

Effect of rearing environment on bone growth of pullets¹

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ABSTRACT Alternative housing systems for laying hens provide mechanical loading and help reduce bone loss. Moreover, achieving greater peak bone mass during pullet phase can be crucial to prevent fractures in the production period. The aim of this study was to determine the housing system effects on bone quality of pullets. Tibiae and humeri of White Leghorn pullets reared in conventional cages (CCs) and a cage-free aviary (AV) system were studied. At 16 wk, 120 birds at random from each housing system were euthanized. Right and left tibiae and humeri were collected and further analyzed. Cortical bone density and thickness were measured using computed tomography. Periosteal and endosteal dimensions were measured at the fracture site during mechanical testing. At 4, 8, 12, and 16 wk, serum concentrations of osteocalcin and hydroxylysyl pyridinoline were analyzed as markers of bone formation and resorption. Cortical bone density was higher ($P < 0.05$) in humeri of AV pullets, and tibiae were denser

($P < 0.05$) for AV pullets in the distal section of the bone compared to CC pullets. Ash content was higher ($P < 0.05$) in AV humeri with no difference in tibiae ash content. Tibiae and humeri of AV pullets had a thicker cortex than the CC pullets ($P < 0.05$). Additionally, the tibiae and humeri of AV pullets had greater ($P < 0.05$) second moment of areas than the CC pullets. While some bone material properties between groups were different ($P < 0.05$), the differences were so small ($< 7\%$) that they likely have no clinical significance. Serum osteocalcin concentrations were not different between the treatments, but hydroxylysyl pyridinoline concentrations were higher in CC pullets at 12 wk compared to the AV pullets and the effect reversed at 16 wk ($P < 0.05$). These findings indicate that tibiae and humeri respond differently to load bearing activities during growth. The improved load bearing capability and stiffness in bones of AV pullets were related to increased cross-sectional geometry.

Key words: pullets, aviary, bone, structure, mechanics

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INTRODUCTION

Egg production systems have changed in the past 6 decades, with 90% of laying hens being kept in deep litter in 1954 (Elson, 2011) to 95% of hens in the United States being housed in conventional cages in 2008 (UEP, 2009). Meanwhile, egg production per hen has also increased mainly due to highly intensive farming systems, optimized nutrition, and enhanced genet-

ics. Conventional cages used in intensive layer production have been associated with disuse-osteoporosis and caged layer fatigue since its introduction. Osteoporosis was first reported by Couch (1955) as a condition characterized by high bone loss and has been defined as a net decrease in the amount of mineralized structural bone that over time makes it fragile and prone to fracture (Whitehead and Fleming, 2000s).

Alternative housing systems with provision of perches and greater space are being explored to mitigate the issues of osteoporosis. In vitro and in vivo studies have established the effects of mechanical loading in bone formation and load bearing (Robling et al., 2008; Wan et al., 2013). Birds housed in alternative systems are allowed more area for load bearing exercises like wing flapping and walking or running that, in theory, alter the bone characteristics and make it stronger. On the other hand, inactivity has been reported to promote osteoporosis in birds (Nightingale et al., 1972; Whitehead and Fleming, 2000). Computed tomographic analyses suggest cortical and trabecular regions of bone from

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adult laying hens housed in different systems had similar bone densities despite having significant differences in cortical areas (Jendral et al., 2008; Shipov et al., 2010), indicating that loading improves bone quality in laying hens by chiefly altering its structural property rather than mineral composition. Efforts to improve bone health by loading have often been studied when birds are already into the laying stage and although loading exercise during production has helped to reduce the amount of structural bone loss, the incidences of osteoporosis and fracture in cage systems indicate that either the birds do not have enough bone mass at the time they enter into the laying cycle or the rate of resorption is too high to be compensated by loading exercises. Hence, one strategy to prevent osteoporosis can be targeted at achieving optimum bone mass before the birds enter into lay. Positive effects of exercise during growth in bone mass and mechanical properties have been reported in several human studies (Vuori, 1996; Bass et al., 2002). Prepubertal loading resulted in increased bone mineral content as well as wider cortical and periosteal area, suggesting periosteal bone formation in the humerus of female tennis players (Bass et al., 2002). Some studies have been conducted previously in experimental setting in male chicks (Biewener and Bertram, 1994; Judex and Zernicke, 2000) whereas there is gap of knowledge on response of loading conditions in pullet skeleton. Pullets housed in cages with perches had higher bone mineral content in tibia and humerus at 12 wk compared to the pullets of same age kept in cages without perches (Enneking et al., 2012), suggesting more bone formation in pullets using perches. The present study was aimed at comparing the differences in material, structural, and mechanical properties of the tibia and humerus of pullets, housed in aviary system and conventional cages in a commercial setting. The hypothesis being tested was pullets raised in an aviary system would have increased peak bone mass at the start of lay compared to pullets reared in conventional cages.

MATERIALS AND METHODS

Birds, Management, and Sampling

The experimental protocol was approved by the Michigan State University Institutional Animal Care and Use Committee. Chickens of the Lohmann White strain were raised in a commercial setting. Pullets were housed in conventional pullet cages (Univent starter, Big Dutchman, Holland, MI) and aviary system (Natura rearing, Big Dutchman). Aviary birds were moved from conventional rearing to aviary rearing at 6 wk. Fifteen pullets were kept in each conventional cage with an area of 247.74 cm²/bird. For aviary pullets, 218 birds were housed per cage with space allocation of 159.94 cm²/bird from 0 to 9 wk, after which total cage space was increased to 248.97 cm²/bird. AV pullets had floor access from 6 wk onwards, providing additional space of 100.13 cm²/bird (Jones et al., 2014).

