidates for the secure containment of CO<sub>2</sub>.<sup>5–10</sup> On a global scale, deep saline aquifers offer the most extensive capacity for CO<sub>2</sub> storage in comparison to the two primary alternatives: unmineable coal seams and depleted hydrocarbon reservoirs.<sup>11</sup> The interfacial tension (IFT), which emerges due to variations in intermolecular forces between the surfaces of the two phases in contact, holds a pivotal influence over the behavior of multiphase flow within reservoirs.<sup>12</sup> In the

context of two-phase displacement, the IFT plays a central role in dictating the dynamic characteristics of phase transportation. The way phases displace each other in porous media, including phenomena such as viscous and capillary fingering, is greatly influenced by the interplay of IFT between these phases. Ensuring CCS efficiency requires retaining injected CO<sub>2</sub> in the subsurface to prevent any escape to the surface. This goal is accomplished by using various trapping methods, such as dissolution, residual or capillary, structural, and mineral trapping.<sup>13–17</sup> Structural trapping curbs the ascent of buoyant

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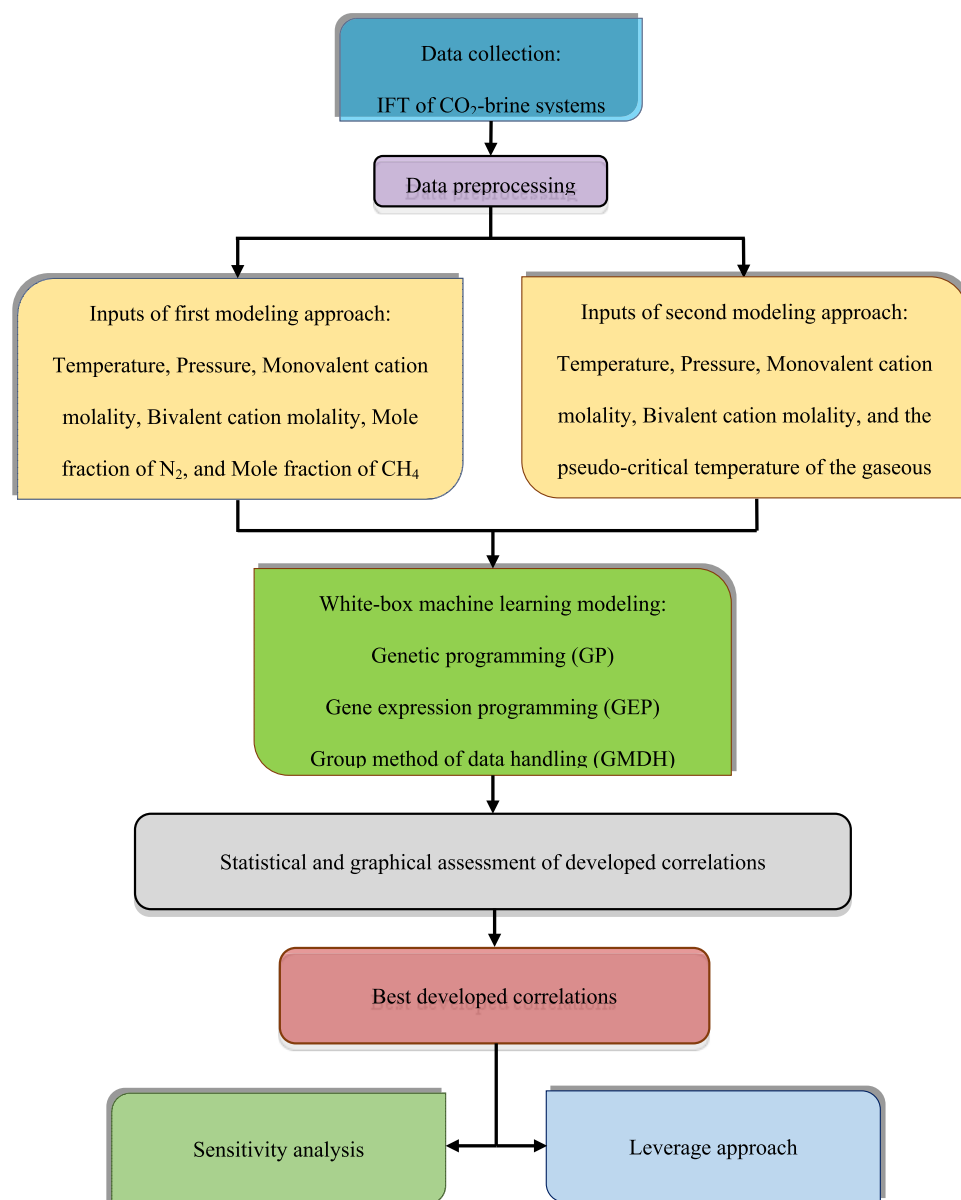
CO<sub>2</sub> gas through the barrier of the cap rock. At a microscopic level, when the saturation of confined CO<sub>2</sub> remains low and drops below a certain threshold, the IFT between CO<sub>2</sub> and brine keeps residual CO<sub>2</sub> in place, leading to residual trapping.<sup>18</sup> When saturation levels are elevated, capillary trapping takes precedence.<sup>19</sup> Consequently, the efficacy of capillary trapping hinges on the IFT governing the equilibrium between vertical gravity and capillarity within a transitional capillary zone.<sup>20,21</sup> Furthermore, CO<sub>2</sub> can be crucially sequestered as small clusters within the gaps of rock pores, which is extremely important for the effective implementation of CCS projects. This containment is accomplished through the interaction between CO<sub>2</sub>-brine IFT.<sup>22</sup>

A significant hurdle in implementing CCS is the considerable expense of isolating pure CO<sub>2</sub> from mixed anthropogenic sources. Direct utilization and subsequent underground injection of this flue gas present an appealing alternative. However, this approach is also susceptible to impurities such as nitrogen (N<sub>2</sub>) and methane (CH<sub>4</sub>). Although the ultimate aspiration is to sequester pure CO<sub>2</sub>, practical economic considerations steer the preference toward utilizing the accessible impure CO<sub>2</sub>.<sup>23</sup> As a result, it is customary for the injected CO<sub>2</sub> stream to encompass or be amalgamated with diverse impurities originating from various sources.<sup>24,25</sup> CH<sub>4</sub> as a greenhouse gas contributes to both indirect and direct mechanisms for retaining infrared radiation via the process of oxidation.<sup>26</sup> Co-injecting CO<sub>2</sub> with other substances has the potential to alter different properties, such as viscosity, diffusion coefficient, and density. The alteration of IFT in the resulting fluid systems, especially in gas-brine systems within saline formations, is substantial. These changes collectively influence the migration and entrapment of CO<sub>2</sub> within subsurface reservoirs.<sup>26,27</sup>

Accurate and reliable IFT values between CO<sub>2</sub> and brine under in situ conditions are of utmost importance. These values are essential for accurately assessing various aspects, such as the spread of CO<sub>2</sub> in displacement scenarios, its storage processes, and the final immobilization of CO<sub>2</sub> below the Earth's surface. Recent years have witnessed a significant amount of research dedicated to estimating the IFT between gas containing pure or impure CO<sub>2</sub> and brine. A multitude of experimental investigations have been conducted to furnish IFT data for these systems across varying temperature ranges, pressure conditions, salt types, salinity levels, and compositions of CO<sub>2</sub>-containing gas.<sup>28–36</sup> These inquiries mainly depend on the pendant drop method because of its inherent advantages. This method allows for accurate measurement of the IFT even at high pressures and temperatures. However, it is crucial to acknowledge that this experimental method can be time-consuming and financially taxing, requiring subsequent interpretive methods. In contrast, only a small number of modeling investigations have been aimed at generating practical correlations. Furthermore, theoretical underpinnings for comprehending the effects of factors like temperature and pressure on IFT and rock wettability have also been established through the execution of molecular dynamics simulations. Besides, these models may overestimate predictions, particularly when dealing with high pressures.<sup>37–39</sup> Several researchers have put forward different correlations for predicting the pure CO<sub>2</sub>-water IFT, specifically in scenarios where salinity is absent.<sup>30,35,40</sup> In addition, scientists have developed several empirical correlations to explain the IFT in pure CO<sub>2</sub>-brine systems.<sup>32,41,42</sup> Conversely, employing the

linear gradient theory, Yan et al.<sup>33</sup> proposed correlations for impure CO<sub>2</sub>-brine mixtures to assess the IFT in gas–water combinations encompassing CO<sub>2</sub>, N<sub>2</sub>, and CH<sub>4</sub>. However, the model exhibited limited precision, particularly when applied to gas mixtures containing CO<sub>2</sub>. Utilizing the alternating condition expectation algorithm, IFT predictions spanning a broad pressure and temperature range of 0.1–60 MPa and 5.25–175 °C were conducted by Li et al.<sup>43</sup> However, despite the model's intricacy, it shows a lack of accuracy, coupled with an error exceeding 10%, emphasizing the critical necessity for the development of a more dependable predictive approach. Therefore, researchers explored artificial intelligence modeling due to its capacity to effectively represent intricate systems encompassing diverse included parameters.<sup>44,45</sup> Zhang et al.<sup>46</sup> employed a neural network to model CO<sub>2</sub>-brine IFT, utilizing a database containing a total of 1716 data points. Kamari et al.<sup>47</sup> employed the identical database of 1716 data points, utilizing multiple machine learning (ML) models to establish a predictive model based on four input variables, including temperature, pressure, monovalent cation molality, and divalent cation molality for CO<sub>2</sub>-brine IFT. Niroomand-Toomaj et al.<sup>48</sup> introduced a Radial Basis Function model, for the prediction of CO<sub>2</sub>/aquifer brine IFT. This model is developed using 378 data points, encompassing various temperatures, pressures, and salinities. Partovi et al.<sup>49</sup> harnessed 1716 data points of CO<sub>2</sub>-brine IFT and leveraged computer-based models to formulate hybrid models. These models yielded notably more accurate results compared with empirical correlations. Rashid et al.<sup>50</sup> employed 1019 experimentally measured IFT values within their intelligent modeling approach. Amooie et al.<sup>51</sup> employed a novel database containing 2517 experimental data points encompassing both pure and impure CO<sub>2</sub>-brine systems. They applied several white-box and black-box ML techniques to predict the IFT in impure CO<sub>2</sub>-brine systems. Nait Amar<sup>52</sup> employed the genetic programming (GP) approach to estimate IFT in both pure and impure CO<sub>2</sub>-brine systems across diverse operational scenarios. Their study incorporated 2346 validated IFT measurements. Safaei-Farouji et al.<sup>53</sup> utilized a data set comprising 2184 experimental data points and employed robust ML methods to predict IFT within the CO<sub>2</sub>-brine system. Drawing from a data set of 2517 experimental data points, Zhang et al.<sup>54</sup> conducted a study involving the modeling of CO<sub>2</sub>-brine IFT. The findings indicated that increased pressure and/or decreased geothermal gradients result in a significant increase in the maximum structural trapping capacity. Evidently, in recent times, researchers have consistently dedicated efforts toward refining IFT prediction conditions, striving for broader and more inclusive modeling approaches. This entails the incorporation of a growing body of authentic experimental data spanning a diverse array of operational conditions. However, recognizing the significance of carbon sequestration in saline reservoirs, the utilization of expanded data sets, and the inclusion of impurity variables within the system hold the promise of constructing a comprehensive model endowed with advanced capabilities.