Feeding, lighting, and health management were same for both groups, and are explained in more detail by Jones et al. (2014) as the same flock was used for the current study. At 16 wk, 120 birds from each housing system were randomly sampled for bone analysis. Birds were euthanized by cervical dislocation and the right and left tibiae, humeri were excised, and samples from each bird were stored in separate plastic zip-lock bags at -20°C.

Brachial vein blood samples were collected from 30 randomly selected pullets of each housing system at 4, 8, and 12 wk, and 60 pullets were sampled in similar fashion at 16 wk from each housing system for quantification of systemic bone markers. Serum was separated and frozen at -20°C prior to analysis. Serum osteocalcin (marker of bone formation) and hydroxylysyl pyridinoline (marker of bone resorption) concentrations were quantified using commercially available ELISA tests (Quidel Corporation, San Diego, CA). Samples with values greater than the standard curve were diluted according to manufacturer's recommendations in the assay buffer for the analysis.

Computed Tomography and Bone Ash

Prior to analysis, the right tibia and humerus were thawed overnight, and a quantitative computed tomography scan of the bone along with surrounding soft tissues was taken using a BrightSpeed scanner (General Electric Healthcare, Princeton, NJ). Ends of the bone were located to obtain total bone length, which was then divided by 4 to set the location for the cross-sectional x-ray image at proximal (one-fourth), middle, and distal (three-fourths) regions. Mimics software (Materialise, Plymouth, MI) was used to measure total bone length and analyze the resulting 1 mm cross sections for cortical bone thickness, and cortical bone density at each of the 3 regions. The orientation of the cortical region in relation to the skeletal axis was identified. Cortical bone thickness and cortical bone density were measured for antero-posterior and medio-lateral planes. Density of bone cortex was measured as an average density within a 10 × 20 mm region at each of anterior, posterior, medial, and lateral region, and a further average of whole cross-sectional slice was measured. Profile line feature of the software was used to calculate appropriate threshold density to mask only the cortical region for measurements. The Haugh units values obtained from the quantitative computed tomography scans were converted to milligrams per cubic centimeter in reference to the standard phantoms that were scanned along with the bones.

Each sample, after quantitative computed tomography scans, was further analyzed for ash content. The bones were cleaned of surrounding muscles and soft tissues. Tibia was separated from fibula, and both humerus and tibia were cut into pieces to fit into a Soxhlet for ether extraction. Ether extracted bone pieces were dried and weighed and placed in crucibles, and

further dried at 105°C for 24 h in a DN-81 constant-temperature oven (American Scientific, Portland, OR). Finally bones were placed in an ash oven (Thermolyne 30400, Barnstead International, Dubuque, IA) at 600°C for 6 h and the ash percentage was determined.

Mechanical Testing

Two days prior to mechanical testing, the left legs and wings were thawed at room temperature. The tibia and humerus were harvested and cleaned of all soft tissue. The bones were wrapped in saline soaked gauze and kept moist throughout all preparations and testing procedures. A uniform middiaphysis section, 20 mm long for the humerus and 30 mm for the tibia, was identified for testing and the remaining ends were potted in cups filled with polyester resin (Martin Senour Fiber Strand Plus 6371, Sherwin-Williams, Cleveland, OH). A custom rig secured the bones in alignment with the cups while the resin cured. After potting, anterior-posterior and medial-lateral outer dimensions of the bones were measured at the ends and center with digital calipers.

The potted specimens were installed in a 4-point bending fixture mounted on a servohydraulic testing machine (model 1331, Instron, Norwood, MA). Freely pivoting cups secured the potted ends and a crossbar resting on pins attached to the cups transferred the linear displacement of the testing machine actuator to rotation of the cups. This setup applied an equal bending moment to each end of the specimen, uniformly loading the test section in pure bending. An actuator preload of 2 N was applied to eliminate residual system compliance before bone failure was induced with a 1 Hz, 10 mm haversine displacement. Load and displacement output of the actuator were recorded at 5,000 Hz with a 100 lb load cell (model 1500ASK-100, Interface, Scottsdale, AZ) and a 6 in linear variable differential transformer mounted on the actuator (model HR 3000, Measurement Specialties, Hampton, VA). The tibiae were oriented with the lateral surface loaded in tension and humeri with the posterior surface loaded in tension. The orientation was selected based on the assumption that the tibiae were likely to break when landing with the distal end medial of the proximal, putting the lateral side in tension. For the humeri, the orientation was selected based on the supposition that wing flapping, namely, adduction was the action most likely to result in a fracture.

After fracture, the bone fragments were reassembled in order to measure anterior, posterior, medial, and lateral cortical thicknesses at the fracture site. Outer dimensions and diaphysis thicknesses were used to approximate the cortical cross-section as a hollow ellipse.

The material properties of the bones were determined based on classical beam theory with the exposed bone test section modeled as a uniform beam with a mo-

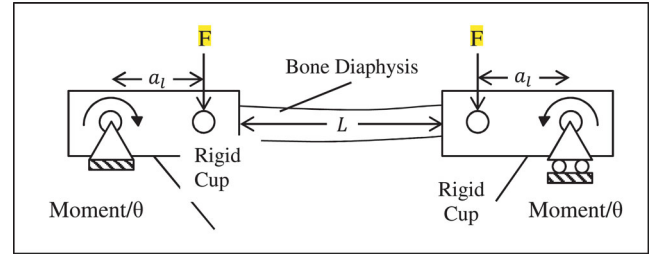


Figure 1. Four-point bending mechanical test setup.

ment applied to each end. The computations required the bone's geometrical resistance to bending, called the second moment of area I , to be computed using the expression

$$I = \frac{\pi a_0 b_0^3}{4} - \frac{\pi a_1 b_1^3}{4} \quad (1)$$

where α and b were the radii parallel and perpendicular to the neutral axis of the bone, and subscripts 0 and 1 denoted outer and inner dimensions of the bone, respectively. The applied bending moment to each end of the specimen was calculated from the actuator force using the expression

$$M = \frac{a_l F}{2} \quad (2)$$

where F was the actuator force applied to both cups, and a_l was the distance between the pivot and load application points on the cups (Figure 1). Bone-end deflection angles θ were calculated using the expression

$$\theta = \sin^{-1} \frac{d}{a_l} \quad (3)$$

where d was the actuator displacement. Whole-bone bending stiffness, K , was determined by the slope of a line fit to the initial, linear portion of the moment-bone rotation plot. This mechanical stiffness and bone geometry were substituted into classical beam equations to compute material stiffness, known as Young's modulus E , using the equation

$$E = (K) \frac{L}{2I} \quad (4)$$

where L was the length of the test section (Figure 1). The material strength of each bone was determined based on a computation of the maximum (failure) bending stress (σ_f) in the bone using the expression

$$\sigma_f = \frac{M_f b}{I} \quad (5)$$

where M_f was the maximum bending moment exerted on each rigid cup at the ends of the specimen at failure (Figure 1).

Statistical Analysis

Data were analyzed by using the multivariate PROC MIXED analysis of SAS Version 9.3 (SAS Institute, Cary, NC). Repeated measures statement with the model including fixed effect of housing and section of bone, the interaction between housing and section, and the residual error was used to analyze all data other than length. Differences between means were tested using Fisher's least-square mean with significance accepted at $P < 0.05$. Data are presented as least-square means with their respective standard errors (least-square mean \pm standard error of the mean). Mechanical data for tibia and humerus were analyzed using the Student's *t*-test.

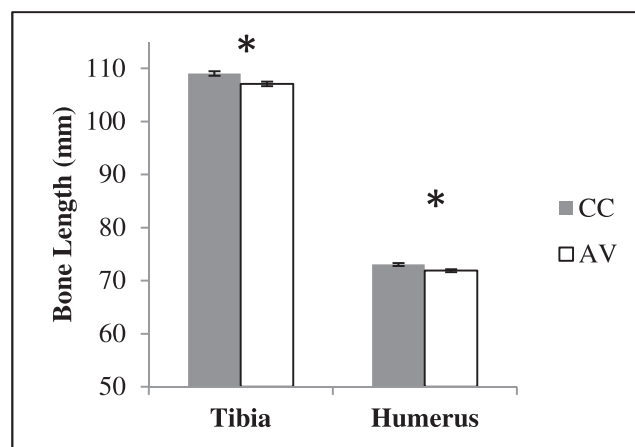
RESULTS

Bone Geometrical and Compositional Properties

Tibiae and humeri were longer in conventional-cage (CC) pullets compared to aviary (AV) system pullets ($P < 0.05$; Figure 2A). However, cortical thickness of both tibiae and humeri were wider in AV pullets, compared to CC pullets in proximal, middle, and distal sections, along all anatomical planes except the antero-posterior plane in proximal tibia ($P < 0.05$; Table 1). There was neither a difference in the medio-lateral nor antero-posterior outer dimensions of the tibia between housing systems (Table 4). Cortical thickness measured manually at the fracture site corroborated with quantitative computed tomography measurements for both bones with tibial and humeral cortex wider in AV birds compared to the CC birds ($P < 0.01$; Table 3). Unlike the tibia, medio-lateral and antero-posterior outer dimensions of the humerus were higher in AV birds compared to the CC birds ($P < 0.01$; Table 3). Cross-sectional areas of tibiae and humeri were greater in AV birds than those of CC birds, which eventually translated into higher values of second moments of area in bones of AV birds compared to CC birds ($P < 0.01$; Table 5). The difference in second moments of inertia between the housing conditions was more pronounced in the humerus than in the tibia.

The changes in geometrical properties of the humerus of AV birds compared to the humerus of CC birds were accompanied by changes in compositional parameters. AV birds had humeri with denser cortex compared to CC birds in all planes in proximal, middle, and distal sections ($P < 0.01$; Table 2). Bone mineral content as measured by ash percentage of humerus was also higher in AV birds compared to the CC birds ($P < 0.05$; Figure 2B). Average cortical bone density of tibia was not different between the housing systems, except for distal tibia where AV birds had a denser cortex compared to CC birds (Table 2).

A.



B.