The objective of this research is to formulate enhanced, explicit mathematical correlations to estimate the IFT in CO<sub>2</sub>-brine systems. This project is built on the most extensive data set gathered to date, covering 2811 data points. To achieve this goal, three renowned white-box ML methodologies, namely, genetic programming (GP), gene expression programming (GEP), and group method of data handling (GMDH), are employed. A variety of statistical and graphical assessment



**Figure 1.** Research steps for modeling the CO<sub>2</sub>-brine IFT.

techniques are used to validate these correlations. Furthermore, sensitivity analysis is conducted using Spearman rank correlation to investigate the influence of input variables on the output. Lastly, the leverage method is employed to determine the practical application range of the established correlations. Figure 1 illustrates the research process undertaken in this study to model the IFT between CO<sub>2</sub> and brine.

## 2. DATA COLLECTION

In order to model the IFT of both impure and pure CO<sub>2</sub>-brine systems, 2811 experimental data points were gathered from reliable literature sources.<sup>28–36,41,42,55–71</sup> This database is the most comprehensive collected for the IFT of CO<sub>2</sub>-brine to date, containing about 290 or more data from similar studies. Typically, in these investigations, impure brine is synthesized through the introduction of salts such as KCl, NaCl, CaCl<sub>2</sub>, Na<sub>2</sub>SO<sub>4</sub>, and MgCl<sub>2</sub>. Yet, it has been demonstrated that the resultant IFT of CO<sub>2</sub>-brine primarily hinges on the valence of the cations present. Hence, the classification of brine impurities

is undertaken through the bifurcation of input variables into two distinct categories: the molalities of monovalent and divalent cations. It is important to note that in the context of pure water, the molality values for both monovalent and divalent cations are designated as zero. In the context of the available experimental data, the impurity within the CO<sub>2</sub>-rich gas phase is attributed solely to differing concentrations of the CH<sub>4</sub> and N<sub>2</sub> components. However, a fresh perspective is adopted, wherein individual impurities are not isolated based on their specific identities. Instead, the impure mixture is approached as a unified whole, discerned by the introduction of a novel critical parameter tailored for this distinction. This study employed two distinct modeling methodologies, one involving 6 inputs and the other involving 5 inputs. The initial approach encompassed 6 inputs: temperature, pressure, monovalent cation molality, bivalent cation molality, mole fraction of N<sub>2</sub>, and mole fraction of CH<sub>4</sub> within the injected gas. Conversely, the second approach encompassed 5 inputs, specifically temperature, pressure, monovalent cation molality,

Table 1. Statistical Details of the Gathered Databank in This Research

	pressure (MPa)	temperature (K)	monovalent cation molality (mol/kg)	bivalent cation molality (mol/kg)	CH <sub>4</sub> (mole fraction)	N <sub>2</sub> (mole fraction)	Tcm (K)	IFT (mN/m)
mean	14.02	333.46	1.02	0.45	0.02	0.02	298.96	39.91
median	9.06	323.40	0.05	0.00	0.00	0.00	304.20	37.19
mode	2.00	373.15	0.00	0.00	0.00	0.00	304.20	31.90
SD	12.89	38.18	1.38	1.02	0.11	0.09	20.73	11.51
Kurtosis	3.37	-0.29	0.91	9.26	32.13	42.87	19.67	0.02
Skewness	1.82	0.71	1.35	2.99	5.64	6.48	-4.39	0.74
minimum	0.08	278.15	0.00	0.00	0.00	0.00	170.65	12.40
maximum	69.51	448.15	5.13	5.00	0.80	0.75	304.20	76.10
count	2811	2811	2811	2811	2811	2811	2811	2811
status	input	input	input	input	input	input	input	target

bivalent cation molality, and the pseudocritical temperature of the gaseous mixture (Tcm). To elucidate, in the second approach, rather than integrating the concentrations of CH<sub>4</sub> and N<sub>2</sub> as separate input variables, we introduce a solitary input variable (i.e., Tcm) that encapsulates the entirety of the mixture's composition. This consolidated approach effectively captures the essence of its constituents and is computed as follows:<sup>72</sup>

$$T_{cm} = \sum_i^{nc,g} y_i T_{c_i} \quad (1)$$

where  $y_i$  represents the mole fraction of every component, with a corresponding critical temperature of  $T_{c_i}$ . Additionally,  $nc,g$  denotes the number of components present in the gas mixture.

Table 1 presents the statistical summary detailing the input and target parameters of the data set employed for the modeling process. A visualization known as a box plot portrays the five-number summary derived from a data set. This summary includes the minimum, first quartile, median, third quartile, and maximum values. In the construction of a box plot, a box spans from the first quartile to the third quartile, while a vertical line intersects the box at the median value. Figure 2 presents a collection of box plots representing all variables present within the database utilized in this study. The data presented in Table 1 illustrate the experimental IFT measurements, spanning a broad spectrum of operating pressures, ranging from 0.08 to 69.51 (MPa), and temperatures spanning from 278.15 to 448.15 (K). The extensive range of model input parameters and their varied span offer a robust foundation for constructing an inclusive predictive correlation for the IFT of CO<sub>2</sub>-brine. To partition the data, a random separation of the databank into two subsets was employed, resulting in a training set comprising 80% of the entire data set, and a test set encompassing the remaining 20%.

### 3. MODEL DEVELOPMENT

**3.1. Genetic Programming (GP).** GP constitutes a specialized area within artificial intelligence and evolutionary computation.<sup>73</sup> It operates by drawing on concepts derived from natural selection and evolution to autonomously produce computer programs or models with the capacity to address distinct tasks or challenges. In scenarios characterized by nonlinearity and significant levels of imprecision, the employment of the GP method is widespread for the derivation of correlations.<sup>74,75</sup> GP systems exhibit structures reminiscent of those of trees. Nodes within these structures are categorized into internal or external groups based on their positions.<sup>76</sup> The process of the GP approach is illustrated in Figure 3 using a

flowchart configuration. Employing an iterative methodology, this dependable, bioinspired technique ultimately yields a precise mathematical representation. Upon input of the data, the initial phase involves establishing a random community. Subsequently, an objective function is employed to assess the performance of the model. Following this, parent candidates with elevated correlation values are selected for modification using genetic operators, giving rise to offspring.<sup>77</sup> Successive iterations are produced following the same procedure, and the quality of subsequent generations is enhanced as desired knowledge from proficient individuals is transmitted to their progeny. The process concludes when the desired level of accuracy is achieved or the predetermined maximum number of iterations is attained.<sup>78</sup>

**3.2. Gene Expression Programming (GEP).** The GEP, pioneered by Ferreira in 2001,<sup>79</sup> stands as a sophisticated approach within the realm of soft computing. Operating within the evolutionary algorithm framework, it harnesses the tenets of evolution to achieve its goals. The distinctive benefit of GEP lies in its capacity to produce precise mathematical representations of the systems under examination. From a conceptual standpoint, GEP is considered an enhanced iteration of GP, which was first introduced by Koza.<sup>73</sup> GEP effectively addresses the challenges inherent in GP, notably the constraints posed by regression strategies.<sup>79</sup> Like any other evolutionary algorithm, GEP undertakes exploration for the optimal expression model by utilizing chromosomes that encode and represent potential solutions. Moreover, GEP introduces a pivotal component known as the expression tree into its framework. The process of obtaining the expression tree involves the conversion of chromosomes into tangible candidates. Within the structure of GEP, genes are utilized, encompassing both terminals and a head that encompasses functions. Each gene is characterized by a predetermined sequence of symbols, which correspond to various operators like  $\{+, -, \times, /, \sqrt{\quad}, \log\}$ , alongside a terminal set encompassing  $\{x, y, z\}$ .<sup>80</sup> The GEP process involves several key stages. To begin, GEP parameters are established, encompassing critical aspects, such as population size, termination conditions, and gene length. Subsequently, an initial population of chromosomes is created, each representing a distinct mathematical expression and selected at random.<sup>81</sup> A fitness evaluation is then conducted, gauging the chromosomes' suitability based on a designated fitness function. The most promising individuals are identified and retained for the subsequent generation, while tournament selection is employed to detect candidates for recombination, yielding new offspring. Within this framework, options for recombination

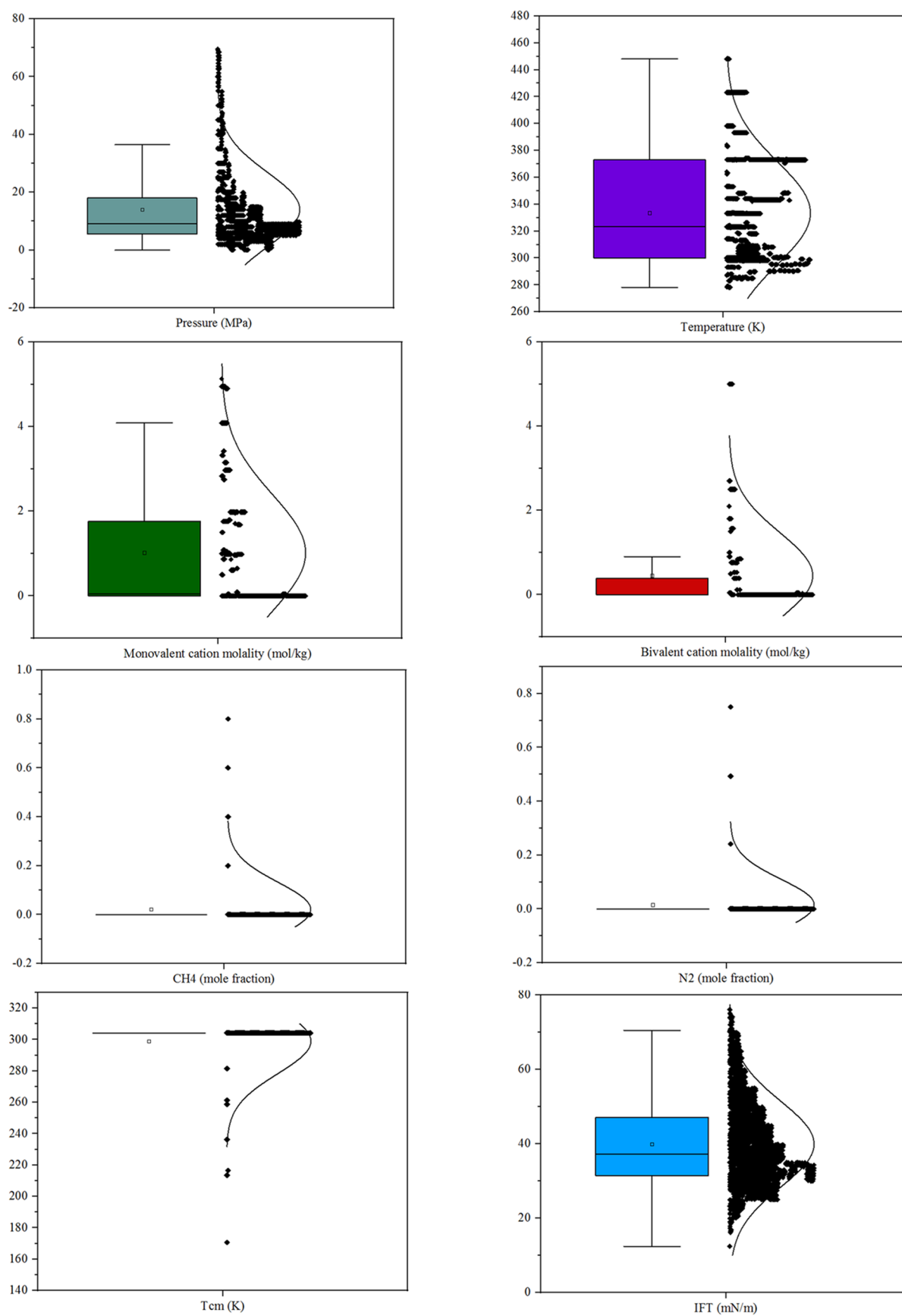


Figure 2. Box plots of all variables present within the database utilized in this study.

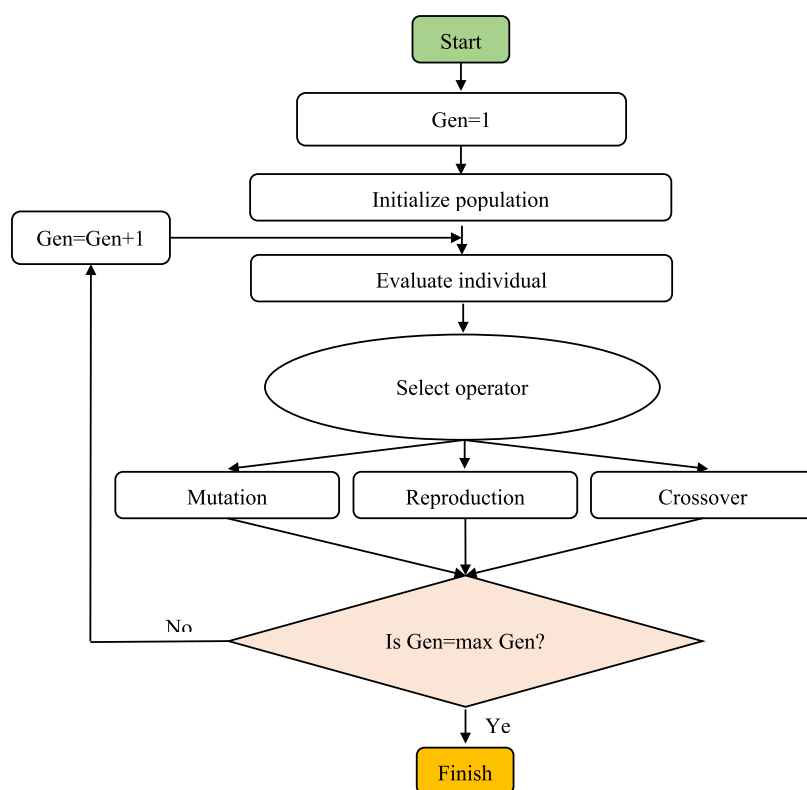


Figure 3. Flowchart of the GP approach.

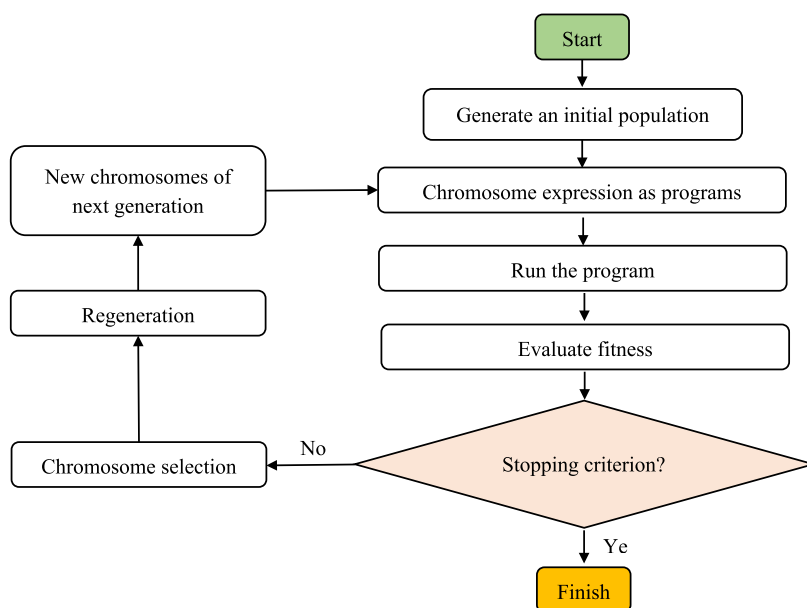


Figure 4. Flowchart of the GEP approach.

include both one- and two-point recombination techniques. The process is enriched by a mutation operation, which substantially impacts GEP's genomic makeup by substituting one element for another. Additionally, the concept of transposition and insertion is integrated, allowing specific sections of a chromosome's genome to be activated and repositioned.<sup>79</sup> These steps, encompassing fitness evaluation, selection, recombination, mutation, and genomic manipulation, are iteratively undertaken until a predefined termination

criterion is satisfied. Figure 4 shows the flowchart of the GEP approach.

**3.3. Group Method of Data Handling (GMDH).** Ivakhnenko<sup>82</sup> pioneered the GMDH technique, an approach designed to model intricate systems characterized by multifaceted input data converging into a singular output. The fundamental objective of the GMDH approach involves constructing a feed-forward system function through the utilization of a second-order transfer function. This technique establishes the number of hidden layers, the number of

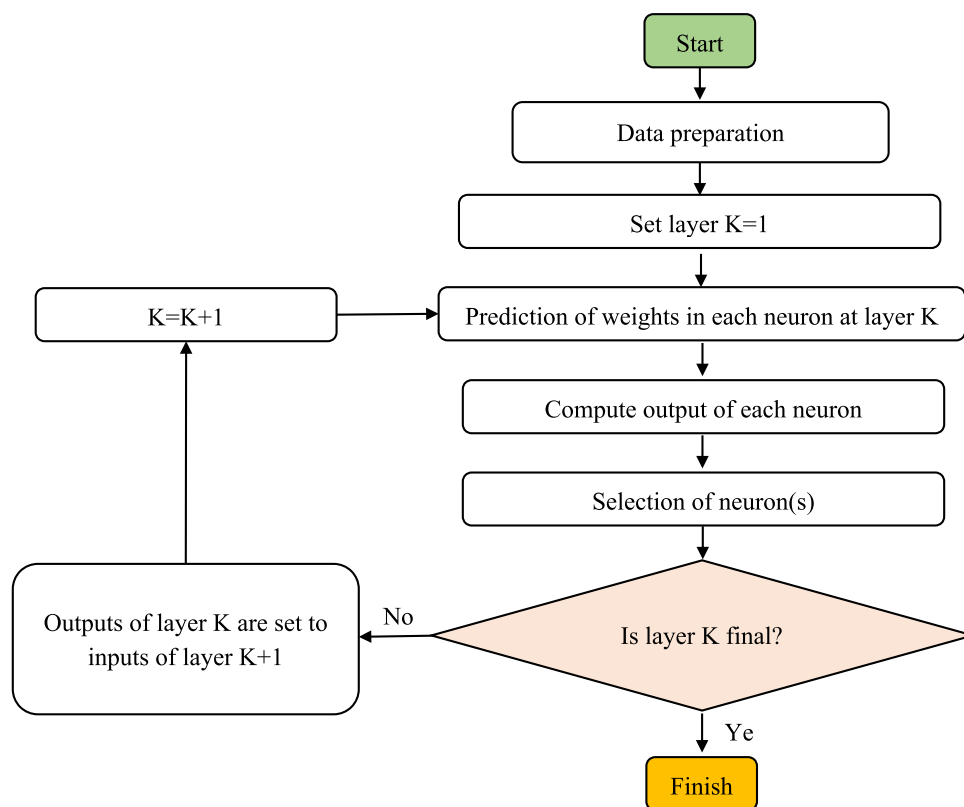


Figure 5. Flowchart of the GMDH approach.

neurons within those layers, and the most suitable model configuration. The interrelation between the dependent and independent variables in GMDH is represented by a nonlinear function termed the Volterra series, formulated as eq 2. To evaluate the Volterra series as a two-variable second-order polynomial, eq 3 is employed:<sup>83</sup>

$$\hat{y} = a_0 + \sum_{i=1}^m a_i x_i + \sum_{i=1}^m \sum_{j=1}^m a_{ij} x_i x_j + \sum_{i=1}^m \sum_{j=1}^m \sum_{k=1}^m x_j a_{ijk} x_i x_j x_k \dots \quad (2)$$

$$G(x_i, x_j) = a_0 + a_1 x_i + a_2 x_j + a_3 x_i^2 + a_4 x_j^2 + a_5 x_i x_j \quad (3)$$

The objective of the GMDH approach is to ascertain the unspecified parameters, denoted as  $a_i$ , within the Volterra series. These  $a_i$  parameters are computed for every pairing of input variables  $x_i$  and  $x_j$  inputs using regression methodologies.<sup>84,85</sup> Building upon this principle and accounting for

the notion of least-squares error, the  $G$  function can be formulated as follows for a given set of  $M$  observations involving multi-input and single-output data pairs:<sup>86,87</sup>

$$E = \frac{\sum_{i=1}^M (y_i - G_i O)^2}{M} \quad (4)$$

$$y_i = f(x_{i1}, x_{i2}, \dots, x_{im}), \quad i = 1, 2, \dots, m \quad (5)$$

A simple flowchart of the GMDH algorithm is shown in Figure 5.