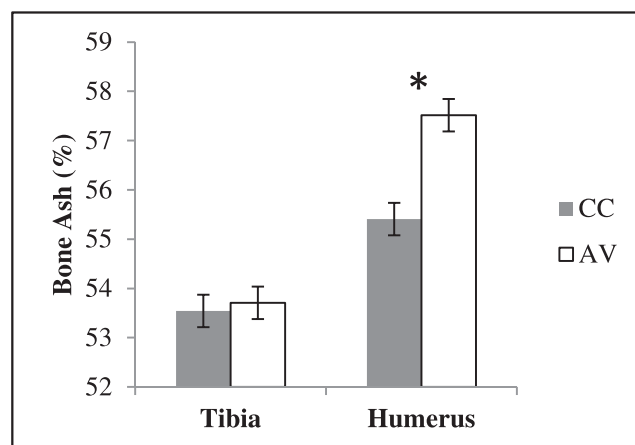


Figure 2. A = Mean total length; B = percentage ash content of tibia and humerus, with respective standard error of the mean of 16 wk Lohmann White pullets housed in AV system and CCs.

Serum Bone Markers

No effect of age or housing condition was observed for mean serum OC levels in the pullets (Figure 3A). Serum hydroxylysyl pyridinoline level increased from 4 to 8 weeks of age with no effect of housing system observed until 12 wk (Figure 3B). The hydroxylysyl pyridinoline concentration was 15.2% higher in caged pullets at 12 wk and the opposite was observed by 16 wk when the hydroxylysyl pyridinoline level was 12.2% higher in aviary pullets than caged pullets ($P < 0.05$; Figure 3B).

Bone Mechanical Properties

An overlay of representative moment-rotation data of a bone from each housing condition illustrates the general differences in bone mechanics up to failure (Figure 4). The failure moment, M_f , was greater for AV tibia and humerus than that of the CC birds ($P < 0.001$; Figure 5A). As a result, aviary birds had stiffer tibiae and

Table 1. Humerus and tibia cortical thickness (millimeters) of 16 wk White Leghorn pullets housed in AV system and CCs.¹

Bone type and housing	Planar orientation of bone			
	Medial ²	Lateral	Anterior	Posterior
Humerus				
Proximal				
AV	1.02 ± 0.02	1.02 ± 0.02	1.18 ± 0.02	1.29 ± 0.02
CC	0.86 ± 0.02	0.88 ± 0.02	0.91 ± 0.02	1 ± 0.02
<i>P</i> value	<.0001	<.0001	<.0001	<.0001
Mid				
AV	1.26 ± 0.02	1.21 ± 0.02	1.39 ± 0.02	1.45 ± 0.02
CC	1.03 ± 0.02	1.02 ± 0.02	1.07 ± 0.02	1.16 ± 0.02
<i>P</i> value	<.0001	<.0001	<.0001	<.0001
Distal				
AV	1.24 ± 0.02	1.40 ± 0.03	1.32 ± 0.02	1.37 ± 0.02
CC	1.03 ± 0.02	1.12 ± 0.03	1.06 ± 0.03	1.08 ± 0.02
<i>P</i> value	<.0001	<.0001	<.0001	<.0001
Tibia				
Proximal				
AV	1.52 ± 0.03	1.70 ± 0.03	1.52 ± 0.02	1.32 ± 0.02
CC	1.44 ± 0.03	1.57 ± 0.03	1.49 ± 0.02	1.36 ± 0.02
<i>P</i> value	0.0261	0.0007	0.4318	0.1334
Mid				
AV	1.59 ± 0.03	1.65 ± 0.03	1.54 ± 0.02	1.48 ± 0.02
CC	1.47 ± 0.03	1.55 ± 0.03	1.42 ± 0.02	1.39 ± 0.02
<i>P</i> value	0.0015	0.0124	<.0001	0.0032
Distal				
AV	1.53 ± 0.02	1.48 ± 0.02	1.23 ± 0.02	1.38 ± 0.02
CC	1.34 ± 0.02	1.36 ± 0.02	1.13 ± 0.02	1.25 ± 0.02
<i>P</i> value	<.0001	0.0002	<.0001	<.0001

¹AV = aviary system; CC = conventional cages.

²Values are presented as least-squares mean ± standard error of the mean.

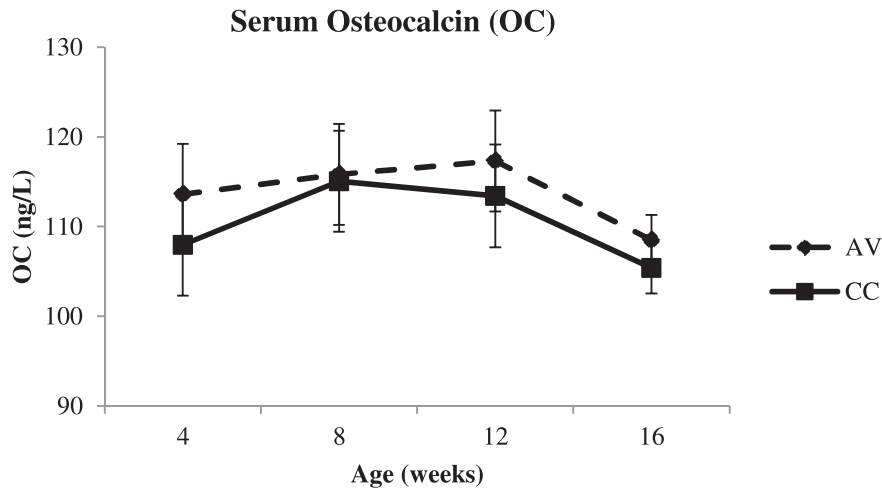
Table 2. Humerus and tibia cortical density (milligrams per cubic centimeter) of 16 wk White Leghorn pullets housed in AV system and CCs.¹