## 4. RESULTS AND DISCUSSION

**4.1. Developed Correlations.** As previously indicated, the utilization of GP, GEP, and GMDH led to the creation of numerous equations by considering five and six input parameters to estimate impure and pure CO<sub>2</sub> and brine IFT. The formulated equations are outlined as follows:

GP correlation (6 inputs):

$$\text{IFT} = \left( \left( c_0 * \text{BCM} + c_1 * P + c_2 * \text{MCM} + \exp(c_3 * \text{CH}_4) * c_4 + \frac{c_5 * T}{(c_6 * P + c_7)} + \frac{c_8}{(c_9 * N_2 + c_{10})} + c_{11} \right) * c_{12} + c_{13} \right) \quad (6)$$

$$\begin{aligned} c_0 &= 1.7933 \\ c_1 &= 0.02595 \\ c_2 &= 1.0789 \\ c_3 &= 0.375 \\ c_4 &= 25.226 \\ c_5 &= 1.227 \\ c_6 &= 3.603 \end{aligned}$$

$$\begin{aligned} c_7 &= 14.895 \\ c_8 &= 1.0291 \\ c_9 &= -0.007072 \\ c_{10} &= -0.02436 \\ c_{11} &= 24.592 \\ c_{12} &= 2.0911 \\ c_{13} &= 0.014857 \end{aligned}$$

GP correlation (5 inputs):

$$\text{IFT} = \left( \left( c_0 * T_{\text{cm}} + c_1 * \text{MCM} + c_2 * \text{BCM} + \frac{c_3 * T_{\text{cm}}}{(c_4 * P + c_5)} + \frac{c_6 * T}{(c_7 * P + c_8)} + c_9 \right) + c_{10} \right) \quad (7)$$

$$c_0 = -0.14747 \\ c_1 = 2.5728$$

$$c_2 = 4.5562 \\ c_3 = -0.29192 \\ c_4 = -0.9349 \\ c_5 = -3.3606 \\ c_6 = -0.29668 \\ c_7 = -0.86023 \\ c_8 = -3.3606 \\ c_9 = 62.314 \\ c_{10} = 4.7827 \times 10^{-9} \\ \text{GEP correlation (6 inputs):}$$

$$\text{IFT} = \left( \frac{1}{T * \left( c_1 * T + \frac{(c_2 * \text{MCM} + c_3 * \text{BCM} + c_4)}{c_5 * P} + c_6 \right) * (c_7 * N_2 + c_8) * (c_9 * \text{BCM} + (c_{10} * \text{MCM} + c_{11}) * (c_{12} * \text{CH}_4 + c_{13}) + c_{14}) * c_{15}} + c_{16} \right) \quad (8)$$

$$c_1 = -0.017632 \\ c_2 = -1.4104 \\ c_3 = -2.4452 \\ c_4 = -16.302 \\ c_5 = -0.55608 \\ c_6 = 14.208 \\ c_7 = 1.648 \\ c_8 = 1.9531 \\ c_9 = -2.5993$$

$$c_{10} = -0.37481 \\ c_{11} = -13.088 \\ c_{12} = 2.057 \\ c_{13} = 3.8507 \\ c_{14} = 18.404 \\ c_{15} = 9.3247 \times 10^{-8} \\ c_{16} = 78.36 \\ \text{GEP correlation (5 inputs):}$$

$$\text{IFT} = \left( \frac{\left( c_0 * \text{MCM} + c_1 * \text{BCM} + \frac{T_{\text{cm}} * P * c_2}{(c_3 * P + \frac{c_4 * T}{c_5 * T_{\text{cm}}})} + c_6 \right)}{c_7 * T} + c_8 \right) \quad (9)$$

$$c_0 = 1446.8 \\ c_1 = 2461.0 \\ c_2 = 356.77 \\ c_3 = -3.0301 \\ c_4 = 2.4591$$

$$c_5 = -0.21942 \\ c_6 = 16147.0 \\ c_7 = 1.8543 \\ c_8 = 48.195 \\ \text{GMDH correlation (6 inputs):}$$

$$\begin{aligned} Y1 &= -237.329 + N12 * 8.59043 - N12 * N3 * 0.029114 - N12^2 * 0.0683583 + N3 * 2.32834 - N3^2 * 0.00170334 \\ N3 &= -5.70709 + N4 * 0.945527 + N4 * N7 * 0.0422513 - N4^2 * 0.0241664 + N7 * 0.242468 - N7^2 * 0.0187927 \\ N4 &= -42.6855 - N8 * 1.61476 - N8 * N10 * 0.00503938 + N8^2 * 0.0359466 + N10 * 3.40845 - N10^2 * 0.0254462 \\ N7 &= 60.3427 + \text{MCM} * N9 * 0.0398817 + \text{MCM}^2 * 0.129818 - N9 * 2.41246 + N9^2 * 0.0444492 \\ N8 &= -131.961 - P * 1.61189 + P^2 * 0.0194535 + T * 1.01047 - T^2 * 0.00132743 \\ N9 &= 52.8677 - P * 1.50791 + P * \text{BCM} * 0.0254271 + P^2 * 0.0188808 + \text{BCM} * 1.96934 + \text{BCM}^2 * 0.20259 \\ N10 &= 38.635 - \text{MCM} * 1.5212 + \text{MCM} * \text{BCM} * 3.24198 + \text{MCM}^2 * 0.517975 + \text{BCM}^2 * 0.516763 \\ N12 &= 39.3559 + (\text{CH}_4)^2 * 25.6457 + (N_2)^2 * 24.5578 \end{aligned} \quad (10)$$

GMDH correlation (5 inputs):



$$\begin{aligned}
Y1 &= -7.1885 + N7^*0.689503 - N7^*N2^*0.0131058 + N2^*0.626504 + (N2)^{2^*}0.00974851 \\
N2 &= -14.6423 + P^*0.706114 - P^*N3^*0.0138623 - P^{2^*}0.00531772 + N3^*1.53122 - (N3)^{2^*}0.00456879 \\
N3 &= -5.28129 + MCM^*5.23378 - MCM^*N4^*0.0590986 - MCM^{2^*}0.738552 + N4^*1.11658 \\
N4 &= 18.5756 - N13^*2.47684 - N13^*N6^*0.0738438 + (N13)^{2^*}0.0658759 + N6^*2.66314 + (N6)^{2^*}0.0157403 \\
N6 &= -227.611 + T^*1.05442 - T^*N9^*0.00392383 - T^{2^*}0.00122593 + N9^*2.90394 - (N9)^{2^*}0.00581509 \\
N7 &= -42.6855 - N12^*1.61476 - N12^*N14^*0.00503938 + (N12)^{2^*}0.0359466 + N14^*3.40845 - (N14)^{2^*}0.0254462 \\
N9 &= -135.413 - N11^*2.43339 + N11^*N15^*0.00798595 + (N11)^{2^*}0.041285 + N15^*8.00916 - (N15)^{2^*}0.0802109 \\
N11 &= 52.8677 - P^*1.50791 + P^*BCM^*0.0254271 + P^{2^*}0.0188808 + BCM^*1.96934 + BCM^{2^*}0.20259 \\
N12 &= -131.961 - P^*1.61189 + P^{2^*}0.0194535 + T^*1.01047 - T^{2^*}0.00132743 \\
N13 &= 61.9661 + BCM^*Tcm^*0.0122519 - BCM^{2^*}0.268553 - Tcm^{2^*}0.000260694 \\
N14 &= 38.635 - MCM^*1.5212 + MCM^*BCM^*3.24198 + MCM^{2^*}0.517975 + BCM^{2^*}0.516763 \\
N15 &= 61.3114 - MCM^*5.51071 + MCM^*Tcm^*0.015966 + MCM^{2^*}0.5061 - Tcm^{2^*}0.000247395
\end{aligned} \tag{11}$$

where  $T$  is the temperature (K),  $P$  is the pressure (MPa), MCM stands for monovalent cation molality (mol/kg), BCM stands for bivalent cation molality (mol/kg),  $T_{cm}$  is the pseudocritical temperature of the gaseous mixture, and  $N_2$  and  $CH_4$  show mole fractions of  $N_2$  and  $CH_4$  within the injected gas, respectively.

**4.2. Assessment of the Correlations.** Using seven statistical indicators, we assessed the precision of the proposed models. The study incorporated the following metrics for evaluation:<sup>88</sup>

1. Mean absolute percentage error (MAPE, %): MAPE measures the average percentage difference between predicted and actual values, indicating the overall accuracy of the model.

$$MAPE = \frac{1}{n} \sum_{i=1}^n \text{abs} \left( \left[ \frac{(y)_{\text{exp}} - (y)_{\text{pred}}}{y_{\text{exp}}} \right] \right) \times 100 \tag{12}$$

2. Standard deviation (SD): SD quantifies the dispersion or spread of predicted values around the actual values, giving insight into the variability of the model's performance.

$$SD = \sqrt{\frac{1}{n-1} \sum_{i=1}^n \left( \frac{y_{\text{exp}} - y_{\text{pred}}}{y_{\text{exp}}} \right)^2} \tag{13}$$

3. Root mean square error (RMSE): RMSE calculates the average magnitude of the differences between predicted and actual values, reflecting the model's overall prediction error.

$$RMSE = \sqrt{\frac{1}{n} \sum_{i=1}^n (y_{\text{exp}} - y_{\text{pred}})^2} \tag{14}$$

4. Determination coefficient ( $R^2$ ):  $R^2$  assesses the proportion of variance in the dependent variable that is

explained by the independent variables in the model. It indicates how well the model fits the data.

$$R^2 = 1 - \frac{\sum_{i=1}^N (y_{\text{exp}} - y_{\text{pred}})^2}{\sum_{i=1}^N (y_{\text{exp}} - \bar{y}_{\text{exp}})^2} \tag{15}$$

in this context,  $N$  represents the number of data,  $y_{\text{exp}}$  denotes the experimental data, and  $y_{\text{pred}}$  signifies the data predicted by the correlations proposed in the study.

5. Mean absolute error (MAE): MAE computes the average absolute differences between predicted and actual values, providing a measure of the average prediction error. This assessment corresponds to a risk evaluation that mirrors the expected outcome of the absolute error loss or  $l_1$ -norm loss. If  $\hat{y}_i$  represents the expected outcome of the  $i$ th instance, and  $y_i$  denotes the corresponding actual value, the computed MAE for a total of " $n_{\text{data}}$ " can be expressed as follows:

$$MAE = \frac{1}{n} \sum_{i=1}^n |y_i - \hat{y}_i| \tag{16}$$

6. Mean bias error (MBE): MBE calculates the average difference between predicted and actual values, indicating the overall bias or tendency of the model to overestimate or underestimate.

$$MBE = \frac{1}{n} \sum_{i=1}^n (\hat{y}_i - y_i) \tag{17}$$

7. Nash–Sutcliffe efficiency (NSE): NSE evaluates the model's performance by comparing the predicted values to the mean observed value. It assesses how well the model captures the variation in the observed data.

$$NSE = 1 - \frac{\sum_{i=1}^n (y_o^t - y_m^t)^2}{\sum_{i=1}^n (y_o^t - \bar{y}_o)^2} \tag{18}$$

Table 2. Results of Statistical Error Analysis for All Models

statistical criteria		RMSE	SD	R <sup>2</sup>	MAPE (%)	MBE	MAE	NSE
GP (6 inputs)	test	4.8733	0.1389	0.8379	9.8978	−0.1404	3.6904	0.8151
	train	4.4064	0.1169	0.8495	8.4081	0.0352	3.2446	0.8204
	all	4.5038	0.1217	0.8470	8.7064	4.1 × 10 <sup>−13</sup>	3.3339	0.8193
GEP (6 inputs)	test	4.2900	0.1296	0.8744	9.2988	−0.0469	3.3839	0.8567
	train	4.1060	0.1106	0.8693	8.0647	0.0631	3.0523	0.8489
	all	4.1435	0.1147	0.8705	8.3119	0.0410	3.1187	0.8507
GMDH (6 inputs)	test	4.9537	0.1497	0.8326	10.3991	−0.1281	3.7652	0.8055
	train	4.6396	0.1296	0.8331	9.5159	0.0321	3.5744	0.7977
	all	4.7042	0.1339	0.8330	9.6928	−2.3 × 10 <sup>−11</sup>	3.6126	0.7996
GP (5 inputs)	test	4.7648	0.1424	0.8410	10.3019	−0.0889	3.7533	0.8203
	train	4.4857	0.1241	0.8451	9.0998	0.0223	3.4299	0.8141
	all	4.5430	0.1280	0.8443	9.3405	−2.9 × 10 <sup>−11</sup>	3.4947	0.8156
GEP (5 inputs)	test	4.2197	0.1305	0.8785	9.1968	−0.0516	3.3016	0.8628
	train	3.9132	0.1124	0.8813	8.0600	0.0129	2.9911	0.8650
	all	3.9764	0.1163	0.8807	8.2877	1.7 × 10 <sup>−13</sup>	3.0533	0.8645
GMDH (5 inputs)	test	3.7919	0.1095	0.8943	7.6343	0.1059	2.8170	0.8803
	train	3.5825	0.1020	0.9025	7.3111	−0.0265	2.7166	0.8923
	all	3.6254	0.1035	0.9008	7.3759	1.9 × 10 <sup>−14</sup>	2.7367	0.8899

Here,  $\bar{y}_o$  represents the mean of observed data, while  $y_m$  signifies the simulated data. Additionally,  $y_o^t$  denotes the data being released at time instant  $t$ .