Bone type and housing	Planar orientation of bone				
	Medial ²	Lateral	Anterior	Posterior	Average
Humerus					
Proximal					
AV	247.18 ± 7.09	259.25 ± 7.65	296.10 ± 8.47	280.36 ± 8.12	275.58 ± 7.08
CC	203.28 ± 7.37	219.36 ± 7.94	210.42 ± 8.80	217.62 ± 8.43	218.73 ± 7.28
<i>P</i> value	<.0001	0.0004	<.0001	<.0001	<.0001
Mid					
AV	376.93 ± 10.25	378.94 ± 10.17	422.61 ± 11.06	420.14 ± 10.79	391.72 ± 9.85
CC	300.48 ± 10.64	295.44 ± 10.55	318.91 ± 11.48	322.48 ± 11.20	304.60 ± 10.13
<i>P</i> value	<.0001	<.0001	<.0001	<.0001	<.0001
Distal					
AV	344.30 ± 9.20	422.85 ± 10.51	385.22 ± 10.10	395.52 ± 10.57	385.93 ± 9.47
CC	284.31 ± 9.46	331.42 ± 10.81	282.11 ± 10.38	289.55 ± 10.87	298.90 ± 9.74
<i>P</i> value	<.0001	<.0001	<.0001	<.0001	<.0001
Tibia					
Proximal					
AV	567.69 ± 31.23	589.16 ± 10.05	601.41 ± 10.85	557.46 ± 11.35	575.90 ± 9.99
CC	594.41 ± 31.23	571.07 ± 10.05	591.11 ± 10.85	569.89 ± 11.35	571.22 ± 10.03
<i>P</i> value	0.5449	0.2037	0.5021	0.4385	0.7409
Mid					
AV	639.40 ± 12.80	655.86 ± 12.83	663.15 ± 33.76	632.14 ± 12.36	643.22 ± 12.19
CC	605.09 ± 12.80	617.84 ± 2.83	657.69 ± 33.76	602.55 ± 12.36	609.45 ± 12.30
<i>P</i> value	0.0594	0.0373	0.909	0.0919	0.0524
Distal					
AV	668.92 ± 13.29	605.15 ± 12.54	559.69 ± 12.02	590.98 ± 11.77	612.06 ± 11.90
CC	615.33 ± 13.29	574.85 ± 12.54	519.21 ± 12.02	545.93 ± 11.77	571.64 ± 11.96
<i>P</i> value	0.0048	0.0889	0.0181	0.0073	0.0174

¹AV = aviary system; CC = conventional cages.

²Values are presented as least-squares mean ± standard error of the mean.

A.



B.

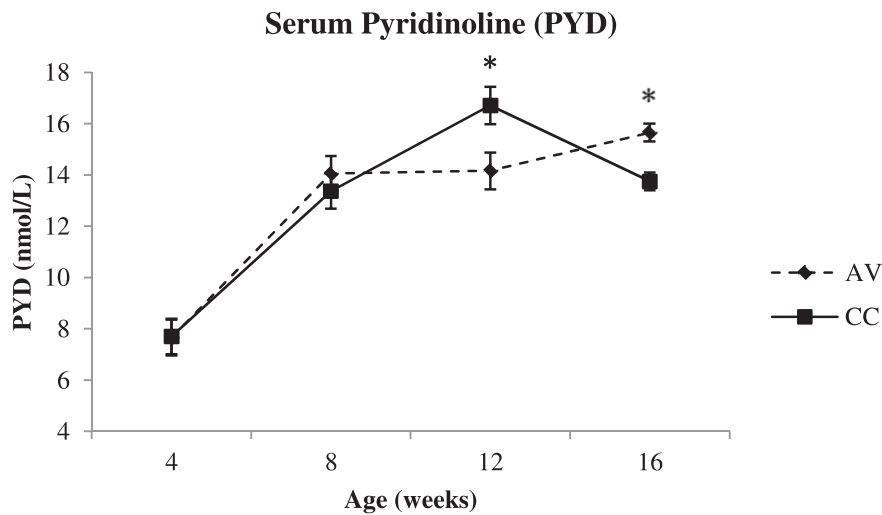


Figure 3. Effect of age and housing systems in systemic markers of bone formation and resorption in Lohmann White pullets housed in AV system and CCs: A = serum osteocalcin concentration; B = serum pyridinoline concentration.

humeri compared to the caged birds, as represented by the slope of the curve (Figure 4).

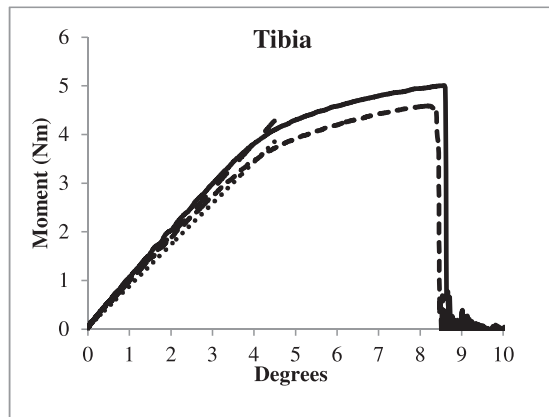
Aviary birds also had stronger bones with tibia material strength, σ_f , 3.7% greater than that of the CC tibia ($P = 0.012$) and humerus strength 6.3% greater than that of the CC humerus ($P = 0.002$; Figure 5B). There was no difference in Young's modulus, E , of the tibia between housing conditions ($P = 0.4889$; Table 5). In contrast, E of CC humeri were greater than that of AV humeri ($P < 0.05$; Table 5).