These metrics collectively provide a comprehensive evaluation of the accuracy and reliability of the suggested correlations in predicting the desired outcomes. The computed values of the aforementioned statistical parameters are listed in Table 2. Based on the statistical assessment presented in Table 2, it is evident that the GMDH correlation utilizing five inputs has demonstrated the utmost precision and dependability across all indicators. Notably, its MAPE values for the testing, training, and complete data sets are recorded at 7.63, 7.31, and 7.38%, respectively. On the other hand, in the case of six-input models, the GEP correlation displayed the highest precision, with MAPE values of 9.30, 8.06, and 8.31 for the testing, training, and total data sets, respectively. Taking into account all of the statistical parameters, the sequence of correlations based on accuracy is as follows: GMDH (5 inputs), GEP (5 inputs), GEP (6 inputs), GP (6 inputs), GP (5 inputs), and GMDH (6 inputs). The consolidated approach (5 inputs), which utilizes Tcm of a gaseous mixture rather than treating CH<sub>4</sub> and N<sub>2</sub> as separate input variables, effectively captures the essence of its constituents, represents impurities in CO<sub>2</sub>-containing gas, and reduces the complexity of mathematical models with higher accuracy compared to those involving six inputs.

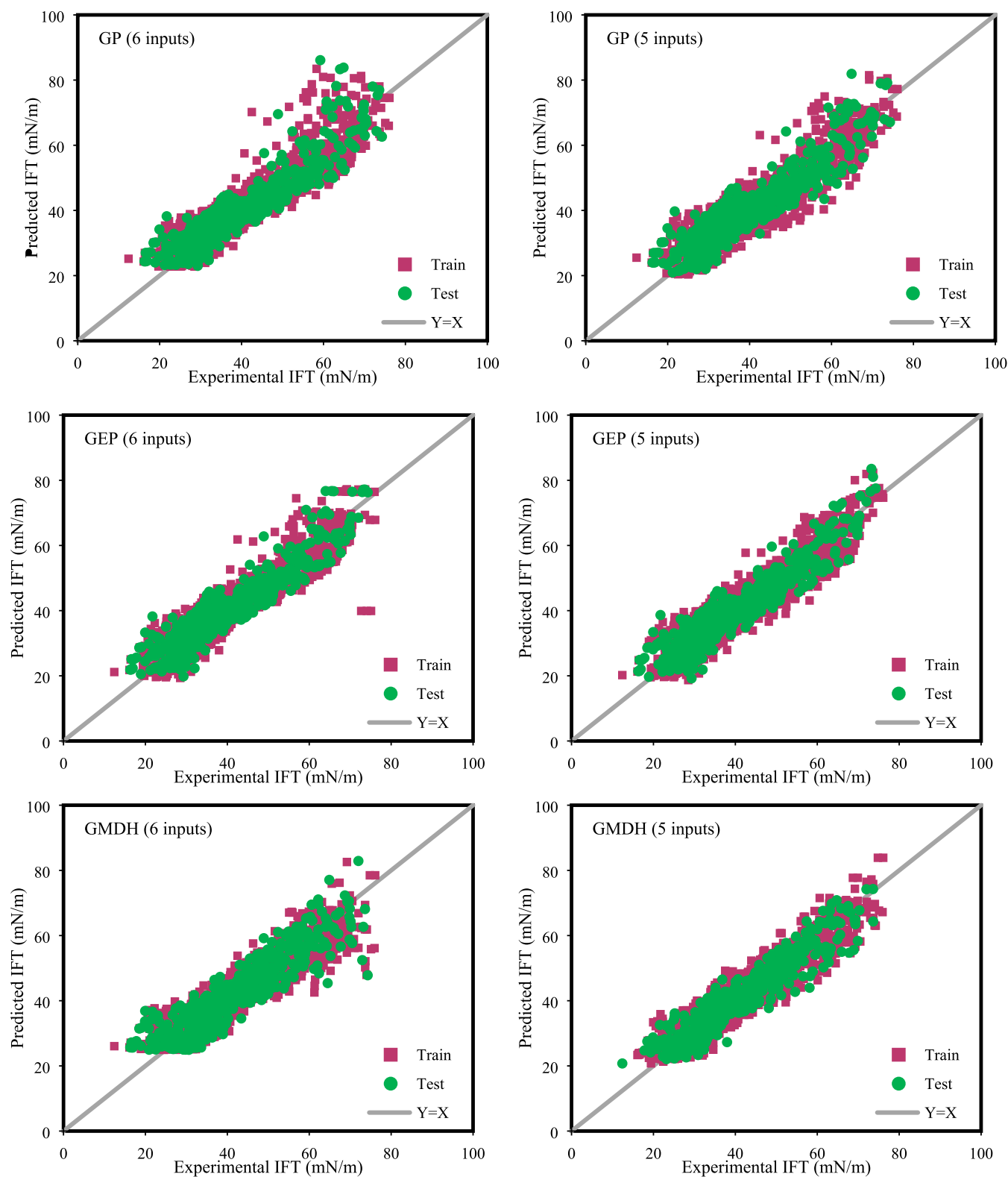
Moving forward, a graphical examination can be employed to evaluate the precision of the suggested correlations. To initiate this investigation, graphical representations showcasing the cross-plots of IFT values predicted by the correlations against the corresponding experimental values were depicted in Figure 6. Within the cross-plots, a significant clustering of data points around the  $X = Y$  reference line is observed across all models, indicative of the correlations' commendable accuracy. Notably, the GMDH model formulated with five inputs exhibits a notably enhanced concentration around the  $X = Y$  line, underscoring its superior predictive capability for the CO<sub>2</sub>-brine interfacial tension.

Furthermore, Figure 7 provides insight into the distribution of errors during both the testing and training phases of the models. A thorough examination of the error distribution

graphs reveals the absence of any discernible error pattern with the majority of computed errors clustering around the zero-error line. Notably, the GMDH model constructed using five inputs exhibits a reduced dispersion of errors compared to the other models, underscoring its elevated accuracy in predicting the IFT of both impure and pure CO<sub>2</sub>-brine systems.

After the analyses outlined in this study were conducted, a cumulative frequency plot depicting the entirety of the data against absolute error values has been generated for all predictive correlations, as depicted in Figure 8. This visual representation reveals that over 70% of the predicted IFT data using all correlations exhibit an absolute error of less than 10%. Furthermore, more than 90% of the predicted data demonstrate an absolute error of less than 20%. In contrast, the GMDH model employing five inputs displays absolute errors of approximately 8 and 15% for 70% and 90% of the IFT data, respectively. This highlights the exceptional accuracy of the GMDH correlation when compared to the other correlations.

**4.3. Trend Analysis.** During the following stage of graphical analysis, the accuracy of the most well-established correlations, specifically GMDH (employing 5 inputs) and GEP (employing 6 inputs), is examined for their ability to predict the expected physical trend of IFT in CO<sub>2</sub>-brine systems. Initially, the impact of the pressure on IFT measurements is investigated for a pure CO<sub>2</sub> and brine system. This assessment is conducted under a consistent temperature of 333 K, encompassing a wide pressure spectrum ranging from 1 to 68 MPa. The system under consideration maintains a monovalent cation molality of 1.98 mol/kg, while the divalent cation molality remains at zero, aligning with experimental observations detailed in the literature.<sup>68</sup> The objective is to employ established correlations to project the experimental outcomes. As illustrated in Figure 9, the overall IFT of the CO<sub>2</sub>-brine system experiences a decline as the pressure increases. The trend of IFT reduction with respect to pressure reveals two discernible segments: an initial sharp decline, succeeded by a considerably gradual decrease within a subsequent pseudo-steady plateau phase. CO<sub>2</sub> possesses critical conditions at a temperature of 304.2 K and a pressure of 7.38 MPa.<sup>89</sup> For the examined system at a constant



**Figure 6.** Cross-plots of the developed correlations.

temperature of 333 K, which surpasses the critical temperature of  $\text{CO}_2$ , the state of  $\text{CO}_2$  is influenced by pressure. When the pressure remains below the critical pressure of  $\text{CO}_2$ , the  $\text{CO}_2$  exists in a gaseous phase. However, as the pressure surpasses the critical point,  $\text{CO}_2$  transitions into a supercritical state. In this context, the IFT displays a distinct behavior. At lower pressures, the IFT experiences a sharp decrease. This is

primarily attributed to the enhancing (partial) dissolution of  $\text{CO}_2$  gas within the aqueous phase coupled with its heightened affinity for adsorption at the interface with rising pressure. As pressure continues to rise, the  $\text{CO}_2$ -brine IFT reaches a pseudo-plateau, coinciding with the point at which  $\text{CO}_2$  enters the supercritical state. Other researchers have also documented this phenomenon for the supercritical or liquid phase of

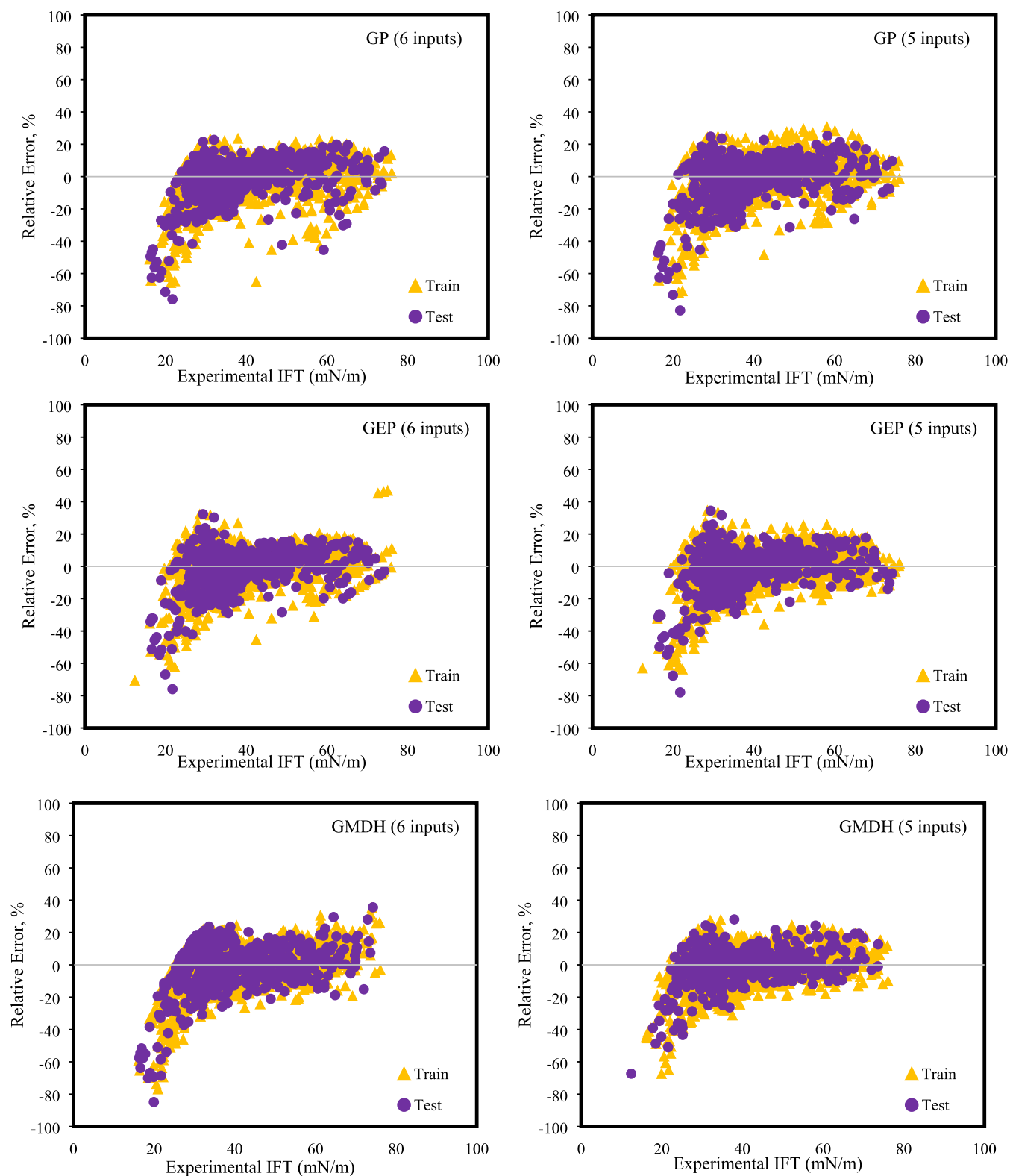


Figure 7. Error distribution plots of the developed correlations.

CO<sub>2</sub>.<sup>28,42,63,69,28,42,63,69</sup> During the supercritical or liquid phase, CO<sub>2</sub> transforms into a semifluid state with minimal or no compressibility, leading to nearly constant density differences within the CO<sub>2</sub>-brine. Notably, the IFT of the CO<sub>2</sub>-brine exhibits limited pressure dependency after achieving the pseudo-plateau state. Overall, the intricate temperature and pressure interactions impacting the IFT of CO<sub>2</sub>-brine are

found to be more intricate than was theoretically expected. This complexity can be attributed to the phase changes of CO<sub>2</sub> and its solubility effects within the brine, influenced by alterations in pressure and temperature.<sup>63</sup> As illustrated in Figure 9, both correlations effectively capture the trend of decreasing IFT with increasing pressure and provide accurate estimations.

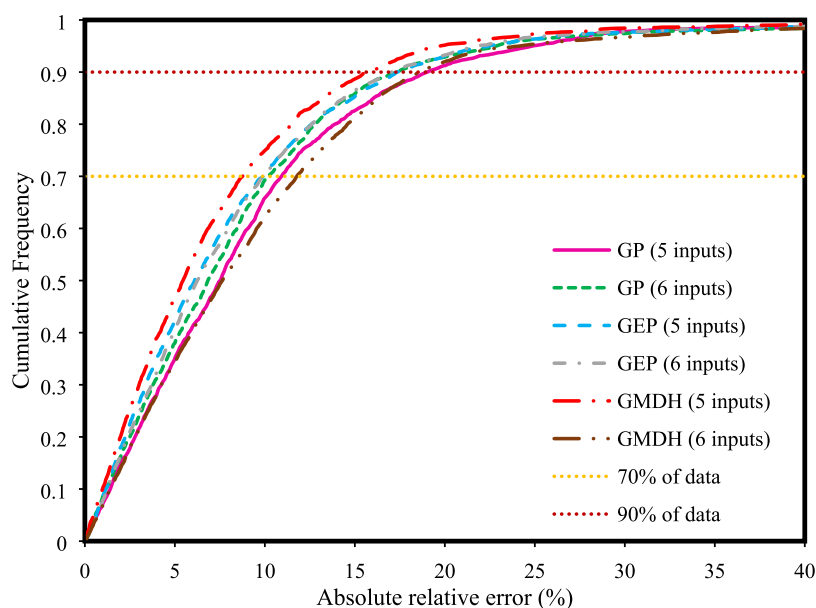


Figure 8. Cumulative frequency plot of the developed correlations.

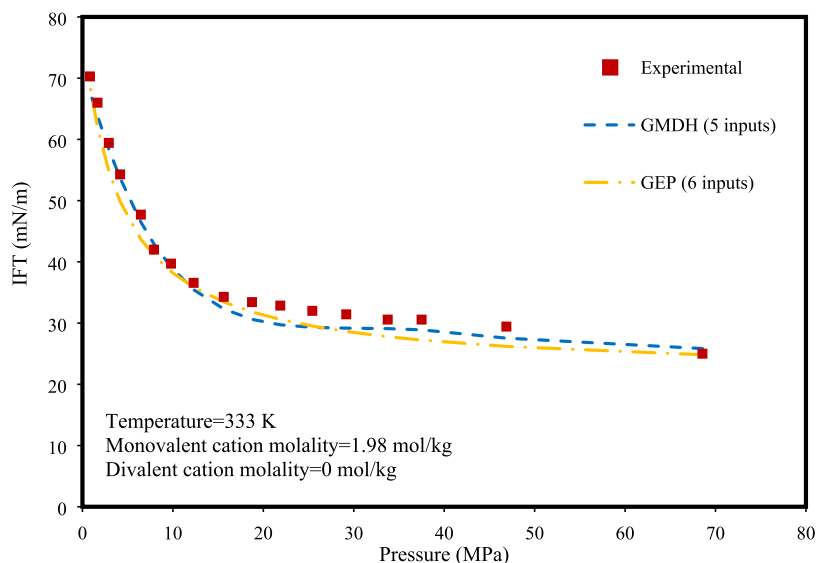


Figure 9. Experimental data<sup>68</sup> and prediction of correlations for the impact of pressure on IFT of a pure CO<sub>2</sub>-brine system.

The subsequent analysis involves examining the influence of the temperature on the IFT of a pure CO<sub>2</sub>-brine system composed of NaCl and KCl. This investigation maintains a monovalent cation molality of 1.98 mol/kg, while the divalent cation molality remains at zero. This experimental setup aligns with prior research detailed in the literature.<sup>63</sup> As depicted in Figure 10, there is a general trend of increasing the IFT for the CO<sub>2</sub>-brine system as the temperature rises. This phenomenon is accurately captured by correlations, demonstrating low error in their predictions. While the presented example indicates an increasing trend, it is crucial to acknowledge that the impact of temperature on the CO<sub>2</sub>-brine IFT is not always like this. In fact, the relationship between temperature and the CO<sub>2</sub>-brine IFT is nonmonotonic, meaning it does not follow a consistent upward or downward trajectory. This behavior has been observed in various studies. The effect of temperature on IFT can vary based on the specific temperature and pressure ranges. In some cases, increasing temperature may lead to an increase

in IFT, while in others, it could result in a decrease or no significant change in IFT.<sup>42,51,55,63</sup> This complex behavior is attributed to factors such as solubility changes and phase alterations induced by temperature and pressure variations. The interplay of these factors contributes to the intricate behavior of CO<sub>2</sub>-brine IFT under different conditions.<sup>63</sup>

Moving forward, the investigation delves into the impact of salinity on the CO<sub>2</sub>-brine IFT under constant temperature and pressure conditions. The objective is to evaluate the predictive capabilities of correlations in capturing IFT variations with changing salinity. To accomplish this, multiple CO<sub>2</sub>-brine systems with different salinities are considered, featuring equivalent molalities of monovalent and divalent cations, as illustrated in Figure 11. This experimental setup aligns with prior research detailed in the literature.<sup>55</sup> An established notion suggests that as water salinity increases, the solubility of CO<sub>2</sub> in brine decreases.<sup>90</sup> Consequently, the IFT between CO<sub>2</sub> and brine exhibits a consistent upward trend in response to salinity

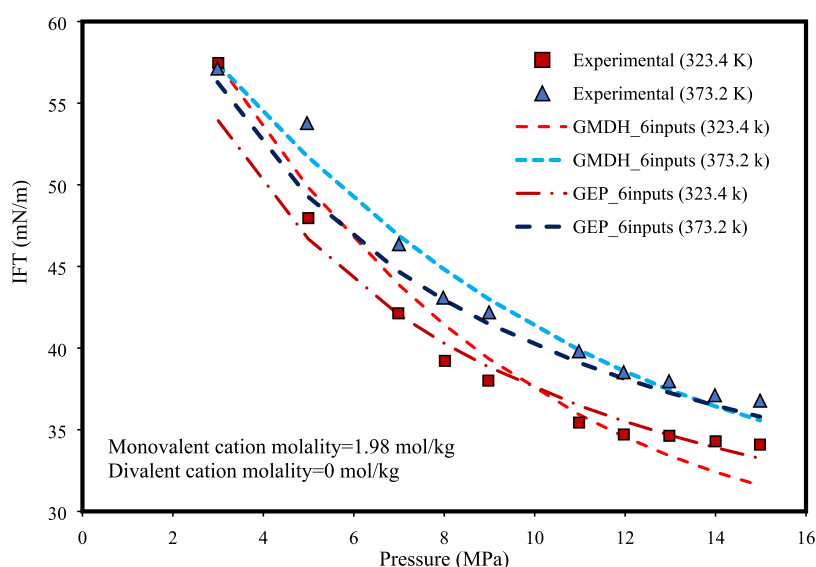


Figure 10. Experimental data<sup>63</sup> and prediction of correlations for the impact of temperature on IFT of a pure CO<sub>2</sub>-brine system.