DISCUSSION

Previous research exploring bone qualities in laying hens has often done so when the birds are in the lay-

ing stage. This study examines the effect of loading provided by difference in housing system in the tibia and humerus of growing pullets. The aviary (AV) system provides birds with more opportunity of dynamic loading exercises like running and flying which are not possible in cages. Early mechanical loading has been reported to result in narrower growth plates and shorter bones in broiler chicks (Reich et al., 2005). The common response of bones undergoing loading in compression is shortening in length and widening in cross section (Seeman and Delmas, 2006) which was also the case in this study, even though the percentage change in length was very small. Conventionally housed pullets had longer tibiae and humeri at the end of the pullet phase compared to those kept in an AV system, whereas

A.



B.

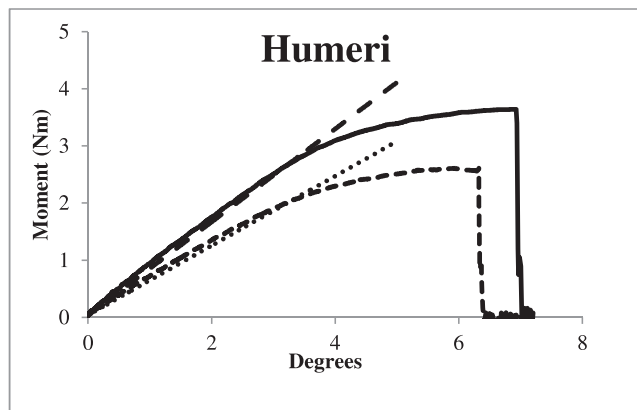
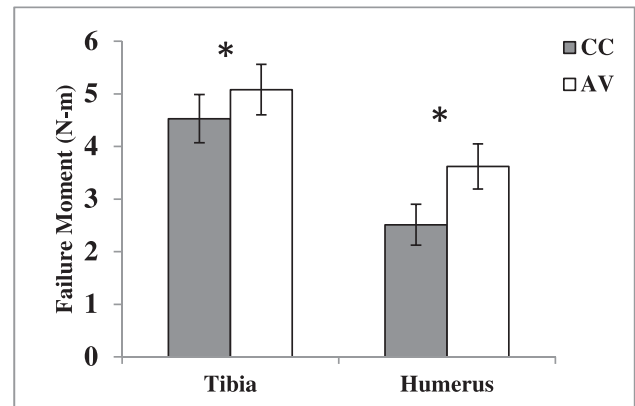


Figure 4. Representative moment-rotation curves showing the mechanical behavior in bending up to failure of 16 wk Lohmann White pullets housed in AV system and CCs: A = behavior of the tibia; B = behavior of the humerus; stiffness was determined from the slope of the initial, linear portion of the curves.

AV birds had greater bone width and cortical thickness. Measurements of bone thickness from quantitative computed tomography scans as well as the measurements taken after fracture found that bones from birds reared in AV systems developed a thicker cortex than birds from conventional rearing systems.

In the tibiae, there was no difference in the outer (periosteal) dimensions between housing conditions. Thus, the increased cross-sectional area of AV tibiae was due to a narrowed medullary canal [Figure 6 (i)]. Contrary to the results of this study, increase in cortical area in 8 wk male White Leghorn chicks under controlled exercise regimen has been reported to be a result of periosteal deposition rather than endosteal apposition (Biewener and Bertram, 1994). In another study, the effect of high-impact exercise like jumping was limited to periosteal surface until 16 wk in the tarsometatarsus of male Leghorn chicks; however, after that age, growth was more pronounced at the endocortical surface (Judex and Zernicke, 2000). The varied response of growing leg bone in White Leghorns to mechanical

A.



B.

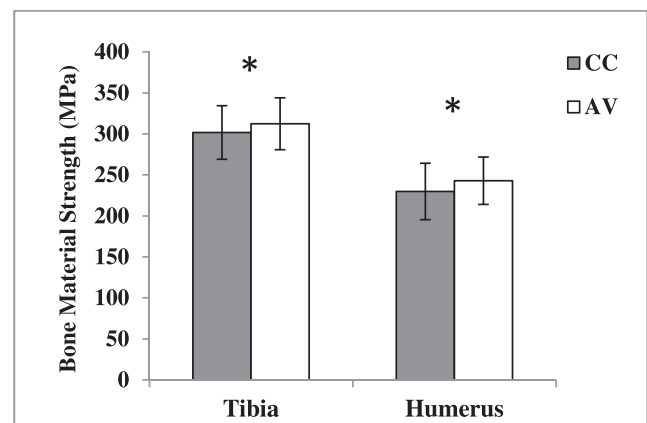


Figure 5. A = Ability of tibia and humerus to withstand bending moments; B = breaking strength (least-squares mean \pm standard error of the mean) of tibia and humerus in 16 wk Lohmann White pullets housed in AV system and CCs.

stimuli is likely to be the result of differences in age, sex, and the mechanical environment in which the birds are reared. Whereas such inward growth (as observed in present study) increases the second moment of area, the addition of bone more proximal to the neutral axis means that second moment of area differences were not as pronounced as cross-sectional area differences. The primary function of endosteal growth is to increase a bone's axial rigidity as has been observed in response to *in vivo* dynamic longitudinal compressive loading (Robling et al., 2002). Thus, the cross-sectional geometry differences observed suggests that the additional loading on AV system pullet tibiae may have been primarily along the axis of the bone.