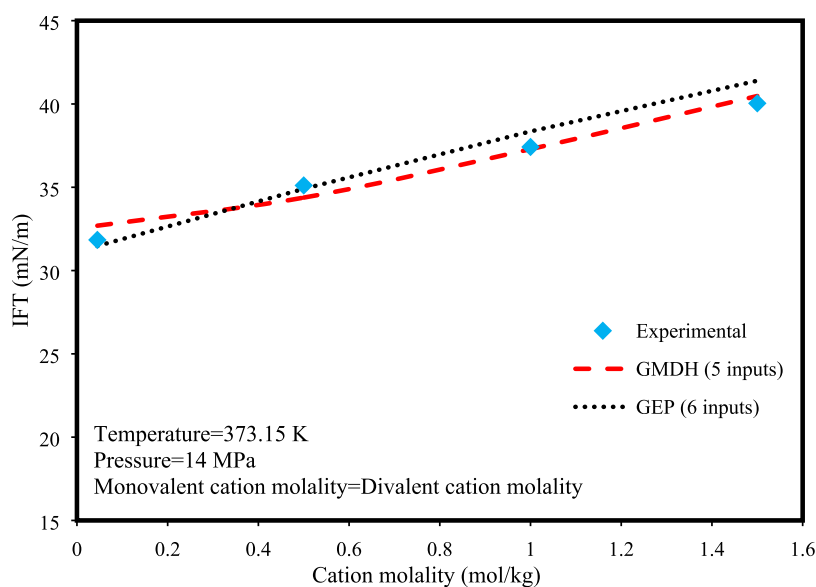


Figure 11. Experimental data<sup>55</sup> and prediction of correlations for the impact of salinity on IFT of a pure CO<sub>2</sub>-brine system.

changes, regardless of the specific salt type. The mechanism underlying this behavior is intertwined with the distribution of cations within the aqueous phase. Typically, cations exhibit a minimal affinity for accumulation at the interface, resulting in their concentration in the bulk aqueous phase. This leads to a negative adsorption phenomenon at the interface, causing a depletion of cations. Consequently, water molecules tend to migrate from the interface into the solution to compensate for this effect.<sup>91</sup> As a consequence of this interaction, the mutual solubility between CO<sub>2</sub> and water is diminished, ultimately contributing to an increase in the IFT between them. This intricate interplay between cation distribution, water-CO<sub>2</sub> mutual solubility, and resultant IFT behavior emphasizes the complexity of these phenomena.<sup>51</sup> As shown in Figure 11, again, the developed correlations exhibit a promising level of accuracy in capturing the aforementioned trends.

Subsequently, we turn our attention to investigating the influence of impurities present in a gas stream on the IFT within the systems of impure CO<sub>2</sub> and water. This analysis is

conducted under conditions of constant temperature and pressure. The objective is to gain insight into how the presence of impurities impacts the IFT between CO<sub>2</sub> and water. Taking into account the critical temperatures of CO<sub>2</sub>, CH<sub>4</sub>, and N<sub>2</sub> as 304.2, 190.85, and 126.2 K, respectively, the determination of Tcm can be achieved using eq 1. This calculation involves considering different compositions of CH<sub>4</sub>, N<sub>2</sub>, and CO<sub>2</sub>. Given the substantial variance between the critical temperatures of these impurities and those of pure CO<sub>2</sub>, it follows that the Tcm for an impure mixture is notably less than that of pure CO<sub>2</sub> gas. Consequently, a reduced Tcm indicates a diminished CO<sub>2</sub> composition while signifying an increased prevalence of impurities within the gas stream.<sup>31,33,43</sup> Figure 12 visually represents the influence of impurities on the IFT of CO<sub>2</sub>-water under a constant pressure of 15 MPa and a temperature of 313.15 K, as experimentally investigated in the literature.<sup>31,33</sup> Additionally, the predictions generated by GMDH (5 inputs) are presented in the same context. The depicted figure underscores the accurate representation by the GMDH

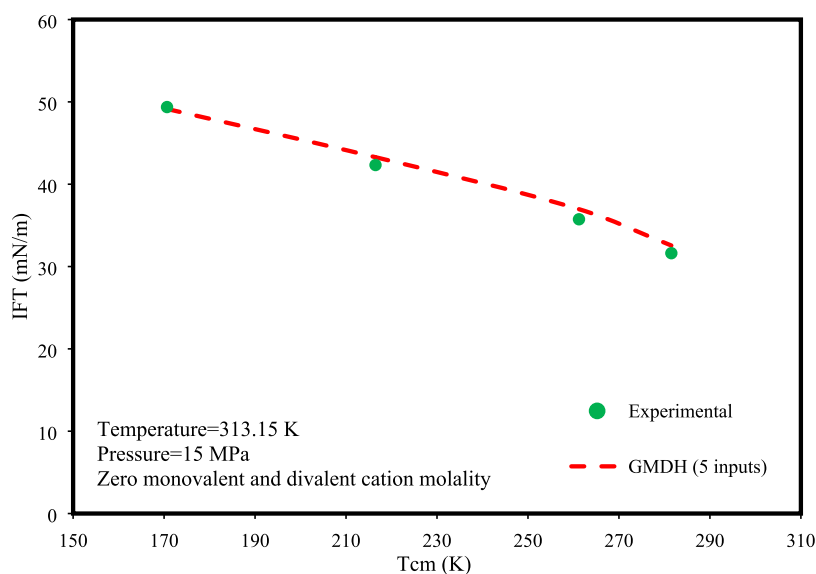


Figure 12. Experimental data<sup>31,33</sup> and prediction of GMDH correlation for the impact of impurities on IFT of impure CO<sub>2</sub>-water systems.

correlation of the escalating pattern in the IFT corresponding to the rise in impurities (or, inversely, the decline in T<sub>cm</sub>). The fundamental explanation for the observed IFT augmentation in the presence of non-CO<sub>2</sub> constituents lies in their diminished solubility, such as N<sub>2</sub>, in comparison to the notable solubility of CO<sub>2</sub> in water.<sup>27</sup>

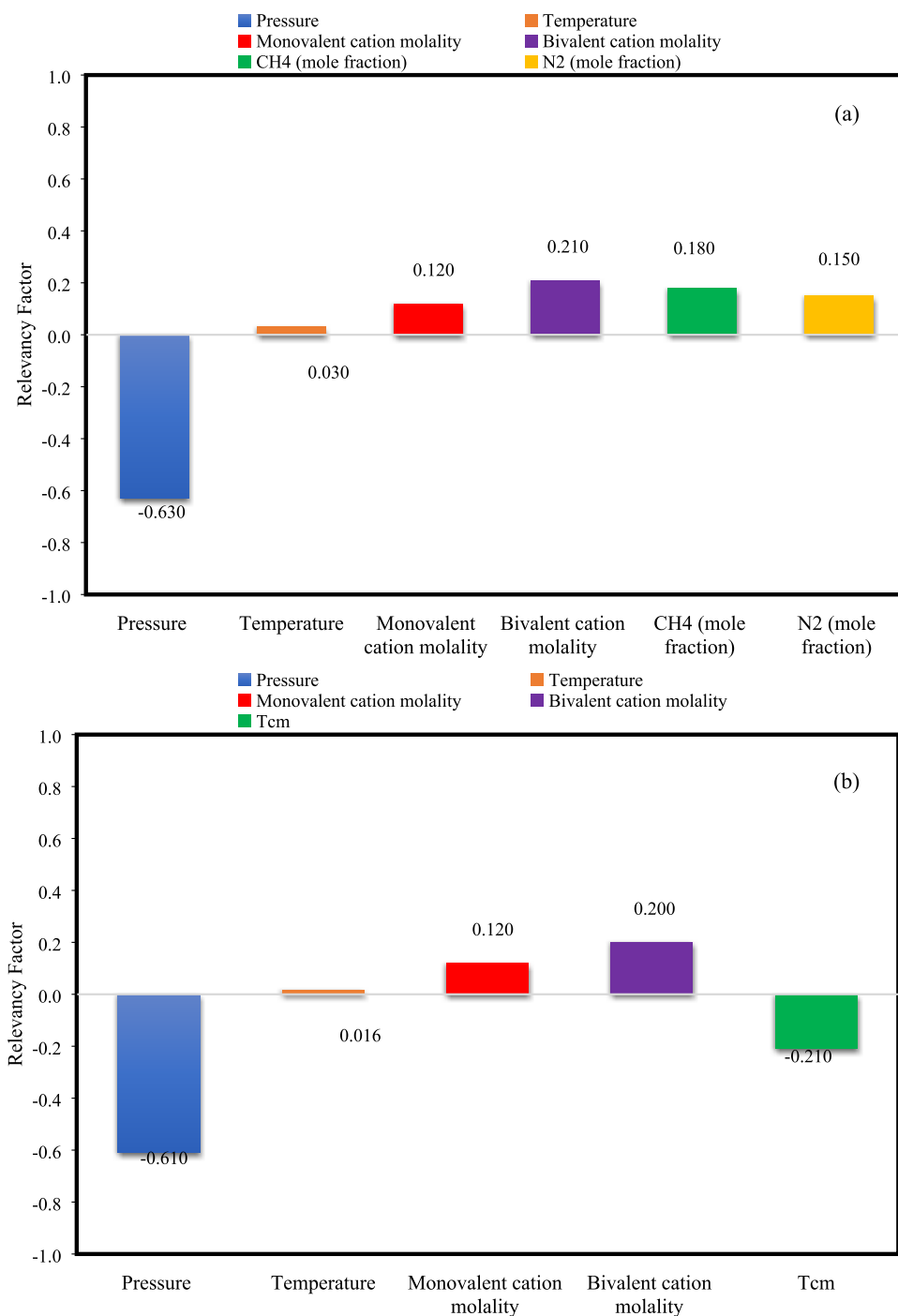
**4.4. Sensitivity Analysis.** In the context of parametric investigations, it is of great significance to ascertain the effects of various inputs on the resulting outcome. As a point to bear in mind, this study employed two distinct modeling methodologies, one involving 5 inputs and the other involving 6 inputs. The initial approach encompassed 6 inputs: temperature, pressure, monovalent cation molality, bivalent cation molality, mole fraction of N<sub>2</sub>, and mole fraction of CH<sub>4</sub> within the injected gas. Conversely, the second approach encompassed 5 inputs, specifically temperature, pressure, monovalent cation molality, bivalent cation molality, and T<sub>cm</sub> of the injected gas. In this context, the Pearson correlation coefficient<sup>92</sup> was calculated to determine the influence exerted by individual input variables on the response of both the GEP model (utilizing 6 inputs) and the GMDH model (utilizing 5 inputs), representing the most robust correlations established within this study. A greater value of the relevancy factor (*r*) associated with an input parameter signifies a more pronounced significance and impact on the IFT of CO<sub>2</sub>-brine. The ensuing equation was employed to quantify the relevance factor:<sup>93,94</sup>

$$r(\text{inp}_i, \text{IFT}) = \frac{\sum_{j=1}^n (\text{inp}_{i,j} - \text{inp}_{a,i})(\text{IFT}_j - \text{IFT}_a)}{\sqrt{\sum_{j=1}^n (\text{inp}_{i,j} - \text{inp}_{a,i})^2 \sum_{j=1}^n (\text{IFT}_j - \text{IFT}_a)^2}} \quad (19)$$

where  $\text{inp}_{a,i}$  and  $\text{inp}_{i,j}$  denote the average value and the *j*th value of the *i*th input, respectively (where *i* can represent any of the input variables). Also,  $\text{IFT}_j$  represents the *j*th value of estimated IFT data and  $\text{IFT}_a$  stands for the average value of the IFT data. Figure 13 portrays the comparative influences of the input variables under consideration on the IFT between CO<sub>2</sub> and brine. As depicted in Figure 13, it is evident in both modeling methodologies that pressure exhibited the most

substantial influence on the IFT of CO<sub>2</sub>-brine, demonstrating a detrimental effect. Conversely, within the framework of both modeling strategies, temperature is observed to exert the least pronounced impact on the IFT. Nevertheless, as temperature exhibits a nonmonotonic nature, we hold the view that the acquired coefficient modestly underestimates its influence. In Figure 13a, it is evident that the influence on IFT ranges from the highest to the lowest in the following order: pressure, bivalent cation molality, mole fraction of CH<sub>4</sub>, mole fraction of N<sub>2</sub>, monovalent cation molality, and temperature. On the other hand, Figure 13a shows that pressure, T<sub>cm</sub>, bivalent cation molality, monovalent cation molality, and temperature had the greatest to lowest influences on the IFT, respectively. Our analysis reveals a notable and adverse influence of the T<sub>cm</sub> of CO<sub>2</sub>-containing gas on the IFT between impure CO<sub>2</sub> and brine. This observation implies that any impurity possessing a T<sub>c</sub> lower than that of CO<sub>2</sub> leads to an elevation in the IFT within the system and conversely. Consequently, heightened impurity concentrations align with lower T<sub>cm</sub> values, consequently resulting in an elevated IFT. While this trend holds true for CH<sub>4</sub> and N<sub>2</sub>, it is essential to verify the universality of this pattern for other non-CO<sub>2</sub> components that were not part of the current investigation. To conclude, the monovalent and divalent cation molalities demonstrate an escalating influence on the IFT, with divalent cations notably indicating approximately double the impact of monovalent cations.

**4.5. Leverage Technique.** The Leverage approach<sup>95–97</sup> is a potent technique in statistical analysis for identifying influential data points within regression models. Central to this method are standardized residuals (*R*) and Hat matrix leverage (*H*), which quantify deviations of predicted values from real data and measure the influence of individual observations, respectively. Critical leverage (*H*<sup>\*</sup>) value establishes a threshold for identifying high-leverage points.<sup>98</sup> The Leverage approach's elements form a comprehensive framework for assessing model reliability and data quality in regression analysis. Set within the mathematical realm of  $-3 \leq R \leq 3$  and  $H \leq H^*$ , data points assume the distinguished role of “valid” representatives, resolutely navigating the intricate pathways of statistical thresholds. These valid data are in the



**Figure 13.** Sensitivity analysis using the results of (a) GEP (6 inputs) and (b) GMDH (5 inputs).

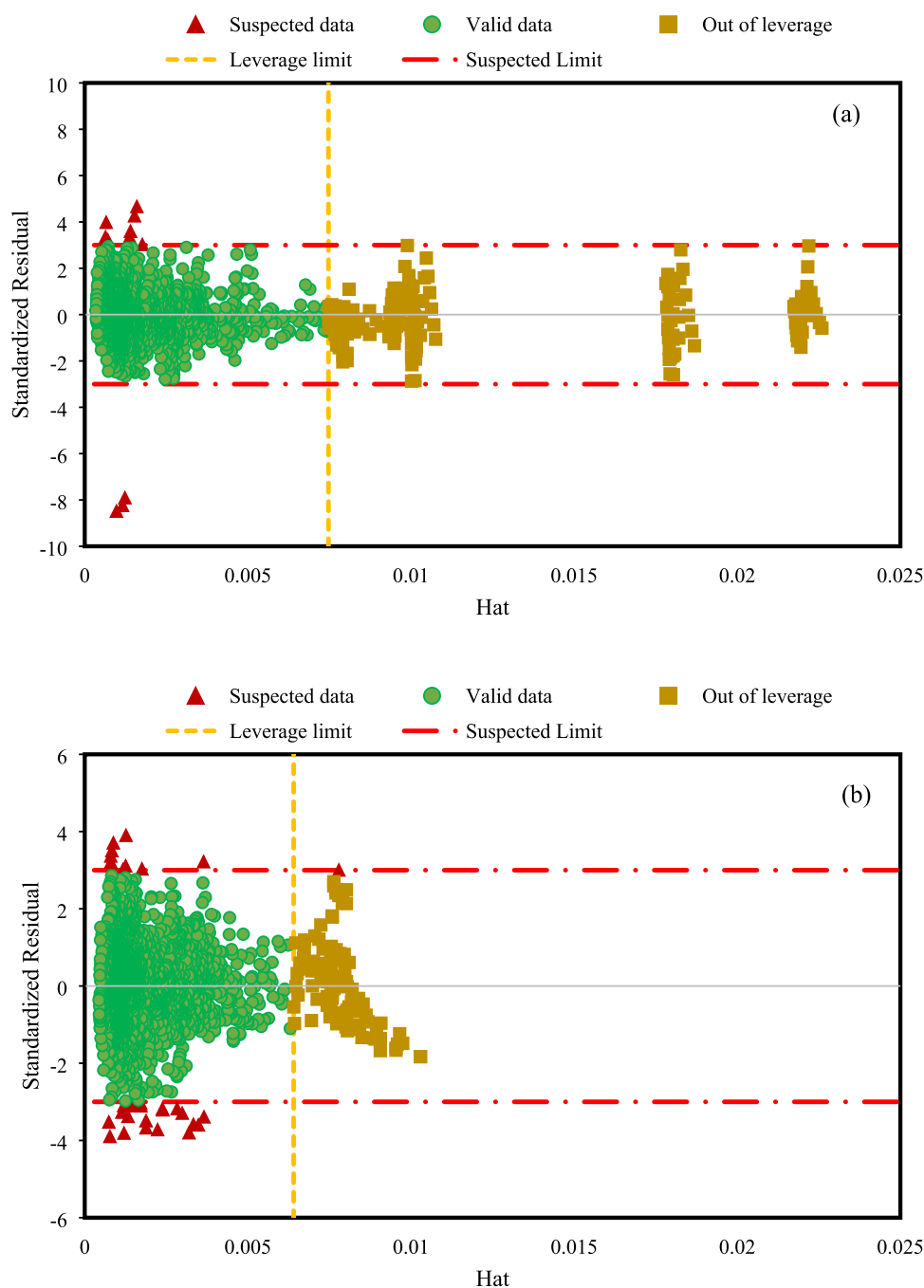
applicability domain of the model. Data points within  $-3 \leq R \leq 3$  and  $H^* \leq H$  are deemed “good high-leverage data”, which are outside of the applicability domain of the model extending beyond statistical bounds yet well-predicted by the model. In contrast, data points exceeding  $R$  values of 3 or falling below  $-3$  are categorized as “suspected” reflecting greater predictive uncertainty and are considered experimentally doubtful.<sup>99</sup> The utilization of William’s plot becomes viable for delineating the range of applicability for the GEP model (6 inputs) and the GMDH model (5 inputs), representing the most robust correlation established within this study, as illustrated in Figure 14. Both of these correlations exhibit the majority of data falling within the realm of validity, and they are duly

acknowledged for their credibility. The GEP model, featuring 6 inputs, showcased approximately 6.5% outliers alongside a mere 0.5% of suspected data. Similarly, the GMDH model, with 5 inputs, exhibited roughly 3.9% outliers and 1% suspected data. These findings collectively endorse the substantial application scope and reliability of both correlations, affirming the robust validity and reliability of the database employed in the modeling process.

## 5. SUMMARY AND CONCLUSIONS

This study employed three white-box machine learning (ML) models to forecast the IFT of the CO<sub>2</sub>-brine systems. A total of





**Figure 14.** Identification of applicability scope of correlations: (a) GEP (6 inputs) and (b) GMDH (5 inputs).

2811 experimental IFT data points, encompassing diverse pressure and temperature operational conditions, were gathered from literature sources. These data incorporated impurities from both the gas (primarily  $N_2$  and  $CH_4$ ) and aqueous phases (including monovalent and divalent salt types). The following conclusions can be deduced from the acquired findings:

1. Among the correlations tested, the GMDH model, utilizing five inputs, showcased remarkable accuracy and reliability across all metrics. Its MAPE values for testing, training, and complete data sets were 7.63, 7.31, and 7.38%, respectively. Conversely, in the case of six-input models, the GEP correlation achieved superior precision,

with MAPE values of 9.30, 8.06, and 8.31% for testing, training, and total data sets, respectively.

2. Taking into account all of the statistical parameters, the sequence of correlations based on accuracy is as follows: GMDH (5 inputs), GEP (5 inputs), GEP (6 inputs), GP (6 inputs), GP (5 inputs), and GMDH (6 inputs). The consolidated approach (5 inputs), which utilizes Tcm of a gaseous mixture rather than treating  $CH_4$  and  $N_2$  as separate input variables, effectively captures the essence of its constituents, represents impurities in  $CO_2$ -containing gas, and reduces the complexity of mathematical models with higher accuracy compared to those involving six inputs.

- The sensitivity analysis indicated that pressure had the most significant impact on CO<sub>2</sub>-brine IFT, resulting in a detrimental effect. Temperature, in contrast, exhibited the least pronounced influence on IFT, though its effect might be slightly underestimated due to its nonlinear behavior. In the context of the six-input modeling approach, pressure, bivalent cation molality, CH<sub>4</sub> mole fraction, N<sub>2</sub> mole fraction, monovalent cation molality, and temperature ranked from highest to lowest in terms of their impact on IFT. Similarly, within the five-input modeling approach, pressure, CO<sub>2</sub>-containing gas pseudocritical temperature (T<sub>cm</sub>), bivalent cation molality, monovalent cation molality, and temperature exerted the most to least influence on IFT, respectively.
- There was an adverse influence of gas T<sub>cm</sub> on the IFT between impure CO<sub>2</sub> and brine. This relationship leads to higher impurity concentrations aligning with lower T<sub>cm</sub> values and subsequently elevated IFT. Moreover, monovalent and divalent cation molalities escalate the influence on IFT, with divalent cations exhibiting approximately double the influence of monovalent cations.
- The Leverage approach confirmed both the strong reliability of the experimental data and the robust statistical validity of the best correlations established in this study. Specifically, the GEP model with 6 inputs revealed around 0.5% of potentially suspected data points, while the GMDH model with 5 inputs displayed approximately 1% of such instances.

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### Notes

The authors declare no competing financial interest.

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