The increased cross-sectional area in the humerus of AV birds was due to increased periosteal diameters with the endosteal dimensions remaining largely unchanged [Figure 6 (ii)]. In addition to increasing axial rigidity, outward expansion of the cortex greatly increases the second moment of area. The humeri's second moment of area increased more dramatically than the

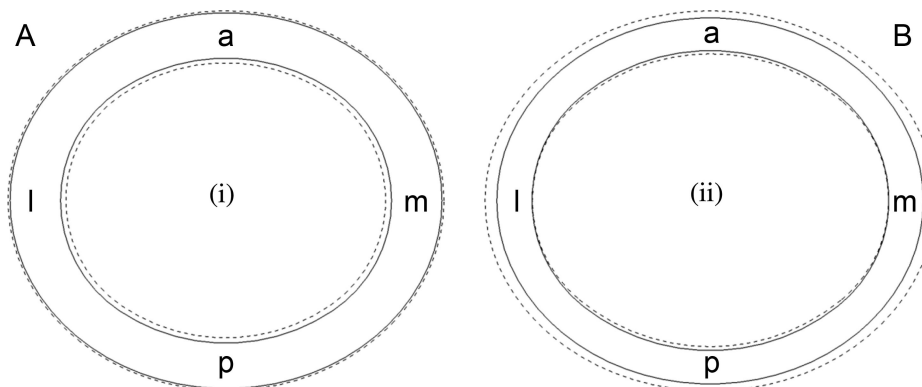


Figure 6. Diagrammatic representation of bone cross-sections reconstructed using average measurements of 16 wk White Leghorn pullets housed in AV system (dashed line) and CCs (solid line): A = measurements for tibiae; B = measurements for humeri.

Table 3. Geometrical properties of humerus of 16 wk pullets housed in AV system and CCs.¹

Dependent variable	Housing		P value
	AV	CC	
Geometrical properties			
Area (mm ²)	12.92 ± 0.12 ²	9.42 ± 0.13	<.0001
Medial thickness (mm)	0.74 ± 0.01	0.54 ± 0.01	<.0001
Lateral thickness (mm)	0.75 ± 0.01	0.55 ± 0.01	<.0001
Anterior thickness (mm)	0.68 ± 0.01	0.52 ± 0.01	<.0001
Posterior thickness (mm)	0.70 ± 0.01	0.52 ± 0.01	<.0001
Average medio-lateral thickness (mm)	0.74 ± 0.01	0.55 ± 0.01	<.0001
Average antero-posterior thickness (mm)	0.69 ± 0.01	0.52 ± 0.01	<.0001
Average thickness (mm)	0.72 ± 0.01	0.53 ± 0.01	<.0001
Proximal medio-lateral diameter (mm)	7.52 ± 0.03	7.17 ± 0.03	<.0001
Mid medio-lateral diameter (mm)	6.82 ± 0.03	6.39 ± 0.03	<.0001
Distal medio-lateral diameter (mm)	6.88 ± 0.03	6.46 ± 0.04	<.0001
Prox antero-posterior diameter (mm)	5.98 ± 0.02	5.74 ± 0.02	<.0001
Mid antero-posterior diameter (mm)	5.79 ± 0.02	5.59 ± 0.02	<.0001
Distal antero-posterior diameter (mm)	5.92 ± 0.02	5.73 ± 0.02	<.0001
Average medio-lateral diameter (mm)	7.07 ± 0.03	6.68 ± 0.03	<.0001
Average antero-posterior diameter (mm)	5.90 ± 0.02	5.69 ± 0.02	<.0001
Average diameter (mm)	6.49 ± 0.02	6.18 ± 0.02	<.0001

¹AV = aviary system; CC = conventional cages.

²Values are presented as least-squares mean ± standard error of the mean.

cross-sectional area in AV housing conditions. An increased second moment of area is a characteristic response in bone that has been subjected to additional bending or torsional loads (Bass et al., 2002; Ducher et al., 2009) such as wing flapping which was possible in the AV systems. These findings suggest that humerus loading might be different to tibia, resulting in distinct growth patterns in each bone. The study results corroborate the findings that torsional resistance is the principal component to drive humerus structural design, while axial bending drives the structure of tibiotarsus in birds (de Margerie et al., 2005).

Structural improvement in AV pullets' humeri was accompanied by an increase in volumetric bone density and bone ash. The effect in cortical density of tibia was limited to the distal section and no difference was observed in the ash content. Concentration of hydroxylsyl pyridinoline decreased in the pullets switched to AV until 12 wk but then increased to even higher levels compared to CC pullets at 16 wk. Although net

bone resorption is decreased in birds undergoing exercise (Fleming et al., 2006), why the level went up after 12 wk was unclear. Unlike deoxypyridinoline which is often used as bone specific marker of collagen turnover, hydroxylsyl pyridinoline used in this study is not bone-specific and the ambiguous result might be due to collagen turnover in muscles and other organs of the growing pullets. Bone strength and modulus were calculated from the geometry and moment-bone rotation data to assess the material properties of the bones. Although the differences between groups for some of these quantities were statistically significant, the percentage changes were small. The statistically significant material differences were likely a product of the large sample sizes that boosted the sensitivity or due to the differences in structure and properties of organic matrix of the bone, which was not studied in this experiment. The changes in bone structure and density were not highly reflected by the mechanical testing when young bull calves were subjected to exercise (Hiney et al., 2004).

Table 4. Geometrical properties of tibia of 16 wk pullets housed in AV system and CCs.¹

Dependent variable	Housing		P value
	AV	CC	
Geometrical properties			
Area (mm ²)	14.16 ± 0.11 ²	12.52 ± 0.12	<.0001
Medial thickness (mm)	0.90 ± 0.01	0.78 ± 0.01	<.0001
Lateral thickness (mm)	0.88 ± 0.01	0.78 ± 0.01	<.0001
Anterior thickness (mm)	0.80 ± 0.01	0.70 ± 0.01	<.0001
Posterior thickness (mm)	0.80 ± 0.01	0.70 ± 0.01	<.0001
Average medio-lateral thickness (mm)	0.89 ± 0.01	0.78 ± 0.01	<.0001
Average antero-posterior thickness (mm)	0.80 ± 0.01	0.70 ± 0.01	<.0001
Average thickness (mm)	0.84 ± 0.01	0.74 ± 0.01	<.0001
Proximal medio-lateral diameter (mm)	6.73 ± 0.03	6.69 ± 0.03	0.3825
Middle medio-lateral diameter (mm)	6.44 ± 0.03	6.37 ± 0.03	0.1121
Distal medio-lateral diameter (mm)	6.81 ± 0.03	6.73 ± 0.03	0.0912
Prox antero-posterior diameter (mm)	6.07 ± 0.03	5.94 ± 0.03	0.0029
Middle antero-posterior diameter (mm)	5.57 ± 0.02	5.51 ± 0.03	0.1252
Distal antero-posterior diameter (mm)	5.67 ± 0.03	5.67 ± 0.03	0.9947
Average medio-lateral diameter (mm)	6.66 ± 0.03	6.60 ± 0.03	0.1125
Average antero-posterior diameter (mm)	5.77 ± 0.02	5.71 ± 0.02	0.0831
Average diameter (mm)	6.21 ± 0.02	6.15 ± 0.02	0.0585

¹AV = aviary system; CC = conventional cages.

²Values are presented as least-squares mean ± standard error of the mean.

Table 5. Mechanical and geometrical properties of tibia and humerus of 16 wk pullets housed in AV system and CCs.¹

Dependent variable	Housing		P value
	AV	CC	
Tibia			
Mechanical properties			
Failure moment (Nm)	5.08 ± 0.48 ²	4.53 ± 0.46	<0.001
Failure rotation (degree)	8.90 ± 1.15	8.57 ± 1.27	0.042
Stiffness (Nm/degree)	0.94 ± 0.10	0.85 ± 0.11	<0.001
Failure stress (MPa)	312.40 ± 31.50	301.80 ± 32.70	0.012
Young's modulus (GPa)	13.65 ± 1.20	13.74 ± 1.42	0.627
Second moment of inertia (mm ⁴)	59.91 ± 8.53	53.55 ± 8.02	<0.001
Humerus			
Mechanical properties			
Failure moment (Nm)	3.62 ± 0.43	2.51 ± 0.39	<0.001
Failure rotation (degree)	6.97 ± 1.05	6.49 ± 1.01	0.001
Stiffness (Nm/degree)	0.82 ± 0.11	0.61 ± 0.09	<0.001
Failure stress (MPa)	242.90 ± 28.80	229.80 ± 34.30	0.002
Young's modulus (GPa)	10.25 ± 1.22	10.77 ± 1.30	0.002
Second moment of inertia (mm ⁴)	46.25 ± 7.13	32.91 ± 5.64	<0.001

¹AV = aviary system; CC = conventional cages.

²Values are presented as least-squares mean ± standard error of the mean.

The researchers suggested that physical measurements may provide more reliable assessment of bone mineral content than quantitative computed tomography, especially with smaller bones. Similar results were observed in mature White Leghorn roosters, where cortical areas and load bearing capacity were improved with exercise but the Young's modulus was not (Loitz and Zernicke, 1992). Laying hens housed in aviary houses have been reported to have significantly wider tibio-tarsal cortical area along with heavier bone mass, and denser tibia and humeri, compared to conventionally caged birds (Fleming et al., 2006). Whereas more recent quantitative computed tomography studies of bones in laying hens have demonstrated no changes in volumetric density of cortical and trabecular tissues between the housing systems despite having significant differences

in structure (Jendral et al., 2008; Shipov et al., 2010), which suggests that increased bone mineral content was a response to increased bone quantity and not a result of improved bone mineral density. Enneking et al. (2012) reported no difference in pooled data of various bones and ages for areal density, bone length, and width in pullets housed in cages with perches compared to pullets in cages without perches. However, the bone mineral content of tibia and humerus were significantly different at 12 wk between the groups.

This study indicated that skeletal loading provided by activities within pullet AV housing resulted in structural and material changes that improved the load-bearing capability and stiffness to the tibia and humerus. Providing greater access to activities including flying, perching, and running during pullet phase

can be crucial to the increased bone quantity that might help prevent fractures due to osteoporosis in cage birds, and impact injuries during the production phase in the extensive systems.

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